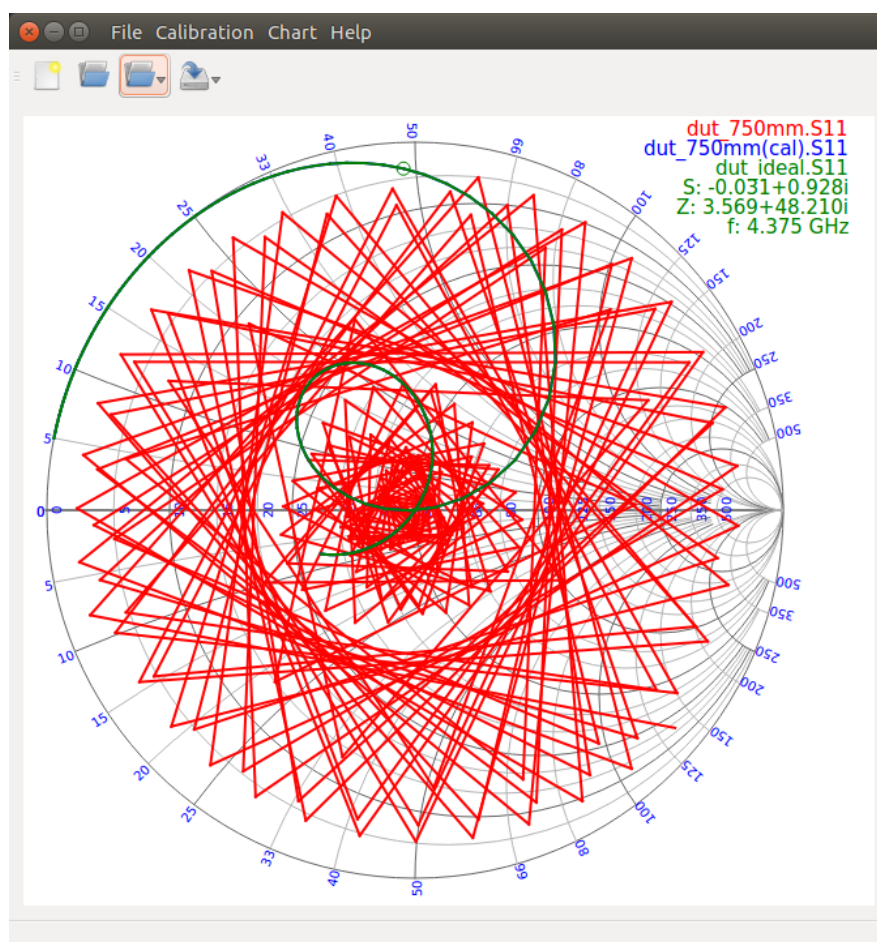


# DeEmbed, User manual ant theory of operation

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# 1 Introduction

DeEmbed is a GUI application that can read raw S-Parameter files in TouchStone format. There is support for 1 to 4 port s-parameter files. The s-parameters can be de-embedded using the SOLTI (Short, Open, Load, Through, Isolation) method. If you create 1 or 2 port s-parameter files from your cables (through + isolation) and measure 1-port s-parameter files of a short, open and load, the original DUT can be shown in the different graphs as if they were measured without cables.

By default the application shows the data in a smith chart, but different charts are supported (Db, phase, magnitude, VSWR, polar and some combinations).

The application automatically interpolates (spline) the calibration sets to the desired touchstone file. Note that the frequency range of the first touchstone file is leading, any file loaded afterwards will also be interpolated.

## 2 DeEmbed User Guide

This section will walk you through the usage of DeEmbed, we will show which files can be loaded and how to use calibration files. Also the navigation through the chart will be explained shortly.

### 2.1 Loading Calibration files

In order to deembed the actual S-Parameters  $S$  from the measured S-Parameters  $S_M$ , you need to supply the measured (or simulated) calibration files for Short, Open, Load, Through and Isolation.

