Pole Shed App Ver 01 2022	
Job Number:	BWhite
Issue:	Consulting Ltd
PRODUCER STATEMENT-PS1-DESIGN	
ISSUED BY: BWhite Consulting Ltd (Design Engineer: Bevan White)	
TO BE SUPPLIED TO: Invercargill District Council IN RESPECT OF: Proposed NEW Farm Shed	
AT: 557 West Plains Road, Invercargill, New Zealand	
LEGAL DES CRIPTION	
We have been engaged by <b>Ezequote Pty Ltd</b> to provide <b>Specific Structural Engineering Design</b> se requirements of Clause(s) <b>B1</b> of the Building Code for part only (as specified in the attachment to the building work.	-
☐ ALL	connections
The design has been prepared in accordance with compliance documents to NZ Building Code issue Innovation & Employment Clauses <b>B1/VM1</b> and <b>B1/VM4</b>	ed by Ministry of Business,
The proposed building work covered by the producer statement is described on <b>Ezequote</b> drawings A101 - A111 Rev-02 dated 05/12/2024 together with the following specification, and other documen attached to this statement: <b>Design Featured Report Dated 06/12/2024 and numbered "Second Page</b> "	nts set out in the schedule
On behalf of BWhite Consulting Ltd, and subject to:	
<ol> <li>Site verification of the following design assumptions: an Ultimate foundation bearing pressure with NZS3604:2011</li> <li>The building has a design life of 50 years and am Importance Level 1</li> <li>Unless specifically noted, compliance of the drawings to None-Specific codes such as NZS3 been checked by this practice</li> <li>This Certificate does not cover any other building code clause including weather tightness</li> <li>Inspections of the building to be completed by Invercargill District Council. As BWhite Coundertaking inspections, we cannot issue a producer Statement-PS4- Construction Review</li> </ol>	604 and NZS4229 have not
6. This Producer Statement- Design is valid for a building consent issued within 1 year from 7. All proprietary products meeting their performance specification requirements	
I believe on reasonable grounds that a) the building, if constructed in accordance with the drawings documents provided or listed in the attached schedule, will comply with the relevant provisions of the presons who have undertaken the design have the necessary competency to do so. I also reconstruction monitoring/observation:	he Building Code and that b),
☑ CM1 ☐ CM2 ☐ CM3 ☐ CM4 ☐ CM5 or as per agreement with owner/developer (stated above	e)
I, <b>Bevan White</b> am CPEng <b>108276</b> I am Member of Engineering New Zealand and hold the following holds a current policy of Professional Indemnity Insurance no less than \$200,000	qualification: BECivil and
Signed by Bevan White on behalf of BWhite Consulting Ltd Dated: 06/12/2024	
Email: bwhitecpeng@gmail.com Phone: 0211-979786	

Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement accrues to the Design Firm only. The total maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work, whether in contract, tort or otherwise(including negligence), is limited to the sum of \$200,000.

This form is to accompany Form 2 of the Building (Forms) Regulations 2004 for the application of a Building Consent

Date: 06/12/2024

BWhite

Consulting Ltd

Bell Block New Plymouth 4312

New Zealand File No:

# DESIGN FEATURES SUMMARY FOR PROPOSED NEW FARM SHED 557 WEST PLAINS ROAD, INVERCARGILL, NEW ZEAL AND

#### Site Specific Loads

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & EQ ARI	100 Years	Max Height	4 m
Wind Region	NZ4	Terrain Category	2.04	Design Wind Speed	42.62 m/s
Wind Pressure	1.09 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years

#### Timber

Sawn Timber to be graded to the properties of SG6 and SG8 or better as mentioned on plans, with moisture content of 18% or less for dry and 25% or less for wet.

