**Job No.:** 446-276266 **Address:** Lot 1 DP 401501, Wards Road, Charing **Date:** 04/04/2025

Cross, New Zealand

**Latitude:** -43.537451 **Longitude:** 172.144285 **Elevation:** 156.5 m

### **General Input**

| Roof Live Load   | 0.25 KPa | Roof Dead Load                 | 0.25 KPa  | Roof Live Point Load | 1.1 Kn    |
|------------------|----------|--------------------------------|-----------|----------------------|-----------|
| Snow Zone        | N4       | Ground Snow Load               | 0.92 KPa  | Roof Snow Load       | 0.65 KPa  |
| Earthquake Zone  | 2        | Subsoil Category               | D         | Exposure Zone        | В         |
| Importance Level | 1        | Ultimate wind & Earthquake ARI | 100 Years | Max Height           | 4.2 m     |
| Wind Region      | NZ2      | Terrain Category               | 2.0       | Design Wind Speed    | 38.22 m/s |
| Wind Pressure    | 0.88 KPa | Lee Zone                       | NO        | Ultimate Snow ARI    | 50 Years  |
| Wind Category    | High     | Earthquake ARI                 | 100       |                      |           |

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

#### **Pressure Coefficients and Pressues**

Shed Type = Mono Open

For roof Cp,i = 0.6543

For roof CP,e from 0 m To 3.95 m Cpe = -0.9 pe = -0.55 KPa pnet = -1.03 KPa

For roof CP,e from 3.95 m To 7.90 m Cpe = -0.5 pe = -0.31 KPa pnet = -0.79 KPa

For wall Windward Cp, i = 0.6543 side Wall Cp, i = -0.5651

For wall Windward and Leeward CP,e from 0 m To 13.59 m Cpe = 0.7 pe = 0.55 KPa pnet = 1.09 KPa

For side wall CP,e from 0 m To 3.95 m Cpe = pe = -0.51 KPa pnet = 0.03 KPa

Maximum Upward pressure used in roof member Design = 1.03 KPa

Maximum Downward pressure used in roof member Design = 0.70 KPa

Maximum Wall pressure used in Design = 1.09 KPa

Maximum Racking pressure used in Design = 0.94 KPa

#### **Design Summary**

### **Intermediate Design Front and Back**

Intermediate Spacing = 2265 mm Intermediate Span = 3550 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

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K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.71

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

# **Capacity Checks**

Mwind+Snow 3.89 Kn-m Capacity 7.46 Kn-m Passing Percentage 191.77 % V<sub>0.9D-WnUp</sub> 4.38 Kn Capacity -32.16 Kn Passing Percentage 734.25 %

#### **Deflections**

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 26.15 mm Limit byWoolcock et al, 1999 Span/100 = 35.50 mm

#### Reactions

Maximum = 4.38 kn

# **Intermediate Design Sides**

Intermediate Spacing = 2745.576571079927 Intermediate Span = 3987 Try Intermediate 2x250x50 SG8 mm Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 1.00 S1 Downward = 12.68 S1 Upward = 0.84

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

Mwind+Snow 2.97 Kn-m Capacity 11.66 Kn-m Passing Percentage 392.59 % V<sub>0.9D-WnUp</sub> 2.98 Kn Capacity 40.2 Kn Passing Percentage 1348.99 %

### Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 25.835 mm Limit by Woolcock et al, 1999 Span/100 = 39.87 mm

# Reactions

Maximum = 2.98 kn

# **Girt Design Front and Back**

Girt's Spacing = 1300 mm Girt's Span = 2265 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.89 S1 Downward =9.63 S1 Upward =15.28

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### **Capacity Checks**

Mwind+snow 0.91 Kn-m Capacity 1.87 Kn-m Passing Percentage 205.49 % V<sub>0.9D-WnUp</sub> 1.60 Kn Capacity 12.06 Kn Passing Percentage 753.75 %

#### Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 8.23 mm Limit by Woolcock et al, 1999 Span/100 = 22.65 mm Sag during installation = 1.60 mm

#### Reactions

Maximum = 1.60 kn

# **Girt Design Sides**

Girt's Spacing = 1300 mm Girt's Span = 2746 mm Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.82 S1 Downward =9.63 S1 Upward =16.82

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### **Capacity Checks**

Mwind+Snow 1.34 Kn-m Capacity 1.73 Kn-m Passing Percentage 129.10 %

V<sub>0.9D-WnUp</sub> 1.95 Kn Capacity 12.06 Kn Passing Percentage **618.46 %** 

#### Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 17.76 mm Limit by Woolcock et al. 1999 Span/100 = 27.46 mm Sag during installation = 3.45 mm

#### Reactions

Maximum = 1.95 kn

# **Uplift Check**

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1700) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1700)

Skin Friction = 23.34 Kn

Weight of Pile + Pile Skin Friction = 27.76 Kn

Uplift on one Pile = 20.02 Kn

Uplift is ok