

Job No.: 399-96428C - 1

Address: 153 Ridge Road, Paengaroa, New Zealand

Date: 24/01/2024

Latitude: -41.142231

Longitude: 174.988781

Elevation: 263.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	5 m
Wind Region	NZ3	Terrain Category	3.0	Design Wind Speed	59.53 m/s
Wind Pressure	2.13 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	extra High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 5 m $C_{p,e} = -0.9$ $p_e = -1.72$ KPa $p_{net} = -1.72$ KPa

For roof $C_{p,e}$ from 5 m To 10 m $C_{p,e} = -0.5$ $p_e = -0.96$ KPa $p_{net} = -0.96$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 25.2 m $C_{p,e} = 0.7$ $p_e = 1.34$ KPa $p_{net} = 1.98$ KPa

For side wall $C_{p,e}$ from 0 m To 5 m $C_{p,e} =$ $p_e = -1.24$ KPa $p_{net} = -1.24$ KPa

Maximum Upward pressure used in roof member Design = 1.72 KPa

Maximum Downward pressure used in roof member Design = 1.02 KPa

Maximum Wall pressure used in Design = 1.98 KPa

Maximum Racking pressure used in Design = 1.69 KPa

Design Summary

Girt Design Front and Back

Girt's Spacing = 900 mm

Girt's Span = 4200 mm

Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 0.87 S1 Downward = 12.68 S1 Upward = 15.81

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	3.93 Kn-m	Capacity	5.06 Kn-m	Passing Percentage	128.75 %
$V_{0.9D-WnUp}$	3.74 Kn-m	Capacity	20.10 Kn-m	Passing Percentage	537.43 %

Deflections

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Pole Shed App Ver 01 2022

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 16.55 mm

Limit by Woolcock et al, 1999 Span/100 = 42.00 mm

Sag during installation = 18.87 mm

Reactions

Maximum = 3.74 kn

Girt Design Sides

Girt's Spacing = 900 mm

Girt's Span = 4540 mm

Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =0.97

K8 Upward =0.84 S1 Downward =12.68 S1 Upward =16.44

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	4.59 Kn-m	Capacity	4.90 Kn-m	Passing Percentage	106.75 %
V _{0.9D-WnUp}	4.05 Kn-m	Capacity	20.10 Kn-m	Passing Percentage	496.30 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 22.60 mm

Limit by Woolcock et al. 1999 Span/100 = 45.40 mm

Sag during installation =25.76 mm

Reactions

Maximum = 4.05 kn

Middle Pole Design

Geometry

275 SED H5 (Minimum 300 dia. at Floor Level)	Dry Use	Height	3800 mm
Area	64885 mm ²	As	48663.8671875 mm ²
I _x	335197731 mm ⁴	Z _x	2331810 mm ³
I _y	335197731 mm ⁴	Z _y	2331810 mm ³
Lateral Restraint	3800 mm c/c		

Loads

Total Area over Pole = 25.2 m²

Dead	6.30 Kn	Live	6.30 Kn
Wind Down	25.70 Kn	Snow	0.00 Kn
Moment wind	33.19 Kn-m		
Phi	0.8	K8	0.96
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	895.43 Kn	PhiMnx Wind	64.90 Kn-m	PhiVnx Wind	115.24 Kn
PhiNcx Dead	537.26 Kn	PhiMnx Dead	38.94 Kn-m	PhiVnx Dead	69.14 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.55 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.30 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 28.55 \text{ mm} < 38.00 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	2200 mm	Pile embedment length
f1 =	3750 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	33.19 Kn-m
Shear Wind =	8.85 Kn

Pile Properties

Safety Factory	0.55	
Hu =	15.95 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	36.25 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.92 < 1 \text{ OK}$$

Uplift Check

$$\text{Density of Concrete} = 24 \text{ Kn/m}^3$$

$$\text{Density of Timber Pole} = 5 \text{ Kn/m}^3$$

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of $\frac{3}{4}$

internal friction

Ks (Lateral Earth Pressure Coefficient) for cast in place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (2200) x Ks (1.5) x 0.5 x tan(30) x π x Dia of Pile (0.6) x Height of Pile (2200)

Skin Friction = 39.09 Kn

Weight of Pile + Pile Skin Friction = 42.94 Kn

Uplift on one Pile = 37.67 Kn

Uplift is ok