Pole Shed App Ver 01 2022

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Job No.: Southern Pastures Mamaku-Training	**Address:** 142 Mamaku South Road Kinleith New Zealand, Tokoroa, New Zealand	**Date:** 16/06/2025
Latitude: -38.251015	**Longitude:** 176.054543	**Elevation:** 608 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.75 m
Wind Region	NZ2	Terrain Category	2.27	Design Wind Speed	45.85 m/s
Wind Pressure	1.26 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Very High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Mono Open

For roof Cp,i = 0.656

For roof CP,e from 0 m To 3.75 m Cpe = -0.9 pe = -1.00 KPa pnet = -1.88 KPa

For roof CP,e from 3.75 m To 7.50 m Cpe = -0.5 pe = -0.56 KPa pnet = -1.44 KPa

For wall Windward Cp,i = 0.656 side Wall Cp,i = -0.5682

For wall Windward and Leeward CP,e from 0 m To 13.5 m Cpe = 0.7 pe = 0.79 KPa pnet = 1.57 KPa

For side wall CP,e from 0.0 m To 3.75 m Cpe = pe = -0.74 KPa pnet = 0.04 KPa

Maximum Upward pressure used in roof member Design = 1.88 KPa

Maximum Downward pressure used in roof member Design = 1.01 KPa

Maximum Wall pressure used in Design = 1.57 KPa

Maximum Racking pressure used in Design = 1.34 KPa

Design Summary

Purlin Design

Purlin Spacing = 900 mm	Purlin Span = 4350 mm	Try Purlin 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

Second page

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 =1 K5 =1 K8 Downward =0.97

K8 Upward =0.69 S1 Downward =12.68 S1 Upward =19.59

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.72 Kn-m	Capacity	3.40 Kn-m	Passing Percentage	**472.22 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	2.79 Kn-m	Capacity	4.53 Kn-m	Passing Percentage	**162.37 %**
$M_{0.9D-WnUp}$	-3.52 Kn-m	Capacity	-4.02 Kn-m	Passing Percentage	**114.20 %**
$V_{1.35D}$	0.66 Kn	Capacity	12.06 Kn	Passing Percentage	**1827.27 %**
$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	2.56 Kn	Capacity	16.08 Kn	Passing Percentage	**628.12 %**
$V_{0.9D-WnUp}$	-3.24 Kn	Capacity	-20.10 Kn	Passing Percentage	**620.37 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 8.77 mm	Limit by Woolcock et al, 1999 Span/240 = 17.92 mm
Deflection under Dead and Service Wind = 9.23 mm	Limit by Woolcock et al, 1999 Span/100 = 43.00 mm

Reactions

Maximum downward =2.56 kn Maximum upward = -3.24 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4500 mm Internal Rafter Span = 3850 mm Try Rafter 2x300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =6.81 S1 Upward =6.81

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	2.81 Kn-m	Capacity	10.08 Kn-m	Passing Percentage	**358.72 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	10.92 Kn-m	Capacity	13.44 Kn-m	Passing Percentage	**123.08 %**

$M_{0.9D\text{-}WnUp}$	-13.80 Kn-m	Capacity	-16.8 Kn-m	Passing Percentage	**121.74 %**
$V_{1.35D}$	2.92 Kn	Capacity	28.94 Kn	Passing Percentage	**991.10 %**
$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	11.35 Kn	Capacity	38.6 Kn	Passing Percentage	**340.09 %**
$V_{0.9D\text{-}WnUp}$	-14.34 Kn	Capacity	-48.24 Kn	Passing Percentage	**336.40 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 3.335 mm Limit by Woolcock et al, 1999 Span/240 = 16.67 mm
Deflection under Dead and Service Wind = 6.205 mm Limit by Woolcock et al, 1999 Span/100 = 40.00 mm

Reactions

Maximum downward =11.35 kn Maximum upward = -14.34 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters =J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 100 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 21.67 Kn > -14.34 Kn

Rafter Design External

External Rafter Load Width = 2250 mm External Rafter Span = 3808 mm Try Rafter 300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 =1 K5 =1 K8 Downward =0.94

K8 Upward =0.94 S1 Downward =13.93 S1 Upward =13.93

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	1.38 Kn-m	Capacity	4.72 Kn-m	Passing Percentage	**342.03 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	5.34 Kn-m	Capacity	6.30 Kn-m	Passing Percentage	**117.98 %**
$M_{0.9D-WnUp}$	-6.75 Kn-m	Capacity	-7.87 Kn-m	Passing Percentage	**116.59 %**
$V_{1.35D}$	1.45 Kn	Capacity	14.47 Kn	Passing Percentage	**997.93 %**
$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	5.61 Kn	Capacity	19.30 Kn	Passing Percentage	**344.03 %**
$V_{0.9D-WnUp}$	-7.09 Kn	Capacity	-24.12 Kn	Passing Percentage	**340.20 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 3.70 mm	Limit by Woolcock et al, 1999 Span/240= 16.67 mm
Deflection under Dead and Service Wind = 6.20 mm	Limit by Woolcock et al, 1999 Span/100 = 40.00 mm

Reactions

Maximum downward =5.61 kn Maximum upward = -7.09 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters =J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 50 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