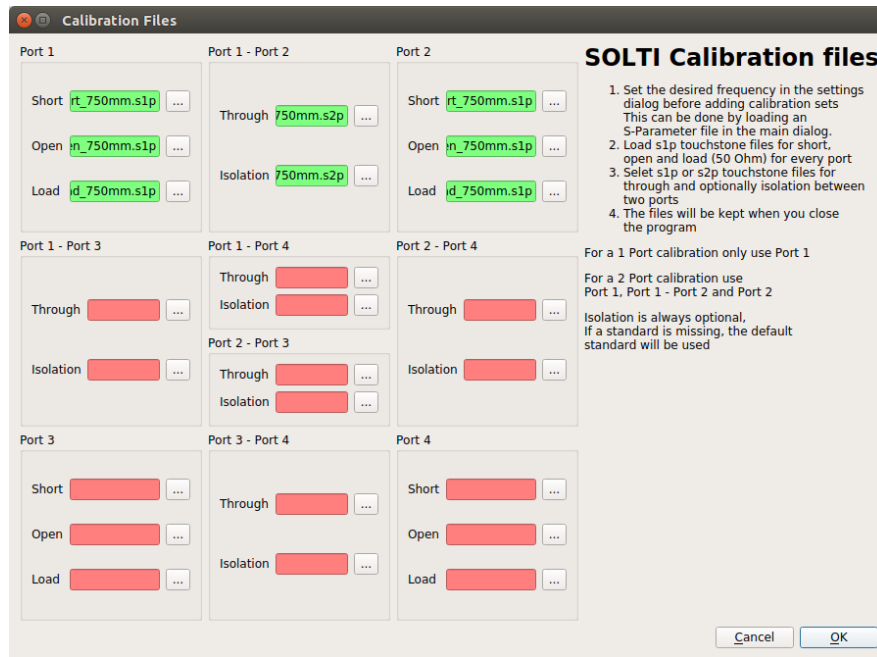


Figure 1: Calibration files dialog

Figure 1 shows the dialog in which the filenames of the measured calibration standards are specified. Depending on the number of ports of the DUT (Device under Test) a number of TouchStone files with measured standards must be supplied. For every port, the following files must be present:

- **Short:** A measured trace with an uncalibrated network analyzer of the short standard. The file is a one port Touchstone file (.s1p)
- **Open:** A measured trace with an uncalibrated network analyzer of the open standard. The file is a one port Touchstone file (.s1p)
- **Load:** A measured trace with an uncalibrated network analyzer of the  $50\Omega$  load standard. The file is a one port Touchstone file (.s1p)

If the DUT consists of more than one port, also through and optionally isolation standards should be supplied.

- **Through:** A measured trace with an uncalibrated network analyzer between the two corresponding ports, with the two cables connected together with a through connector. The file is a two port Touchstone file (.s2p)

- **Through:** A measured trace with an uncalibrated network analyzer between the two corresponding ports, with the two cables both connected to a  $50\Omega$  load. The file is a two port Touchstone file (.s2p)

The format of the Touchstone files is described in [2].

If you want to de-embed a two port S-Parameter file, only Short, Open and Load for Port 1 and 2 need to be supplied plus the Through and Isolation between Port 1-2, this calibration set is shown in figure 1.

If the file supplied with the browse button (...) can be found, the filename colors green, otherwise the box turns red. The green color does not indicate that the file is a valid Touchstone file.

The application DeEmbed comes with some example calibration files, and two DUT files:

The files are located in `installation prefix/share/examples/`

- **short\_750mm.s1p:** Ideal short simulated with 750mm coaxial cable (qucs)
- **open\_750mm.s1p:** Ideal open simulated with 750mm coaxial cable (qucs)
- **load\_750mm.s1p:** Ideal  $50\Omega$  load simulated with 750mm coaxial cable (qucs)
- **through\_750mm.s2p:** Ideal through simulated with 2 times 750mm coaxial cable (qucs)
- **isolation\_750mm.s2p:** 2 times 750mm coaxial cable simulated with an open end (qucs)
- **dut\_750mm.s2p:** Low pass filter simulated with 2x 750mm coaxial cable (qucs)
- **dut\_ideal.s2p:** The same low pass filter simulated without cable

If you load the right calibration files (2x short open load and 1x through + isolation) the non-calibrated trace of dut\_ideal will exactly follow the calibrated trace of dut\_750mm. The calibration standards should be chosen as ideal.

## 2.2 Setting calibration standards

The measured calibration standards described in 2.1 are usually not measured with perfect calibration standards, unless a simulator is used to generate the calibration files. In case of a perfect calibration kit, the calibration set "Ideal" can be used. The equations and the different components in the calibration standards are explained in 3.4.

