

Pole Shed App Ver 01 2022

**Job No.:** N & I Service - 1      **Address:** 504 Cissy Bay Road, Cissy Bay,  
Marlborough Sounds, New Zealand      **Date:** 9/14/2023  
**Latitude:** -40.989404      **Longitude:** 173.823865      **Elevation:** 16.5 m

**General Input**

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	D
Importance Level	2	Ultimate wind & Earthquake ARI	500 Years	Max Height	4.2 m
Wind Region	NZ3	Terrain Category	1.0	Design Wind Speed	49.54 m/s
Wind Pressure	1.47 KPa	Lee Zone	NO	Ultimate Snow ARI	150 Years
Wind Category	Very High	Earthquake ARI	500		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

**Pressure Coefficients and Pressures**

Shed Type = Mono Enclosed

For roof  $C_{p,i} = -0.3$

For roof  $C_{p,e}$  from 0 m To 3.70 m  $C_{p,e} = -0.9$   $p_e = -1.19$  KPa  $p_{net} = -1.19$  KPa

For roof  $C_{p,e}$  from 3.7 m To 7.40 m  $C_{p,e} = -0.5$   $p_e = -0.66$  KPa  $p_{net} = -0.66$  KPa

For wall Windward  $C_{p,i} = -0.3$  side Wall  $C_{p,i} = -0.3$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 10.2 m  $C_{p,e} = 0.7$   $p_e = 0.93$  KPa  $p_{net} = 1.37$  KPa

For side wall  $C_{p,e}$  from 0 m To 3.70 m  $C_{p,e} =$   $p_e = -0.86$  KPa  $p_{net} = -0.86$  KPa

Maximum Upward pressure used in roof member Design = 1.19 KPa

Maximum Downward pressure used in roof member Design = 0.57 KPa

Maximum Wall pressure used in Design = 1.37 KPa

Maximum Racking pressure used in Design = 1.46 KPa

**Design Summary**

**Girt Design Front and Back**

Girt's Spacing = 900 mm      Girt's Span = 2025 mm      Try Girt 150x50 SG8 Dry

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Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =0.92    S1 Downward =9.63    S1 Upward =14.45

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

M <sub>Wind+Snow</sub>	0.63 Kn-m	Capacity	1.93 Kn-m	Passing Percentage	<b>306.35 %</b>
V <sub>0.9D-WnUp</sub>	1.25 Kn-m	Capacity	12.06 Kn-m	Passing Percentage	<b>964.80 %</b>

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 2.87 mm    Limit by Woolcock et al, 1999 Span/250 = 8.10 mm

Sag during installation = 1.02 mm

#### **Reactions**

Maximum = 1.25 kn

#### **Girt Design Sides**

Girt's Spacing = 900 mm                      Girt's Span = 2250 mm                      Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =0.89    S1 Downward =9.63    S1 Upward =15.23

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

#### **Capacity Checks**

M <sub>Wind+Snow</sub>	0.78 Kn-m	Capacity	1.87 Kn-m	Passing Percentage	<b>239.74 %</b>
V <sub>0.9D-WnUp</sub>	1.39 Kn-m	Capacity	12.06 Kn-m	Passing Percentage	<b>867.63 %</b>

#### **Deflections**

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 4.37 mm    Limit by Woolcock et al. 1999 Span/100 = 9.00 mm

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Sag during installation = 1.55 mm

### Reactions

Maximum = 1.39 kn

### Middle Pole Design

#### Geometry

225 SED H5 (Minimum 250 dia. at Floor Level)	Dry Use	Height	3900 mm
Area	44279 mm <sup>2</sup>	As	33209.1796875 mm <sup>2</sup>
Ix	156100441 mm <sup>4</sup>	Zx	1314530 mm <sup>3</sup>
Iy	156100441 mm <sup>4</sup>	Zx	1314530 mm <sup>3</sup>
Lateral Restraint	3900 mm c/c		

#### Loads

Total Area over Pole = 18.225 m<sup>2</sup>

Dead	4.56 Kn	Live	4.56 Kn
Wind Down	10.39 Kn	Snow	0.00 Kn
Moment wind	13.01 Kn-m		
Phi	0.8	K8	0.84
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

