



**Job No.:** 240501**Address:** 30 Sam John Place,, Lake Hawea, New Zealand**Date:** 22/05/2024**Latitude:** -44.615641**Longitude:** 169.274377**Elevation:** 352 m**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N5	Ground Snow Load	0.99 KPa	Roof Snow Load	0.7 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.6 m
Wind Region	NZ2	Terrain Category	3.0	Design Wind Speed	34.86 m/s
Wind Pressure	0.73 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	Medium	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

**Pressure Coefficients and Pressures**

Shed Type = Mono Enclosed

For roof  $C_{p,i} = -0.3$

For roof  $C_{p,e}$  from 0 m To 1.65 m  $C_{p,e} = -0.94$   $p_e = -0.62$  KPa  $p_{net} = -0.62$  KPa

For roof  $C_{p,e}$  from 1.65 m To 3.30 m  $C_{p,e} = -0.88$   $p_e = -0.58$  KPa  $p_{net} = -0.58$  KPa

For wall Windward  $C_{p,i} = -0.3$  side Wall  $C_{p,i} = -0.3$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 6 m  $C_{p,e} = 0.7$   $p_e = 0.46$  KPa  $p_{net} = 0.68$  KPa

For side wall  $C_{p,e}$  from 0 m To 3.30 m  $C_{p,e} =$   $p_e = -0.43$  KPa  $p_{net} = -0.43$  KPa

Maximum Upward pressure used in roof member Design = 0.62 KPa

Maximum Downward pressure used in roof member Design = 0.20 KPa

Maximum Wall pressure used in Design = 0.68 KPa

Maximum Racking pressure used in Design = 0.40 KPa

**Design Summary****Purlin Design**

Purlin Spacing = 900 mm

Purlin Span = 5850 mm

Try Purlin 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 0.28 S1 Downward = 12.68 S1 Upward = 32.18

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

$M_{1.35D}$	1.3 Kn-m	Capacity	3.40 Kn-m	Passing Percentage	<b>261.54 %</b>
$M_{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}$	3.85 Kn-m	Capacity	4.53 Kn-m	Passing Percentage	<b>117.66 %</b>
$M_{0.9D-W_nUp}$	-1.52 Kn-m	Capacity	-1.65 Kn-m	Passing Percentage	<b>177.42 %</b>
$V_{1.35D}$	0.89 Kn	Capacity	12.06 Kn	Passing Percentage	<b>1355.06 %</b>

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V <sub>1.2D+1.5L 1.2D+Sn 1.2D+WnDn</sub>	2.63 Kn	Capacity	16.08 Kn	Passing Percentage	<b>611.41 %</b>
V <sub>0.9D-WnUp</sub>	-1.04 Kn	Capacity	-20.10 Kn	Passing Percentage	<b>1932.69 %</b>

**Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = 18.24 mm Limit by Woolcock et al, 1999 Span/240 = 24.17 mm

Deflection under Dead and Service Wind = 18.24 mm Limit by Woolcock et al, 1999 Span/100 = 58.00 mm

**Reactions**

Maximum downward = 2.63 kn Maximum upward = -1.04 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

**Rafter Design External**

External Rafter Load Width = 3000 mm External Rafter Span = 5830 mm Try Rafter 300x45 LVL11

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K<sub>1</sub> Short term = 1 K<sub>1</sub> Medium term = 0.8 K<sub>1</sub> Long term = 0.6 K<sub>4</sub> = 1 K<sub>5</sub> = 1 K<sub>8</sub> Downward = 0.88

K<sub>8</sub> Upward = 0.88 S<sub>1</sub> Downward = 15.50 S<sub>1</sub> Upward = 15.50

Shear Capacity of timber = 5 MPa Bending Capacity of timber = 38 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>1.35D</sub>	4.30 Kn-m	Capacity	10.84 Kn-m	Passing Percentage	<b>252.09 %</b>
M <sub>1.2D+1.5L 1.2D+Sn 1.2D+WnDn</sub>	12.75 Kn-m	Capacity	14.45 Kn-m	Passing Percentage	<b>113.33 %</b>
M <sub>0.9D-WnUp</sub>	-5.03 Kn-m	Capacity	-18.07 Kn-m	Passing Percentage	<b>359.24 %</b>
V <sub>1.35D</sub>	2.95 Kn	Capacity	21.71 Kn	Passing Percentage	<b>735.93 %</b>
V <sub>1.2D+1.5L 1.2D+Sn 1.2D+WnDn</sub>	8.74 Kn	Capacity	28.94 Kn	Passing Percentage	<b>331.12 %</b>
V <sub>0.9D-WnUp</sub>	-3.45 Kn	Capacity	-36.18 Kn	Passing Percentage	<b>1048.70 %</b>

**Deflections**

Modulus of Elasticity = 9900 MPa NZS3603 Amt 4, Table 2.3

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = 15.15 mm Limit by Woolcock et al, 1999 Span/240 = 25.00 mm

Deflection under Dead and Service Wind = 15.15 mm Limit by Woolcock et al, 1999 Span/100 = 60.00 mm