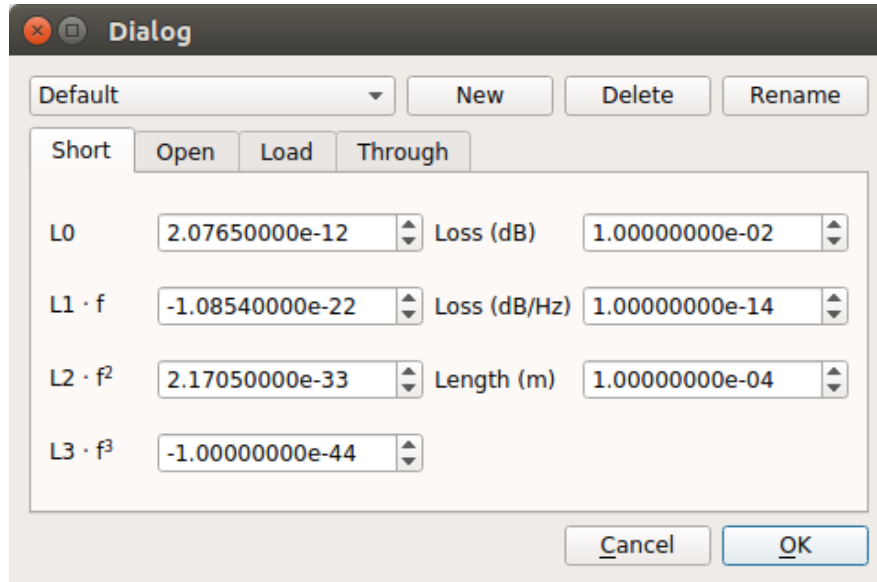


Figure 2: Calibration standards dialog

An actual calibration kit should come with the different parameters, or the measured calibration kit can be fitted using a simulator to obtain the right standard constants.

A realistic calibration kit (Default) comes with the application, note that this kit does not refer to any commercially available calibration kit.

If you change the calibration standard in this dialog while Touchstone files and calibration files are loaded, the graph will update instantly while changing the constants. This way it is also easy to fit two traces together.

## 2.3 Open and save Touchstone files

From the GUI, Touchstone files can be loaded and saved. DeEmbed handles 1, 2, 3 and 4 port Touchstone files [2], both to open and save.

## 2.4 Navigate the chart

The chart can be navigated using the mouse wheel and combinations of Shift and Control:

- Scrolling zooms the smith chart and centers
- Scrolling moves a cartesian chart
- Ctrl+scrolling zooms a cartesian chart
- Shift+scrolling moves the right cartesian axis
- Shift+Ctrl+scrolling zooms the right cartesian axis
- A marker can be set by right clicking near to one of the traces.

