

Job No.: wallace - 2
Latitude: -44.691873

Address: 90 Rattrays Rd, Waimate, New Zealand
Longitude: 171.06932

Date: 13/04/2024
Elevation: 65.5 m

General Input

| | | | | | |
|------------------|----------|--------------------------------|-----------|----------------------|-----------|
| Roof Live Load | 0.25 KPa | Roof Dead Load | 0.25 KPa | Roof Live Point Load | 1.1 Kn |
| Snow Zone | N4 | Ground Snow Load | 0.9 KPa | Roof Snow Load | 0.63 KPa |
| Earthquake Zone | 1 | Subsoil Category | D | Exposure Zone | B |
| Importance Level | 1 | Ultimate wind & Earthquake ARI | 100 Years | Max Height | 6 m |
| Wind Region | NZ2 | Terrain Category | 2.0 | Design Wind Speed | 41.79 m/s |
| Wind Pressure | 1.05 KPa | Lee Zone | NO | Ultimate Snow ARI | 50 Years |
| Wind Category | High | Earthquake ARI | 100 | | |

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Enclosed

For roof $C_{p,i} = -0.3$

For roof $C_{p,e}$ from 0 m To 5.35 m $C_{p,e} = -0.9$ $p_e = -0.85$ KPa $p_{net} = -0.85$ KPa

For roof $C_{p,e}$ from 5.35 m To 10.70 m $C_{p,e} = -0.5$ $p_e = -0.47$ KPa $p_{net} = -0.47$ KPa

For wall Windward $C_{p,i} = -0.3$ side Wall $C_{p,i} = -0.3$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 13.60 m $C_{p,e} = 0.7$ $p_e = 0.66$ KPa $p_{net} = 0.97$ KPa

For side wall $C_{p,e}$ from 0 m To 5.35 m $C_{p,e} =$ $p_e = -0.61$ KPa $p_{net} = -0.61$ KPa

Maximum Upward pressure used in roof member Design = 0.85 KPa

Maximum Downward pressure used in roof member Design = 0.40 KPa

Maximum Wall pressure used in Design = 0.97 KPa

Maximum Racking pressure used in Design = 1.13 KPa

Design Summary

Girt Design Front and Back

Girt's Spacing = 0 mm Girt's Span = 2800 mm Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 = 1 K5 = 1 K8 Downward = 1.00

K8 Upward = 0.68 S1 Downward = 11.27 S1 Upward = 19.88

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

| | | | | | |
|-----------------|-----------|----------|-----------|--------------------|------------|
| $M_{Wind+Snow}$ | 0.00 Kn-m | Capacity | 2.52 Kn-m | Passing Percentage | Infinity % |
| $V_{0.9D-WnUp}$ | 0.00 Kn | Capacity | 16.08 Kn | Passing Percentage | Infinity % |

Deflections

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Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 0.00 mm

Limit by Woolcock et al, 1999 Span/100 = 28.00 mm

Sag during installation = 3.73 mm

Reactions

Maximum = 0.00 kn

Girt Design Sides

Girt's Spacing = 0 mm

Girt's Span = 4533 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.77 S1 Downward =11.27 S1 Upward =17.89

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

| | | | | | |
|------------------------|-----------|----------|-----------|--------------------|------------|
| M _{Wind+Snow} | 0.00 Kn-m | Capacity | 2.89 Kn-m | Passing Percentage | Infinity % |
| V _{0.9D-WnUp} | 0.00 Kn | Capacity | 16.08 Kn | Passing Percentage | Infinity % |

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 0.00 mm

Limit by Woolcock et al. 1999 Span/100 = 45.33 mm

Sag during installation =25.61 mm

Reactions

Maximum = 0.00 kn

Middle Pole Design

Geometry

| | | | |
|--|---------------------------|----------------|-------------------------------|
| 275 SED H5 (Minimum 300 dia. at Floor Level) | Dry Use | Height | 5700 mm |
| Area | 64885 mm ² | As | 48663.8671875 mm ² |
| I _x | 335197731 mm ⁴ | Z _x | 2331810 mm ³ |
| I _y | 335197731 mm ⁴ | Z _y | 2331810 mm ³ |
| Lateral Restraint | 5700 mm c/c | | |

Loads

Total Area over Pole = 38.08 m²

| | | | |
|-------------|------------|-------------|-----------|
| Dead | 9.52 Kn | Live | 9.52 Kn |
| Wind Down | 15.23 Kn | Snow | 23.99 Kn |
| Moment wind | 28.40 Kn-m | Moment snow | 5.03 Kn-m |
| Phi | 0.8 | K8 | 0.68 |
| K1 snow | 0.8 | K1 Dead | 0.6 |
| K1 wind | 1 | | |

Material

| | | | |
|---------|----------|--------|----------|
| Peeling | Steaming | Normal | Dry Use |
| fb = | 36.3 MPa | fs = | 2.96 MPa |
| fc = | 18 MPa | fp = | 7.2 MPa |
| ft = | 22 MPa | E = | 9257 MPa |

Capacities

| | | | | | |
|-------------|-----------|-------------|------------|-------------|-----------|
| PhiNcx Wind | 633.98 Kn | PhiMnx Wind | 45.95 Kn-m | PhiVnx Wind | 115.24 Kn |
| PhiNcx Dead | 380.39 Kn | PhiMnx Dead | 27.57 Kn-m | PhiVnx Dead | 69.14 Kn |
| PhiNcx Snow | 507.19 Kn | PhiMnx Snow | 36.76 Kn-m | PhiVnx Snow | 92.19 Kn |

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.70 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.46 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 43.99 \text{ mm} < 57.00 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

| | | | | | |
|-------|-----------------------------------|----------------|--------|----------|---------|
| Gamma | 18 Kn/m3 | Friction angle | 30 deg | Cohesion | 0 Kn/m3 |
| K0 = | $(1 - \sin(30)) / (1 + \sin(30))$ | | | | |
| Kp = | $(1 + \sin(30)) / (1 - \sin(30))$ | | | | |

Geometry For Middle Bay Pole

| | | |
|------|---------|--|
| Ds = | 0.6 mm | Pile Diameter |
| L = | 2000 mm | Pile embedment length |
| f1 = | 4500 mm | Distance at which the shear force is applied |
| f2 = | 0 mm | Distance of top soil at rest pressure |

Loads

| | | | |
|---------------|------------|---------------|---------|
| Moment Wind = | 28.40 Kn-m | Moment Snow = | Kn-m |
| Shear Wind = | 6.31 Kn | Shear Snow = | 5.03 Kn |

Pile Properties

| | | |
|----------------|------------|---|
| Safety Factory | 0.55 | |
| Hu = | 10.97 Kn | Ultimate Lateral Strength of the Pile, Short pile |
| Mu = | 29.06 Kn-m | Ultimate Moment Capacity of Pile |

Checks

$$\text{Applied Forces/Capacities} = 0.98 < 1 \text{ OK}$$

Uplift Check

$$\text{Density of Concrete} = 24 \text{ Kn/m}^3$$

$$\text{Density of Timber Pole} = 5 \text{ Kn/m}^3$$

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Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K_s (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil (18) x Height of Pile (2000) x K_s (1.5) x 0.5 x $\tan(30)$ x π x Dia of Pile (0.6) x Height of Pile (2000)

Skin Friction = 32.31 Kn

Weight of Pile + Pile Skin Friction = 35.80 Kn

Uplift on one Pile = 23.80 Kn

Uplift is ok