

Job No.: Justin Mills - 1**Address:** 2 Robinson Street, Cambridge 3434, New Zealand**Date:** 08/11/2024**Latitude:** -37.884276**Longitude:** 175.476739**Elevation:** 70.5 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.5 m
Wind Region	NZ1	Terrain Category	3.0	Design Wind Speed	40.08 m/s
Wind Pressure	0.96 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 4.38 m $C_{p,e} = -0.9$ $p_e = -0.78$ KPa $p_{net} = -0.78$ KPa

For roof $C_{p,e}$ from 4.38 m To 8.75 m $C_{p,e} = -0.5$ $p_e = -0.43$ KPa $p_{net} = -0.43$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 11 m $C_{p,e} = 0.7$ $p_e = 0.61$ KPa $p_{net} = 0.90$ KPa

For side wall $C_{p,e}$ from 0 m To 4.38 m $C_{p,e} =$ $p_e = -0.56$ KPa $p_{net} = -0.56$ KPa

Maximum Upward pressure used in roof member Design = 0.78 KPa

Maximum Downward pressure used in roof member Design = 0.38 KPa

Maximum Wall pressure used in Design = 0.78 KPa

Maximum Racking pressure used in Design = 1.04 KPa

Design Summary**Girt Design Front and Back**

Girt's Spacing = 1300 mm

Girt's Span = 2750 mm

Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.76 S1 Downward = 10.36 S1 Upward = 18.11

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.96 Kn-m	Capacity	1.26 Kn-m	Passing Percentage	131.25 %
$V_{0.9D-WnUp}$	1.39 Kn	Capacity	10.13 Kn	Passing Percentage	728.78 %

Deflections

Pole Shed App Ver 01 2022

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 10.95 mm

Limit by Woolcock et al, 1999 Span/100 = 27.50 mm

Sag during installation = 4.28 mm

Reactions

Maximum = 1.39 kn

Girt Design Sides

Girt's Spacing = 1300 mm

Girt's Span = 2100 mm

Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.87 S1 Downward =10.36 S1 Upward =15.83

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.56 Kn-m	Capacity	1.43 Kn-m	Passing Percentage	255.36 %
V _{0.9D-WnUp}	1.06 Kn	Capacity	10.13 Kn	Passing Percentage	955.66 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 3.73 mm

Limit by Woolcock et al. 1999 Span/100 = 21.00 mm

Sag during installation =1.46 mm

Reactions

Maximum = 1.06 kn

Middle Pole Design

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	3260 mm
Area	35448 mm ²	As	26585.7421875 mm ²
I _x	100042702 mm ⁴	Z _x	941578 mm ³
I _y	100042702 mm ⁴	Z _y	941578 mm ³
Lateral Restraint	3400 mm c/c		

Loads

Total Area over Pole = 16.5 m²

Dead	4.13 Kn	Live	4.13 Kn
Wind Down	6.27 Kn	Snow	0.00 Kn
Moment wind	13.11 Kn-m		
Phi	0.8	K8	0.86
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	438.78 Kn	PhiMnx Wind	23.50 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	263.27 Kn	PhiMnx Dead	14.10 Kn-m	PhiVnx Dead	37.77 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.59 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.34 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 22.69 \text{ mm} < 32.60 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1600 mm	Pile embedment length
f1 =	2625 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	13.11 Kn-m
Shear Wind =	4.99 Kn

Pile Properties

Safety Factory	0.55	
Hu =	8.64 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	13.81 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.95 < 1 \text{ OK}$$

End Pole Design

Geometry For End Bay Pole

Geometry

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200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	3350 mm
Area	35448 mm ²	As	26585.7421875 mm ²
I _x	100042702 mm ⁴	Z _x	941578 mm ³
I _y	100042702 mm ⁴	Z _y	941578 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 11.550577528876442 m²

Dead	2.89 Kn	Live	2.89 Kn
Wind Down	4.39 Kn	Snow	0.00 Kn
Moment Wind	5.40 Kn-m		
Phi	0.8	K ₈	0.87
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{cx} Wind	443.93 Kn	PhiM _{nx} Wind	23.78 Kn-m	PhiV _{nx} Wind	62.96 Kn
PhiN _{cx} Dead	266.36 Kn	PhiM _{nx} Dead	14.27 Kn-m	PhiV _{nx} Dead	37.77 Kn

Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.25 < 1$ OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.07 < 1$ OK

Deflection at top under service lateral loads = 10.00 mm < 34.91 mm

D _s =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f ₁ =	2625 mm	Distance at which the shear force is applied
f ₂ =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 11.550577528876442 m²

Moment Wind =	5.40 Kn-m
Shear Wind =	2.06 Kn

Pile Properties

Safety Factory	0.55	
H _u =	4.99 Kn	Ultimate Lateral Strength of the Pile, Short pile
M _u =	7.79 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.69 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f1 =	2625 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	5.40 Kn-m
Shear Wind =	2.06 Kn

Pile Properties

Safety Factory	0.55	
Hu =	4.99 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	7.79 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.69 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1600) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1600)

Skin Friction = 20.68 Kn

Weight of Pile + Pile Skin Friction = 24.83 Kn

Uplift on one Pile = 9.16 Kn

Uplift is ok