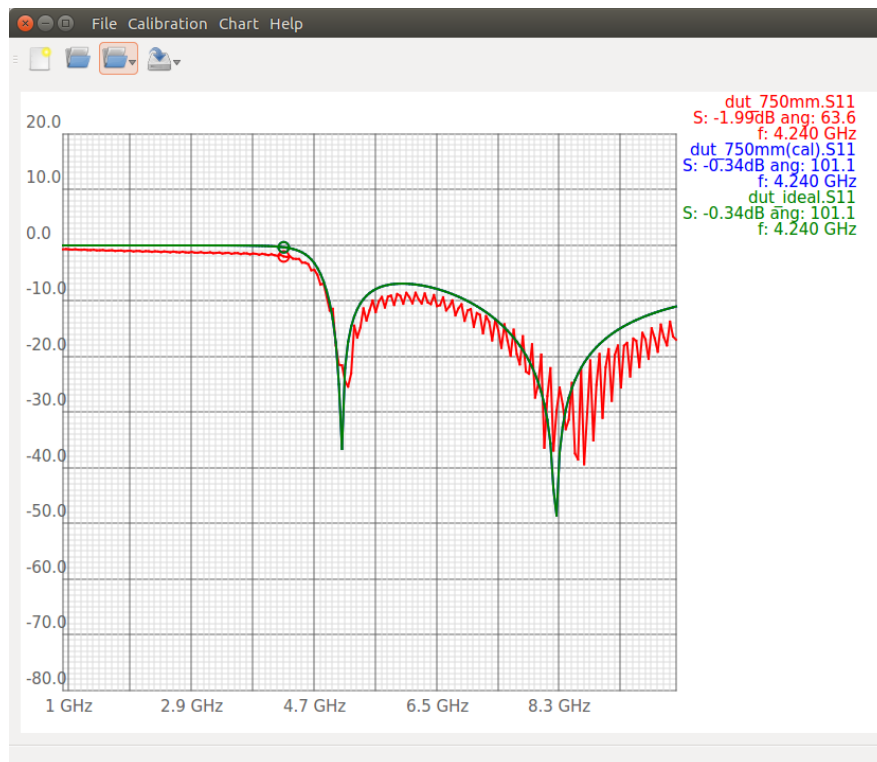


Figure 3: The main window showing the graph in dB mode

### 3 Calibration

SOLT Calibration is a commonly used calibration method in network analyzers. SOL stands for Short-Open-Load, the standards that are commonly used for a single port calibration. In order to calibrate the s-parameters between different ports, also Through-Isolation (TI) can be used to calibrate  $S_{21}$  and  $S_{12}$ .

#### 3.1 SOL Calibration

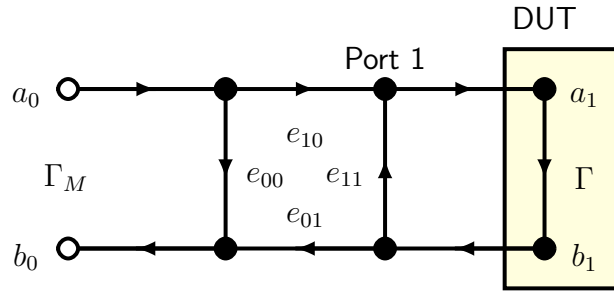


Figure 4: One port model

The measured S-parameter data can be de-embedded to the actual DUT with the lengths of the cables and the error coefficients of the network analyzer taken out of the data as if the DUT was measured directly.

$$S_{11} = \frac{S_{11_M} - e_{00}}{(S_{11_M} e_{11}) - \Delta_e} \quad (1)$$

- $e_{00}$  is the Directivity
- $e_{11}$  is the port match
- $\Delta_e = e_{00}e_{11} - (e_{10}e_{01})$ , of which  $(e_{10}e_{01})$  is the tracking.
- $S_{11}$  is the one port S-parameter that you want to display (De-embedded)
- $S_{11_M}$  is the measured S-parameter including the cable and the errors of the port

The 3 error coefficients can be obtained from 3 independent measurements of known standards. The commonly used standards are Short, Open and Load, but any known standard can be used instead. (see section 3.1.1)



### 3.1.1 Obtaining error coefficients for SOL calibration

Equation 1 contains 3 error coefficients  $e_{00}$ ,  $e_{11}$  and  $\Delta_e$ . From [1] the equations 2, 3 and 4 are obtained. We see 3 times the same equations, but with different measurements.  $\Gamma_1$ ,  $\Gamma_2$  and  $\Gamma_3$  are the known independent calibration standards, in this case Short, Open and Load. The standards don't have to be perfect though, a short can for instance have some series inductance or loss (see 3.4).  $\Gamma_{M1}$ ,  $\Gamma_{M2}$  and  $\Gamma_{M3}$  are the measured traces, this data is obtained by connecting the well-defined calibration standard to the network analyzer, through the cable that is also used in the measurement and measure the reflection (S11). Equations 2, 3 and 4 still contain our 3 unknown error coefficients  $e_{00}$ ,  $e_{11}$  and  $\Delta_e$  that we need to solve equation 1.

$$\Gamma_{M1} = e_{00} + \Gamma_1 \Gamma_{M1} e_{11} - \Gamma_1 \Delta_e \quad (2)$$

$$\Gamma_{M2} = e_{00} + \Gamma_2 \Gamma_{M2} e_{11} - \Gamma_2 \Delta_e \quad (3)$$

$$\Gamma_{M3} = e_{00} + \Gamma_3 \Gamma_{M3} e_{11} - \Gamma_3 \Delta_e \quad (4)$$

In order to solve  $e_{00}$ ,  $e_{11}$  and  $\Delta_e$  we need to substitute equations 2, 3 and 4 into one equation and extract the 3 error coefficients. The result is 3 lengthy equations, but with modern computers they can easily be computed for all the data points in our measurement.

