

Job No.: ITM Takaka - PB Shed

Address: 7 Buxton Lane, Takaka, New Zealand

Date: 18/03/2024

Latitude: -40.858081

Longitude: 172.807206

Elevation: 9.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.45 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	38.22 m/s
Wind Pressure	0.88 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 4.45 m $C_{p,e} = -0.9$ $p_e = -0.71$ KPa $p_{net} = -0.71$ KPa

For roof $C_{p,e}$ from 4.45 m To 8.90 m $C_{p,e} = -0.5$ $p_e = -0.39$ KPa $p_{net} = -0.39$ KPa

For wall Windward $C_{p,i} = 0.6731$ side Wall $C_{p,i} = -0.6$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 14 m $C_{p,e} = 0.7$ $p_e = 0.55$ KPa $p_{net} = 0.81$ KPa

For side wall $C_{p,e}$ from 0 m To 4.45 m $C_{p,e} =$ $p_e = -0.51$ KPa $p_{net} = -0.51$ KPa

Maximum Upward pressure used in roof member Design = 0.71 KPa

Maximum Downward pressure used in roof member Design = 0.42 KPa

Maximum Wall pressure used in Design = 0.81 KPa

Maximum Racking pressure used in Design = 0.94 KPa

Design Summary

Girt Design Front and Back

Girt's Spacing = 0 mm

Girt's Span = 4106 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.00 Kn-m	Capacity	0.00 Kn-m	Passing Percentage	NaN %

Deflections

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Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm

Limit by Woolcock et al, 1999 Span/100 = 41.05 mm

Sag during installation = NaN mm

Reactions

Maximum = 0.00 kn

Girt Design Sides

Girt's Spacing = 0 mm

Girt's Span = 7000 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.00 Kn-m	Capacity	0.00 Kn-m	Passing Percentage	NaN %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm

Limit by Woolcock et al. 1999 Span/100 = 70.00 mm

Sag during installation =NaN mm

Reactions

Maximum = 0.00 kn

Middle Pole Design

Geometry

250 SED H5 (Minimum 275 dia. at Floor Level)	Dry Use	Height	3900 mm
Area	54091 mm ²	As	40568.5546875 mm ²
I _x	232952248 mm ⁴	Z _x	1774874 mm ³
I _y	232952248 mm ⁴	Z _y	1774874 mm ³
Lateral Restraint	3900 mm c/c		

Loads

Total Area over Pole = 57.477 m²

Dead	14.37 Kn	Live	14.37 Kn
Wind Down	24.14 Kn	Snow	0.00 Kn
Moment wind	28.59 Kn-m		
Phi	0.8	K8	0.91
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	705.21 Kn	PhiMnx Wind	46.67 Kn-m	PhiVnx Wind	96.07 Kn
PhiNcx Dead	423.13 Kn	PhiMnx Dead	28.00 Kn-m	PhiVnx Dead	57.64 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.69 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.45 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 32.33 \text{ mm} < 39.00 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
$K_0 =$	$(1 - \sin(30)) / (1 + \sin(30))$				
$K_p =$	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

$D_s =$	0.6 mm	Pile Diameter
$L =$	2100 mm	Pile embedment length
$f_1 =$	3338 mm	Distance at which the shear force is applied
$f_2 =$	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	28.59 Kn-m
Shear Wind =	8.57 Kn

Pile Properties

Safety Factory	0.55	
$H_u =$	15.18 Kn	Ultimate Lateral Strength of the Pile, Short pile
$M_u =$	30.98 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.92 < 1 \text{ OK}$$

End Pole Design

Geometry For End Bay Pole

Geometry

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225 SED H5 (Minimum 250 dia. at Floor Level)	Dry Use	Height	4300 mm
Area	44279 mm ²	As	33209.1796875 mm ²
I _x	156100441 mm ⁴	Z _x	1314530 mm ³
I _y	156100441 mm ⁴	Z _y	1314530 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 57.477 m²

Dead	14.37 Kn	Live	14.37 Kn
Wind Down	24.14 Kn	Snow	0.00 Kn
Moment Wind	14.29 Kn-m		
Phi	0.8	K ₈	0.76
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _c Wind	486.59 Kn	PhiM _n Wind	29.13 Kn-m	PhiV _n Wind	78.64 Kn
PhiN _c Dead	291.96 Kn	PhiM _n Dead	17.48 Kn-m	PhiV _n Dead	47.18 Kn

Checks

$(M_x/\Phi M_n) + (N/\Phi N_c) = 0.60 < 1$ OK

$(M_x/\Phi M_n)^2 + (N/\Phi N_c) = 0.35 < 1$ OK

Deflection at top under service lateral loads = 27.45 mm < 44.39 mm

D _s =	0.6 mm	Pile Diameter
L =	1600 mm	Pile embedment length
f ₁ =	3338 mm	Distance at which the shear force is applied
f ₂ =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 57.477 m²

Moment Wind =	14.29 Kn-m
Shear Wind =	4.28 Kn

Pile Properties

Safety Factor	0.55	
H _u =	7.39 Kn	Ultimate Lateral Strength of the Pile, Short pile
M _u =	14.63 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.98 < 1$ OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1600 mm	Pile embedment length
f1 =	3338 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	14.29 Kn-m
Shear Wind =	4.28 Kn

Pile Properties

Safety Factory	0.55	
Hu =	7.39 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	14.63 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.98 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(2100) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(2100)

Skin Friction = 35.62 Kn

Weight of Pile + Pile Skin Friction = 39.84 Kn

Uplift on one Pile = 27.88 Kn

Uplift is ok