V = phi x k1 x k4 x k5 x fs x b x ds .... (Eq 4.12) = -25.20 kn > -7.09 Kn

Single Shear Capacity under short term loads = -10.84 Kn > -7.09 Kn

Intermediate Design Front and Back

Intermediate Spacing = 2250 mm   Intermediate Span = 3099 mm   Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =1.00   S1 Downward =11.27   S1 Upward =0.66

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	4.24 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	**175.94 %**
$V_{0.9D\text{-}WnUp}$	5.47 Kn	Capacity	-32.16 Kn	Passing Percentage	**587.93 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 11.79 mm   Limit byWoolcock et al, 1999 Span/100 = 30.99 mm

Reactions

Maximum = 5.47 kn

Intermediate Design Sides

Intermediate Spacing = 2000 mm   Intermediate Span = 3475 mm   Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =1.00   S1 Downward =11.27   S1 Upward =0.70

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	2.37 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	**314.77 %**
$V_{0.9D\text{-}WnUp}$	2.73 Kn	Capacity	32.16 Kn	Passing Percentage	**1178.02 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 16.56 mm Limit by Woolcock et al, 1999 Span/100 = 34.75 mm

Reactions

Maximum = 2.73 kn

Girt Design Front and Back

Girt's Spacing = 900 mm Girt's Span = 2250 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.78 S1 Downward =11.27 S1 Upward =17.82

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.89 Kn-m	Capacity	2.90 Kn-m	Passing Percentage	**325.84 %**
$V_{0.9D-WnUp}$	1.59 Kn	Capacity	16.08 Kn	Passing Percentage	**1011.32 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 2.11 mm Limit by Woolcock et al, 1999 Span/100 = 22.50 mm
Sag during installation = 1.55 mm

Reactions

Maximum = 1.59 kn

Girt Design Sides

Girt's Spacing = 900 mm Girt's Span = 2000 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.82 S1 Downward =11.27 S1 Upward =16.80

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.71 Kn-m	Capacity	3.08 Kn-m	Passing Percentage	**433.80 %**
$V_{0.9D-WnUp}$	1.41 Kn	Capacity	16.08 Kn	Passing Percentage	**1140.43 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 1.32 mm Limit by Woolcock et al. 1999 Span/100 = 20.00 mm
Sag during installation =0.97 mm

Reactions

Maximum = 1.41 kn

Middle Pole Design

Geometry

250 SED H5 (Minimum 275 dia. at Floor Level)	Dry Use	Height	3750 mm
Area	13125 mm2	As	9843.75 mm2
Ix	75366211 mm4	Zx	574219 mm3
Iy	75366211 mm4	Zx	574219 mm3
Lateral Restraint	3750 mm c/c		

Loads

Total Area over Pole = 18 m2

Dead	4.50 Kn	Live	4.50 Kn
Wind Down	18.18 Kn	Snow	0.00 Kn
Moment wind	10.57 Kn-m		
Phi	0.8	K8	0.93
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa

ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	174.97 Kn	PhiMnx Wind	15.44 Kn-m	PhiVnx Wind	23.31 Kn
PhiNcx Dead	104.98 Kn	PhiMnx Dead	9.26 Kn-m	PhiVnx Dead	13.99 Kn

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.84 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.62 < 1 OK

Deflection at top under service lateral loads = 29.94 mm < 37.50 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m3	Friction angle	30 deg	Cohesion	0 Kn/m3
K0 =	(1-sin(30)) / (1+sin(30))				
Kp =	(1+sin(30)) / (1-sin(30))				

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2813 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	10.57 Kn-m
Shear Wind =	3.76 Kn

Pile Properties

Safety Factory	0.55	
Hu =	6.97 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	11.76 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.90 < 1 OK

End Pole Design

Geometry For End Bay Pole

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	3450 mm
Area	10625 mm2	As	7968.75 mm2
Ix	39982096 mm4	Zx	376302 mm3
Iy	39982096 mm4	Zx	376302 mm3
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 4.5 m2

Dead	1.13 Kn	Live	1.13 Kn
Wind Down	4.54 Kn	Snow	0.00 Kn
Moment Wind	5.29 Kn-m		
Phi	0.8	K8	0.85
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	130.00 Kn	PhiMnx Wind	9.28 Kn-m	PhiVnx Wind	18.87 Kn
PhiNcx Dead	78.00 Kn	PhiMnx Dead	5.57 Kn-m	PhiVnx Dead	11.32 Kn

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.62 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.38 < 1 OK

Deflection at top under service lateral loads = 28.15 mm < 37.41 mm

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length

f1 =	2813 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 4.5 m2

Moment Wind =	5.29 Kn-m
Shear Wind =	1.88 Kn

Pile Properties

Safety Factory	0.55	
Hu =	6.97 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	11.76 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.45 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m3	Friction angle	30 deg	Cohesion	0 Kn/m3
K0 =	(1-sin(30)) / (1+sin(30))				
Kp =	(1+sin(30)) / (1-sin(30))				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2813 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	5.29 Kn-m
Shear Wind =	1.88 Kn

Pile Properties

Safety Factory	0.55	
Hu =	6.97 Kn	Ultimate Lateral Strength of the Pile, Short pile

Mu = 11.76 Kn-m Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.45 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient)for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 21.19 Kn

Uplift on one Pile = 29.79 Kn

Uplift is ok