**Job No.:** 2502034 - 1 **Address:** 659 Long Plain Road, Tākaka 7183, New **Date:** 02/04/2025

Zealand

**Latitude:** -40.910046 **Longitude:** 172.762292 **Elevation:** 93.5 m

### **General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	В
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.7 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	38.22 m/s
Wind Pressure	0.88 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

#### **Pressure Coefficients and Pressues**

Shed Type = Gable Enclosed

For roof Cp, i = -0.3

For roof CP,e from 0 m To 4.05 m Cpe = -0.9 pe = -0.71 KPa pnet = -0.71 KPa

For roof CP,e from 4.05 m To 8.10 m Cpe = -0.5 pe = -0.39 KPa pnet = -0.39 KPa

For wall Windward Cp, i = -0.3 side Wall Cp, i = -0.3

For wall Windward and Leeward CP,e from 0 m To 13.5 m Cpe = 0.7 pe = 0.55 KPa pnet = 0.81 KPa

For side wall CP,e from 0 m To 4.05 m Cpe = pe = -0.51 KPa pnet = -0.51 KPa

Maximum Upward pressure used in roof member Design = 0.71 KPa

Maximum Downward pressure used in roof member Design = 0.42 KPa

Maximum Wall pressure used in Design = 0.81 KPa

Maximum Racking pressure used in Design = 0.79 KPa

#### **Design Summary**

## Girt Design Front and Back

Girt's Spacing = 0 mm Girt's Span = 2250 mm Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

Second page

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

## **Capacity Checks**

$M_{Wind+Snow}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$ m V_{0.9D ext{-}WnUp}$	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm Limit by Woolcock et al, 1999 Span/100 = 22.50 mm Sag during installation = NaN mm

#### Reactions

Maximum = 0.00 kn

## **Girt Design Sides**

Girt's Spacing = 0 mm Girt's Span = 3000 mm Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = NaN

K8 Upward =NaN S1 Downward =NaN S1 Upward =NaN

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

## **Capacity Checks**

$M_{Wind+Snow}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9 D\text{-W} n U p}$	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm Limit by Woolcock et al. 1999 Span/100 = 30.00 mm Sag during installation = NaN mm

#### Reactions

Maximum = 0.00 kn

## Middle Pole Design

## Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	4340 mm
Area	35448 mm2	As	26585.7421875 mm2
Ix	100042702 mm4	Zx	941578 mm3
Iy	100042702 mm4	Zx	941578 mm3
Lateral Restraint	4340 mm c/c		

#### Loads

Total Area over Pole = 27.0000000000675 m2

Dead	6.75 Kn	Live	6.75 Kn
Wind Down	11.34 Kn	Snow	0.00 Kn
Moment wind	12.59 Kn-m		
Phi	0.8	K8	0.65
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

#### Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	$f_S =$	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

## Capacities

PhiNex Wind	331.45 Kn	PhiMnx Wind	17.76 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	198.87 Kn	PhiMnx Dead	10.65 Kn-m	PhiVnx Dead	37.77 Kn

## Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.78 < 1 OK

 $(Mx/PhiMnx)^2 + (N/phiNcx) = 0.58 < 1 \text{ OK}$ 

Deflection at top under service lateral loads = 38.96 mm < 43.40 mm

## Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

#### **Assumed Soil Properties**

Gamma 18 Kn/m3 Friction angle 30 deg Cohesion 0 Kn/m3

 $K0 = \frac{(1-\sin(30))}{(1+\sin(30))}$  $Kp = \frac{(1+\sin(30))}{(1-\sin(30))}$ 

### Geometry For Middle Bay Pole

 $D_S = 0.6 \text{ mm}$  Pile Diameter

L= 1700 mm Pile embedment length

f1 = 3525 mm Distance at which the shear force is applied

f2 = 0 mm Distance of top soil at rest pressure

#### Loads

Moment Wind = 12.59 Kn-mShear Wind = 3.57 Kn

#### Pile Properties

Safety Factory 0.55

Hu = 8.38 Kn Ultimate Lateral Strength of the Pile, Short pile

Mu = 17.52 Kn-m Ultimate Moment Capacity of Pile

#### Checks

Applied Forces/Capacities = 0.72 < 1 OK

## **Uplift Check**

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1700) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1700)

Skin Friction = 23.34 Kn

Weight of Pile + Pile Skin Friction = 27.76 Kn

Uplift on one Pile = 13.10 Kn

Uplift is ok