$$e_{00} = - \frac{(\Gamma_2 \Gamma_{M3} - \Gamma_3 \Gamma_{M3}) \Gamma_1 \Gamma_{M2} - (\Gamma_2 \Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_3 \Gamma_{M3} - (\Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_{M3}) \Gamma_1) \Gamma_{M1}}{\Gamma_1 (\Gamma_2 - \Gamma_3) \Gamma_{M1} + \Gamma_2 \Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_3 \Gamma_{M3} - (\Gamma_2 \Gamma_{M2} - \Gamma_3 \Gamma_{M3}) \Gamma_1} \quad (5)$$

$$e_{11} = \frac{(\Gamma_2 - \Gamma_3) \Gamma_{M1} - \Gamma_1 (\Gamma_{M2} - \Gamma_{M3}) + \Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_{M3}}{\Gamma_1 (\Gamma_2 - \Gamma_3) \Gamma_{M1} + \Gamma_2 \Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_3 \Gamma_{M3} - (\Gamma_2 \Gamma_{M2} - \Gamma_3 \Gamma_{M3}) \Gamma_1} \quad (6)$$

$$\Delta_e = - \frac{(\Gamma_1 (\Gamma_{M2} - \Gamma_{M3}) - \Gamma_2 \Gamma_{M2} + \Gamma_3 \Gamma_{M3}) \Gamma_{M1} + (\Gamma_2 \Gamma_{M3} - \Gamma_3 \Gamma_{M3}) \Gamma_{M2}}{\Gamma_1 (\Gamma_2 - \Gamma_3) \Gamma_{M1} + \Gamma_2 \Gamma_3 \Gamma_{M2} - \Gamma_2 \Gamma_3 \Gamma_{M3} - (\Gamma_2 \Gamma_{M2} - \Gamma_3 \Gamma_{M3}) \Gamma_1} \quad (7)$$

### 3.2 Full two port calibration

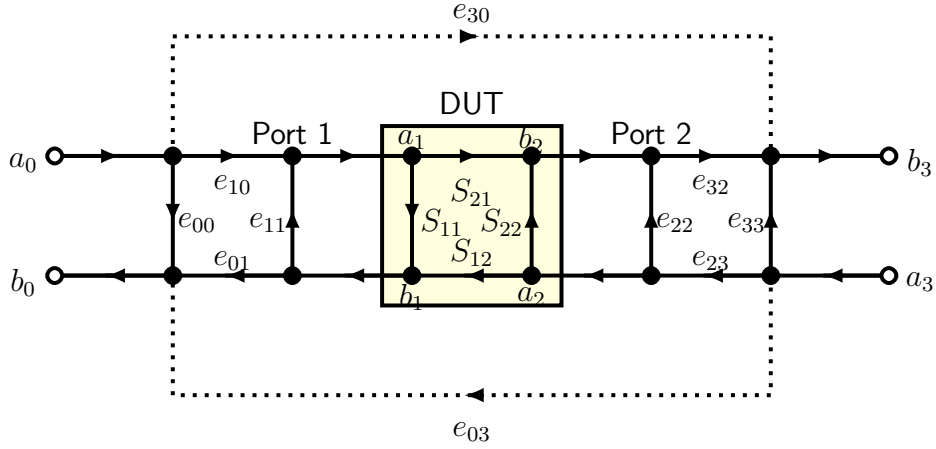


Figure 5: Two port model

Where the SOL calibration is using 3 error coefficients, the full two port calibration needs 12 for SOLTI calibration (Short - Open - Load - Through - Isolation). In order to obtain the 12 error terms, we need Short Open Load measurements for every port as performed in section 3.1. Apart from the SOL measurements we also need a Through measurement (two cables connected) and an isolation measurement. An additional standard is also introduced, a non-perfect through standard (see section 3.4). The 12 error coefficients needed for SOLTI calibration are obtained in section 3.2.1.

