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Job No.: Ensura Building Services-1   **Address:** 340 MT Wesley Road, Dargaville,New Zealand   **Date:** 09/05/2024

Latitude: -35.966901   **Longitude:** 173.835559   **Elevation:** 41 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	1	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.5 m
Wind Region	NZ1	Terrain Category	2.0	Design Wind Speed	40.38 m/s
Wind Pressure	0.98 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressues

Shed Type = Gable   Enclosed

For roof $C_{p,i}$ = -0.6177

For roof $C_{P,e}$ from 0 m To 4.25 m C_{pe} = -0.43   pe = -0.37 KPa   pnet = -0.82 KPa

For roof $C_{P,e}$ from 4.25 m To 8.50 m C_{pe} = -0.58   pe = -0.50 KPa   pnet = -0.95 KPa

For wall Windward $C_{p,i}$ = 0.4778   side Wall $C_{p,i}$ = -0.6177

For wall Windward and Leeward $C_{P,e}$ from 0 m To 20 m C_{pe} = 0.7   pe = 0.59 KPa   pnet = 1.17 KPa

For side wall $C_{P,e}$ from 0 m To 4.25 m C_{pe} =   pe = -0.55 KPa   pnet = 0.03 KPa

Maximum Upward pressure used in roof member Design = 0.82 KPa

Maximum Downward pressure used in roof member Design = 0.75 KPa

Maximum Wall pressure used in Design = 1.17 KPa

Maximum Racking pressure used in Design = 0.96 KPa

Design Summary

Rafter Design Internal

Internal Rafter Load Width = 5000 mm   Internal Rafter Span = 8350 mm   Try Rafter 2x360x63 LVL13

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K1 Medium term = 0.8   K1 Long term = 0.6   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =1.00   S1 Downward =5.90   S1 Upward =5.90

Shear Capacity of timber =5.3 MPa   Bending Capacity of timber =48 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	14.71 Kn-m	Capacity	60.82 Kn-m	Passing Percentage	**413.46 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	45.76 Kn-m	Capacity	81.1 Kn-m	Passing Percentage	**177.23 %**
$M_{0.9D-WnUp}$	-25.93 Kn-m	Capacity	-101.38 Kn-m	Passing Percentage	**390.98 %**
$V_{1.35D}$	7.05 Kn	Capacity	77.32 Kn	Passing Percentage	**1096.74 %**

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$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	21.92 Kn	Capacity	103.08 Kn	Passing Percentage	**470.26 %**
$V_{0.9D-WnUp}$	-12.42 Kn	Capacity	-128.86 Kn	Passing Percentage	**1037.52 %**

Deflections

Modulus of Elasticity = 11000 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 17.03 mm   Limit by Woolcock et al, 1999 Span/240 = 35.42 mm

Deflection under Dead and Service Wind = 27.59 mm   Limit by Woolcock et al, 1999 Span/100 = 85.00 mm

Reactions

Maximum downward =21.92 kn   Maximum upward = -12.42 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 3

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters =J2 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 12.6 fpj = 22.7 Mpa for Rafter with effective thickness = 126 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 43.67 Kn > -12.42 Kn

Rafter Design External

External Rafter Load Width = 2500 mm   External Rafter Span = 2786 mm   Try Rafter 290x45 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K1 Medium term = 0.8   K1 Long term = 0.6   K4 =1   K5 =1   K8 Downward =0.89

K8 Upward =0.89   S1 Downward =15.23   S1 Upward =15.23

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{1.35D}$	0.82 Kn-m	Capacity	3.78 Kn-m	Passing Percentage	**460.98 %**
$M_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	2.55 Kn-m	Capacity	5.04 Kn-m	Passing Percentage	**197.65 %**
$M_{0.9D-WnUp}$	-1.44 Kn-m	Capacity	-6.29 Kn-m	Passing Percentage	**436.81 %**
$V_{1.35D}$	1.18 Kn	Capacity	12.59 Kn	Passing Percentage	**1066.95 %**
$V_{1.2D+1.5L\ 1.2D+Sn\ 1.2D+WnDn}$	3.66 Kn	Capacity	16.79 Kn	Passing Percentage	**458.74 %**
$V_{0.9D-WnUp}$	-2.07 Kn	Capacity	-20.98 Kn	Passing Percentage	**1013.53 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 1.24 mm   Limit by Woolcock et al, 1999 Span/240= 11.73 mm

Deflection under Dead and Service Wind = 1.81 mm   Limit by Woolcock et al, 1999 Span/100 = 28.16 mm

Reactions

Maximum downward =3.66 kn   Maximum upward = -2.07 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 3

