Job Number:	RW/hite
Issue:	BWhite Consulting Ltd
PRODUCER STATEMENT-PS1-DESIGN	8
ISSUED BY: BWhite Consulting Ltd (Design Engineer: Bevan White)	
TO BE SUPPLIED TO: Southland District Council IN RESPECT OF: Proposed NEW Farm Shed	
AT: 555 Hutchinson Road, Richmond Downs 3371, New Zealand	
LEGAL DES CRIPTION	
We have been engaged by Ezequote Pty Ltd to provide Specific Structural Engineering Design requirements of Clause(s) B1 of the Building Code for part only (as specified in the attachment to building work.	<u> </u>
☐ ALL ☑ Part only as specified: Purlins, Rafters, Girts, Poles, Columns, Pole embedment and	all connections
The design has been prepared in accordance with compliance documents to NZ Building Code is Innovation & Employment Clauses B1/VM1 and B1/VM4	sued by Ministry of Business,
The proposed building work covered by the producer statement is described on Ezequote drawing A101 - A116 Rev-1 dated 21/05/2025 together with the following specification, and other docum attached to this statement: Design Featured Report Dated 3/11/2025 and numbered "Second Page	ents set out in the schedule
On behalf of BWhite Consulting Ltd, and subject to:	
 Site verification of the following design assumptions: an Ultimate foundation bearing pre with NZS3604:2011 The building has a design life of 50 years and am Importance Level 2 Unless specifically noted, compliance of the drawings to None-Specific codes such as NZ been checked by this practice This Certificate does not cover any other building code clause including weather tightne Inspections of the building to be completed by Southland District Council. As BWhite Coinspections, we cannot issue a producer Statement-PS4- Construction Review. This Producer Statement- Design is valid for a building consent issued within 1 year from All proprietary products meeting their performance specification requirements 	S3604 and NZS4229 have not ess onsulting Ltd are not undertaking
I believe on reasonable grounds that a) the building, if constructed in accordance with the drawin documents provided or listed in the attached schedule, will comply with the relevant provisions of the presons who have undertaken the design have the necessary competency to do so. I also reconstruction monitoring/observation:	of the Building Code and that b),
✓ CM1 ☐ CM2 ☐ CM3 ☐ CM4 ☐ CM5 or as per agreement with owner/developer (stated al	oove)
I, Bevan White am CPEng 108276 I am Member of Engineering New Zealand and hold the follow holds a current policy of Professional Indemnity Insurance no less than \$200,000	ing qualification: BECivil and
Signed by Bevan White on behalf of BWhite Consulting Ltd Dated: 3/11/2025	
Email: bwhitecpeng@gmail.com Phone: 0211-979786	
Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Au	

This form is to accompany Form 2 of the Building (Forms) Regulations 2004 for the application of a Building Consent

whether in contract, tort or otherwise(including negligence), is limited to the sum of \$200,000.

Date: 3/11/2025

BWhite

18B Jules Crescent,

Consulting Ltd

Bell Block New Plymouth 4312

New Zealand File No:

DESIGN FEATURES SUMMARY FOR PROPOSED NEW FARM SHED 555 HUTCHINSON ROAD, RICHMOND DOWNS 3371, NEW ZEALAND

Site Specific Loads

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	В
Importance Level	2	Ultimate wind & EQ ARI	100 Years	Max Height	4.05 m
Wind Region	NZ1	Terrain Category	2.0	Design Wind Speed	44.63 m/s
Wind Pressure	1.2 KPa	Lee Zone	NO	Ultimate Snow ARI	150 Years

Timber

Sawn Timber to be graded to the properties of SG6 and SG8 or better as mentioned on plans, with moisture content of 18% or less for dry and 25% or less for wet.

