

Job No.: 511-5026100**Address:** 9 Tuarangi Road, Netherby, Ashburton 7700, New Zealand **Date:** 29/10/2024**Latitude:** -43.898495**Longitude:** 171.771433**Elevation:** 93 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N4	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.6 m
Wind Region	NZ2	Terrain Category	2.77	Design Wind Speed	35.62 m/s
Wind Pressure	0.76 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Medium	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof $C_{p,i} = 0.6899$

For roof $C_{p,e}$ from 0 m To 3.3 m $C_{p,e} = -0.9$ $p_e = -0.49$ KPa $p_{net} = -0.94$ KPa

For roof $C_{p,e}$ from 3.3 m To 6.6 m $C_{p,e} = -0.5$ $p_e = -0.27$ KPa $p_{net} = -0.72$ KPa

For wall Windward $C_{p,i} = 0.6899$ side Wall $C_{p,i} = -0.6312$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 18.6 m $C_{p,e} = 0.7$ $p_e = 0.46$ KPa $p_{net} = 0.96$ KPa

For side wall $C_{p,e}$ from 0 m To 3.3 m $C_{p,e} =$ $p_e = -0.43$ KPa $p_{net} = 0.07$ KPa

Maximum Upward pressure used in roof member Design = 0.94 KPa

Maximum Downward pressure used in roof member Design = 0.63 KPa

Maximum Wall pressure used in Design = 0.96 KPa

Maximum Racking pressure used in Design = 0.82 KPa

Design Summary**Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 4650 mm

Try Purlin 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.77 S1 Downward = 11.27 S1 Upward = 18.02

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.82 Kn-m	Capacity	2.23 Kn-m	Passing Percentage	271.95 %
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	2.26 Kn-m	Capacity	2.97 Kn-m	Passing Percentage	131.42 %
$M_{0.9D-W_nUp}$	-1.74 Kn-m	Capacity	-2.86 Kn-m	Passing Percentage	186.93 %
$V_{1.35D}$	0.71 Kn	Capacity	9.65 Kn	Passing Percentage	1359.15 %

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V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	1.95 Kn	Capacity	12.86 Kn	Passing Percentage	659.49 %
V _{0.9D-WnUp}	-1.50 Kn	Capacity	-16.08 Kn	Passing Percentage	1072.00 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 14.10 mm Limit by Woolcock et al, 1999 Span/240 = 19.17 mm

Deflection under Dead and Service Wind = 19.15 mm Limit by Woolcock et al, 1999 Span/100 = 46.00 mm

Reactions

Maximum downward = 1.95 kn Maximum upward = -1.50 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4800 mm Internal Rafter Span = 4350 mm Try Rafter 2x300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₁ Medium term = 0.8 K₁ Long term = 0.6 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 1.00 S₁ Downward = 6.81 S₁ Upward = 6.81

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	3.83 Kn-m	Capacity	10.08 Kn-m	Passing Percentage	263.19 %
M _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	10.56 Kn-m	Capacity	13.44 Kn-m	Passing Percentage	127.27 %
M _{0.9D-WnUp}	-8.12 Kn-m	Capacity	-16.8 Kn-m	Passing Percentage	206.90 %
V _{1.35D}	3.52 Kn	Capacity	28.94 Kn	Passing Percentage	822.16 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	9.71 Kn	Capacity	38.6 Kn	Passing Percentage	397.53 %
V _{0.9D-WnUp}	-7.46 Kn	Capacity	-48.24 Kn	Passing Percentage	646.65 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 5.695 mm Limit by Woolcock et al, 1999 Span/240 = 18.75 mm

Deflection under Dead and Service Wind = 8.595 mm Limit by Woolcock et al, 1999 Span/100 = 45.00 mm

Reactions

Maximum downward = 9.71 kn Maximum upward = -7.46 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 14.9$ $f_{pj} = 12.9$ Mpa for Rafter with effective thickness = 100 mm

For Parallel to grain loading

$K_{11} = 2.0$ $f_{ej} = 36.1$ Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 21.67 Kn > -7.46 Kn

Rafter Design External

External Rafter Load Width = 2400 mm

External Rafter Span = 4310 mm

Try Rafter 300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K_1 Short term = 1 K_1 Medium term = 0.8 K_1 Long term = 0.6 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 0.94

