



**Job No.:** 2409020-2**Address:** 4 Collinson Street, Pākawau,, Collingwood, New Zealand**Date:** 12/09/2024**Latitude:** -40.579639**Longitude:** 172.688896**Elevation:** 8.5 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	D
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	2.76 m
Wind Region	NZ2	Terrain Category	1.37	Design Wind Speed	37.73 m/s
Wind Pressure	0.85 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

**Pressure Coefficients and Pressures**

Shed Type = Mono Open

For roof  $C_{p,i} = 0.5649$

For roof  $C_{p,e}$  from 0 m To 1.32 m  $C_{p,e} = -1.2013$   $p_e = -0.9$  KPa  $p_{net} = -1.37$  KPa

For roof  $C_{p,e}$  from 1.32 m To 2.63 m  $C_{p,e} = -0.7493$   $p_e = -0.56$  KPa  $p_{net} = -1.03$  KPa

For wall Windward  $C_{p,i} = 0.5649$  side Wall  $C_{p,i} = -0.5842$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 11 m  $C_{p,e} = 0.7$   $p_e = 0.54$  KPa  $p_{net} = 1.04$  KPa

For side wall  $C_{p,e}$  from 0 m To 2.63 m  $C_{p,e} =$   $p_e = -0.5$  KPa  $p_{net} = 0$  KPa

Maximum Upward pressure used in roof member Design = 1.37 KPa

Maximum Downward pressure used in roof member Design = 0.65 KPa

Maximum Wall pressure used in Design = 1.04 KPa

Maximum Racking pressure used in Design = 0.89 KPa

**Design Summary****Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 10850 mm

Try Purlin 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.19 S1 Downward = 11.27 S1 Upward = 39.05

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>1.35D</sub>	4.47 Kn-m	Capacity	2.23 Kn-m	Passing Percentage	<b>49.89 %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>nDn</sub></sub>	12.58 Kn-m	Capacity	2.97 Kn-m	Passing Percentage	<b>23.61 %</b>
M <sub>0.9D-W<sub>nUp</sub></sub>	-15.16 Kn-m	Capacity	-0.73 Kn-m	Passing Percentage	<b>4.82 %</b>
V <sub>1.35D</sub>	1.65 Kn	Capacity	9.65 Kn	Passing Percentage	<b>584.85 %</b>

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V <sub>1.2D+1.5L 1.2D+Sn 1.2D+WnDn</sub>	4.64 Kn	Capacity	12.86 Kn	Passing Percentage	277.16 %
V <sub>0.9D-WnUp</sub>	-5.59 Kn	Capacity	-16.08 Kn	Passing Percentage	287.66 %

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = 428.33 mm	Limit by Woolcock et al, 1999 Span/240 = 45.00 mm
Deflection under Dead and Service Wind = 588.95 mm	Limit by Woolcock et al, 1999 Span/100 = 108.00 mm

**Reactions**

Maximum downward = 4.64 kn Maximum upward = -5.59 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

**Girt Design Front and Back**

Girt's Spacing = 0 mm	Girt's Span = 5500 mm	Try Girt SG8 Dry
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Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K<sub>1</sub> Short term = 1 K<sub>4</sub> = 1 K<sub>5</sub> = 1 K<sub>8</sub> Downward = NaN

K<sub>8</sub> Upward = NaN S<sub>1</sub> Downward = NaN S<sub>1</sub> Upward = NaN

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>Wind+Snow</sub>	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
V <sub>0.9D-WnUp</sub>	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm	Limit by Woolcock et al, 1999 Span/100 = 55.00 mm
Sag during installation = NaN mm	

**Reactions**

Maximum = 0.00 kn

**Girt Design Sides**

Girt's Spacing = 0 mm	Girt's Span = 1500 mm	Try Girt SG8 Dry
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Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

K<sub>1</sub> Short term = 1 K<sub>4</sub> = 1 K<sub>5</sub> = 1 K<sub>8</sub> Downward = NaN

K<sub>8</sub> Upward = NaN S<sub>1</sub> Downward = NaN S<sub>1</sub> Upward = NaN

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

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M <sub>Wind+Snow</sub>	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
V <sub>0.9D-WnUp</sub>	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm

Limit by Woolcock et al. 1999 Span/100 = 15.00 mm

Sag during installation = NaN mm

**Reactions**

Maximum = 0.00 kn

**Uplift Check**

Density of Concrete = 24 Kn/m<sup>3</sup>

Density of Timber Pole = 5 Kn/m<sup>3</sup>

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K<sub>s</sub> (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile() x K<sub>s</sub>(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile()

Skin Friction = 0.00 Kn

Weight of Pile + Pile Skin Friction = 0.00 Kn

Uplift on one Pile = 18.89 Kn

Uplift is ok