Job Number:	BWhite
Issue:	Consulting Ltd
PRODUCER STATEMENT-PS1-DESIGN	C
ISSUED BY: BWhite Consulting Ltd (Design Engineer: Bevan White)	
TO BE SUPPLIED TO: Far North District Council IN RESPECT OF: Proposed NEW Farm Shed	
AT: 1263A Bulls Rd, Kerikeri, New Zealand	
LEGAL DESCRIPTION	
We have been engaged by <b>Ezequote Pty Ltd</b> to provide <b>Specific Structural Engineering Design</b> so requirements of Clause(s) <b>B1</b> of the Building Code for part only (as specified in the attachment to the building work.	_
☐ ALL	l connections
The design has been prepared in accordance with compliance documents to NZ Building Code issu Innovation & Employment Clauses B1/VM1 and B1/VM4	ned by Ministry of Business,
The proposed building work covered by the producer statement is described on <b>Ezequote</b> drawings <b>A101-A117 REV-1</b> dated <b>11/24/2023</b> together with the following specification, and other documen attached to this statement: <b>Design Featured Report Dated 11/22/2023 and numbered "Second Pag</b>	ts set out in the schedule
On behalf of BWhite Consulting Ltd, and subject to:	
<ol> <li>Site verification of the following design assumptions: an Ultimate foundation bearing press with NZS3604:2011</li> <li>The building has a design life of 50 years and am Importance Level 1</li> <li>Unless specifically noted, compliance of the drawings to None-Specific codes such as NZS been checked by this practice</li> <li>This Certificate does not cover any other building code clause including weather tightness</li> <li>Inspections of the building to be completed by Far North District Council. As BWhite Con inspections, we cannot issue a producer Statement-PS4- Construction Review.</li> <li>This Producer Statement- Design is valid for a building consent issued within 1 year from 7. All proprietary products meeting their performance specification requirements</li> </ol>	3604 and NZS4229 have not s sulting Ltd are not undertaking
I believe on reasonable grounds that a) the building, if constructed in accordance with the drawing documents provided or listed in the attached schedule, will comply with the relevant provisions of the presons who have undertaken the design have the necessary competency to do so. I also reconstruction monitoring/observation:	the Building Code and that b),
☑ CM1 ☐ CM2 ☐ CM3 ☐ CM4 ☐ CM5 or as per agreement with owner/developer (stated about	ve)
I, Bevan White am CPEng 108276 I am Member of Engineering New Zealand and hold the followin	g qualification: <b>BECivil</b>
BW hite Consulting Ltd holds a current policy of Professional Indemnity Insurance no less than \$20	00,000.
Signed by Bevan White on behalf of BWhite Consulting Ltd Dated: 11/22/2023	
Fmail: hwhitecneng@gmail.com.Phone: 0211-979786	

This form is to accompany Form 2 of the Building (Forms) Regulations 2004 for the application of a Building Consent

whether in contract, tort or otherwise(including negligence), is limited to the sum of \$200,000.

Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement accrues to the Design Firm only. The total maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work,

Date: 11/22/2023

BWhite

18B Jules Crescent,

Consulting Ltd

Bell Block New Plymouth 4312

New Zealand File No:

# DESIGN FEATURES SUMMARY FOR PROPOSED NEW FARM SHED 1263A BULLS RD, KERIKERI, NEW ZEALAND

## **Site Specific Loads**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & EQ ARI	100 Years	Max Height	4.4 m
Wind Region	NZ1	Terrain Category	2.96	Design Wind Speed	43.23 m/s
Wind Pressure	1.12 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years

#### Timber

Sawn Timber to be graded to the properties of SG6 and SG8 or better as mentioned on plans, with moisture content of 18% or less for dry and 25% or less for wet.

The following standards have been used in the design of this structure

- NZS 3603:1993 Timber Structures Standard
- NZS 3604:2011 Timber Framed Buildings. Standards New Zealand, 2011
- NZS 3404:1997 Steel Structures
- AS/NZS 1170 2003 Structural Design Actions
- AS/NZS 1170.2 2021 Structural Design Actions-Wind Action
- Branz. "Engineering Basis of NZS 3604". April 2013

Yours Faithfully

#### **BWhite CONSULTING LTD**

#### **Bevan White**

Director | BE Civil . CMengNZ CPEng

Email: bwhitecpeng@gmail.com Contact: 0211 979 786

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 Job No.:
 618411
 Address:
 1263A Bulls Rd, Kerikeri, New Zealand
 Date:
 11/22/2023