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters =J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 14.9 fpj = 12.9 Mpa for Rafter with effective thickness = 45 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

V = phi x k1 x k4 x k5 x fs x b x ds .... (Eq 4.12) = -21.73 kn > -2.07 Kn

Single Shear Capacity under short term loads = -14.63 Kn > -2.07 Kn

Intermediate Design Front and Back

Intermediate Spacing = 2500 mm   Intermediate Span = 1849 mm   Try Intermediate 2x140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =1.00   S1 Downward =10.36   S1 Upward =0.47

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.25 Kn-m	Capacity	3.3 Kn-m	Passing Percentage	**264.00 %**
$V_{0.9D-WnUp}$	2.70 Kn	Capacity	-20.26 Kn	Passing Percentage	**750.37 %**

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 4.005 mm   Limit byWoolcock et al, 1999 Span/100 = 18.49 mm

Reactions

Maximum = 2.70 kn

Girt Design Front and Back

Girt's Spacing = 1300 mm   Girt's Span = 2500 mm   Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.80   S1 Downward =10.36   S1 Upward =17.27

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.19 Kn-m	Capacity	1.32 Kn-m	Passing Percentage	**110.92 %**
$V_{0.9D-WnUp}$	1.90 Kn	Capacity	10.13 Kn	Passing Percentage	**533.16 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 11.22 mm   Limit by Woolcock et al, 1999 Span/100 = 25.00 mm
Sag during installation = 2.92 mm

Reactions

Maximum = 1.90 kn

Girt Design Sides

Girt's Spacing = 1300 mm   Girt's Span = 2816 mm   Try Girt 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1   K4 =1   K5 =1   K8 Downward =1.00

K8 Upward =0.96   S1 Downward =10.36   S1 Upward =12.96

Shear Capacity of timber =3 MPa   Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

$M_{Wind+Snow}$	1.51 Kn-m	Capacity	1.59 Kn-m	Passing Percentage	**105.30 %**
$V_{0.9D-WnUp}$	2.14 Kn	Capacity	10.13 Kn	Passing Percentage	**473.36 %**

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 18.05 mm   Limit by Woolcock et al. 1999 Span/100 = 28.16 mm
Sag during installation =4.70 mm

Reactions

Maximum = 2.14 kn

Middle Pole Design

Geometry

200 SED H5 (Minimum 225 dia. at Floor Level)		Dry Use		Height	3140 mm
Area		35448 mm2		As	26585.7421875 mm2
Ix		100042702 mm4		Zx	941578 mm3
Iy		100042702 mm4		Zx	941578 mm3
Lateral Restraint		3140 mm c/c			

Loads

Total Area over Pole = 21.25 m2

Dead	5.31 Kn	Live	5.31 Kn
Wind Down	15.94 Kn	Snow	0.00 Kn
Moment wind	11.00 Kn-m		
Phi	0.8	K8	0.91
K1 snow	0.8	K1 Dead	0.6
K1wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f_b =	36.3 MPa	f_s =	2.96 MPa
f_c =	18 MPa	f_p =	7.2 MPa
f_t =	22 MPa	E =	9257 MPa

Capacities

| PhiNcx Wind | 463.67 Kn | PhiMnx Wind | 24.84 Kn-m | PhiVnx Wind | 62.96 Kn |
| PhiNcx Dead | 278.20 Kn | PhiMnx Dead | 14.90 Kn-m | PhiVnx Dead | 37.77 Kn |

Checks

(Mx/PhiMnx)+(N/phiNcx) = 0.50 < 1 OK

(Mx/PhiMnx)^2+(N/phiNcx) = 0.25 < 1 OK

Deflection at top under service lateral loads = 18.34 mm < 31.40 mm

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m3		Friction angle	30 deg	Cohesion	0 Kn/m3
K_0 =	(1-sin(30)) / (1+sin(30))					
K_p =	(1+sin(30)) / (1-sin(30))					

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2625 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =   11.00 Kn-m

Shear Wind =   4.19 Kn

Pile Properties

Safety Factory   0.55

Hu =   7.29 Kn   Ultimate Lateral Strength of the Pile, Short pile

Mu =   11.57 Kn-m   Ultimate Moment Capacity of Pile

Checks

Applied Forces/Capacities = 0.95 < 1 OK

Uplift Check

Density of Concrete = 24 Kn/m3

Density of Timber Pole = 5 Kn/m3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient)for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safecty factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x 0.5 x tan(30) x Pi x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 22.07 Kn

Uplift on one Pile = 12.64 Kn

Uplift is ok

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