

Pole Shed App Ver 01 2022

Job No.: Oran Sinclair

Address: 536 Marshamns Road, Ashley, New Zealand **Date:** 10/30/2023

Latitude: -43.231757

Longitude: 172.634273

Elevation: 60.5 m

General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N4	Ground Snow Load	0.9 KPa	Roof Snow Load	0.63 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	B
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	4.2 m
Wind Region	NZ2	Terrain Category	2.0	Design Wind Speed	38.22 m/s
Wind Pressure	0.88 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High	Earthquake ARI	100		

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

Pressure Coefficients and Pressures

Shed Type = Mono Open

For roof $C_{p,i} = 0.6551$

For roof $C_{p,e}$ from 0 m To 3.0 m $C_{p,e} = -0.9$ $p_e = -0.58$ KPa $p_{net} = -1.08$ KPa

For roof $C_{p,e}$ from 3.90 m To 7.80 m $C_{p,e} = -0.5$ $p_e = -0.32$ KPa $p_{net} = -0.82$ KPa

For wall Windward $C_{p,i} = 0.6551$ side Wall $C_{p,i} = 0.5665$

For wall Windward and Leeward $C_{p,e}$ from 0 m To 13.50 m $C_{p,e} = 0.7$ $p_e = 0.55$ KPa $p_{net} = 1.09$ KPa

For side wall $C_{p,e}$ from 0 m To 3.90 m $C_{p,e} =$ $p_e = -0.51$ KPa $p_{net} = 0.03$ KPa

Maximum Upward pressure used in roof member Design = 1.08 KPa

Maximum Downward pressure used in roof member Design = 0.70 KPa

Maximum Wall pressure used in Design = 1.09 KPa

Maximum Racking pressure used in Design = 0.94 KPa

Design Summary

Purlin Design

Purlin Spacing = 850 mm

Purlin Span = 4350 mm

Try Purlin 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet

condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.47 S1 Downward =11.27 S1 Upward =24.64

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	0.68 Kn-m	Capacity	2.23 Kn-m	Passing Percentage	327.94 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	2.01 Kn-m	Capacity	2.97 Kn-m	Passing Percentage	147.76 %
M _{0.9D-W_nUp}	-1.72 Kn-m	Capacity	-1.76 Kn-m	Passing Percentage	130.37 %
V _{1.35D}	0.62 Kn	Capacity	9.65 Kn	Passing Percentage	1556.45 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_nD_n}	1.85 Kn	Capacity	12.86 Kn	Passing Percentage	695.14 %
V _{0.9D-W_nUp}	-1.58 Kn	Capacity	-16.08 Kn	Passing Percentage	1017.72 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 10.17 mm Limit by Woolcock et al, 1999 Span/240 = 17.92 mm

Deflection under Dead and Service Wind = 14.40 mm Limit by Woolcock et al, 1999 Span/100 = 43.00 mm

Reactions

Maximum downward =1.85 kn Maximum upward = -1.58 kn

Number of Blocking = 0 if 0 then no blocking required, if 1 then one midspan blocking required

Rafter Design Internal

Internal Rafter Load Width = 4500 mm Internal Rafter Span = 3850 mm Try Rafter 2x250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =1.00 S1 Downward =6.13 S1 Upward =6.13

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

Pole Shed App Ver 01 2022

M _{1.35D}	2.81 Kn-m	Capacity	7 Kn-m	Passing Percentage	249.11 %
M _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	8.34 Kn-m	Capacity	9.34 Kn-m	Passing Percentage	111.99 %
M _{0.9D-WnUp}	-7.13 Kn-m	Capacity	-11.66 Kn-m	Passing Percentage	163.53 %
V _{1.35D}	2.92 Kn	Capacity	24.12 Kn	Passing Percentage	826.03 %
V _{1.2D+1.5L 1.2D+Sn 1.2D+WnDn}	8.66 Kn	Capacity	32.16 Kn	Passing Percentage	371.36 %
V _{0.9D-WnUp}	-7.41 Kn	Capacity	-40.2 Kn	Passing Percentage	542.51 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 5.76 mm Limit by Woolcock et al, 1999 Span/240 = 16.67 mm

Deflection under Dead and Service Wind = 9.065 mm Limit by Woolcock et al, 1999 Span/100 = 40.00 mm

Reactions

Maximum downward = 8.66 kn Maximum upward = -7.41 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K₁₁ = 14.9 f_{pj} = 12.9 Mpa for Rafter with effective thickness = 100 mm

For Parallel to grain loading

K₁₁ = 2.0 f_{cj} = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 21.67 Kn > -7.41 Kn

Rafter Design External

External Rafter Load Width = 2250 mm External Rafter Span = 3811 mm Try Rafter 250x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

