

Pole Shed App Ver 01 2022

Job No.: 446-276454

Address: 52 Hobbs Road, Methven, New Zealand

Date: 02/04/2025

Latitude: -43.633535

Longitude: 171.632525

Elevation: 321.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N4	Ground Snow Load	1.52 KPa	Roof Snow Load	1.06 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3 m
Wind Region	NZ2	Terrain Category	2.5	Design Wind Speed	46.57 m/s
Wind Pressure	1.3 KPa	Lee Zone	YES	Ultimate Snow ARI	50 Years
Wind Category	Very High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Open

For roof $C_{p,i} = 0.6706$

For roof $C_{p,e}$ from 0 m To 1.43 m $C_{p,e} = -1.07$ $p_e = -0.68$ KPa $p_{net} = -1.20$ KPa

For roof $C_{p,e}$ from 1.43 m To 2.85 m $C_{p,e} = -0.815$ $p_e = -0.52$ KPa $p_{net} = -1.04$ KPa

For wall Windward $C_{p,i} = 0.6706$ side Wall $C_{p,i} = -0.5954$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 9 m $C_{p,e} = 0.7$ $p_e = 0.82$ KPa $p_{net} = 1.66$ KPa

For side wall $C_{p,e}$ from 0 m To 2.85 m $C_{p,e} =$ $p_e = -0.76$ KPa $p_{net} = 0.08$ KPa

Maximum Upward pressure used in roof member Design = 1.20 KPa

Maximum Downward pressure used in roof member Design = 1.07 KPa

Maximum Wall pressure used in Design = 1.66 KPa

Maximum Racking pressure used in Design = 1.41 KPa

Design Summary

Purlin Design

Purlin Spacing = 900 mm

Purlin Span = 5850 mm

Try Purlin 240x45 LVL13

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

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K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.94

K8 Upward = 0.47 S1 Downward = 13.82 S1 Upward = 24.81

Shear Capacity of timber = 5.3 MPa Bending Capacity of timber = 48 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	1.3 Kn-m	Capacity	9.37 Kn-m	Passing Percentage	720.77 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	5.27 Kn-m	Capacity	12.49 Kn-m	Passing Percentage	237.00 %
M _{0.9D-W_nUp}	-3.75 Kn-m	Capacity	-7.73 Kn-m	Passing Percentage	206.13 %
V _{1.35D}	0.89 Kn	Capacity	18.41 Kn	Passing Percentage	2068.54 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	3.61 Kn	Capacity	24.54 Kn	Passing Percentage	679.78 %
V _{0.9D-W_nUp}	-2.57 Kn	Capacity	-30.68 Kn	Passing Percentage	1193.77 %

Deflections

Modulus of Elasticity = 12100 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 17.70 mm Limit by Woolcock et al, 1999 Span/240 = 24.17 mm

Deflection under Dead and Service Wind = 21.88 mm Limit by Woolcock et al, 1999 Span/100 = 58.00 mm

Reactions

Maximum downward = 3.61 kn Maximum upward = -2.57 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Intermediate Design Front and Back

Intermediate Spacing = 3000 mm Intermediate Span = 2550 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.60

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+S_{now}}	4.05 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	184.20 %
V _{0.9D-W_nUp}	6.35 Kn	Capacity	-32.16 Kn	Passing Percentage	506.46 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 14.59 mm Limit by Woolcock et al, 1999 Span/100 = 25.50 mm

Reactions

Maximum = 6.35 kn

Intermediate Design Sides

Intermediate Spacing = 2000 mm Intermediate Span = 2700 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.62

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.51 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	494.04 %
V _{0.9D-WnUp}	2.24 Kn	Capacity	32.16 Kn	Passing Percentage	1435.71 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 12.225 mm Limit by Woolcock et al, 1999 Span/100 = 27.00 mm

Reactions

Maximum = 2.24 kn

Girt Design Front and Back

Girt's Spacing = 800 mm Girt's Span = 3000 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

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K8 Upward =0.79 S1 Downward =9.63 S1 Upward =17.59

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.49 Kn-m	Capacity	1.65 Kn-m	Passing Percentage	110.74 %
V _{0.9D-WnUp}	1.99 Kn	Capacity	12.06 Kn	Passing Percentage	606.03 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 24.36 mm Limit by Woolcock et al, 1999 Span/100 = 30.00 mm
Sag during installation = 4.91 mm

Reactions

Maximum = 1.99 kn

Girt Design Sides

Girt's Spacing = 1100 mm Girt's Span = 2000 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.92 S1 Downward =9.63 S1 Upward =14.36

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.91 Kn-m	Capacity	1.94 Kn-m	Passing Percentage	213.19 %
V _{0.9D-WnUp}	1.83 Kn	Capacity	12.06 Kn	Passing Percentage	659.02 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 6.62 mm Limit by Woolcock et al. 1999 Span/100 = 20.00 mm
Sag during installation =0.97 mm

Reactions

Maximum = 1.83 kn

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1400) x Ks(1.5) x $0.5 \times \tan(30) \times \pi \times \text{Dia of Pile}(0.6) \times \text{Height of Pile}(1400)$

Skin Friction = 15.83 Kn

Weight of Pile + Pile Skin Friction = 19.92 Kn

Uplift on one Pile = 11.70 Kn

Uplift is ok