

Job No.: 446-260231**Address:** 47 Parnassus Street (2), Waiau, New Zealand**Date:** 26/06/2024**Latitude:** -37.087929**Longitude:** 175.289513**Elevation:** 29.5 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	4	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	5.5 m
Wind Region	NZ1	Terrain Category	2.01	Design Wind Speed	41.06 m/s
Wind Pressure	1.01 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof $C_{p,i} = 0.636$

For roof $C_{p,e}$ from 0 m To 4.95 m $C_{p,e} = -0.9$ $p_e = -0.63$ KPa $p_{net} = -1.16$ KPa

For roof $C_{p,e}$ from 4.95 m To 9.90 m $C_{p,e} = -0.5$ $p_e = -0.35$ KPa $p_{net} = -0.88$ KPa

For wall Windward $C_{p,i} = 0.6369$ side Wall $C_{p,i} = 0.5329$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 20 m $C_{p,e} = 0.7$ $p_e = 0.61$ KPa $p_{net} = 1.12$ KPa

For side wall $C_{p,e}$ from 0 m To 4.95 m $C_{p,e} =$ $p_e = -0.57$ KPa $p_{net} = -0.06$ KPa

Maximum Upward pressure used in roof member Design = 1.16 KPa

Maximum Downward pressure used in roof member Design = 0.69 KPa

Maximum Wall pressure used in Design = 1.12 KPa

Maximum Racking pressure used in Design = 1.05 KPa

Design Summary**Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 4850 mm

Try Purlin 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 0.64 S1 Downward = 12.68 S1 Upward = 20.70

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.89 Kn-m	Capacity	3.40 Kn-m	Passing Percentage	382.02 %
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	2.62 Kn-m	Capacity	4.53 Kn-m	Passing Percentage	172.90 %
$M_{0.9D-W_nUp}$	-2.47 Kn-m	Capacity	-3.71 Kn-m	Passing Percentage	150.20 %
$V_{1.35D}$	0.74 Kn	Capacity	12.06 Kn	Passing Percentage	1629.73 %

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V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	2.16 Kn	Capacity	16.08 Kn	Passing Percentage	744.44 %
V _{0.9D-WnUp}	-2.04 Kn	Capacity	-20.10 Kn	Passing Percentage	985.29 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 8.56 mm Limit by Woolcock et al, 1999 Span/240 = 20.00 mm

Deflection under Dead and Service Wind = 12.05 mm Limit by Woolcock et al, 1999 Span/100 = 48.00 mm

Reactions

Maximum downward = 2.16 kn Maximum upward = -2.04 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 5000 mm Internal Rafter Span = 4850 mm Try Rafter 2x300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₁ Medium term = 0.8 K₁ Long term = 0.6 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 1.00 S₁ Downward = 6.81 S₁ Upward = 6.81

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	-2.53 Kn-m	Capacity	10.08 Kn-m	Passing Percentage	-398.42 %
M _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	-7.41 Kn-m	Capacity	13.44 Kn-m	Passing Percentage	-181.38 %
M _{0.9D-WnUp}	-7.00 Kn-m	Capacity	-16.8 Kn-m	Passing Percentage	240.00 %
V _{1.35D}	5.40 Kn	Capacity	28.94 Kn	Passing Percentage	535.93 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	15.85 Kn	Capacity	38.6 Kn	Passing Percentage	243.53 %
V _{0.9D-WnUp}	20.15 Kn	Capacity	-48.24 Kn	Passing Percentage	239.40 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 6.145 mm Limit by Woolcock et al, 1999 Span/240 = 20.83 mm

Deflection under Dead and Service Wind = 17.31 mm Limit by Woolcock et al, 1999 Span/100 = 50.00 mm

Reactions

Maximum downward = 7.60 kn Maximum upward = 7.18 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

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Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 14.9$ $f_{pj} = 12.9$ Mpa for Rafter with effective thickness = 100 mm

For Parallel to grain loading

$K_{11} = 2.0$ $f_{ej} = 36.1$ Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 21.67 Kn > 7.18 Kn

Prop on Sides = 1 2/SG815050Dry 1000mm Reaction Prop = 15.85 Kn down 20.15 Kn Up

Prop Combined axial and bending ratios $(M_y/\Phi \times M_{ny}) + (N_c/\Phi \times N_{cy})$ should be less than or equal to 1

For Short Term Load = 0.61 < 1 OK

For Medium Term Load = 0.24 < 1 OK

For Long Term Load = 0.06 < 1 OK

Prop Connection check

Effective width of Pole used in Calculations = 225 mm - 20mm (Margin for chamfer)

Bolt Size = M12 Number of Bolts = 2

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Angle of prop = 45 degree

Prop Connection Capacity under Short term loads: 24.85 Kn > 12.0 Kn OK

Prop Connection Capacity under Medium term loads: 19.88 Kn > 3.89 Kn OK

Prop Connection Capacity under Long term loads: 14.91 Kn > 0.76 Kn OK

Intermediate Design Sides

Intermediate Spacing = 2500 mm

Intermediate Span = 5287 mm

Try Intermediate 2x250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K_1 Short term = 1 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 0.97