Pole Shed App Ver 01 2022

K1 Short term = 1 K1 Medium term = 0.8 K1 Long term = 0.6 K4 = 1 K5 = 1 K8 Downward = 0.97

K8 Upward = 0.97 S1 Downward = 12.68 S1 Upward = 12.68

Shear Capacity of timber = 3 MPa Bending Capacity of timber = 14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{1.35D}	1.38 Kn-m	Capacity	3.40 Kn-m	Passing Percentage	246.38 %
M _{1.2D+1.5L 1.2D+S_n 1.2D+W_{nDn}}	4.08 Kn-m	Capacity	4.53 Kn-m	Passing Percentage	111.03 %
M _{0.9D-W_{nUp}}	-3.49 Kn-m	Capacity	-5.67 Kn-m	Passing Percentage	162.46 %
V _{1.35D}	1.45 Kn	Capacity	12.06 Kn	Passing Percentage	831.72 %
V _{1.2D+1.5L 1.2D+S_n 1.2D+W_{nDn}}	4.29 Kn	Capacity	16.08 Kn	Passing Percentage	374.83 %
V _{0.9D-W_{nUp}}	-3.67 Kn	Capacity	-20.10 Kn	Passing Percentage	547.68 %

Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

k₂ for Long Term Loads = 2

Deflection under Dead and Live Load = 6.40 mm Limit by Woolcock et al, 1999 Span/240 = 16.67 mm

Deflection under Dead and Service Wind = 9.07 mm Limit by Woolcock et al, 1999 Span/100 = 40.00 mm

Reactions

Maximum downward = 4.29 kn Maximum upward = -3.67 kn

Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J5 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K₁₁ = 14.9 f_{pj} = 12.9 Mpa for Rafter with effective thickness = 50 mm

For Parallel to grain loading

K₁₁ = 2.0 f_{cj} = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

V = $\phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s$ (Eq 4.12) = -19.95 kn > -3.67 Kn

Single Shear Capacity under short term loads = -10.84 Kn > -3.67 Kn

Girt Design Front and Back

Girt's Spacing = 900 mm

Girt's Span = 4500 mm

Try Girt 200x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.78 S1 Downward =11.27 S1 Upward =17.82

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	2.48 Kn-m	Capacity	2.90 Kn-m	Passing Percentage	116.94 %
V _{0.9D-WnUp}	2.21 Kn-m	Capacity	16.08 Kn-m	Passing Percentage	727.60 %

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 37.01 mm Limit by Woolcock et al, 1999 Span/100 = 45.00 mm

Sag during installation = 24.86 mm

Reactions

Maximum = 2.21 kn

Girt Design Sides

Girt's Spacing = 600 mm

Girt's Span = 4000 mm

Try Girt 150x50 SG8 Dry

Moisture Condition = Dry (Moisture in timber is less than 16% and does not remain in continuous wet condition after installation)

K1 Short term = 1 K4 =1 K5 =1 K8 Downward =1.00

K8 Upward =0.65 S1 Downward =9.63 S1 Upward =20.31

Shear Capacity of timber =3 MPa Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

Capacity Checks

M _{Wind+Snow}	1.31 Kn-m	Capacity	1.38 Kn-m	Passing Percentage	105.34 %
------------------------	-----------	----------	-----------	--------------------	-----------------

Pole Shed App Ver 01 2022

V _{0.9D-WnUp}	1.31 Kn-m	Capacity	12.06 Kn-m	Passing Percentage	920.61 %
------------------------	-----------	----------	------------	--------------------	----------

Deflections

Modulus of Elasticity = 6700 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 36.51 mm Limit by Woolcock et al. 1999 Span/100 = 40.00 mm
Sag during installation = 15.52 mm

Reactions

Maximum = 1.31 kn

Middle Pole Design

Geometry

175 SED H5 (Minimum 200 dia. at Floor Level)	Dry Use	Height	3900 mm
Area	27598 mm ²	As	20698.2421875 mm ²
I _x	60639381 mm ⁴	Z _x	646820 mm ³
I _y	60639381 mm ⁴	Z _y	646820 mm ³
Lateral Restraint	3400 mm c/c		

Loads

Total Area over Pole = 18 m²

Dead	4.50 Kn	Live	4.50 Kn
Wind Down	12.60 Kn	Snow	11.34 Kn
Moment wind	9.30 Kn-m	Moment snow	2.83 Kn-m
Phi	0.8	K ₈	0.76
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{Cx} Wind	302.65 Kn	PhiM _{Nx} Wind	14.30 Kn-m	PhiV _{Nx} Wind	49.01 Kn
-------------------------	-----------	-------------------------	------------	-------------------------	----------

