

Pole Shed App Ver 01 2022

Job No.: Steve Maley-Canopy **Address:** 48 Morven Lane, Fairhall, New Zealand **Date:** 3/13/2025
Latitude: -41.547677 **Longitude:** 173.886444 **Elevation:** 49.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	3	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	2.4 m
Wind Region	NZ2	Terrain Category	2.57	Design Wind Speed	39.18 m/s
Wind Pressure	0.92 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Open

For roof $C_{p,i} = 0.49$

For roof $C_{p,e}$ from 0 m To 1.2 m $C_{p,e} = -1.3$ $p_e = -1.03$ KPa $p_{net} = -1.46$ KPa

For roof $C_{p,e}$ from 1.20 m To 1.50 m $C_{p,e} = -0.7$ $p_e = -0.55$ KPa $p_{net} = -0.98$ KPa

For wall Windward $C_{p,i} = 0.49$ side Wall $C_{p,i} = -0.65$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 3.50 m $C_{p,e} = 0.7$ $p_e = 0.57$ KPa $p_{net} = 1.16$ KPa

For side wall $C_{p,e}$ from 0 m To 2.40 m $C_{p,e} =$ $p_e = -0.53$ KPa $p_{net} = 0.06$ KPa

Maximum Upward pressure used in roof member Design = 1.46 KPa

Maximum Downward pressure used in roof member Design = 0.50 KPa

Maximum Wall pressure used in Design = 1.16 KPa

Maximum Racking pressure used in Design = 0.99 KPa

Design Summary

Purlin Design

Purlin Spacing = 700 mm Purlin Span = 3350 mm Try Purlin 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

Pole Shed App Ver 01 2022

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.98

K8 Upward = 0.52 S1 Downward = 12.23 S1 Upward = 23.41

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	0.33 Kn-m	Capacity	1.79 Kn-m	Passing Percentage	542.42 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	1.68 Kn-m	Capacity	2.38 Kn-m	Passing Percentage	141.67 %
M _{0.9D-W_nUp}	-1.21 Kn-m	Capacity	-1.56 Kn-m	Passing Percentage	128.93 %
V _{1.35D}	0.40 Kn	Capacity	8.25 Kn	Passing Percentage	2062.50 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	0.94 Kn	Capacity	11.00 Kn	Passing Percentage	1170.21 %
V _{0.9D-W_nUp}	-1.45 Kn	Capacity	-13.75 Kn	Passing Percentage	948.28 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 7.92 mm Limit by Woolcock et al, 1999 Span/240 = 13.75 mm

Deflection under Dead and Service Wind = 4.70 mm Limit by Woolcock et al, 1999 Span/100 = 33.00 mm

Reactions

Maximum downward = 0.94 kn Maximum upward = -1.45 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design External

External Rafter Load Width = 1750 mm External Rafter Span = 1313 mm Try Rafter 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.98

K8 Upward = 0.98 S1 Downward = 12.23 S1 Upward = 12.23

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	0.13 Kn-m	Capacity	1.79 Kn-m	Passing Percentage	1376.92 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	0.47 Kn-m	Capacity	2.38 Kn-m	Passing Percentage	506.38 %

Pole Shed App Ver 01 2022

M _{0.9D-WnUp}	-0.47 Kn-m	Capacity	-2.98 Kn-m	Passing Percentage	634.04 %
V _{1.35D}	0.39 Kn	Capacity	8.25 Kn	Passing Percentage	2115.38 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	0.92 Kn	Capacity	11.00 Kn	Passing Percentage	1195.65 %
V _{0.9D-WnUp}	-1.42 Kn	Capacity	-13.75 Kn	Passing Percentage	968.31 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 0.25 mm Limit by Woolcock et al, 1999 Span/240= 6.25 mm

Deflection under Dead and Service Wind = 0.31 mm Limit by Woolcock et al, 1999 Span/100 = 15.00 mm

Reactions

Maximum downward = 0.92 kn Maximum upward = -1.42 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K₁₁ = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 45 mm

For Parallel to grain loading

K₁₁ = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

V = $\phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s$ (Eq 4.12) = -12.28 kn > -1.42 Kn

Single Shear Capacity under short term loads = -9.75 Kn > -1.42 Kn

Girt Design Front and Back

Girt's Spacing = 0 mm

Girt's Span = 3500 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

Pole Shed App Ver 01 2022

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
V _{0.9D-WnUp}	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm Limit by Woolcock et al, 1999 Span/100 = 35.00 mm

Sag during installation = NaN mm

Reactions

Maximum = 0.00 kn

Girt Design Sides

Girt's Spacing = 0 mm

Girt's Span = 1500 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
V _{0.9D-WnUp}	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm Limit by Woolcock et al. 1999 Span/100 = 15.00 mm

Sag during installation =NaN mm

Pole Shed App Ver 01 2022

Reactions

Maximum = 0.00 kn

End Pole Design

Geometry For End Bay Pole

Geometry

125x125 SG8 Dry	Dry Use	Height	2200 mm
Area	15625 mm ²	As	11718.75 mm ²
Ix	20345052 mm ⁴	Zx	325521 mm ³
Iy	20345052 mm ⁴	Zy	325521 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 2.625 m²

Dead	0.66 Kn	Live	0.66 Kn
Wind Down	1.31 Kn	Snow	0.00 Kn
Moment Wind	1.87 Kn-m		
Phi	0.8	K8	0.79
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Shaving	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	177.16 Kn	PhiMnx Wind	7.44 Kn-m	PhiVnx Wind	27.75 Kn
PhiNcx Dead	106.29 Kn	PhiMnx Dead	4.47 Kn-m	PhiVnx Dead	16.65 Kn

Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.27 < 1$ OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.08 < 1$ OK

Pole Shed App Ver 01 2022

Deflection at top under service lateral loads = 8.00 mm < 23.94 mm

Ds =	0.6 mm	Pile Diameter
L =	850 mm	Pile embedment length
f1 =	1800 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 2.625 m²

Moment Wind =	1.87 Kn-m
Shear Wind =	1.04 Kn

Pile Properties

Safety Factory	0.55	
Hu =	2.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	2.20 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.85 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	850 mm	Pile embedment length
f1 =	1800 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	1.87 Kn-m
Shear Wind =	1.04 Kn

Pile Properties

Safety Factor	0.55	
Hu =	2.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	2.20 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.85 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1400) x Ks(1.5) x $0.5 \times \tan(30)$ x π x Dia of Pile(0.6) x Height of Pile(1400)

Skin Friction = 15.83 Kn

Weight of Pile + Pile Skin Friction = 20.41 Kn

Uplift on one Pile = 3.24 Kn

Uplift is ok