K_8 Upward = 0.94 S_1 Downward = 13.93 S_1 Upward = 13.93

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	1.88 Kn-m	Capacity	4.72 Kn-m	Passing Percentage	251.06 %
$M_{1.2D+1.5L \ 1.2D+S_n \ 1.2D+W_nD_n}$	5.18 Kn-m	Capacity	6.30 Kn-m	Passing Percentage	121.62 %
$M_{0.9D-W_nUp}$	-3.98 Kn-m	Capacity	-7.87 Kn-m	Passing Percentage	197.74 %
$V_{1.35D}$	1.75 Kn	Capacity	14.47 Kn	Passing Percentage	826.86 %
$V_{1.2D+1.5L \ 1.2D+S_n \ 1.2D+W_nD_n}$	4.81 Kn	Capacity	19.30 Kn	Passing Percentage	401.25 %
$V_{0.9D-W_nUp}$	-3.70 Kn	Capacity	-24.12 Kn	Passing Percentage	651.89 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k_2 for Long Term Loads = 2

Deflection under Dead and Live Load = 6.33 mm

Limit by Woolcock et al, 1999 Span/240 = 18.75 mm

Deflection under Dead and Service Wind = 8.60 mm

Limit by Woolcock et al, 1999 Span/100 = 45.00 mm

Reactions

Maximum downward = 4.81 kn Maximum upward = -3.70 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 14.9$ $f_{pj} = 12.9$ Mpa for Rafter with effective thickness = 50 mm

For Parallel to grain loading

$K_{11} = 2.0$ $f_{c,j} = 36.1$ Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

$V = \phi_i \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s \dots\dots\dots$ (Eq 4.12) = -25.20 kn > -3.70 Kn

Single Shear Capacity under short term loads = -10.84 Kn > -3.70 Kn

Intermediate Design Front and Back

Intermediate Spacing = 2400 mm

Intermediate Span = 2849 mm

Try Intermediate 2x150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K_1 Short term = 1 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 1.00

K_8 Upward = 1.00 S_1 Downward = 9.63 S_1 Upward = 0.54

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	2.34 Kn-m	Capacity	4.2 Kn-m	Passing Percentage	179.49 %
$V_{0.9D-WnUp}$	3.28 Kn	Capacity	-24.12 Kn	Passing Percentage	735.37 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 25.215 mm

Limit by Woolcock et al, 1999 Span/100 = 28.49 mm

Reactions

Maximum = 3.28 kn

Intermediate Design Sides

Intermediate Spacing = 2250 mm

Intermediate Span = 3300 mm

Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K_1 Short term = 1 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 1.00

K_8 Upward = 1.00 S_1 Downward = 11.27 S_1 Upward = 0.68

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.47 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	507.48 %
$V_{0.9D-WnUp}$	1.78 Kn	Capacity	32.16 Kn	Passing Percentage	1806.74 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 17.945 mm

Limit by Woolcock et al, 1999 Span/100 = 33.00 mm

Reactions

Maximum = 1.78 kn

Girt Design Front and Back

Girt's Spacing = 1300 mm

Girt's Span = 2400 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.87 S1 Downward =9.63 S1 Upward =15.73

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.90 Kn-m	Capacity	1.83 Kn-m	Passing Percentage	203.33 %
$V_{0.9D-WnUp}$	1.50 Kn	Capacity	12.06 Kn	Passing Percentage	804.00 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 9.48 mm

Limit by Woolcock et al, 1999 Span/100 = 24.00 mm

Sag during installation = 2.01 mm

Reactions

Maximum = 1.50 kn

Girt Design Sides

Girt's Spacing = 1300 mm

Girt's Span = 2250 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.89 S1 Downward =9.63 S1 Upward =15.23

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.79 Kn-m	Capacity	1.87 Kn-m	Passing Percentage	236.71 %
$V_{0.9D-WnUp}$	1.40 Kn	Capacity	12.06 Kn	Passing Percentage	861.43 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 7.32 mm

Limit by Woolcock et al. 1999 Span/100 = 22.50 mm

Sag during installation =1.55 mm

Reactions

Maximum = 1.40 kn

Middle Pole Design

Geometry

175 SED H5 (Minimum 200 dia. at Floor Level)	Dry Use	Height	3300 mm
Area	27598 mm ²	As	20698.2421875 mm ²
I _x	60639381 mm ⁴	Z _x	646820 mm ³
I _y	60639381 mm ⁴	Z _y	646820 mm ³
Lateral Restraint	3300 mm c/c		