 Latitude:
 -35.268603
 Longitude:
 173.938025
 Elevation:
 172.5 m

#### **General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.4 m
Wind Region	NZ1	Terrain Category	2.96	Design Wind Speed	43.23 m/s
Wind Pressure	1.12 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

#### **Pressure Coefficients and Pressues**

Shed Type = Mono Open

For roof Cp,i = 0.6475

For roof CP,e from 0 m To 4.0 m Cpe = -0.9 pe = -0.81 KPa pnet = -1.51 KPa

For roof CP,e from 4.0 m To 8.0 m Cpe = -0.5 pe = -0.45 KPa pnet = -1.15 KPa

For wall Windward Cp, i = 0.6475 side Wall Cp, i = -0.5525

For wall Windward and Leeward CP,e from 0 m To 11.0 m Cpe = 0.7 pe = 0.71 KPa pnet = 1.30 KPa

For side wall CP,e from 0 m To 4.0 m Cpe = pe = -0.66 KPa pnet = -0.66 KPa

Maximum Upward pressure used in roof member Design = 1.51 KPa

Maximum Downward pressure used in roof member Design = 0.82 KPa

Maximum Wall pressure used in Design = 1.30 KPa

Maximum Racking pressure used in Design = 1.21 KPa

## **Design Summary**

#### **Purlin Design**

Purlin Spacing = 900 mm Purlin Span = 3450 mm Try Purlin 300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.94

K8 Upward =0.40 S1 Downward =13.93 S1 Upward =27.08

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

## **Capacity Checks**

$M_{1.35D}$	0.45 Kn-m	Capacity	4.72 Kn-m	Passing Percentage	1048.89 %
M1.2D+1.5L 1.2D+Sn 1.2D+WnDn	1.5 Kn-m	Capacity	6.30 Kn-m	Passing Percentage	420.00 %
$M_{0.9D\text{-W}nUp}$	-1.72 Kn-m	Capacity	-3.32 Kn-m	Passing Percentage	193.02 %
V <sub>1.35D</sub>	0.52 Kn	Capacity	14.47 Kn	Passing Percentage	2782.69 %
V1.2D+1.5L 1.2D+Sn 1.2D+WnDn	1.74 Kn	Capacity	19.30 Kn	Passing Percentage	1109.20 %
$ m V_{0.9D ext{-}WnUp}$	-1.99 Kn	Capacity	-24.12 Kn	Passing Percentage	1212.06 %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 1.25 mm

Limit by Woolcock et al, 1999 Span/240 = 14.17 mm

Deflection under Dead and Service Wind = 1.89 mm Limit by Woolcock et al, 1999 Span/100 = 34.00 mm

## Reactions

Maximum downward = 1.74 kn Maximum upward = -1.99 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

## **Girt Design Front and Back**

Girt's Spacing = 600 mm Girt's Span = 3600 mm Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.98

K8 Upward =0.48 S1 Downward =12.23 S1 Upward =24.46

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### **Capacity Checks**

$M_{Wind+Snow}$	1.26 Kn-m	Capacity	1.45 Kn-m	Passing Percentage	115.08 %
$ m V_{0.9D ext{-}WnUp}$	1.40 Kn-m	Capacity	13.75 Kn-m	Passing Percentage	982.14 %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 9.90 mm Limit by Woolcock et al, 1999 Span/100 = 36.00 mm Sag during installation = 12.57 mm

#### Reactions

Maximum = 1.40 kn

## **Girt Design Sides**

Girt's Spacing = 600 mm

Girt's Span = 5500 mm

Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward =0.57 S1 Downward =12.68 S1 Upward =22.16

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

MWind+Snow	2.95 Kn-m	Capacity	3.31 Kn-m	Passing Percentage	112.20 %
$ m V_{0.9D ext{-}WnUp}$	2.15 Kn-m	Capacity	20.10 Kn-m	Passing Percentage	934.88 %

## **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 21.31 mm Limit by Woolcock et al. 1999 Span/100 = 55.00 mm Sag during installation = 55.48 mm

#### Reactions

Maximum = 2.15 kn

## **Uplift Check**

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1700) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1700)

Skin Friction = 23.34 Kn

Weight of Pile + Pile Skin Friction = 27.24 Kn

Uplift on one Pile = 25.44 Kn

Uplift is ok