

Job Number: {this.jobNumber}

Issue:

**BWhite  
Consulting Ltd**

**PRODUCER STATEMENT-PS1-DESIGN**

ISSUED BY: **alice**

TO BE SUPPLIED TO: **D District Council** IN RESPECT OF: **Proposed NEW Farm Shed**

AT: **xyz**

**LEGAL DESCRIPTION**

We have been engaged by **Ezequote Pty Ltd** to provide **Specific Structural Engineering Design** services in respect of the requirements of Clause(s) **B1** of the Building Code for part only (as specified in the attachment to this statement), of the proposed building work.

☐ ALL ☒ Part only as specified: Purlins, Rafters, Girts, Poles, Columns, Pole embedment and all connections

The design has been prepared in accordance with compliance documents to NZ Building Code issued by Ministry of Business, Innovation & Employment Clauses **B1/VM1 and B1/VM4**

The proposed building work covered by the producer statement is described on **Ezequote** drawings title **abc123** and numbered dated together with the following specification, and other documents set out in the schedule attached to this statement: **Design Featured Report Dated 2025-07-18 and numbered "Second Page"**

On behalf of **BWhite Consulting Ltd**, and subject to:

1. Site verification of the following design assumptions: **an Ultimate foundation bearing pressure of 300 kPa in accordance with NZS3604:2011**
2. **The building has a design life of 50 years and an Importance Level 1**
3. **Unless specifically noted, compliance of the drawings to Non-Specific codes such as NZS3604 and NZS4229 have not been checked by this practice**
4. **This Certificate does not cover any other building code clause including weather tightness**
5. **Inspections of the building to be completed by D District Council. As BWhite Consulting Ltd are not undertaking inspections, we cannot issue a producer Statement-PS4- Construction Review.**
6. **This Producer Statement- Design is valid for a building consent issued within 1 year from the date of issue**
7. All proprietary products meeting their performance specification requirements

**I believe on reasonable grounds** that a) the building, if constructed in accordance with the drawings, specifications, and other documents provided or listed in the attached schedule, will comply with the relevant provisions of the Building Code and that b), the persons who have undertaken the design have the necessary competency to do so. I also recommend the follow level of construction monitoring/observation:

☒ CM1 ☐ CM2 ☐ CM3 ☐ CM4 ☐ CM5 or as per agreement with owner/developer (**stated above**)

I, **Bevan White** am CPEng **108276** I am Member of Engineering New Zealand and hold the following qualification: **BE.Civil** and holds a current policy of Professional Indemnity Insurance no less than \$200,000

Signed by **Bevan White** on behalf of **BWhite Consulting Ltd** Dated: **2025-07-18**

Email: **bwhitecpeng@gmail.com** Phone: **0211-979786**

Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement accrues to the Design Firm only. The total maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work, whether in contract, tort or otherwise(including negligence), is limited to the sum of \$200,000.

This form is to accompany Form 2 of the Building(Forms) Regulations 2004 for the application of a Building Consent

**Date:** 2025-07-18

18B Jules Crescent,

Bell Block New Plymouth 4312

New Zealand

**BWhite  
Consulting Ltd**

File No:

**DESIGN FEATURES SUMMARY FOR PROPOSED NEW FARM SHED XYZ**

**Site Specific Loads**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & EQ ARI	0 Years	Max Height	1 m
Wind Region		Terrain Category		Design Wind Speed	1 m/s
Wind Pressure	0 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years

**Timber**

Sawn Timber to be graded to the properties of SG6 and SG8 or better as mentioned on plans, with moisture content of 18% or less for dry and 25% or less for wet.

