Job No.: N & I Service - 3   **Address:** 504 Cissy Bay Road, Cissy Bay,   **Date:** 9/14/2023
Marlborough Sounds, New Zealand

Latitude: -40.989404   **Longitude:** 173.823865   **Elevation:** 16.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	D
Importance Level	2	Ultimate wind & Earthquake ARI	500 Years	Max Height	4.2 m
Wind Region	NZ3	Terrain Category	1.0	Design Wind Speed	49.54 m/s
Wind Pressure	1.47 KPa	Lee Zone	NO	Ultimate Snow ARI	150 Years
Wind Category	Very High	Earthquake ARI	500		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Mono   Enclosed

For roof $C_{p,i}$ = -0.3

For roof CP,e from 0 m To 3.53 m C_{pe} = -0.9   pe = -1.05 KPa   pnet = -1.05 KPa

For roof CP,e from 3.53 m To 7.07 m C_{pe} = -0.5   pe = -0.59 KPa   pnet = -0.59 KPa

For wall Windward $C_{p,i}$ = -0.3   side Wall $C_{p,i}$ = -0.3

For wall Windward and Leeward CP,e from 0 m To 9 m C_{pe} = 0.7   pe = 0.82 KPa   pnet = 1.21 KPa

For side wall CP,e from 0 m To 3.53 m C_{pe} =   pe = -0.76 KPa   pnet = -0.76 KPa

Maximum Upward pressure used in roof member Design = 1.05 KPa

Maximum Downward pressure used in roof member Design = 0.51 KPa

Maximum Wall pressure used in Design = 1.21 KPa

Maximum Racking pressure used in Design = 1.3 KPa

Design Summary

Purlin Design

Purlin Spacing = 900 mm   Purlin Span = 2850 mm   Try Purlin 150x50 SG8 Dry

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Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1   K1 Medium term = 0.8   K1 Long term = 0.6   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.82   S1 Downward =9.63   S1 Upward =16.99

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.31 Kn-m	Capacity	1.26 Kn-m	Passing Percentage	**406.45 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	1.06 Kn-m	Capacity	1.68 Kn-m	Passing Percentage	**158.49 %**
$M_{0.9D-WnUp}$	-0.75 Kn-m	Capacity	-1.71 Kn-m	Passing Percentage	**128.57 %**
$V_{1.35D}$	0.43 Kn	Capacity	7.24 Kn	Passing Percentage	**1683.72 %**
$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	1.04 Kn	Capacity	9.65 Kn	Passing Percentage	**927.88 %**
$V_{0.9D-WnUp}$	-1.06 Kn	Capacity	-12.06 Kn	Passing Percentage	**1137.74 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 4.59 mm   Limit by Woolcock et al, 1999 Span/360 = 7.78 mm
Deflection under Dead and Service Wind = 5.77 mm   Limit by Woolcock et al, 1999 Span/250 = 18.67 mm

Reactions

Maximum downward =1.04 kn   Maximum upward = -1.06 kn

Number of Blocking = 0   if 0 then no blocking required, if 1 then one midspan blocking required

Girt Design Front and Back

Girt's Spacing = 900 mm   Girt's Span = 3000 mm   Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.79   S1 Downward =9.63   S1 Upward =17.59

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

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| $M_{Wind+Snow}$ | 1.23 Kn-m | Capacity | 1.65 Kn-m | Passing Percentage | **134.15 %** |
| $V_{0.9D-WnUp}$ | 1.63 Kn-m | Capacity | 12.06 Kn-m | Passing Percentage | **739.88 %** |

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 12.19 mm   Limit by Woolcock et al, 1999 Span/250 = 12.00 mm
Sag during installation = 4.91 mm

Reactions

Maximum = 1.63 kn

Girt Design Sides

Girt's Spacing = 900 mm   Girt's Span = 2250 mm   Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.89   S1 Downward =9.63   S1 Upward =15.23

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

| $M_{Wind+Snow}$ | 0.69 Kn-m | Capacity | 1.87 Kn-m | Passing Percentage | **271.01 %** |
| $V_{0.9D-WnUp}$ | 1.23 Kn-m | Capacity | 12.06 Kn-m | Passing Percentage | **980.49 %** |