K_8 Upward = 1.00 S_1 Downward = 12.68 S_1 Upward = 0.97

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	4.89 Kn-m	Capacity	11.66 Kn-m	Passing Percentage	238.45 %
$V_{0.9D-WnUp}$	3.70 Kn	Capacity	40.2 Kn	Passing Percentage	1086.49 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 40.52 mm

Limit by Woolcock et al, 1999 Span/100 = 52.87 mm

Reactions

Maximum = 3.70 kn

Girt Design Front and Back

Girt's Spacing = 800 mm

Girt's Span = 2500 mm

Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =0.97

K8 Upward =0.90 S1 Downward =12.68 S1 Upward =14.94

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.70 Kn-m	Capacity	5.26 Kn-m	Passing Percentage	751.43 %
$V_{0.9D-WnUp}$	1.12 Kn	Capacity	20.10 Kn	Passing Percentage	1794.64 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 1.04 mm

Limit by Woolcock et al, 1999 Span/100 = 25.00 mm

Sag during installation = 2.37 mm

Reactions

Maximum = 1.12 kn

Girt Design Sides

Girt's Spacing = 1200 mm

Girt's Span = 2500 mm

Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =0.97

K8 Upward =0.62 S1 Downward =12.68 S1 Upward =21.13

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.05 Kn-m	Capacity	3.59 Kn-m	Passing Percentage	341.90 %
$V_{0.9D-WnUp}$	1.68 Kn	Capacity	20.10 Kn	Passing Percentage	1196.43 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 1.57 mm

Limit by Woolcock et al. 1999 Span/100 = 25.00 mm

Sag during installation =2.37 mm

Reactions

Maximum = 1.68 kn

Middle Pole Design

Geometry

225 SED H5 (Minimum 250 dia. at Floor Level)	Dry Use	Height	4700 mm
Area	44279 mm ²	As	33209.1796875 mm ²
I _x	156100441 mm ⁴	Z _x	1314530 mm ³
I _y	156100441 mm ⁴	Z _y	1314530 mm ³
Lateral Restraint	4700 mm c/c		

Loads

Total Area over Pole = 25 m²

Dead	8.94 Kn	Live	7.16 Kn
Wind Down	24.34 Kn	Snow	0.00 Kn
Moment wind	12.45 Kn-m		
Phi	0.8	K ₈	0.68
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{cx} Wind	433.79 Kn	PhiM _{nx} Wind	25.97 Kn-m	PhiV _{nx} Wind	78.64 Kn
PhiN _{cx} Dead	260.27 Kn	PhiM _{nx} Dead	15.58 Kn-m	PhiV _{nx} Dead	47.18 Kn

Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.64 < 1$ OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.40 < 1$ OK

Deflection at top under service lateral loads = 29.86 mm < 47.00 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K ₀ =	$(1 - \sin(30)) / (1 + \sin(30))$				
K _p =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

D _s =	0.6 mm	Pile Diameter
L =	1600 mm	Pile embedment length
f ₁ =	4125 mm	Distance at which the shear force is applied
f ₂ =	0 mm	Distance of top soil at rest pressure

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Loads

Moment Wind = 12.45 Kn-m
Shear Wind = 2.88 Kn

Pile Properties

Safety Factory 0.55
Hu = 6.37 Kn Ultimate Lateral Strength of the Pile, Short pile
Mu = 15.31 Kn-m Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.81 < 1 OK

End Pole Design

Geometry For End Bay Pole

Geometry

175 SED H5 (Minimum 200 dia. at Floor Level)	Dry Use	Height	5200 mm
Area	27598 mm ²	As	20698.2421875 mm ²
Ix	60639381 mm ⁴	Zx	646820 mm ³
Iy	60639381 mm ⁴	Zy	646820 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 12.5 m²

Dead	3.13 Kn	Live	3.13 Kn
Wind Down	8.63 Kn	Snow	0.00 Kn
Moment Wind	5.94 Kn-m		
Phi	0.8	K8	0.38
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	150.09 Kn	PhiMnx Wind	7.09 Kn-m	PhiVnx Wind	49.01 Kn
PhiNcx Dead	90.05 Kn	PhiMnx Dead	4.26 Kn-m	PhiVnx Dead	29.41 Kn

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.94 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.80 < 1 OK

Deflection at top under service lateral loads = 44.87 mm < 54.86 mm

Ds =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f1 =	4125 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 12.5 m²

Moment Wind =	5.94 Kn-m
Shear Wind =	1.44 Kn

Pile Properties

Safety Factory	0.55	
Hu =	3.61 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	8.55 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.69 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	(1-sin(30)) / (1+sin(30))				
Kp =	(1+sin(30)) / (1-sin(30))				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f1 =	4125 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	5.94 Kn-m
Shear Wind =	1.44 Kn

Pile Properties

Safety Factory	0.55	
Hu =	3.61 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	8.55 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.69 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1600) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1600)

Skin Friction = 20.68 Kn

Weight of Pile + Pile Skin Friction = 24.34 Kn

Uplift on one Pile = 23.38 Kn

Uplift is ok