

Pole Shed App Ver 01 2022

Job No.: Michael Keogh **Address:** 81 Great North Road, Kamo, New Zealand **Date:** 10/31/2023
Latitude: -35.665913 **Longitude:** 174.296446 **Elevation:** 98 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.8 m
Wind Region	NZ1	Terrain Category	2.0	Design Wind Speed	38.22 m/s
Wind Pressure	0.88 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 2.14 m $C_{p,e} = -0.9886$ $p_e = -0.78$ KPa $p_{net} = -0.78$ KPa

For roof $C_{p,e}$ from 2.14 m To 4.28 m $C_{p,e} = -0.8557$ $p_e = -0.67$ KPa $p_{net} = -0.67$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 7 m $C_{p,e} = 0.7$ $p_e = 0.55$ KPa $p_{net} = 0.81$ KPa

For side wall $C_{p,e}$ from 0 m To 4.28 m $C_{p,e} =$ $p_e = -0.51$ KPa $p_{net} = -0.51$ KPa

Maximum Upward pressure used in roof member Design = 0.78 KPa

Maximum Downward pressure used in roof member Design = 0.33 KPa

Maximum Wall pressure used in Design = 0.81 KPa

Maximum Racking pressure used in Design = 0.94 KPa

Design Summary

Girt Design Front and Back

Girt's Spacing = 900 mm

Girt's Span = 4000 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet

condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.50 S1 Downward =11.27 S1 Upward =23.76

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.46 Kn-m	Capacity	1.87 Kn-m	Passing Percentage	128.08 %
V _{0.9D-WnUp}	1.46 Kn-m	Capacity	16.08 Kn-m	Passing Percentage	1101.37 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 10.88 mm Limit by Woolcock et al, 1999 Span/100 = 40.00 mm
Sag during installation = 15.52 mm

Reactions

Maximum = 1.46 kn

Girt Design Sides

Girt's Spacing = 700 mm Girt's Span = 7000 mm Try Girt 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =0.97

K8 Upward =0.65 S1 Downward =12.68 S1 Upward =20.41

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	3.47 Kn-m	Capacity	3.79 Kn-m	Passing Percentage	109.22 %
V _{0.9D-WnUp}	1.98 Kn-m	Capacity	20.10 Kn-m	Passing Percentage	1015.15 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 40.64 mm Limit by Woolcock et al. 1999 Span/100 = 70.00 mm

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Sag during installation = 145.58 mm

Reactions

Maximum = 1.98 kn

Middle Pole Design

Geometry

200x200 SG8 Dry	Dry Use	Height	4560 mm
Area	40000 mm ²	As	30000 mm ²
Ix	133333333 mm ⁴	Zx	1333333 mm ³
Iy	133333333 mm ⁴	Zy	1333333 mm ³
Lateral Restraint	4560 mm c/c		

Loads

Total Area over Pole = 14 m²

Dead	3.50 Kn	Live	3.50 Kn
Wind Down	4.62 Kn	Snow	0.00 Kn
Moment wind	16.20 Kn-m		
Phi	0.8	K8	0.54
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Shaving	Steaming	Normal	Dry Use
fb =	14 MPa	fs =	3 MPa
fc =	18 MPa	fp =	8.9 MPa
ft =	6 MPa	E =	8000 MPa

Capacities

PhiNcx Wind	311.23 Kn	PhiMnx Wind	8.07 Kn-m	PhiVnx Wind	72.00 Kn
PhiNcx Dead	186.74 Kn	PhiMnx Dead	4.84 Kn-m	PhiVnx Dead	43.20 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 2.05 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 4.07 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 46.72 mm < 45.60 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma 18 Kn/m³ Friction angle 30 deg Cohesion 0 Kn/m³
K₀ = $(1 - \sin(30)) / (1 + \sin(30))$
K_p = $(1 + \sin(30)) / (1 - \sin(30))$

Geometry For Middle Bay Pole

D_s = 0.6 mm Pile Diameter
L = 1300 mm Pile embedment length
f₁ = 3600 mm Distance at which the shear force is applied
f₂ = 0 mm Distance of top soil at rest pressure

Loads

Moment Wind = 16.20 Kn-m
Shear Wind = 4.50 Kn

Pile Properties

Safety Factory 0.55
H_u = 3.99 Kn Ultimate Lateral Strength of the Pile, Short pile
M_u = 8.33 Kn-m Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 1.94 < 1 OK

End Pole Design

Geometry For End Bay Pole

Geometry

175x175 SG8 Dry	Dry Use	Height	4560 mm
Area	30625 mm ²	A _s	22968.75 mm ²
I _x	78157552 mm ⁴	Z _x	893229 mm ³
I _y	78157552 mm ⁴	Z _y	893229 mm ³
Lateral Restraint	mm c/c		

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Loads

Total Area over Pole = 14 m²

Dead	3.50 Kn	Live	3.50 Kn
Wind Down	4.62 Kn	Snow	0.00 Kn
Moment Wind	8.10 Kn-m		
Phi	0.8	K8	0.43
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

Material

Shaving	Steaming	Normal	Dry Use
fb =	14 MPa	fs =	3 MPa
fc =	18 MPa	fp =	8.9 MPa
ft =	6 MPa	E =	8000 MPa

Capacities

PhiNcx Wind	187.93 Kn	PhiMnx Wind	4.26 Kn-m	PhiVnx Wind	55.13 Kn
PhiNcx Dead	112.76 Kn	PhiMnx Dead	2.56 Kn-m	PhiVnx Dead	33.08 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 1.96 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 3.67 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 41.84 \text{ mm} < 47.88 \text{ mm}$$

Ds =	0.6 mm	Pile Diameter
L =	1300 mm	Pile embedment length
f1 =	3600 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Total Area over Pole = 14 m²

Moment Wind =	8.10 Kn-m
Shear Wind =	2.25 Kn

Pile Properties

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Safety Factor	0.55	
$H_u =$	3.99 Kn	Ultimate Lateral Strength of the Pile, Short pile
$M_u =$	8.33 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.97 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
$K_0 =$	$(1 - \sin(30)) / (1 + \sin(30))$				
$K_p =$	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For End Bay Pole

$D_s =$	0.6 mm	Pile Diameter
$L =$	1300 mm	Pile embedment length
$f_1 =$	3600 mm	Distance at which the shear force is applied
$f_2 =$	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	8.10 Kn-m
Shear Wind =	2.25 Kn

Pile Properties

Safety Factor	0.55	
$H_u =$	3.99 Kn	Ultimate Lateral Strength of the Pile, Short pile
$M_u =$	8.33 Kn-m	Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.97 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

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Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K_s (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1300) x K_s (1.5) x $0.5 \times \tan(30)$ x π x Dia of Pile(0.6) x Height of Pile(1300)

Skin Friction = 13.65 Kn

Weight of Pile + Pile Skin Friction = 17.23 Kn

Uplift on one Pile = 7.77 Kn

Uplift is ok