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 3.86 mm   Limit by Woolcock et al. 1999 Span/100 = 9.00 mm
Sag during installation =1.55 mm

Reactions

Maximum = 1.23 kn

Middle Pole Design

Geometry

225 SED H5 (Minimum 250 dia. at Floor Level)   Dry Use   Height   3900 mm

Area	44279 mm2	As	33209.1796875 mm2
Ix	156100441 mm4	Zx	1314530 mm3
Iy	156100441 mm4	Zx	1314530 mm3
Lateral Restraint	3900 mm c/c		

Loads

Total Area over Pole = 13.5 m2

Dead	3.38 Kn	Live	3.38 Kn
Wind Down	6.88 Kn	Snow	0.00 Kn
Moment wind	8.58 Kn-m		
Phi	0.8	K8	0.84
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Peeling	Steaming	Normal	Dry Use
$f_b =$	36.3 MPa	$f_s =$	2.96 MPa
$f_c =$	18 MPa	$f_p =$	7.2 MPa
$f_t =$	22 MPa	$E =$	9257 MPa

Capacities

PhiNcx Wind	536.44 Kn	PhiMnx Wind	32.12 Kn-m	PhiVnx Wind	78.64 Kn
PhiNcx Dead	321.86 Kn	PhiMnx Dead	19.27 Kn-m	PhiVnx Dead	47.18 Kn

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.29 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.10 < 1 OK

Deflection at top under service lateral loads = 13.66 mm < 26.00 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma   18 Kn/m3   Friction angle   30 deg   Cohesion   0 Kn/m3

$K0 =$ (1-sin(30)) / (1+sin(30))

$Kp =$ $(1+\sin(30)) / (1-\sin(30))$

Geometry For Middle Bay Pole

$Ds =$	0.6 mm	Pile Diameter
$L =$	1550 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	8.58 Kn-m
Shear Wind =	2.72 Kn

Pile Properties

Safety Factory	0.55	
$Hu =$	7.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
$Mu =$	13.22 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.65 < 1 OK

End Pole Design

Geometry For End Bay Pole

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use		Height	4050 mm
Area	35448 mm2	As	26585.7421875 mm2	
Ix	100042702 mm4	Zx	941578 mm3	
Iy	100042702 mm4	Zx	941578 mm3	
Lateral Restraint	mm c/c			

Loads

Total Area over Pole = 6.75 m2

Dead	1.69 Kn	Live	1.69 Kn
Wind Down	3.44 Kn	Snow	0.00 Kn
Moment Wind	4.29 Kn-m		
Phi	0.8	K8	0.72

K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f_b =	36.3 MPa	f_s =	2.96 MPa
f_c =	18 MPa	f_p =	7.2 MPa
f_t =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	365.76 Kn	PhiMnx Wind	19.59 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	219.46 Kn	PhiMnx Dead	11.76 Kn-m	PhiVnx Dead	37.77 Kn

Checks

$(Mx/PhiMnx)+(N/phiNcx) = 0.24 < 1$ OK

$(Mx/PhiMnx)^2+(N/phiNcx) = 0.07 < 1$ OK

Deflection at top under service lateral loads = 11.45 mm < 27.93 mm

D_s =	0.6 mm	Pile Diameter
L =	1550 mm	Pile embedment length
f_1 =	3150 mm	Distance at which the shear force is applied
f_2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 6.75 m2

Moment Wind =	4.29 Kn-m
Shear Wind =	1.36 Kn

Pile Properties

Safety Factory	0.55	
Hu =	7.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	13.22 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.32 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma   18 Kn/m3   Friction angle   30 deg   Cohesion   0 Kn/m3

$K0 =$ $(1-\sin(30)) / (1+\sin(30))$

$Kp =$ $(1+\sin(30)) / (1-\sin(30))$

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1550 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =   4.29 Kn-m

Shear Wind =   1.36 Kn

Pile Properties

Safety Factory	0.55	
Hu =	7.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	13.22 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.32 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient)for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1550) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1550)

Skin Friction = 19.40 Kn

Weight of Pile + Pile Skin Friction = 22.96 Kn

Uplift on one Pile = 11.14 Kn

Uplift is ok

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