The following standards have been used in the design of this structure

- NZS 3603:1993 Timber Structures Standard
- NZS 3604:2011 Timber Framed Buildings. Standards New Zealand, 2011
- NZS 3404:1997 Steel Structures
- AS/NZS 1170 2003 Structural Design Actions
- AS/NZS 1170.2 2021 Structural Design Actions-Wind Action
- Branz. "Engineering Basis of NZS 3604". April 2013

Yours Faithfully

**BWhite CONSULTING LTD**

**Bevan White**

Director | BE Civil . CMengNZ CPEng

Email: bwhitecpeng@gmail.com Contact: 0211 979 786

Date: 2025-07-18

Council: D Council

***BWhite  
Consulting Ltd***

**Subject: B2 compliance in respect of Proposed shed at xyz**

D Council typically requests a Producer Statement/Other means of compliance for Design for Clause B2 of the Building Code-Durability

We are not able to provide a Producer Statement for durability because compliance needs to be shown on material-by-material basis using a variety of compliance methods, and not all materials used have a clear compliance path.

We can confirm that for the structural elements shown in our documentation under Clause B1:

**Timber**

Timber treatment has been selected to meet or exceed the requirements of table 1A of B2/AS1 and NZS3602

**Steel fixing**

Steel fixings are protected against weather as per table 4.1 and 4.2 of NZS3604-2011. Exposure Zone B

Yours Faithfully

**BWhite CONSULTING LTD**

**Bevan White**

Director | BE Civil . CMengNZ CPEng

Email: bwhitecpeng@gmail.com

Contact: 0211 979 786

Note: This letter shall only be relied on by the Building Consent Authority named in Engineering New Zealand/ACE New Zealand Producer Statement PS1(B1) - Design in relation to the Building Work. Liability under this letter accrues to the Design Review Firm only. The total maximum amount of damages payable arising from this letter and all other statements provided to the Building Consent Authority in relation to this Building Work whether in contract, tort or otherwise (including negligence), is limited to the sum of \$200,000

**Job No.:** abc123

**Address:** xyz

**Date:** 2025-07-18

**Latitude:** 0

**Longitude:** 0

**Elevation:** 1 m

### General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	0 Years	Max Height	1 m
Wind Region		Terrain Category		Design Wind Speed	1 m/s
Wind Pressure	0 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Low	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

### Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof  $C_{p,i} = 1$

For roof  $C_{p,e}$  from 1 m To 1 m  $C_{p,e} = 1$   $p_e = 1$  KPa  $p_{net} = 1$  KPa

For roof  $C_{p,e}$  from 1 m To 1 m  $C_{p,e} = 1$   $p_e = 1$  KPa  $p_{net} = 1$  KPa

For wall Windward  $C_{p,i} = 1$  side Wall  $C_{p,i} = 1$

For wall Windward and Leeward  $C_{p,e}$  from 1 m To 1 m  $C_{p,e} = 1$   $p_e = 1$  KPa  $p_{net} = 1$  KPa

For side wall  $C_{p,e}$  from 1 m To 1 m  $C_{p,e} =$   $p_e = 1$  KPa  $p_{net} = 1$  KPa

Maximum Upward pressure used in roof member Design = 1 KPa

Maximum Downward pressure used in roof member Design = 1 KPa

Maximum Wall pressure used in Design = 1 KPa

Maximum Racking pressure used in Design = 1 KPa

### Design Summary

#### Purlin Design

Purlin Spacing = 1 mm

Purlin Span = 850 mm

Try Purlin 100x50 SG6 Wet

Moisture Condition = Wet (Moisture in timber is less than 25%)

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K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 = 1    K5 = 1    K8 Downward = 1.00

K8 Upward = 1.00    S1 Downward = 7.54    S1 Upward = 7.11

Shear Capacity of timber = 3 MPa    Bending Capacity of timber = 7.5 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>1.35D</sub>	0 Kn-m	Capacity	0.30 Kn-m	Passing Percentage	<b>Infinity %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	0.35 Kn-m	Capacity	0.40 Kn-m	Passing Percentage	<b>114.29 %</b>
M <sub>0.9D-W<sub>n</sub>Up</sub>	0 Kn-m	Capacity	-0.50 Kn-m	Passing Percentage	<b>Infinity %</b>
V <sub>1.35D</sub>	0.00 Kn	Capacity	4.82 Kn	Passing Percentage	<b>Infinity %</b>
V <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	0.00 Kn	Capacity	6.43 Kn	Passing Percentage	<b>Infinity %</b>
V <sub>0.9D-W<sub>n</sub>Up</sub>	-0.00 Kn	Capacity	-8.04 Kn	Passing Percentage	<b>Infinity %</b>

