Job No.: ITM Pole shed - 1 Address: 201 Main St, Greytown, New Zealand Date: 12/05/2025

# **General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N1	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	3	Subsoil Category	D	Exposure Zone	В
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.5 m
Wind Region	NZ2	Terrain Category	2.03	Design Wind Speed	38.11 m/s
Wind Pressure	0.87 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

### **Pressure Coefficients and Pressues**

Shed Type = Mono Enclosed

For roof Cp, i = 0.6516

For roof CP,e from 0 m To 2.08 m Cpe = -1.0533 pe = -0.67 KPa pnet = -1.17 KPa

For roof CP,e from 2.08 m To 4.15 m Cpe = -0.8233 pe = -0.53 KPa pnet = -1.03 KPa

For wall Windward Cp, i = 0.6516 side Wall Cp, i = -0.4904

For wall Windward and Leeward CP,e from 0 m To 15 m Cpe = 0.7 pe = 0.53 KPa pnet = 1.04 KPa

For side wall CP,e from 0 m To 4.15 m Cpe = pe = -0.49 KPa pnet = 0.02 KPa

Maximum Upward pressure used in roof member Design = 1.17 KPa

Maximum Downward pressure used in roof member Design = 0.66 KPa

Maximum Wall pressure used in Design = 1.04 KPa

Maximum Racking pressure used in Design = 0.94 KPa

# **Design Summary**

### **Intermediate Design Front and Back**

Intermediate Spacing = 3750 mm Intermediate Span = 3645 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

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K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.72

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

## **Capacity Checks**

Mwind+Snow 6.48 Kn-m Capacity 7.46 Kn-m Passing Percentage 115.12 % V<sub>0.9D-WnUp</sub> 7.11 Kn Capacity -32.16 Kn Passing Percentage 452.32 %

### **Deflections**

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 24.905 mm Limit by Woolcock et al, 1999 Span/100 = 36.45 mm

### Reactions

Maximum = 7.11 kn

# **Girt Design Front and Back**

Girt's Spacing = 900 mm Girt's Span = 3750 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.94 S1 Downward =9.63 S1 Upward =13.90

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

# **Capacity Checks**

Mwind+Snow 1.65 Kn-m Capacity 1.97 Kn-m Passing Percentage 119.39 % V<sub>0.9D-WnUp</sub> 1.75 Kn Capacity 12.06 Kn Passing Percentage 689.14 %

### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 25.58 mm Limit by Woolcock et al, 1999 Span/100 = 37.50 mm Sag during installation = 11.99 mm

#### Reactions

Maximum = 1.75 kn

## **Girt Design Sides**

Girt's Spacing = 900 mm Girt's Span = 3000 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.79 S1 Downward =9.63 S1 Upward =17.59

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### **Capacity Checks**

$M_{Wind+Snow}$	1.05 Kn-m	Capacity	1.65 Kn-m	Passing Percentage	157.14 %
$ m V_{0.9D-WnUp}$	1.40 Kn	Capacity	12.06 Kn	Passing Percentage	861.43 %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 10.48 mm Limit by Woolcock et al. 1999 Span/100 = 30.00 mm Sag during installation = 4.91 mm

#### Reactions

Maximum = 1.40 kn

# **Uplift Check**

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1900) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1900)

Skin Friction = 29.16 Kn

Weight of Pile + Pile Skin Friction = 33.51 Kn

Uplift on one Pile = 21.26 Kn

Uplift is ok