Job Number:	BWhite
Issue:	Consulting Ltd
PRODUCER STATEMENT-PS1-DESIGN	
ISSUED BY: BWhite Consulting Ltd (Design Engineer: Bevan White)	
TO BE SUPPLIED TO: Invercargill District Council IN RESPECT OF: Proposed NEW Farm Shed	l
AT: 557 West Plains Road, Invercargill, New Zealand	
LEGAL DESCRIPTION	
We have been engaged by Ezequote Pty Ltd to provide Specific Structural Engineering Design requirements of Clause(s) B1 of the Building Code for part only (as specified in the attachment to building work.	
☐ ALL ☑ Part only as specified: Purlins, Rafters, Girts, Poles, Columns, Pole embedment and a	all connections
The design has been prepared in accordance with compliance documents to NZ Building Code iss Innovation & Employment Clauses B1/VM1 and B1/VM4	sued by Ministry of Business,
The proposed building work covered by the producer statement is described on Ezequote drawing A101 - A111 Rev-02 dated 21/02/2025 together with the following specification, and other docum attached to this statement: Design Featured Report Dated 2/25/2025 and numbered "Second Page	ents set out in the schedule
On behalf of BWhite Consulting Ltd, and subject to:	
 Site verification of the following design assumptions: an Ultimate foundation bearing pres with NZS3604:2011 	sure of 300 kPa in accordance
 The building has a design life of 50 years and am Importance Level 1 Unless specifically noted, compliance of the drawings to None-Specific codes such as NZi been checked by this practice This Certificate does not cover any other building code clause including weather tightness. Inspections of the building to be completed by Invercargill District Council. As BWhite Coundertaking inspections, we cannot issue a producer Statement-PS4- Construction Review. This Producer Statement-Design is valid for a building consent issued within 1 year from the proprietary products meeting their performance specification requirements 	ss Consulting Ltd are not ew.
I believe on reasonable grounds that a) the building, if constructed in accordance with the drawing documents provided or listed in the attached schedule, will comply with the relevant provisions of the presons who have undertaken the design have the necessary competency to do so. I also reconstruction monitoring/observation:	f the Building Code and that b),
✓ CM1 ☐ CM2 ☐ CM3 ☐ CM4 ☐ CM5 or as per agreement with owner/developer (stated ab	ove)
I, Bevan White am CPEng 108276 I am Member of Engineering New Zealand and hold the following holds a current policy of Professional Indemnity Insurance no less than \$200,000	ng qualification: BECivil and
Signed by Bevan White on behalf of BWhite Consulting Ltd Dated: 2/25/2025	
Email: bwhitecpeng@gmail.com Phone: 0211-979786	

This form is to accompany Form 2 of the Building (Forms) Regulations 2004 for the application of a Building Consent

whether in contract, tort or otherwise(including negligence), is limited to the sum of \$200,000.

Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement accrues to the Design Firm only. The total maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work,

Date: 2/25/2025

18B Jules Crescent,

BWhite Consulting Ltd

Bell Block New Plymouth 4312

New Zealand File No:

DESIGN FEATURES SUMMARY FOR PROPOSED NEW FARM SHED 557 WEST PLAINS ROAD, INVERCARGILL, NEW ZEALAND

Site Specific Loads

Roof Live Load	!	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone		N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zon	ne	1	Subsoil Category	D	Exposure Zone	C
Importance Lev	rel	1	Ultimate wind & EQ ARI	100 Years	Max Height	4.2 m
Wind Region		NZ4	Terrain Category	2.05	Design Wind Speed	42.61 m/s
Wind Pressure		1.09 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years

Timber

Sawn Timber to be graded to the properties of SG6 and SG8 or better as mentioned on plans, with moisture content of 18% or less for dry and 25% or less for wet.

The following standards have been used in the design of this structure

- NZS 3603:1993 Timber Structures Standard
- NZS 3604:2011 Timber Framed Buildings. Standards New Zealand, 2011
- NZS 3404:1997 Steel Structures
- AS/NZS 1170 2003 Structural Design Actions
- AS/NZS 1170.2 2021 Structural Design Actions-Wind Action
- Branz. "Engineering Basis of NZS 3604". April 2013

Yours Faithfully

BWhite CONSULTING LTD

Bevan White

 $Director \,|\, BE\,Civil\,.\,CMengNZ\,\,CPEng$

Email: bwhitecpeng@gmail.com Contact: 0211 979 786

Job No.: EHB 294 Address: 557 West Plains Road, Invercargill, New Date: 2/25/2025

Zealand

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.2 m
Wind Region	NZ4	Terrain Category	2.05	Design Wind Speed	42.61 m/s
Wind Pressure	1.09 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Mono Open

For roof Cp, i = 0.6472

For roof CP,e from 0 m To 3.9 m Cpe = -0.9 pe = -0.49 KPa pnet = -0.91 KPa

For roof CP,e from 3.9 m To 7.8 m Cpe = -0.5 pe = -0.27 KPa pnet = -0.69 KPa

For wall Windward Cp, i = 0.6472 side Wall Cp, i = -0.552

For wall Windward and Leeward CP,e from 0 m To 9.6 m Cpe = 0.7 pe = 0.69 KPa pnet = 1.27 KPa

For side wall CP,e from 0 m To 3.9 m Cpe = pe = -0.64 KPa pnet = -0.06 KPa

Maximum Upward pressure used in roof member Design = 0.91 KPa

Maximum Downward pressure used in roof member Design = 0.77 KPa

Maximum Wall pressure used in Design = 1.27 KPa

Maximum Racking pressure used in Design = 1.18 KPa

Design Summary

Intermediate Design Sides

Intermediate Spacing = 2400 mm Intermediate Span = 3900 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.74

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	2.90 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	257.24 %
$ m V_{0.9D ext{-}WnUp}$	2.97 Kn	Capacity	32.16 Kn	Passing Percentage	1082.83 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 43.57 mm Limit by Woolcock et al, 1999 Span/100 = 39.00 mm

Reactions

Maximum = 2.97 kn

Girt Design Front and Back

Girt's Spacing = 700 mm Girt's Span = 2400 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.96 S1 Downward =11.27 S1 Upward =13.02

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.64 Kn-m	Capacity	3.60 Kn-m	Passing Percentage	562.50 %
$V_{0.9D\text{-W}nUp}$	1.07 Kn	Capacity	16.08 Kn	Passing Percentage	1502.80 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 2.57 mm Limit by Woolcock et al, 1999 Span/100 = 24.00 mm Sag during installation = 2.01 mm

Reactions

Maximum = 1.07 kn

Girt Design Sides

Girt's Spacing = 1300 mm

Girt's Span = 2400 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1

K4 = 1

K5 = 1

K8 Downward =1.00

K8 Upward =0.75

S1 Downward =11.27

S1 Upward = 18.41

Shear Capacity of timber = 3 MPa

Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

 $M_{Wind+Snow}$

1.19 Kn-m

Capacity

2.79 Kn-m

Passing Percentage

234.45 %

 $V_{0.9D\text{-W}nUp}$

1.98 Kn

Capacity

16.08 Kn

Passing Percentage

812.12 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 4.78 mm Limit by Woolcock et al. 1999 Span/100 = 24.00 mm Sag during installation = 2.01 mm

Reactions

Maximum = 1.98 kn

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1600) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1600)

Skin Friction = 20.68 Kn

Weight of Pile + Pile Skin Friction = 24.83 Kn

Uplift on one Pile = 15.78 Kn

Uplift is ok