**Deflections**

Modulus of Elasticity = 4000 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k<sub>2</sub> for Long Term Loads = 3

Deflection under Dead and Live Load = 0.70 mm    Limit by Woolcock et al, 1999 Span/240 = 3.33 mm

Deflection under Dead and Service Wind = 0.00 mm    Limit by Woolcock et al, 1999 Span/100 = 8.00 mm

**Reactions**

Maximum downward = 0.00 kn    Maximum upward = -0.00 kn

Number of Blocking = 0    if 0 then no blocking required, if 1 then one midspan blocking required

**Rafter Design Internal**

Internal Rafter Load Width = 1000 mm    Internal Rafter Span = -150 mm    Try Rafter 2xSG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 = 1    K5 = 1    K8 Downward = NaN

K8 Upward = NaN    S1 Downward = NaN    S1 Upward = NaN

Shear Capacity of timber = 3 MPa    Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>1.35D</sub>	-0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	<b>NaN %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	-0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	<b>NaN %</b>

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M <sub>0.9D-WnUp</sub>	-0.00 Kn-m	Capacity	-NaN Kn-m	Passing Percentage	NaN %
V <sub>1.35D</sub>	-0.04 Kn	Capacity	0 Kn	Passing Percentage	0.00 %
V <sub>1.2D+1.5L 1.2D+Sn 1.2D+WnDn</sub>	-0.15 Kn	Capacity	0 Kn	Passing Percentage	0.00 %
V <sub>0.9D-WnUp</sub>	2.15 Kn	Capacity	-0 Kn	Passing Percentage	0.00 %

**Deflections**

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = Infinity mm      Limit by Woolcock et al, 1999 Span/240 = 0.00 mm

Deflection under Dead and Service Wind = Infinity mm      Limit by Woolcock et al, 1999 Span/100 = 0.00 mm

**Reactions**

Maximum downward = -0.02 kn    Maximum upward = -0.04 kn

**Rafter to Pole Connection check**

Bolt Size = M16 Number of Bolts = 1

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 40 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K<sub>11</sub> = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 0 mm

For Parallel to grain loading

K<sub>11</sub> = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 0.00 Kn > -0.04 Kn

Prop on Sides = 1    2/SG815050wet    1mm    Reaction Prop = -0.04 Kn down 2.15 Kn Up

Prop Combined axial and bending ratios (My/Phi x Mny)+(Nc/Phi x Ncy) should be less than or equal to 1

For Short Term Load = 0.00 < 1 OK

For Medium Term Load = 0.00 < 1 OK

For Long Term Load = 0.00 < 1 OK

### Prop Connection check

Effective width of Pole used in Calculations = 150 mm -20mm (Margin for chamfer)

Bolt Size = M16 Number of Bolts = 1

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 80 mm

Angle of prop = 45 degree

Prop Connection Capacity under Short term loads: 18.54 Kn > 1 Kn OK

Prop Connection Capacity under Medium term loads: 14.83 Kn > 1 Kn OK

Prop Connection Capacity under Long term loads: 11.12 Kn > 1 Kn OK

### Rafter Design External

External Rafter Load Width = 500 mm      External Rafter Span = -200 mm      Try Rafter 150x50 SG8 Wet

Moisture Condition = Wet (Moisture in timber is less than 25%)

K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =1.00    S1 Downward =9.63    S1 Upward =9.63

Shear Capacity of timber =3 MPa    Bending Capacity of timber =11.7 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

M <sub>1.35D</sub>	0.00 Kn-m	Capacity	1.05 Kn-m	Passing Percentage	<b>Infinity %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	0.00 Kn-m	Capacity	1.40 Kn-m	Passing Percentage	<b>Infinity %</b>
M <sub>0.9D-W<sub>n</sub>Up</sub>	-0.00 Kn-m	Capacity	-1.75 Kn-m	Passing Percentage	<b>Infinity %</b>
V <sub>1.35D</sub>	-0.02 Kn	Capacity	7.24 Kn	Passing Percentage	<b>-36200.00 %</b>
V <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	-0.07 Kn	Capacity	9.65 Kn	Passing Percentage	<b>-13785.71 %</b>
V <sub>0.9D-W<sub>n</sub>Up</sub>	0.04 Kn	Capacity	-12.06 Kn	Passing Percentage	<b>30150.00 %</b>

