

Job No.: 2401016

Address: Thorpe Orinoco Road, Tasman, New Zealand

Date: 21/02/2024

Latitude: -41.251821

Longitude: 172.881289

Elevation: 196.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N3	Ground Snow Load	0.14 KPa	Roof Snow Load	0.1 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4 m
Wind Region	NZ2	Terrain Category	3.0	Design Wind Speed	55.84 m/s
Wind Pressure	1.87 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	extra High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Open

For roof $C_{p,i} = -0.6027$

For roof $C_{p,e}$ from 0 m To 8 m $C_{p,e} = -0.434$ $p_e = -0.54$ KPa $p_{net} = -1.20$ KPa

For roof $C_{p,e}$ from m To m $C_{p,e} =$ $p_e =$ KPa $p_{net} =$ KPa

For wall Windward $C_{p,i} = 0.4722$ side Wall $C_{p,i} = -0.6027$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 9 m $C_{p,e} = 0.7$ $p_e = 1.18$ KPa $p_{net} = 2.19$ KPa

For side wall $C_{p,e}$ from 0 m To 3.25 m $C_{p,e} =$ $p_e = -1.09$ KPa $p_{net} = -0.08$ KPa

Maximum Upward pressure used in roof member Design = 1.20 KPa

Maximum Downward pressure used in roof member Design = 1.18 KPa

Maximum Wall pressure used in Design = 2.19 KPa

Maximum Racking pressure used in Design = 1.69 KPa

Design Summary

Purlin Design

Purlin Spacing = 650 mm

Purlin Span = 5850 mm

Try Purlin 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 0.54 S1 Downward = 12.68 S1 Upward = 22.76

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	0.94 Kn-m	Capacity	3.40 Kn-m	Passing Percentage	361.70 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	4.12 Kn-m	Capacity	4.53 Kn-m	Passing Percentage	109.95 %
M _{0.9D-W_nUp}	-2.71 Kn-m	Capacity	-3.16 Kn-m	Passing Percentage	355.06 %

Pole Shed App Ver 01 2022

V _{1.35D}	0.64 Kn	Capacity	12.06 Kn	Passing Percentage	1884.38 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	2.81 Kn	Capacity	16.08 Kn	Passing Percentage	572.24 %
V _{0.9D-W_nUp}	-1.85 Kn	Capacity	-20.10 Kn	Passing Percentage	1086.49 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 13.17 mm

Limit by Woolcock et al, 1999 Span/240 = 24.17 mm

Deflection under Dead and Service Wind = 23.93 mm

Limit by Woolcock et al, 1999 Span/100 = 58.00 mm

Reactions

Maximum downward = 2.81 kn Maximum upward = -1.85 kn

Number of Blocking = 1 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4500 mm

Internal Rafter Span = 3850 mm

Try Rafter 2x300x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K₁ Short term = 1 K₁ Medium term = 0.8 K₁ Long term = 0.6 K₄ = 1 K₅ = 1 K₈ Downward = 1.00

K₈ Upward = 1.00 S₁ Downward = 6.81 S₁ Upward = 6.81

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	2.81 Kn-m	Capacity	10.08 Kn-m	Passing Percentage	358.72 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	12.34 Kn-m	Capacity	13.44 Kn-m	Passing Percentage	108.91 %
M _{0.9D-W_nUp}	-8.13 Kn-m	Capacity	-16.8 Kn-m	Passing Percentage	206.64 %
V _{1.35D}	2.92 Kn	Capacity	28.94 Kn	Passing Percentage	991.10 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	12.82 Kn	Capacity	38.6 Kn	Passing Percentage	301.09 %
V _{0.9D-W_nUp}	-8.45 Kn	Capacity	-48.24 Kn	Passing Percentage	570.89 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 3.335 mm

Limit by Woolcock et al, 1999 Span/240 = 16.67 mm

Deflection under Dead and Service Wind = 6.73 mm

Limit by Woolcock et al, 1999 Span/100 = 40.00 mm

Reactions

Maximum downward = 12.82 kn Maximum upward = -8.45 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 3

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Second page

Joint Group for Rafters = J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

$K_{11} = 14.9$ $f_{pj} = 12.9$ Mpa for Rafter with effective thickness = 100 mm

For Parallel to grain loading

$K_{11} = 2.0$ $f_{cj} = 36.1$ Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 32.51 Kn > -8.45 Kn

Girt Design Front and Back

Girt's Spacing = 600 mm

Girt's Span = 3000 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K_1 Short term = 1 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 1.00

K_8 Upward = 0.79 S_1 Downward = 9.63 S_1 Upward = 17.59

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.48 Kn-m	Capacity	1.65 Kn-m	Passing Percentage	111.49 %
$V_{0.9D-WnUp}$	1.97 Kn-m	Capacity	12.06 Kn-m	Passing Percentage	612.18 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 15.38 mm

Limit by Woolcock et al, 1999 Span/100 = 30.00 mm

Sag during installation = 4.91 mm

Reactions

Maximum = 1.97 kn

Girt Design Sides

Girt's Spacing = 900 mm

Girt's Span = 2000 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K_1 Short term = 1 $K_4 = 1$ $K_5 = 1$ K_8 Downward = 1.00

K_8 Upward = 0.92 S_1 Downward = 9.63 S_1 Upward = 14.36

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	0.99 Kn-m	Capacity	1.94 Kn-m	Passing Percentage	195.96 %
$V_{0.9D-WnUp}$	1.97 Kn-m	Capacity	12.06 Kn-m	Passing Percentage	612.18 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 4.56 mm

Limit by Woolcock et al. 1999 Span/100 = 20.00 mm

Sag during installation = 0.97 mm

Reactions

Maximum = 1.97 kn

Uplift Check

Density of Concrete = 24 Kn/m³

Density of Timber Pole = 5 Kn/m³

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (1650) x Ks (1.5) x 0.5 x tan(30) x π x Dia of Pile (0.6) x Height of Pile (1650)

Skin Friction = 21.99 Kn

Weight of Pile + Pile Skin Friction = 26.27 Kn

Uplift on one Pile = 17.55 Kn

Uplift is ok