Loads

Total Area over Pole = 21.6 m²

Dead	5.40 Kn	Live	5.40 Kn
Wind Down	13.61 Kn	Snow	13.61 Kn
Moment wind	6.36 Kn-m	Moment snow	2.59 Kn-m
Phi	0.8	K ₈	0.79
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{cx} Wind	312.81 Kn	PhiM _{nx} Wind	14.79 Kn-m	PhiV _{nx} Wind	49.01 Kn
PhiN _{cx} Dead	187.69 Kn	PhiM _{nx} Dead	8.87 Kn-m	PhiV _{nx} Dead	29.41 Kn
PhiN _{cx} Snow	250.25 Kn	PhiM _{nx} Snow	11.83 Kn-m	PhiV _{nx} Snow	39.21 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.52 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.27 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 18.91 mm < 33.00 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K ₀ =	(1-sin(30)) / (1+sin(30))				
K _p =	(1+sin(30)) / (1-sin(30))				

Geometry For Middle Bay Pole

D _s =	0.6 mm	Pile Diameter
L =	1450 mm	Pile embedment length
f _l =	2700 mm	Distance at which the shear force is applied

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$f_2 =$ 0 mm Distance of top soil at rest pressure

Loads

Moment Wind =	6.36 Kn-m	Moment Snow =	Kn-m
Shear Wind =	2.36 Kn	Shear Snow =	2.59 Kn

Pile Properties

Safety Factory	0.55		
$H_u =$	6.55 Kn	Ultimate Lateral Strength of the Pile, Short pile	
$M_u =$	10.61 Kn-m	Ultimate Moment Capacity of Pile	

Checks

Applied Forces/Capacities = 0.60 < 1 OK

End Pole Design

Geometry For End Bay Pole

Geometry

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	3300 mm
Area	20729 mm ²	A_s	15546.6796875 mm ²
I_x	34210793 mm ⁴	Z_x	421056 mm ³
I_y	34210793 mm ⁴	Z_y	421056 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 10.8 m²

Dead	2.70 Kn	Live	2.70 Kn
Wind Down	6.80 Kn	Snow	6.80 Kn
Moment Wind	3.18 Kn-m	Moment snow	1.29 Kn-m
Φ	0.8	K ₈	0.66
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	E =	9257 MPa

Capacities

ΦH_{Ncx} Wind	195.59 Kn	ΦH_{Mnx} Wind	8.01 Kn-m	ΦV_{Ncx} Wind	36.81 Kn
ΦH_{Ncx} Dead	117.35 Kn	ΦH_{Mnx} Dead	4.81 Kn-m	ΦV_{Ncx} Dead	22.09 Kn
ΦH_{Ncx} Snow	156.47 Kn	ΦH_{Mnx} Snow	6.41 Kn-m	ΦV_{Ncx} Snow	29.45 Kn

Checks

$$(M_x/\phi M_{nx}) + (N/\phi N_{cx}) = 0.47 < 1 \text{ OK}$$

$$(M_x/\phi M_{nx})^2 + (N/\phi N_{cx}) = 0.23 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 18.24 mm < 35.91 mm

Ds =	0.6 mm	Pile Diameter
L =	1450 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 10.8 m²

Moment Wind =	3.18 Kn-m	Moment Snow =	1.29 Kn-m
Shear Wind =	1.18 Kn	Shear Snow =	1.29 Kn

Pile Properties

Safety Factory	0.55	
Hu =	6.55 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	10.61 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.30 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1450 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	3.18 Kn-m	Moment Snow =	1.29 Kn-m
Shear Wind =	1.18 Kn	Shear Snow =	1.29 Kn

Pile Properties

Safety Factory	0.55	
Hu =	6.55 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	10.61 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.30 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m^3

Density of Timber Pole = 5 Kn/m^3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K_s (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) \times Density of Soil (18) \times Height of Pile (1450) $\times K_s$ (1.5) $\times 0.5 \times \tan(30) \times \pi \times \text{Dia of Pile}$ (0.6) \times Height of Pile (1450)

Skin Friction = 16.98 Kn

Weight of Pile + Pile Skin Friction = 21.22 Kn

Uplift on one Pile = 15.44 Kn

Uplift is ok