### Deflections

Modulus of Elasticity = 4400 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 3

Deflection under Dead and Live Load = 0.00 mm      Limit by Woolcock et al, 1999 Span/240= 0.00 mm

Deflection under Dead and Service Wind = 0.00 mm      Limit by Woolcock et al, 1999 Span/100 = 0.00 mm

### Reactions



### Pole Shed App Ver 01 2022

Maximum downward = -0.07 kn    Maximum upward = 0.04 kn

#### **Rafter to Pole Connection check**

Bolt Size = M12    Number of Bolts =

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5    Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 14.9 \text{ f}_{pj} = 12.9 \text{ Mpa}$  for Rafter with effective thickness = 50 mm

For Parallel to grain loading

$K_{11} = 2.0 \text{ f}_{cj} = 36.1 \text{ Mpa}$  for Pole with effective thickness = 100 mm

Eccentric Load check

$V = \phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s \dots\dots\dots (\text{Eq 4.12}) = -9.45 \text{ kn} > 0.04 \text{ Kn}$

Single Shear Capacity under short term loads = -0.00 Kn > 0.04 Kn

#### **Intermediate Design Front and Back**

Intermediate Spacing = 500 mm                      Intermediate Span = 850 mm                      Try Intermediate 2xSG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

$K_1$  Short term = 1     $K_4 = 1$      $K_5 = 1$      $K_8$  Downward = NaN

$K_8$  Upward = NaN     $S_1$  Downward = NaN     $S_1$  Upward = NaN

Shear Capacity of timber = 3 MPa    Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

$M_{\text{Wind+Snow}}$	0.05 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.21 Kn	Capacity	-0 Kn	Passing Percentage	0.00 %

#### **Deflections**

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm    Limit by Woolcock et al, 1999 Span/100 = 8.50 mm

**Reactions**

Maximum = 0.21 kn

**Girt Design Front and Back**

Girt's Spacing = 0 mm

Girt's Span = 500 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =NaN

K8 Upward =NaN    S1 Downward =NaN    S1 Upward =NaN

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

$M_{Wind+Snow}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm    Limit by Woolcock et al, 1999 Span/100 = 5.00 mm

Sag during installation = NaN mm

**Reactions**

Maximum = 0.00 kn

**Girt Design Sides**

Girt's Spacing = 0 mm

Girt's Span = 0 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =NaN

K8 Upward =NaN    S1 Downward =NaN    S1 Upward =NaN

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

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M <sub>Wind+Snow</sub>	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
V <sub>0.9D-WnUp</sub>	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm      Limit by Woolcock et al. 1999 Span/100 = 0.00 mm  
Sag during installation = NaN mm

**Reactions**

Maximum = 0.00 kn

**Middle Pole Design**

**Geometry**

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	mm
Area	20729 mm <sup>2</sup>	As	15546.6796875 mm <sup>2</sup>
I <sub>x</sub>	34210793 mm <sup>4</sup>	Z <sub>x</sub>	421056 mm <sup>3</sup>
I <sub>y</sub>	34210793 mm <sup>4</sup>	Z <sub>y</sub>	421056 mm <sup>3</sup>
Lateral Restraint	mm c/c		

**Loads**

Total Area over Pole = 0 m<sup>2</sup>

Dead	0.00 Kn	Live	0.00 Kn
Wind Down	0.00 Kn	Snow	0.00 Kn
Moment wind	0.00 Kn-m		
Phi	0.8	K <sub>8</sub>	1.00
K <sub>1</sub> snow	0.8	K <sub>1</sub> Dead	0.6
K <sub>1</sub> wind	1		

