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Job No.: Rajasingham Family - 1   **Address:** 134 Hitiri Road, Kinloch, Tirohanga, Waikato, 3377, NZL   **Date:** 10/05/2024

Latitude: -38.633029   **Longitude:** 175.945656   **Elevation:** 463.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.5 m
Wind Region	NZ2	Terrain Category	2.46	Design Wind Speed	40.32 m/s
Wind Pressure	0.98 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Mono   Enclosed

For roof Cp,i = -0.3

For roof CP,e from 0 m To 4.02 m Cpe = -0.9   pe = -0.80 KPa   pnet = -0.80 KPa

For roof CP,e from 4.02 m To 8.03 m Cpe = -0.5   pe = -0.45 KPa   pnet = -0.45 KPa

For wall Windward Cp,i = -0.3   side Wall Cp,i = -0.3

For wall Windward and Leeward CP,e from 0 m   To 13.82 m   Cpe = 0.7   pe = 0.62 KPa   pnet = 0.92 KPa

For side wall CP,e from 0 m   To 4.02 m   Cpe =   pe = -0.58 KPa   pnet = -0.58 KPa

Maximum Upward pressure used in roof member Design = 0.80 KPa

Maximum Downward pressure used in roof member Design = 0.48 KPa

Maximum Wall pressure used in Design = 0.92 KPa

Maximum Racking pressure used in Design = 1.07 KPa

Design Summary

Rafter Design Internal

Internal Rafter Load Width = 4674 mm   Internal Rafter Span = 13950 mm   Try Rafter 2x610x45 LVL11

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K1 Medium term = 0.8   K1 Long term = 0.6   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =1.00   S1 Downward =11.05   S1 Upward =11.05

Shear Capacity of timber =5 MPa   Bending Capacity of timber =38 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	38.37 Kn-m	Capacity	90.18 Kn-m	Passing Percentage	**235.03 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	88.68 Kn-m	Capacity	120.24 Kn-m	Passing Percentage	**135.59 %**
$M_{0.9D-WnUp}$	-65.38 Kn-m	Capacity	-150.28 Kn-m	Passing Percentage	**229.86 %**
$V_{1.35D}$	11.00 Kn	Capacity	88.28 Kn	Passing Percentage	**802.55 %**

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$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	25.43 Kn	Capacity	117.7 Kn	Passing Percentage	**462.84 %**
$V_{0.9D-WnUp}$	-18.75 Kn	Capacity	-147.14 Kn	Passing Percentage	**784.75 %**

Deflections

Modulus of Elasticity = 9900 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 38.535 mm   Limit by Woolcock et al, 1999 Span/240 = 58.75 mm
Deflection under Dead and Service Wind = 52.81 mm   Limit by Woolcock et al, 1999 Span/100 = 141.00 mm

Reactions

Maximum downward =25.43 kn   Maximum upward = -18.75 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 4

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters =J2 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 12.6 fpj = 22.7 Mpa for Rafter with effective thickness = 90 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 58.22 Kn > -18.75 Kn

Girt Design Front and Back

Girt's Spacing = 700 mm   Girt's Span = 4674 mm   Try Girt 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =0.98

K8 Upward =0.68   S1 Downward =12.23   S1 Upward =19.70

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.76 Kn-m	Capacity	2.08 Kn-m	Passing Percentage	**118.18 %**
$V_{0.9D-WnUp}$	1.51 Kn	Capacity	13.75 Kn	Passing Percentage	**910.60 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 23.22 mm   Limit by Woolcock et al, 1999 Span/100 = 46.74 mm
Sag during installation = 35.73 mm

Reactions

Maximum = 1.51 kn

Girt Design Sides

Girt's Spacing = 700 mm   Girt's Span = 4050 mm   Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.88   S1 Downward =10.36   S1 Upward =15.54

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.32 Kn-m	Capacity	1.45 Kn-m	Passing Percentage	**109.85 %**
$V_{0.9D-WnUp}$	1.30 Kn	Capacity	10.13 Kn	Passing Percentage	**779.23 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 32.73 mm   Limit by Woolcock et al. 1999 Span/100 = 40.50 mm
Sag during installation =20.14 mm

Reactions

Maximum = 1.30 kn

Middle Pole Design

Geometry

225 SED H5 (Minimum 250 dia. at Floor Level)	Dry Use	Height	4334 mm
Area	44279 mm2	As	33209.1796875 mm2
Ix	156100441 mm4	Zx	1314530 mm3
Iy	156100441 mm4	Zx	1314530 mm3
Lateral Restraint	4334 mm c/c		

Loads

Total Area over Pole = 32.9517 m2

Dead	8.24 Kn	Live	8.24 Kn
Wind Down	15.82 Kn	Snow	0.00 Kn
Moment wind	18.94 Kn-m		
Phi	0.8	K8	0.76
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use

$fb =$	36.3 MPa	$fs =$	2.96 MPa
$fc =$	18 MPa	$fp =$	7.2 MPa
$ft =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	482.03 Kn	PhiMnx Wind	28.86 Kn-m	PhiVnx Wind	78.64 Kn
PhiNcx Dead	289.22 Kn	PhiMnx Dead	17.32 Kn-m	PhiVnx Dead	47.18 Kn

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.72 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.50 < 1 OK

Deflection at top under service lateral loads = 35.92 mm < 43.34 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m3		Friction angle	30 deg	Cohesion	0 Kn/m3

$K0 =$ (1-sin(30)) / (1+sin(30))

$Kp =$ (1+sin(30)) / (1-sin(30))

Geometry For Middle Bay Pole

$Ds =$	0.6 mm	Pile Diameter
$L =$	1800 mm	Pile embedment length
$f1 =$	3375 mm	Distance at which the shear force is applied
$f2 =$	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	18.94 Kn-m
Shear Wind =	5.61 Kn

Pile Properties

Safety Factory	0.55	
$Hu =$	10.04 Kn	Ultimate Lateral Strength of the Pile, Short pile
$Mu =$	20.32 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.93 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient)for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1800) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1800)

Skin Friction = 26.17 Kn

Weight of Pile + Pile Skin Friction = 30.29 Kn

Uplift on one Pile = 18.95 Kn

Uplift is ok

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