Pole Shed App Ver 01 2022

 Job No.:
 2407032 - 1
 Address:
 2395a Coastal Highway, Motueka, New Zealand
 Date:
 28/10/2024

 Latitude:
 -41.148333
 Longitude:
 173.006631
 Elevation:
 31.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	D
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	6.5 m
Wind Region	NZ2	Terrain Category	1.42	Design Wind Speed	49.1 m/s
Wind Pressure	1.45 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Very High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Gable Enclosed

For roof Cp, i = -0.3

For roof CP,e from 0 m To 5.95 m Cpe = -0.9 pe = -1.17 KPa pnet = -1.17 KPa

For roof CP,e from 5.95 m To 11.90 m Cpe = -0.5 pe = -0.65 KPa pnet = -0.65 KPa

For wall Windward Cp, i = -0.3 side Wall Cp, i = -0.3

For wall Windward and Leeward $\,$ CP,e $\,$ from 0 m $\,$ To 8 m $\,$ Cpe = 0.7 $\,$ pe = 0.91 KPa $\,$ pnet = 1.34 KPa

For side wall CP,e from 0 m To 5.95 m Cpe = pe = -0.85 KPa pnet = -0.85 KPa

Maximum Upward pressure used in roof member Design = 1.17 KPa

Maximum Downward pressure used in roof member Design = 0.56 KPa

Maximum Wall pressure used in Design = 1.34 KPa

Maximum Racking pressure used in Design = 1.31 KPa

Design Summary

Intermediate Design Sides

Intermediate Spacing = 4000 mm Intermediate Span = 6350 mm Try Intermediate 2x300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.94

K8 Upward = 1.00 S1 Downward = 13.93 S1 Upward = 1.17

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	13.51 Kn-m	Capacity	16.8 Kn-m	Passing Percentage	124.35 %
$ m V_{0.9D ext{-}WnUp}$	8.51 Kn	Capacity	48.24 Kn	Passing Percentage	566.86 %

Deflections

Second page

Pole Shed App Ver 01 2022

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 93.395 mm

Limit by Woolcock et al, 1999 Span/100 = 63.50 mm

Reactions

Maximum = 8.51 kn

Girt Design Front and Back

Girt's Spacing = 700 mm

Girt's Span = 5000 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.89 S1 Downward =11.27 S1 Upward =15.34

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	2.93 Kn-m	Capacity	3.31 Kn-m	Passing Percentage	112.97 %
$V_{0.9D\text{-W}nUp}$	2.35 Kn	Capacity	16.08 Kn	Passing Percentage	684.26 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 34.18 mm

Limit by Woolcock et al, 1999 Span/100 = 50.00 mm

Sag during installation = 37.90 mm

Reactions

Maximum = 2.35 kn

Girt Design Sides

Girt's Spacing = 700 mm

Girt's Span = 4000 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.92 S1 Downward =9.63 S1 Upward =14.36

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.88 Kn-m	Capacity	1.94 Kn-m	Passing Percentage	103.19 %
V _{0.9D-WnUp}	1.88 Kn	Capacity	12.06 Kn	Passing Percentage	641.49 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 33.19 mm

Limit by Woolcock et al. 1999 Span/100 = 40.00 mm

Sag during installation =15.52 mm

Pole Shed App Ver 01 2022

Reactions

Maximum = 1.88 kn

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(2200) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(2200)

Skin Friction = 39.09 Kn

Weight of Pile + Pile Skin Friction = 42.94 Kn

Uplift on one Pile = 18.90 Kn

Uplift is ok