

Job No.: Mark Melody-1**Address:** 34 Oram Drive, Turitea - Palmerston North, New Zealand**Date:** 09/05/2024**Latitude:** -40.410267**Longitude:** 175.653346**Elevation:** 111.5 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N1	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	3	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	44.18 m/s
Wind Pressure	1.17 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Very High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 4.25 m $C_{p,e} = -0.9$ $p_e = -0.95$ KPa $p_{net} = -0.95$ KPa

For roof $C_{p,e}$ from 4.25 m To 8.50 m $C_{p,e} = -0.5$ $p_e = -0.53$ KPa $p_{net} = -0.53$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 9 m $C_{p,e} = 0.7$ $p_e = 0.74$ KPa $p_{net} = 1.09$ KPa

For side wall $C_{p,e}$ from 0 m To 4.25 m $C_{p,e} =$ $p_e = -0.69$ KPa $p_{net} = -0.69$ KPa

Maximum Upward pressure used in roof member Design = 0.95 KPa

Maximum Downward pressure used in roof member Design = 0.46 KPa

Maximum Wall pressure used in Design = 1.09 KPa

Maximum Racking pressure used in Design = 1.27 KPa

Design Summary**Rafter Design Internal**

Internal Rafter Load Width = 4500 mm

Internal Rafter Span = 8850 mm

Try Rafter 2x360x63 LVL13

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 5.90 S1 Upward = 5.90

Shear Capacity of timber = 5.3 MPa Bending Capacity of timber = 48 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	14.87 Kn-m	Capacity	60.82 Kn-m	Passing Percentage	409.01 %
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	33.48 Kn-m	Capacity	81.1 Kn-m	Passing Percentage	242.23 %
$M_{0.9D-W_nUp}$	-31.94 Kn-m	Capacity	-101.38 Kn-m	Passing Percentage	317.41 %
$V_{1.35D}$	6.72 Kn	Capacity	77.32 Kn	Passing Percentage	1150.60 %

Pole Shed App Ver 01 2022

V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	15.13 Kn	Capacity	103.08 Kn	Passing Percentage	681.30 %
V _{0.9D-WnUp}	-14.44 Kn	Capacity	-128.86 Kn	Passing Percentage	892.38 %

Deflections

Modulus of Elasticity = 11000 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 19.26 mm

Limit by Woolcock et al, 1999 Span/240 = 37.50 mm

Deflection under Dead and Service Wind = 26.04 mm

Limit by Woolcock et al, 1999 Span/100 = 90.00 mm

Reactions

Maximum downward = 15.13 kn Maximum upward = -14.44 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 3

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J2 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K₁₁ = 12.6 f_{pj} = 22.7 Mpa for Rafter with effective thickness = 126 mm

For Parallel to grain loading

K₁₁ = 2.0 f_{cj} = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 43.67 Kn > -14.44 Kn

Girt Design Front and Back

Girt's Spacing = 800 mm

Girt's Span = 4500 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 0.78 S₁ Downward = 11.27 S₁ Upward = 17.82

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.21 Kn-m	Capacity	2.90 Kn-m	Passing Percentage	131.22 %
V _{0.9D-WnUp}	1.96 Kn	Capacity	16.08 Kn	Passing Percentage	820.41 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 20.85 mm

Limit by Woolcock et al, 1999 Span/100 = 45.00 mm

Sag during installation = 24.86 mm

Reactions

Maximum = 1.96 kn

Girt Design Sides

Girt's Spacing = 800 mm

Girt's Span = 4500 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.78 S1 Downward =11.27 S1 Upward =17.82

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.21 Kn-m	Capacity	2.90 Kn-m	Passing Percentage	131.22 %
V _{0.9D-WnUp}	1.96 Kn	Capacity	16.08 Kn	Passing Percentage	820.41 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 20.85 mm

Limit by Woolcock et al. 1999 Span/100 = 45.00 mm

Sag during installation =24.86 mm

Reactions

Maximum = 1.96 kn

Middle Pole Design

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	3640 mm
Area	35448 mm ²	As	26585.7421875 mm ²
I _x	100042702 mm ⁴	Z _x	941578 mm ³
I _y	100042702 mm ⁴	Z _y	941578 mm ³
Lateral Restraint	3640 mm c/c		

Loads

Total Area over Pole = 20.25 m²

Dead	5.06 Kn	Live	5.06 Kn
Wind Down	9.31 Kn	Snow	0.00 Kn
Moment wind	17.10 Kn-m		
Phi	0.8	K8	0.81
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Peeling	Steaming	Normal	Dry Use
---------	----------	--------	---------

Pole Shed App Ver 01 2022

fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	413.07 Kn	PhiMnx Wind	22.13 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	247.84 Kn	PhiMnx Dead	13.28 Kn-m	PhiVnx Dead	37.77 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.82 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.64 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 37.78 \text{ mm} < 36.40 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1800 mm	Pile embedment length
f1 =	3000 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	17.10 Kn-m
Shear Wind =	5.70 Kn

Pile Properties

Safety Factory	0.55	
Hu =	10.83 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	19.75 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.87 < 1 \text{ OK}$$

Uplift Check

$$\text{Density of Concrete} = 24 \text{ Kn/m}^3$$

$$\text{Density of Timber Pole} = 5 \text{ Kn/m}^3$$

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

$$K_s \text{ (Lateral Earth Pressure Coefficient) for cast into place concrete piles} = 1.5$$

Pole Shed App Ver 01 2022

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1800) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1800)

Skin Friction = 26.17 Kn

Weight of Pile + Pile Skin Friction = 30.84 Kn

Uplift on one Pile = 14.68 Kn

Uplift is ok