

Job No.: 689052**Address:** 4 Penney Crescent, Kaikohe, New Zealand**Date:** 08/11/2024**Latitude:** -35.412363**Longitude:** 173.805951**Elevation:** 192.5 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4 m
Wind Region	NZ1	Terrain Category	2.55	Design Wind Speed	37.37 m/s
Wind Pressure	0.84 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 3.84 m $C_{p,e} = -0.9$ $p_e = -0.68$ KPa $p_{net} = -0.68$ KPa

For roof $C_{p,e}$ from 3.84 m To 7.69 m $C_{p,e} = -0.5$ $p_e = -0.38$ KPa $p_{net} = -0.38$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 6 m $C_{p,e} = 0.7$ $p_e = 0.53$ KPa $p_{net} = 0.78$ KPa

For side wall $C_{p,e}$ from 0 m To 3.84 m $C_{p,e} =$ $p_e = -0.49$ KPa $p_{net} = -0.49$ KPa

Maximum Upward pressure used in roof member Design = 0.68 KPa

Maximum Downward pressure used in roof member Design = 0.33 KPa

Maximum Wall pressure used in Design = 0.78 KPa

Maximum Racking pressure used in Design = 0.91 KPa

Design Summary**Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 4350 mm

Try Purlin 190x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.98

K8 Upward = 0.41 S1 Downward = 12.23 S1 Upward = 26.73

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.72 Kn-m	Capacity	1.79 Kn-m	Passing Percentage	248.61 %
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	1.83 Kn-m	Capacity	2.38 Kn-m	Passing Percentage	130.05 %
$M_{0.9D-W_nUp}$	-0.97 Kn-m	Capacity	-1.23 Kn-m	Passing Percentage	112.84 %
$V_{1.35D}$	0.66 Kn	Capacity	8.25 Kn	Passing Percentage	1250.00 %

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V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	1.32 Kn	Capacity	11.00 Kn	Passing Percentage	833.33 %
V _{0.9D-WnUp}	-0.89 Kn	Capacity	-13.75 Kn	Passing Percentage	1544.94 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 13.95 mm Limit by Woolcock et al, 1999 Span/240 = 17.92 mm

Deflection under Dead and Service Wind = 15.46 mm Limit by Woolcock et al, 1999 Span/100 = 43.00 mm

Reactions

Maximum downward = 1.32 kn Maximum upward = -0.89 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4500 mm Internal Rafter Span = 5850 mm Try Rafter 2x290x45 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₁ Medium term = 0.8 K₁ Long term = 0.6 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 1.00 S₁ Downward = 7.47 S₁ Upward = 7.47

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	6.50 Kn-m	Capacity	8.48 Kn-m	Passing Percentage	130.46 %
M _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	12.99 Kn-m	Capacity	11.3 Kn-m	Passing Percentage	86.99 %
M _{0.9D-WnUp}	-8.76 Kn-m	Capacity	-14.12 Kn-m	Passing Percentage	161.19 %
V _{1.35D}	4.44 Kn	Capacity	25.18 Kn	Passing Percentage	567.12 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	8.88 Kn	Capacity	33.58 Kn	Passing Percentage	378.15 %
V _{0.9D-WnUp}	-5.99 Kn	Capacity	-41.96 Kn	Passing Percentage	700.50 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 20.755 mm Limit by Woolcock et al, 1999 Span/240 = 25.00 mm

Deflection under Dead and Service Wind = 25.56 mm Limit by Woolcock et al, 1999 Span/100 = 60.00 mm

Reactions

Maximum downward = 8.88 kn Maximum upward = -5.99 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 90 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 19.50 Kn > -5.99 Kn

Intermediate Design Front and Back

Intermediate Spacing = 2250 mm

Intermediate Span = 3536 mm

Try Intermediate 2x140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =10.36 S1 Upward =0.65

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.74 Kn-m	Capacity	3.3 Kn-m	Passing Percentage	120.44 %
V _{0.9D-WnUp}	3.10 Kn	Capacity	-20.26 Kn	Passing Percentage	653.55 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 32.13 mm

Limit by Woolcock et al, 1999 Span/100 = 35.36 mm

Reactions

Maximum = 3.10 kn

Girt Design Front and Back

Girt's Spacing = 1300 mm

Girt's Span = 2250 mm

Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.84 S1 Downward =10.36 S1 Upward =16.38

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.64 Kn-m	Capacity	1.39 Kn-m	Passing Percentage	217.19 %
V _{0.9D-WnUp}	1.14 Kn	Capacity	10.13 Kn	Passing Percentage	888.60 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

