

Pole Shed App Ver 01 2022

Job No.: EHB 394 - 2

Address: 64 Blakie Road, Ryal Bush, New Zealand

Date: 21/05/2025

Latitude: -46.272224

Longitude: 168.345241

Elevation: 29 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.35 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	38.22 m/s
Wind Pressure	0.88 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = 0.6631$

For roof $C_{p,e}$ from 0 m To 3.73 m $C_{p,e} = -0.9$ $p_e = -0.70$ KPa $p_{net} = -1.28$ KPa

For roof $C_{p,e}$ from 3.73 m To 7.54 m $C_{p,e} = -0.5$ $p_e = -0.39$ KPa $p_{net} = -0.97$ KPa

For wall Windward $C_{p,i} = 0.6631$ side Wall $C_{p,i} = -0.5815$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 10 m $C_{p,e} = 0.7$ $p_e = 0.55$ KPa $p_{net} = 1.06$ KPa

For side wall $C_{p,e}$ from 0 m To 3.73 m $C_{p,e} =$ $p_e = -0.51$ KPa $p_{net} = 0.00$ KPa

Maximum Upward pressure used in roof member Design = 1.28 KPa

Maximum Downward pressure used in roof member Design = 0.52 KPa

Maximum Wall pressure used in Design = 1.06 KPa

Maximum Racking pressure used in Design = 0.79 KPa

Design Summary

Rafter Design External

External Rafter Load Width = 2500 mm External Rafter Span = 4954 mm Try Rafter 300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

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K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.94

K8 Upward = 0.94 S1 Downward = 13.93 S1 Upward = 13.93

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	2.59 Kn-m	Capacity	4.72 Kn-m	Passing Percentage	182.24 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_{nDn}}	7.13 Kn-m	Capacity	6.30 Kn-m	Passing Percentage	88.36 %
M _{0.9D-W_{nUp}}	-8.09 Kn-m	Capacity	-7.87 Kn-m	Passing Percentage	97.28 %
V _{1.35D}	2.09 Kn	Capacity	14.47 Kn	Passing Percentage	692.34 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_{nDn}}	5.76 Kn	Capacity	19.30 Kn	Passing Percentage	335.07 %
V _{0.9D-W_{nUp}}	-6.53 Kn	Capacity	-24.12 Kn	Passing Percentage	369.37 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 10.05 mm Limit by Woolcock et al, 1999 Span/240 = 20.83 mm

Deflection under Dead and Service Wind = 12.73 mm Limit by Woolcock et al, 1999 Span/100 = 50.00 mm

Reactions

Maximum downward = 5.76 kn Maximum upward = -6.53 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K₁₁ = 14.9 f_{pj} = 12.9 Mpa for Rafter with effective thickness = 50 mm

For Parallel to grain loading

K₁₁ = 2.0 f_{cj} = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

V = $\phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s$ (Eq 4.12) = -25.20 kn > -6.53 Kn

Single Shear Capacity under short term loads = -10.84 Kn > -6.53 Kn

Intermediate Design Front and Back

Intermediate Spacing = 2500 mm Intermediate Span = 2950 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =11.27 S1 Upward =0.65

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.88 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	259.03 %
V _{0.9D-WnUp}	3.91 Kn	Capacity	-32.16 Kn	Passing Percentage	822.51 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 13.415 mm Limit by Woolcock et al, 1999 Span/100 = 29.50 mm

Reactions

Maximum = 3.91 kn

Intermediate Design Sides

Intermediate Spacing = 2500 mm Intermediate Span = 3575 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =11.27 S1 Upward =0.71

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.12 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	351.89 %
V _{0.9D-WnUp}	2.37 Kn	Capacity	32.16 Kn	Passing Percentage	1356.96 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 28.945 mm Limit by Woolcock et al, 1999 Span/100 = 35.75 mm

Reactions

Maximum = 2.37 kn

Girt Design Front and Back

Girt's Spacing = 1300 mm

Girt's Span = 2500 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.86 S1 Downward =9.63 S1 Upward =16.05

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.08 Kn-m	Capacity	1.80 Kn-m	Passing Percentage	166.67 %
V _{0.9D-WnUp}	1.72 Kn	Capacity	12.06 Kn	Passing Percentage	701.16 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 11.86 mm Limit by Woolcock et al, 1999 Span/100 = 25.00 mm

Sag during installation = 2.37 mm

Reactions

Maximum = 1.72 kn

Girt Design Sides

Girt's Spacing = 1300 mm

Girt's Span = 2500 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

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K8 Upward =0.86 S1 Downward =9.63 S1 Upward =16.05

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.08 Kn-m	Capacity	1.80 Kn-m	Passing Percentage	166.67 %
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Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 11.86 mm Limit by Woolcock et al. 1999 Span/100 = 25.00 mm
Sag during installation =2.37 mm

Reactions

Maximum = 1.72 kn

End Pole Design

Geometry For End Bay Pole

Geometry

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	4050 mm
Area	20729 mm ²	As	15546.6796875 mm ²
I _x	34210793 mm ⁴	Z _x	421056 mm ³
I _y	34210793 mm ⁴	Z _y	421056 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 12.5 m²

Dead	3.13 Kn	Live	3.13 Kn
Wind Down	6.50 Kn	Snow	7.88 Kn
Moment Wind	4.66 Kn-m	Moment snow	1.63 Kn-m
Phi	0.8	K8	0.46
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

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Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	138.06 Kn	PhiMnx Wind	5.66 Kn-m	PhiVnx Wind	36.81 Kn
PhiNcx Dead	82.84 Kn	PhiMnx Dead	3.39 Kn-m	PhiVnx Dead	22.09 Kn
PhiNcx Snow	110.45 Kn	PhiMnx Snow	4.52 Kn-m	PhiVnx Snow	29.45 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.94 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.80 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 39.02 \text{ mm} < 43.39 \text{ mm}$$

$D_s =$	0.6 mm	Pile Diameter
$L =$	1300 mm	Pile embedment length
$f_1 =$	3262 mm	Distance at which the shear force is applied
$f_2 =$	0 mm	Distance of top soil at rest pressure

Loads

$$\text{Total Area over Pole} = 12.5 \text{ m}^2$$

Moment Wind =	4.66 Kn-m	Moment Snow =	1.63 Kn-m
Shear Wind =	1.43 Kn	Shear Snow =	1.63 Kn

Pile Properties

Safety Factory	0.55	
$H_u =$	4.29 Kn	Ultimate Lateral Strength of the Pile, Short pile
$M_u =$	8.17 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.57 < 1 \text{ OK}$$

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

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Gamma 18 Kn/m³ Friction angle 30 deg Cohesion 0 Kn/m³

$$K_0 = (1 - \sin(30)) / (1 + \sin(30))$$

$$K_p = (1 + \sin(30)) / (1 - \sin(30))$$

Geometry For End Bay Pole

Ds = 0.6 mm Pile Diameter
L = 1300 mm Pile embedment length
f1 = 3262 mm Distance at which the shear force is applied
f2 = 0 mm Distance of top soil at rest pressure

Loads

Moment Wind = 4.66 Kn-m Moment Snow = 1.63 Kn-m
Shear Wind = 1.43 Kn Shear Snow = 1.63 Kn

Pile Properties

Safety Factor 0.55
Hu = 4.29 Kn Ultimate Lateral Strength of the Pile, Short pile
Mu = 8.17 Kn-m Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.57 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast in place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1700) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1700)

Skin Friction = 23.34 Kn

Weight of Pile + Pile Skin Friction = 28.31 Kn

Uplift on one Pile = 26.38 Kn

Uplift is ok

