



Pole Shed App Ver 01 2022

**Job No.:** 432 TUKAIRANGI ROAD - 1      **Address:** 432 TUKAIRANGI ROAD, Taupo, New Zealand      **Date:** 09/12/2024  
**Latitude:** -38.654353      **Longitude:** 176.018862      **Elevation:** 543 m

**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.328 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	48.03 m/s
Wind Pressure	1.38 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Very High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

**Pressure Coefficients and Pressures**

Shed Type = Gable Enclosed

For roof  $C_{p,i} = -0.3$

For roof  $C_{p,e}$  from 0 m To 4.33 m  $C_{p,e} = -0.9$   $p_e = -1.12$  KPa  $p_{net} = -1.12$  KPa

For roof  $C_{p,e}$  from 4.33 m To 8.66 m  $C_{p,e} = -0.5$   $p_e = -0.62$  KPa  $p_{net} = -0.62$  KPa

For wall Windward  $C_{p,i} = -0.3$  side Wall  $C_{p,i} = -0.3$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 8 m  $C_{p,e} = 0.7$   $p_e = 0.87$  KPa  $p_{net} = 1.29$  KPa

For side wall  $C_{p,e}$  from 0 m To 4.33 m  $C_{p,e} =$   $p_e = -0.81$  KPa  $p_{net} = -0.81$  KPa

Maximum Upward pressure used in roof member Design = 1.12 KPa

Maximum Downward pressure used in roof member Design = 0.67 KPa

Maximum Wall pressure used in Design = 1.29 KPa

Maximum Racking pressure used in Design = 1.37 KPa

**Design Summary**

**Girt Design Front and Back**

Girt's Spacing = 900 mm

Girt's Span = 4009 mm

Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

Second page

Pole Shed App Ver 01 2022

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =0.98

K8 Upward =0.90    S1 Downward =12.23    S1 Upward =14.90

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>Wind+Snow</sub>	2.33 Kn-m	Capacity	2.74 Kn-m	Passing Percentage	<b>117.60 %</b>
V <sub>0.9D-WnUp</sub>	2.33 Kn	Capacity	13.75 Kn	Passing Percentage	<b>590.13 %</b>

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 22.66 mm    Limit by Woolcock et al, 1999 Span/100 = 40.09 mm

Sag during installation = 19.34 mm

**Reactions**

Maximum = 2.33 kn

**Girt Design Sides**

Girt's Spacing = 900 mm

Girt's Span = 4000 mm

Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =0.98

K8 Upward =0.90    S1 Downward =12.23    S1 Upward =14.88

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>Wind+Snow</sub>	2.32 Kn-m	Capacity	2.74 Kn-m	Passing Percentage	<b>118.10 %</b>
V <sub>0.9D-WnUp</sub>	2.32 Kn	Capacity	13.75 Kn	Passing Percentage	<b>592.67 %</b>

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 22.46 mm    Limit by Woolcock et al. 1999 Span/100 = 40.00 mm

Sag during installation =19.16 mm

## Reactions

Maximum = 2.32 kn

## Middle Pole Design

### Geometry

250 UNI H5	Dry Use	Height	4756 mm
Area	49063 mm <sup>2</sup>	As	36796.875 mm <sup>2</sup>
Ix	191650391 mm <sup>4</sup>	Zx	1533203 mm <sup>3</sup>
Iy	191650391 mm <sup>4</sup>	Zx	1533203 mm <sup>3</sup>
Lateral Restraint	1300 mm c/c		

### Loads

Total Area over Pole = 16.036 m<sup>2</sup>

Dead	4.01 Kn	Live	4.01 Kn
Wind Down	10.74 Kn	Snow	0.00 Kn
Moment wind	19.24 Kn-m		
Phi	0.8	K8	1.00
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

### Material

Shaving	Steaming	Normal	Dry Use
fb =	34.325 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	20.75 MPa	E =	8793 MPa

### Capacities

PhiNcx Wind	706.50 Kn	PhiMnx Wind	42.10 Kn-m	PhiVnx Wind	87.14 Kn
PhiNcx Dead	423.90 Kn	PhiMnx Dead	25.26 Kn-m	PhiVnx Dead	52.28 Kn

### Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.48 < 1$  OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.24 < 1$  OK

Deflection at top under service lateral loads = 33.02 mm < 47.56 mm

## **Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile**

### **Assumed Soil Properties**

Gamma 18 Kn/m<sup>3</sup>                      Friction angle 30 deg    Cohesion 0 Kn/m<sup>3</sup>  
K<sub>0</sub> =  $(1 - \sin(30)) / (1 + \sin(30))$   
K<sub>p</sub> =  $(1 + \sin(30)) / (1 - \sin(30))$

### **Geometry For Middle Bay Pole**

D<sub>s</sub> = 0.6 mm                      Pile Diameter  
L = 1800 mm                      Pile embedment length  
f<sub>1</sub> = 3246 mm                      Distance at which the shear force is applied  
f<sub>2</sub> = 0 mm                      Distance of top soil at rest pressure

### **Loads**

Moment Wind = 19.24 Kn-m  
Shear Wind = 5.93 Kn

### **Pile Properties**

Safety Factory 0.55  
H<sub>u</sub> = 10.30 Kn                      Ultimate Lateral Strength of the Pile, Short pile  
M<sub>u</sub> = 20.13 Kn-m                      Ultimate Moment Capacity of Pile

### **Checks**

Applied Forces/Capacities = 0.96 < 1 OK

## **Uplift Check**

Density of Concrete = 24 Kn/m<sup>3</sup>

Density of Timber Pole = 5 Kn/m<sup>3</sup>

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K<sub>s</sub> (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1800) x K<sub>s</sub>(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1800)

Skin Friction = 26.17 Kn

Weight of Pile + Pile Skin Friction = 30.03 Kn

Uplift on one Pile = 14.35 Kn

Uplift is ok