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Deflection under Snow and Service Wind = 4.91 mm

Limit by Woolcock et al, 1999 Span/100 = 22.50 mm

Sag during installation = 1.92 mm

Reactions

Maximum = 1.14 kn

Girt Design Sides

Girt's Spacing = 1300 mm

Girt's Span = 3000 mm

Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.72 S1 Downward =10.36 S1 Upward =18.92

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.14 Kn-m	Capacity	1.19 Kn-m	Passing Percentage	104.39 %
V _{0.9D-WnUp}	1.52 Kn	Capacity	10.13 Kn	Passing Percentage	666.45 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 15.51 mm

Limit by Woolcock et al. 1999 Span/100 = 30.00 mm

Sag during installation =6.06 mm

Reactions

Maximum = 1.52 kn

Middle Pole Design

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	3700 mm
Area	35448 mm ²	As	26585.7421875 mm ²
I _x	100042702 mm ⁴	Z _x	941578 mm ³
I _y	100042702 mm ⁴	Z _y	941578 mm ³
Lateral Restraint	3700 mm c/c		

Loads

Total Area over Pole = 13.5 m²

Dead	3.38 Kn	Live	3.38 Kn
Wind Down	4.46 Kn	Snow	0.00 Kn
Moment wind	12.25 Kn-m		
Phi	0.8	K8	0.80
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

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Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	406.33 Kn	PhiMnx Wind	21.77 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	243.80 Kn	PhiMnx Dead	13.06 Kn-m	PhiVnx Dead	37.77 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.59 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.34 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 27.52 \text{ mm} < 37.00 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
$K_0 =$	$(1 - \sin(30)) / (1 + \sin(30))$				
$K_p =$	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

$D_s =$	0.6 mm	Pile Diameter
$L =$	1550 mm	Pile embedment length
$f_1 =$	3000 mm	Distance at which the shear force is applied
$f_2 =$	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	12.25 Kn-m
Shear Wind =	4.08 Kn

Pile Properties

Safety Factory	0.55	
$H_u =$	7.29 Kn	Ultimate Lateral Strength of the Pile, Short pile
$M_u =$	13.07 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.94 < 1 \text{ OK}$$

End Pole Design

Geometry For End Bay Pole

Geometry

175 SED H5 (Minimum 200 dia. at Floor Level)	Dry Use	Height	3800 mm
Area	27598 mm ²	A_s	20698.2421875 mm ²

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Ix	60639381 mm ⁴	Zx	646820 mm ³
Iy	60639381 mm ⁴	Zy	646820 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 13.5 m²

Dead	3.38 Kn	Live	3.38 Kn
Wind Down	4.46 Kn	Snow	0.00 Kn
Moment Wind	6.13 Kn-m		
Phi	0.8	K8	0.66
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{cx} Wind	261.19 Kn	PhiM _{nx} Wind	12.35 Kn-m	PhiV _{nx} Wind	49.01 Kn
PhiN _{cx} Dead	156.71 Kn	PhiM _{nx} Dead	7.41 Kn-m	PhiV _{nx} Dead	29.41 Kn

Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.54 < 1$ OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.29 < 1$ OK

Deflection at top under service lateral loads = 24.48 mm < 39.90 mm

D _s =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f ₁ =	3000 mm	Distance at which the shear force is applied
f ₂ =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 13.5 m²

Moment Wind =	6.13 Kn-m
Shear Wind =	2.04 Kn

Pile Properties

Safety Factory	0.55	
H _u =	4.55 Kn	Ultimate Lateral Strength of the Pile, Short pile
M _u =	8.02 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.76 < 1$ OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K ₀ =	$(1 - \sin(30)) / (1 + \sin(30))$				
K _p =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

D _s =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f ₁ =	3000 mm	Distance at which the shear force is applied
f ₂ =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	6.13 Kn-m
Shear Wind =	2.04 Kn

Pile Properties

Safety Factory	0.55	
H _u =	4.55 Kn	Ultimate Lateral Strength of the Pile, Short pile
M _u =	8.02 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = $0.76 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K_s (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (1550) x K_s (1.5) x 0.5 x tan(30) x Pi x Dia of Pile (0.6) x Height of Pile (1550)

Skin Friction = 19.40 Kn

Weight of Pile + Pile Skin Friction = 23.43 Kn

Uplift on one Pile = 6.14 Kn

Uplift is ok