The following standards have been used in the design of this structure

- NZS 3603:1993 Timber Structures Standard
- NZS 3604:2011 Timber Framed Buildings. Standards New Zealand, 2011
- NZS 3404:1997 Steel Structures
- AS/NZS 1170 2003 Structural Design Actions
- AS/NZS 1170.2 2021 Structural Design Actions-Wind Action
- Branz. "Engineering Basis of NZS 3604". April 2013

Yours Faithfully

BWhite CONSULTING LTD

Bevan White

Director | BE Civil . CMengNZ CPEng

Email: bwhitecpeng@gmail.com Contact: 0211 979 786

Job No.: 412-Cover Address: 555 Hutchinson Road, Richmond Downs Date: 3/11/2025

3371, New Zealand

Latitude: -37.712492 **Longitude:** 175.639468 **Elevation:** 67 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	В
Importance Level	2	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.05 m
Wind Region	NZ1	Terrain Category	2.0	Design Wind Speed	44.63 m/s
Wind Pressure	1.2 KPa	Lee Zone	NO	Ultimate Snow ARI	150 Years
Wind Category	Very High	Earthquake ARI	500		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Mono Enclosed

For roof Cp, i = 0.6409

For roof CP,e from 0 m To 4.15 m Cpe = -0.9 pe = -0.70 KPa pnet = -1.30 KPa

For roof CP,e from 4.15 m To 8.30 m Cpe = -0.5 pe = -0.39 KPa pnet = -0.99 KPa

For wall Windward Cp, i = 0.6409 side Wall Cp, i = -0.5402

For wall Windward and Leeward CP,e from 0 m To 9 m Cpe = 0.7 pe = 0.75 KPa pnet = 1.38 KPa

For side wall CP,e from 0 m To 4.15 m Cpe = pe = -0.70 KPa pnet = -0.07 KPa

Maximum Upward pressure used in roof member Design = 1.30 KPa

Maximum Downward pressure used in roof member Design = 0.74 KPa

Maximum Wall pressure used in Design = 1.38 KPa

Maximum Racking pressure used in Design = 1.29 KPa

Design Summary

Purlin Design

Purlin Spacing = 900 mm Purlin Span = 5200 mm Try Purlin 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.85 S1 Downward = 9.63 S1 Upward = 16.29

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M1.35D	1.03 Kn-m	Capacity	1.26 Kn-m	Passing Percentage	122.33 %
M1.2D+1.5L 1.2D+Sn 1.2D+WnDn	3.16 Kn-m	Capacity	1.68 Kn-m	Passing Percentage	53.16 %
$M_{0.9D\text{-W}nUp}$	-3.27 Kn-m	Capacity	-1.78 Kn-m	Passing Percentage	54.43 %
V _{1.35D}	0.79 Kn	Capacity	7.24 Kn	Passing Percentage	916.46 %
V _{1.2D+1.5L} 1.2D+Sn 1.2D+WnDn	2.43 Kn	Capacity	9.65 Kn	Passing Percentage	397.12 %
$ m V_{0.9D-WnUp}$	-2.52 Kn	Capacity	-12.06 Kn	Passing Percentage	478.57 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 76.97 mm

Limit by Woolcock et al, 1999 Span/360 = 14.31 mm

Deflection under Dead and Service Wind = 76.12 mm

Limit by Woolcock et al, 1999 Span/250 = 34.33 mm

Reactions

Maximum downward = 2.43 kn Maximum upward = -2.52 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Girt Design Front and Back

Girt's Spacing = 1300 mm Girt's Span = 2675 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.70 S1 Downward =11.27 S1 Upward =19.43

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.60 Kn-m	Capacity	2.61 Kn-m	Passing Percentage	163.13 %
$ m V_{0.9D ext{-}WnUp}$	2.40 Kn	Capacity	16.08 Kn	Passing Percentage	670.00 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 7.80 mm Limit by Woolcock et al, 1999 Span/250 = 10.70 mm Sag during installation = 3.10 mm

Reactions

Maximum = 2.40 kn

Girt Design Sides

Girt's Spacing = 1300 mm Girt's Span = 3429 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.88 S1 Downward =11.27 S1 Upward =15.56

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	2.64 Kn-m	Capacity	3.28 Kn-m	Passing Percentage	124.24 %
$ m V_{0.9D-WnUp}$	3.08 Kn	Capacity	16.08 Kn	Passing Percentage	522.08 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 21.05 mm Limit by Woolcock et al. 1999 Span/100 = 13.71 mm Sag during installation = 8.38 mm

Reactions

Maximum = 3.08 kn

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 22.07 Kn

Uplift on one Pile = 25.88 Kn

Uplift is ok