#### Material

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

#### Capacities

PhiNcx Wind	536.44 Kn	PhiMnx Wind	32.12 Kn-m	PhiVnx Wind	78.64 Kn
PhiNcx Dead	321.86 Kn	PhiMnx Dead	19.27 Kn-m	PhiVnx Dead	47.18 Kn

#### Checks

$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.44 < 1$  OK

$$(M_x/\phi M_{nx})^2 + (N/\phi N_{cx}) = 0.20 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 20.71 mm < 26.00 mm

## **Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile**

### **Assumed Soil Properties**

Gamma 18 Kn/m<sup>3</sup> Friction angle 30 deg Cohesion 0 Kn/m<sup>3</sup>  
K<sub>0</sub> =  $(1 - \sin(30)) / (1 + \sin(30))$   
K<sub>p</sub> =  $(1 + \sin(30)) / (1 - \sin(30))$

### **Geometry For Middle Bay Pole**

D<sub>s</sub> = 0.6 mm Pile Diameter  
L = 1550 mm Pile embedment length  
f<sub>1</sub> = 3150 mm Distance at which the shear force is applied  
f<sub>2</sub> = 0 mm Distance of top soil at rest pressure

### **Loads**

Moment Wind = 13.01 Kn-m  
Shear Wind = 4.13 Kn

### **Pile Properties**

Safety Factory 0.55  
H<sub>u</sub> = 7.06 Kn Ultimate Lateral Strength of the Pile, Short pile  
M<sub>u</sub> = 13.22 Kn-m Ultimate Moment Capacity of Pile

### **Checks**

Applied Forces/Capacities = 0.98 < 1 OK

## **End Pole Design**

### **Geometry For End Bay Pole**

#### **Geometry**

200 SED H5 (Minimum 225 dia. at Floor Level)	Dry Use	Height	4050 mm
Area	35448 mm <sup>2</sup>	A <sub>s</sub>	26585.7421875 mm <sup>2</sup>
I <sub>x</sub>	100042702 mm <sup>4</sup>	Z <sub>x</sub>	941578 mm <sup>3</sup>
I <sub>y</sub>	100042702 mm <sup>4</sup>	Z <sub>y</sub>	941578 mm <sup>3</sup>

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Lateral Restraint

mm c/c

**Loads**

Total Area over Pole = 9.1125 m<sup>2</sup>

Dead	2.28 Kn	Live	2.28 Kn
Wind Down	5.19 Kn	Snow	0.00 Kn
Moment Wind	6.50 Kn-m		
Phi	0.8	K8	0.72
K1 snow	0.8	K1 Dead	0.6
K1 wind	1		

**Material**

Peeling	Steaming	Normal	Dry Use
fb =	36.3 MPa	fs =	2.96 MPa
fc =	18 MPa	fp =	7.2 MPa
ft =	22 MPa	E =	9257 MPa

**Capacities**

PhiNcx Wind	365.76 Kn	PhiMnx Wind	19.59 Kn-m	PhiVnx Wind	62.96 Kn
PhiNcx Dead	219.46 Kn	PhiMnx Dead	11.76 Kn-m	PhiVnx Dead	37.77 Kn

**Checks**

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.36 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.14 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 17.36 mm < 27.93 mm

Ds =	0.6 mm	Pile Diameter
L =	1550 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Total Area over Pole = 9.1125 m<sup>2</sup>

Moment Wind =	6.50 Kn-m
Shear Wind =	2.06 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	7.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	13.22 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = 0.49 < 1 OK

**Drained Lateral Strength of End pile in cohesionless soils Free Head short pile**

**Assumed Soil Properties**

Gamma	18 Kn/m3	Friction angle	30 deg	Cohesion	0 Kn/m3
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

**Geometry For End Bay Pole**

Ds =	0.6 mm	Pile Diameter
L =	1550 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Moment Wind =	6.50 Kn-m
Shear Wind =	2.06 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	7.06 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	13.22 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = 0.49 < 1 OK

**Uplift Check**

Density of Concrete = 24 Kn/m3

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Density of Timber Pole = 5 Kn/m<sup>3</sup>

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1550) x Ks(1.5) x  $0.5 \times \tan(30)$  x  $\pi$  x Dia of Pile(0.6) x Height of Pile(1550)

Skin Friction = 19.40 Kn

Weight of Pile + Pile Skin Friction = 22.96 Kn

Uplift on one Pile = 17.59 Kn

Uplift is ok