Pole Shed App Ver 01 2022

PhiNcx Dead	181.59 Kn	PhiMnx Dead	8.58 Kn-m	PhiVnx Dead	29.41 Kn
PhiNcx Snow	242.12 Kn	PhiMnx Snow	11.44 Kn-m	PhiVnx Snow	39.21 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.73 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.50 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 38.15 \text{ mm} < 39.00 \text{ mm}$$

Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

Geometry For Middle Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1400 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	9.30 Kn-m	Moment Snow =	Kn-m
Shear Wind =	2.95 Kn	Shear Snow =	2.83 Kn

Pile Properties

Safety Factory	0.55	
Hu =	5.37 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	9.97 Kn-m	Ultimate Moment Capacity of Pile

Checks

$$\text{Applied Forces/Capacities} = 0.93 < 1 \text{ OK}$$

End Pole Design

Geometry For End Bay Pole

Pole Shed App Ver 01 2022

Geometry

175 SED H5 (Minimum 200 dia. at Floor Level)	Dry Use	Height	3950 mm
Area	27598 mm ²	As	20698.2421875 mm ²
I _x	60639381 mm ⁴	Z _x	646820 mm ³
I _y	60639381 mm ⁴	Z _y	646820 mm ³
Lateral Restraint	mm c/c		

Loads

Total Area over Pole = 9 m²

Dead	2.25 Kn	Live	2.25 Kn
Wind Down	6.30 Kn	Snow	5.67 Kn
Moment Wind	4.65 Kn-m	Moment snow	1.41 Kn-m
Phi	0.8	K ₈	0.62
K ₁ snow	0.8	K ₁ Dead	0.6
K ₁ wind	1		

Material

Peeling	Steaming	Normal	Dry Use
f _b =	36.3 MPa	f _s =	2.96 MPa
f _c =	18 MPa	f _p =	7.2 MPa
f _t =	22 MPa	E =	9257 MPa

Capacities

PhiN _{cx} Wind	245.87 Kn	PhiM _{nx} Wind	11.62 Kn-m	PhiV _{nx} Wind	49.01 Kn
PhiN _{cx} Dead	147.52 Kn	PhiM _{nx} Dead	6.97 Kn-m	PhiV _{nx} Dead	29.41 Kn
PhiN _{cx} Snow	196.70 Kn	PhiM _{nx} Snow	9.30 Kn-m	PhiV _{nx} Snow	39.21 Kn

Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.45 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.21 < 1 \text{ OK}$$

Deflection at top under service lateral loads = 20.49 mm < 41.90 mm

D _s =	0.6 mm	Pile Diameter
L =	1400 mm	Pile embedment length
f _l =	3150 mm	Distance at which the shear force is applied

Pole Shed App Ver 01 2022

f2 = 0 mm Distance of top soil at rest pressure

Loads

Total Area over Pole = 9 m²

Moment Wind =	4.65 Kn-m	Moment Snow =	1.41 Kn-m
Shear Wind =	1.48 Kn	Shear Snow =	1.41 Kn

Pile Properties

Safety Factory	0.55		
Hu =	5.37 Kn	Ultimate Lateral Strength of the Pile, Short pile	
Mu =	9.97 Kn-m	Ultimate Moment Capacity of Pile	

Checks

Applied Forces/Capacities = 0.47 < 1 OK

Drained Lateral Strength of End pile in cohesionless soils Free Head short pile

Assumed Soil Properties

Gamma	18 Kn/m ³	Friction angle	30 deg	Cohesion	0 Kn/m ³
K0 =	(1-sin(30)) / (1+sin(30))				
Kp =	(1+sin(30)) / (1-sin(30))				

Geometry For End Bay Pole

Ds =	0.6 mm	Pile Diameter
L =	1400 mm	Pile embedment length
f1 =	3150 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

Loads

Moment Wind =	4.65 Kn-m	Moment Snow =	1.41 Kn-m
Shear Wind =	1.48 Kn	Shear Snow =	1.41 Kn

Pile Properties

Safety Factory	0.55		
Hu =	5.37 Kn	Ultimate Lateral Strength of the Pile, Short pile	
Mu =	9.97 Kn-m	Ultimate Moment Capacity of Pile	

Checks

Applied Forces/Capacities = $0.47 < 1$ OK

Uplift Check

Density of Concrete = 24 Kn/m^3

Density of Timber Pole = 5 Kn/m^3

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

K_s (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1400) x $K_s(1.5)$ x $0.5 \times \tan(30)$ x π x Dia of Pile(0.6) x Height of Pile(1400)

Skin Friction = 15.83 Kn

Weight of Pile + Pile Skin Friction = 19.92 Kn

Uplift on one Pile = 15.39 Kn

Uplift is ok