

Job No.: 5115024588 - 1**Address:** 1763 Mitcham Rd, Ashburton, New Zealand**Date:** 14/08/2024**Latitude:** -43.751515**Longitude:** 171.862671**Elevation:** 160 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N4	Ground Snow Load	0.94 KPa	Roof Snow Load	0.66 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.6 m
Wind Region	NZ2	Terrain Category	2.04	Design Wind Speed	38.08 m/s
Wind Pressure	0.87 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Gable Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 1.95 m $C_{p,e} = -1.02$ $p_e = -0.80$ KPa $p_{net} = -0.80$ KPa

For roof $C_{p,e}$ from 1.95 m To 3.90 m $C_{p,e} = -0.84$ $p_e = -0.66$ KPa $p_{net} = -0.66$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 18 m $C_{p,e} = 0.7$ $p_e = 0.55$ KPa $p_{net} = 0.81$ KPa

For side wall $C_{p,e}$ from 0 m To 3.90 m $C_{p,e} =$ $p_e = -0.51$ KPa $p_{net} = -0.51$ KPa

Maximum Upward pressure used in roof member Design = 0.80 KPa

Maximum Downward pressure used in roof member Design = 0.42 KPa

Maximum Wall pressure used in Design = 0.81 KPa

Maximum Racking pressure used in Design = 0.75 KPa

Design Summary**Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 4350 mm

Try Purlin 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.47 S1 Downward = 11.27 S1 Upward = 24.64

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.72 Kn-m	Capacity	2.23 Kn-m	Passing Percentage	309.72 %
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	2.04 Kn-m	Capacity	2.97 Kn-m	Passing Percentage	145.59 %
$M_{0.9D-W_nUp}$	-1.22 Kn-m	Capacity	-1.76 Kn-m	Passing Percentage	144.26 %
$V_{1.35D}$	0.66 Kn	Capacity	9.65 Kn	Passing Percentage	1462.12 %

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V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	1.88 Kn	Capacity	12.86 Kn	Passing Percentage	684.04 %
V _{0.9D-WnUp}	-1.13 Kn	Capacity	-16.08 Kn	Passing Percentage	1423.01 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 10.76 mm Limit by Woolcock et al, 1999 Span/240 = 17.92 mm

Deflection under Dead and Service Wind = 12.74 mm Limit by Woolcock et al, 1999 Span/100 = 43.00 mm

Reactions

Maximum downward = 1.88 kn Maximum upward = -1.13 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4500 mm Internal Rafter Span = 5850 mm Try Rafter 2x300x45 LVL11

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₁ Medium term = 0.8 K₁ Long term = 0.6 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 1.00 S₁ Downward = 7.61 S₁ Upward = 7.61

Shear Capacity of timber = 5 MPa Bending Capacity of timber = 38 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	6.50 Kn-m	Capacity	24.62 Kn-m	Passing Percentage	378.77 %
M _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	18.48 Kn-m	Capacity	32.84 Kn-m	Passing Percentage	177.71 %
M _{0.9D-WnUp}	-11.07 Kn-m	Capacity	-41.04 Kn-m	Passing Percentage	370.73 %
V _{1.35D}	4.44 Kn	Capacity	43.42 Kn	Passing Percentage	977.93 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	12.64 Kn	Capacity	57.88 Kn	Passing Percentage	457.91 %
V _{0.9D-WnUp}	-7.57 Kn	Capacity	-72.36 Kn	Passing Percentage	955.88 %

Deflections

Modulus of Elasticity = 9900 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 10.225 mm Limit by Woolcock et al, 1999 Span/240 = 25.00 mm

Deflection under Dead and Service Wind = 13.445 mm Limit by Woolcock et al, 1999 Span/100 = 60.00 mm

Reactions

Maximum downward = 12.64 kn Maximum upward = -7.57 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J2 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 12.6 fpj = 22.7 Mpa for Rafter with effective thickness = 90 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 29.11 Kn > -7.57 Kn

Intermediate Design Sides

Intermediate Spacing = 3000 mm

Intermediate Span = 3450 mm

Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =11.27 S1 Upward =0.70

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.10 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	355.24 %
V _{0.9D-WnUp}	2.43 Kn	Capacity	32.16 Kn	Passing Percentage	1323.46 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 26.9 mm

Limit by Woolcock et al, 1999 Span/100 = 34.50 mm

Reactions

Maximum = 2.43 kn

Girt Design Front and Back

Girt's Spacing = 900 mm

Girt's Span = 4500 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.78 S1 Downward =11.27 S1 Upward =17.82

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.85 Kn-m	Capacity	2.90 Kn-m	Passing Percentage	156.76 %
V _{0.9D-WnUp}	1.64 Kn	Capacity	16.08 Kn	Passing Percentage	980.49 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

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Deflection under Snow and Service Wind = 31.63 mm

Limit by Woolcock et al, 1999 Span/100 = 45.00 mm

Sag during installation = 24.86 mm

Reactions

Maximum = 1.64 kn

Girt Design Sides

Girt's Spacing = 900 mm

Girt's Span = 3000 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.92 S1 Downward =11.27 S1 Upward =14.55

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	0.82 Kn-m	Capacity	3.42 Kn-m	Passing Percentage	417.07 %
V _{0.9D-WnUp}	1.09 Kn	Capacity	16.08 Kn	Passing Percentage	1475.23 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 6.25 mm

Limit by Woolcock et al. 1999 Span/100 = 30.00 mm

Sag during installation =4.91 mm

Reactions

Maximum = 1.09 kn

End Pole Design

Geometry For End Bay Pole

Geometry

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	3300 mm
Area	20729 mm ²	As	15546.6796875 mm ²
I _x	34210793 mm ⁴	Z _x	421056 mm ³
I _y	34210793 mm ⁴	Z _y	421056 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 13.5 m²

Dead	3.38 Kn	Live	3.38 Kn
Wind Down	5.67 Kn	Snow	8.91 Kn
Moment Wind	4.09 Kn-m	Moment snow	1.90 Kn-m
Phi	0.8	K8	0.66
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

Capacities

PhiNcx Wind	195.59 Kn	PhiMnx Wind	8.01 Kn-m	PhiVnx Wind	36.81 Kn
PhiNcx Dead	117.35 Kn	PhiMnx Dead	4.81 Kn-m	PhiVnx Dead	22.09 Kn
PhiNcx Snow	156.47 Kn	PhiMnx Snow	6.41 Kn-m	PhiVnx Snow	29.45 Kn

Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.60 < 1$ OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.35 < 1$ OK

Deflection at top under service lateral loads = 23.46 mm < 35.91 mm

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 13.5 m²

Moment Wind =	4.09 Kn-m	Moment Snow =	1.90 Kn-m
Shear Wind =	1.51 Kn	Shear Snow =	1.90 Kn

Pile Properties

Safety Factory	0.55	
Hu =	7.16 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	11.65 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.35 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied

$f_2 =$ 0 mm Distance of top soil at rest pressure

Loads

Moment Wind =	4.09 Kn-m	Moment Snow =	1.90 Kn-m
Shear Wind =	1.51 Kn	Shear Snow =	1.90 Kn

Pile Properties

Safety Factory	0.55		
Hu =	7.16 Kn	Ultimate Lateral Strength of the Pile, Short pile	
Mu =	11.65 Kn-m	Ultimate Moment Capacity of Pile	

Checks

Applied Forces/Capacities = $0.35 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x $0.5 \times \tan(30)$ x π x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 23.08 Kn

Uplift on one Pile = 7.76 Kn

Uplift is ok