**Reactions**

Maximum downward = 8.74 kn Maximum upward = -3.45 kn

**Rafter to Pole Connection check**

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J2 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 12.6 \text{ f}_{pj} = 22.7 \text{ Mpa}$  for Rafter with effective thickness = 45 mm

For Parallel to grain loading

$K_{11} = 2.0 \text{ f}_{cj} = 36.1 \text{ Mpa}$  for Pole with effective thickness = 100 mm

Eccentric Load check

$V = \phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s \dots\dots\dots (\text{Eq 4.12}) = -37.80 \text{ kn} > -3.45 \text{ Kn}$

Single Shear Capacity under short term loads = -14.56 Kn > -3.45 Kn

### Girt Design Front and Back

Girt's Spacing = 0 mm

Girt's Span = 3000 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

$K_1$  Short term = 1     $K_4 = 1$      $K_5 = 1$      $K_8$  Downward = NaN

$K_8$  Upward = NaN     $S_1$  Downward = NaN     $S_1$  Upward = NaN

Shear Capacity of timber = 3 MPa    Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

$M_{\text{Wind+Snow}}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

### Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm

Limit by Woolcock et al, 1999 Span/100 = 30.00 mm

Sag during installation = NaN mm

### Reactions

Maximum = 0.00 kn

### Girt Design Sides

Girt's Spacing = 0 mm

Girt's Span = 3000 mm

Try Girt SG8 Dry

Moisture Condition = Wet (Moisture in timber is less than 18% and timber does not remain in continuous wet condition after installation)

$K_1$  Short term = 1     $K_4 = 1$      $K_5 = 1$      $K_8$  Downward = NaN

$K_8$  Upward = NaN     $S_1$  Downward = NaN     $S_1$  Upward = NaN

Shear Capacity of timber = 3 MPa    Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

$M_{\text{Wind+Snow}}$	0.00 Kn-m	Capacity	NaN Kn-m	Passing Percentage	NaN %
$V_{0.9D-WnUp}$	0.00 Kn	Capacity	0.00 Kn	Passing Percentage	NaN %

## Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = NaN mm

Limit by Woolcock et al. 1999 Span/100 = 30.00 mm

Sag during installation = NaN mm

## Reactions

Maximum = 0.00 kn

## End Pole Design

### Geometry For End Bay Pole

#### Geometry

150 SED H5 (Minimum 175 dia. at Floor Level)	Dry Use	Height	3400 mm
Area	20729 mm <sup>2</sup>	As	15546.6796875 mm <sup>2</sup>
Ix	34210793 mm <sup>4</sup>	Zx	421056 mm <sup>3</sup>
Iy	34210793 mm <sup>4</sup>	Zx	421056 mm <sup>3</sup>
Lateral Restraint	mm c/c		

## Loads

Total Area over Pole = 18 m<sup>2</sup>

Dead	4.50 Kn	Live	4.50 Kn
Wind Down	3.60 Kn	Snow	12.60 Kn
Moment Wind	2.91 Kn-m	Moment snow	2.67 Kn-m
Phi	0.8	K8	0.63
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

## Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

## Capacities

PhiNcx Wind	186.72 Kn	PhiMnx Wind	7.65 Kn-m	PhiVnx Wind	36.81 Kn
PhiNcx Dead	112.03 Kn	PhiMnx Dead	4.59 Kn-m	PhiVnx Dead	22.09 Kn
PhiNcx Snow	149.38 Kn	PhiMnx Snow	6.12 Kn-m	PhiVnx Snow	29.45 Kn

## Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.57 < 1$  OK

$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.32 < 1$  OK

Deflection at top under service lateral loads = 16.68 mm < 35.91 mm

Ds = 0.6 mm      Pole Diameter

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L =	1300 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Total Area over Pole = 18 m<sup>2</sup>

Moment Wind =	2.91 Kn-m	Moment Snow =	2.67 Kn-m
Shear Wind =	1.08 Kn	Shear Snow =	2.67 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	4.89 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	7.84 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = 0.54 < 1 OK

**Drained Lateral Strength of End pile in cohesionless soils Free Head short pile**

**Assumed Soil Properties**

Gamma	18 Kn/m <sup>3</sup>	Friction angle	30 deg	Cohesion	0 Kn/m <sup>3</sup>
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

**Geometry For End Bay Pole**

Ds =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Moment Wind =	2.91 Kn-m	Moment Snow =	2.67 Kn-m
Shear Wind =	1.08 Kn	Shear Snow =	2.67 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	4.89 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	7.84 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = 0.54 < 1 OK

**Uplift Check**

Density of Concrete = 24 Kn/m<sup>3</sup>

Density of Timber Pole = 5 Kn/m<sup>3</sup>

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Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

$K_s$  (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (1300) x  $K_s$  (1.5) x 0.5 x  $\tan(30)$  x  $\pi$  x Dia of Pile (0.6) x Height of Pile (1300)

Skin Friction = 13.65 Kn

Weight of Pile + Pile Skin Friction = 17.91 Kn

Uplift on one Pile = 7.11 Kn

Uplift is ok