**Material**

Peeling	Steaming	Normal	Dry Use
f <sub>b</sub> =	36.3 MPa	f <sub>s</sub> =	2.96 MPa
f <sub>c</sub> =	18 MPa	f <sub>p</sub> =	7.2 MPa
f <sub>t</sub> =	22 MPa	E =	9257 MPa

**Capacities**

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PhiNcx Wind	298.50 Kn	PhiMnx Wind	12.23 Kn-m	PhiVnx Wind	36.81 Kn
PhiNcx Dead	179.10 Kn	PhiMnx Dead	7.34 Kn-m	PhiVnx Dead	22.09 Kn

**Checks**

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.00 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.00 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 0.00 \text{ mm} < 0.00 \text{ mm}$$

**Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile**

**Assumed Soil Properties**

Gamma	18 Kn/m <sup>3</sup>	Friction angle	30 deg	Cohesion	0 Kn/m <sup>3</sup>
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

**Geometry For Middle Bay Pole**

Ds =	0.6 mm	Pile Diameter
L =	mm	Pile embedment length
f1 =	750 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Moment Wind =	0.00 Kn-m
Shear Wind =	0.25 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	0.00 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	0.00 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

$$\text{Applied Forces/Capacities} = N/N < 1 \text{ OK}$$

**End Pole Design**

**Geometry For End Bay Pole**

Pole Shed App Ver 01 2022

**Geometry**

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	800 mm
Area	20729 mm <sup>2</sup>	As	15546.6796875 mm <sup>2</sup>
Ix	34210793 mm <sup>4</sup>	Zx	421056 mm <sup>3</sup>
Iy	34210793 mm <sup>4</sup>	Zx	421056 mm <sup>3</sup>
Lateral Restraint	mm c/c		

**Loads**

Total Area over Pole = 0 m<sup>2</sup>

Dead	0.00 Kn	Live	0.00 Kn
Wind Down	0.00 Kn	Snow	0.00 Kn
Moment Wind	0.09 Kn-m		
Phi	0.8	K8	1.00
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

**Material**

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

**Capacities**

PhiNcx Wind	298.50 Kn	PhiMnx Wind	12.23 Kn-m	PhiVnx Wind	36.81 Kn
PhiNcx Dead	179.10 Kn	PhiMnx Dead	7.34 Kn-m	PhiVnx Dead	22.09 Kn

**Checks**

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.01 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.00 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 0.04 \text{ mm} < 9.97 \text{ mm}$$

Ds =	0.6 mm	Pile Diameter
L =	mm	Pile embedment length
f1 =	750 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Total Area over Pole = 0 m<sup>2</sup>

Moment Wind = 0.09 Kn-m

Shear Wind = 0.12 Kn

**Pile Properties**

Safety Factory 0.55

Hu = 0.00 Kn Ultimate Lateral Strength of the Pile, Short pile

Mu = 0.00 Kn-m Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = Infinity < 1 OK

**Drained Lateral Strength of End pile in cohesionless soils Free Head short pile**

**Assumed Soil Properties**

Gamma 18 Kn/m<sup>3</sup> Friction angle 30 deg Cohesion 0 Kn/m<sup>3</sup>

K0 =  $(1 - \sin(30)) / (1 + \sin(30))$

Kp =  $(1 + \sin(30)) / (1 - \sin(30))$

**Geometry For End Bay Pole**

Ds = 0.6 mm Pile Diameter

L = mm Pile embedment length

f1 = 750 mm Distance at which the shear force is applied

f2 = 0 mm Distance of top soil at rest pressure

**Loads**

Moment Wind = 0.09 Kn-m

Shear Wind = 0.12 Kn

**Pile Properties**

Safety Factory 0.55

Hu = 0.00 Kn Ultimate Lateral Strength of the Pile, Short pile

Mu = 0.00 Kn-m Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = Infinity < 1 OK

## **Uplift Check**

Density of Concrete = 24 Kn/m<sup>3</sup>

Density of Timber Pole = 5 Kn/m<sup>3</sup>

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile() x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile()

Skin Friction = 0.00 Kn

Weight of Pile + Pile Skin Friction = 0.00 Kn

Uplift on one Pile = 0.00 Kn

Uplift is ok