The following standards have been used in the design of this structure

- NZS 3603:1993 Timber Structures Standard
- NZS 3604:2011 Timber Framed Buildings. Standards New Zealand, 2011
- NZS 3404:1997 Steel Structures
- AS/NZS 1170 2003 Structural Design Actions
- AS/NZS 1170.2 2021 Structural Design Actions-Wind Action
- Branz. "Engineering Basis of NZS 3604". April 2013

Yours Faithfully

**BWhite CONSULTING LTD** 

### **Bevan White**

Director | BE Civil . CMengNZ CPEng

Email: bwhitecpeng@gmail.com Contact: 0211 979 786

Job No.: EHB 294 Address: 557 West Plains Road, Invercargill, New Date: 06/12/2024

Zealand

# **General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4 m
Wind Region	NZ4	Terrain Category	2.04	Design Wind Speed	42.62 m/s
Wind Pressure	1.09 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

# **Pressure Coefficients and Pressues**

Shed Type = Mono Open

For roof Cp, i = 0.6472

For roof CP,e from 0 m To 3.7 m Cpe = -0.9 pe = -0.49 KPa pnet = -0.91 KPa

For roof CP,e from 3.7 m To 7.4 m Cpe = -0.5 pe = -0.27 KPa pnet = -0.69 KPa

For wall Windward Cp, i = 0.6472 side Wall Cp, i = -0.552

For wall Windward and Leeward CP,e from 0 m To 9.6 m Cpe = 0.7 pe = 0.69 KPa pnet = 1.27 KPa

For side wall CP,e from 0 m To 3.7 m Cpe = pe = -0.64 KPa pnet = -0.06 KPa

Maximum Upward pressure used in roof member Design = 0.91 KPa

Maximum Downward pressure used in roof member Design = 0.77 KPa

Maximum Wall pressure used in Design = 1.27 KPa

Maximum Racking pressure used in Design = 1.18 KPa

# **Design Summary**

# **Intermediate Design Sides**

Intermediate Spacing = 2400 mm Intermediate Span = 3700 mm Try Intermediate 2x200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 1.00 S1 Downward = 11.27 S1 Upward = 0.72

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

$M_{Wind+Snow}$	2.61 Kn-m	Capacity	7.46 Kn-m	Passing Percentage	285.82 %
$ m V_{0.9D ext{-}WnUp}$	2.82 Kn	Capacity	32.16 Kn	Passing Percentage	1140.43 %

#### **Deflections**

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 35.295 mm Limit by Woolcock et al, 1999 Span/100 = 37.00 mm

#### Reactions

Maximum = 2.82 kn

# **Girt Design Front and Back**

Girt's Spacing = 700 mm Girt's Span = 2400 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward =0.75 S1 Downward =11.27 S1 Upward =18.41

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

# Capacity Checks

$M_{Wind+Snow}$	0.64 Kn-m	Capacity	2.79 Kn-m	Passing Percentage	435.94 %
$V_{0.9D\text{-W}nUp}$	1.07 Kn	Capacity	16.08 Kn	Passing Percentage	1502.80 %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 2.57 mm Limit by Woolcock et al, 1999 Span/100 = 24.00 mm Sag during installation = 2.01 mm

#### Reactions

Maximum = 1.07 kn

# **Girt Design Sides**

Girt's Spacing = 1300 mm

Girt's Span = 2400 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1

K4 = 1

K5 = 1

K8 Downward =1.00

K8 Upward = 0.75

S1 Downward =11.27

S1 Upward = 18.41

Shear Capacity of timber = 3 MPa

Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

# Capacity Checks

 $M_{Wind+Snow}$ 

1.19 Kn-m

Capacity

2.79 Kn-m

Passing Percentage

234.45 %

 $V_{0.9D\text{-W}nUp}$ 

1.98 Kn

Capacity

16.08 Kn

Passing Percentage

812.12 %

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 4.78 mm Limit by Woolcock et al. 1999 Span/100 = 24.00 mm Sag during installation = 2.01 mm

#### Reactions

Maximum = 1.98 kn

# **Uplift Check**

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 22.07 Kn

Uplift on one Pile = 15.78 Kn

Uplift is ok