

**Job No.:** 2312001 - 1

**Address:** 49 Martin Loop, Mariri, New Zealand

**Date:** 30/01/2024

**Latitude:** -41.168836

**Longitude:** 173.03198

**Elevation:** 2.5 m

### General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	D
Importance Level	2	Ultimate wind & Earthquake ARI	500 Years	Max Height	4.75 m
Wind Region	NZ2	Terrain Category	1.0	Design Wind Speed	43.31 m/s
Wind Pressure	1.13 KPa	Lee Zone	NO	Ultimate Snow ARI	150 Years
Wind Category	High	Earthquake ARI	500		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

### Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof  $C_{p,i} = -0.3$

For roof  $C_{p,e}$  from 0 m To 2.61 m  $C_{p,e} = -0.891$   $p_e = -0.90$  KPa  $p_{net} = -0.90$  KPa

For roof  $C_{p,e}$  from 2.61 m To 5.23 m  $C_{p,e} = -0.891$   $p_e = -0.90$  KPa  $p_{net} = -0.90$  KPa

For wall Windward  $C_{p,i} = -0.3$  side Wall  $C_{p,i} = -0.3$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 10 m  $C_{p,e} = 0.7$   $p_e = 0.71$  KPa  $p_{net} = 1.05$  KPa

For side wall  $C_{p,e}$  from 0 m To 5.23 m  $C_{p,e} =$   $p_e = -0.66$  KPa  $p_{net} = -0.66$  KPa

Maximum Upward pressure used in roof member Design = 0.90 KPa

Maximum Downward pressure used in roof member Design = 0.33 KPa

Maximum Wall pressure used in Design = 1.05 KPa

Maximum Racking pressure used in Design = 0.91 KPa

### Design Summary

#### Girt Design Front and Back

Girt's Spacing = 600 mm

Girt's Span = 5000 mm

Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.98

K8 Upward = 0.65 S1 Downward = 12.23 S1 Upward = 20.38

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

$M_{Wind+Snow}$	1.97 Kn-m	Capacity	1.98 Kn-m	Passing Percentage	<b>100.51 %</b>
$V_{0.9D-WnUp}$	1.57 Kn-m	Capacity	13.75 Kn-m	Passing Percentage	<b>875.80 %</b>

### Deflections

First Page

### Pole Shed App Ver 01 2022

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 29.75 mm

Limit by Woolcock et al, 1999 Span/250 = 20.00 mm

Sag during installation = 46.79 mm

#### Reactions

Maximum = 1.57 kn

#### Girt Design Sides

Girt's Spacing = 600 mm

Girt's Span = 5000 mm

Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =0.98

K8 Upward =0.65   S1 Downward =12.23   S1 Upward =20.38

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

#### Capacity Checks

$M_{Wind+Snow}$	1.97 Kn-m	Capacity	1.98 Kn-m	Passing Percentage	<b>100.51 %</b>
$V_{0.9D-WnUp}$	1.57 Kn-m	Capacity	13.75 Kn-m	Passing Percentage	<b>875.80 %</b>

#### Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 29.75 mm

Limit by Woolcock et al. 1999 Span/100 = 20.00 mm

Sag during installation =46.79 mm

#### Reactions

Maximum = 1.57 kn

#### Middle Pole Design

##### Geometry

275 SED H5 (Minimum 300 dia. at Floor Level)	Dry Use	Height	4750 mm
Area	64885 mm <sup>2</sup>	As	48663.8671875 mm <sup>2</sup>
I <sub>x</sub>	335197731 mm <sup>4</sup>	Z <sub>x</sub>	2331810 mm <sup>3</sup>
I <sub>y</sub>	335197731 mm <sup>4</sup>	Z <sub>y</sub>	2331810 mm <sup>3</sup>
Lateral Restraint	4750 mm c/c		

#### Loads

Total Area over Pole = 25 m<sup>2</sup>

Dead	6.25 Kn	Live	6.25 Kn
Wind Down	8.25 Kn	Snow	0.00 Kn
Moment wind	19.20 Kn-m		
Phi	0.8	K8	0.84
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

#### Material

Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

#### Capacities

PhiNcx Wind	781.92 Kn	PhiMnx Wind	56.67 Kn-m	PhiVnx Wind	115.24 Kn
PhiNcx Dead	469.15 Kn	PhiMnx Dead	34.00 Kn-m	PhiVnx Dead	69.14 Kn

#### Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.37 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.14 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 19.62 \text{ mm} < 31.67 \text{ mm}$$

### Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

#### Assumed Soil Properties

Gamma	18 Kn/m <sup>3</sup>	Friction angle	30 deg	Cohesion	0 Kn/m <sup>3</sup>
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

#### Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1800 mm	Pile embedment length
f1 =	3563 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

#### Loads

Moment Wind =	19.20 Kn-m
Shear Wind =	5.39 Kn

#### Pile Properties

Safety Factory	0.55	
Hu =	9.69 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	20.58 Kn-m	Ultimate Moment Capacity of Pile

#### Checks

$$\text{Applied Forces/Capacities} = 0.93 < 1 \text{ OK}$$

### Uplift Check

$$\text{Density of Concrete} = 24 \text{ Kn/m}^3$$

$$\text{Density of Timber Pole} = 5 \text{ Kn/m}^3$$

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of  $\frac{3}{4}$

internal friction

Ks (Lateral Earth Pressure Coefficient) for cast in place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (1800) x Ks (1.5) x 0.5 x tan(30) x  $\pi$  x Dia of Pile (0.6) x Height of Pile (1800)

Skin Friction = 26.17 Kn

Weight of Pile + Pile Skin Friction = 29.32 Kn

Uplift on one Pile = 16.88 Kn

Uplift is ok