$$D = \left[ 1 + \frac{S_{11M} - e_{00}}{e_{10}e_{01}}e_{11} \right] \left[ 1 + \frac{S_{22M} - e_{33}}{e_{23}e_{32}}e_{22} \right] - \frac{S_{21M} - e_{30}}{e_{10}e_{32}} \frac{S_{12M} - e_{03}}{e_{23}e_{01}}e'_{22}e'_{11} \quad (8)$$

$$S_{11} = \frac{\frac{S_{11M} - e_{00}}{e_{10}e_{01}} \left[ 1 + \frac{S_{22M} - e_{33}}{e_{23}e_{32}}e_{22} \right] - e'_{22} \frac{S_{21M} - e_{30}}{e_{10}e_{32}} \frac{S_{12M} - e_{03}}{e_{23}e_{01}}}{D} \quad (9)$$

$$S_{21} = \frac{\frac{S_{21M} - e_{30}}{e_{10}e_{32}} \left[ 1 + \frac{S_{22M} - e_{33}}{e_{23}e_{32}}(e_{22} - e'_{22}) \right]}{D} \quad (10)$$

$$S_{12} = \frac{\frac{S_{12M} - e_{03}}{e_{23}e_{01}} \left[ 1 + \frac{S_{11M} - e_{00}}{e_{10}e_{01}}(e_{11} - e'_{11}) \right]}{D} \quad (11)$$

$$S_{22} = \frac{\frac{S_{22M} - e_{33}}{e_{23}e_{32}} \left[ 1 + \frac{S_{11M} - e_{00}}{e_{10}e_{01}}e_{11} \right] - e'_{11} \frac{S_{12M} - e_{03}}{e_{23}e_{01}} \frac{S_{21M} - e_{30}}{e_{10}e_{32}}}{D} \quad (12)$$

- $e_{00}$ : Port 1 directivity
- $e_{11}$ : Port 1 match
- $e_{10}e_{01}$ : Port 1 reflection tracking
- $e_{10}e_{32}$ : Forward transmission tracking
- $e'_{22}$ : Port 2 match seen from port 1
- $e_{30}$ : Forward transmission leakage
- $e_{33}$ : Port 2 directivity
- $e_{22}$ : Port 2 match
- $e_{23}e_{32}$ : Port 2 reflection tracking
- $e_{23}e_{01}$ : Reverse transmission tracking
- $e'_{11}$ : Port 1 match seen from port 2
- $e_{03}$ : Reverse transmission leakage

### 3.2.1 obtaining the error coefficients for SOLT Calibration

The Through - Isolation calibration depends on the SOL calibration, this calibration has to be done first.  $e_{00}$ ,  $e_{11}$  and  $\Delta_{eP1}$  are obtained from the measurements in 3.1.1,  $e_{33}$ ,  $e_{22}$  and  $\Delta_{eP2}$  use the same equations but with Short / Open / Load measurements taken from port 2.

- $e_{00}$  and  $e_{33}$  are obtained from equation 5
- $e_{11}$  and  $e_{22}$  are obtained from equation 6
- $\Delta_{eP1}$  and  $\Delta_{eP2}$  are obtained from equation 7

$$(e_{10}e_{01}) = -\Delta_{eP1} + e_{11}e_{00} \quad (13)$$

$$(e_{23}e_{32}) = -\Delta_{eP2} + e_{22}e_{33} \quad (14)$$

For the next set of equations, we determine 5 sets of 2-port s-parameter matrices.

- $S_i$ : The isolation measurement executed with the two measurement cables connected to 50 $\Omega$  loads. From this matrix only  $S_{21i}$  and  $S_{12i}$  are used.
- $S_t$ : The through measurement, this s-parameter contains data of the measured through standard with the uncalibrated network analyzer.
- $S_s$ : The through standard (see paragraph 3.4)
- $S_M$ : The measured S-parameter matrix of the 2-port DUT
- $S$ : This is the resulting calibrated S-parameter matrix containing  $S_{11}$ ,  $S_{21}$ ,  $S_{12}$  and  $S_{22}$

The two port isolation measurement file is created with the measurement cables connected to a 50 $\Omega$  load. From this file the following error terms are obtained:

- $e_{30} = S_{21i}$ , this is the forward isolation
- $e_{03} = S_{12i}$ , this is the reverse isolation

$e'_{22}$  is in fact the same error term as  $e_{22}$ , but it is seen from port 1, for that reason we use a different calculation. Instead we use the SOL calibration method to de-embed the reflection measured at the through measurement  $S_{11t}$ , normalized to the standard  $S_{21s}$ . The same is true for  $e'_{11}$ .

$$e'_{22} = \frac{\frac{S_{11t}}{S_{21s}} - e_{00}}{\frac{S_{11t}}{S_{21s}}e_{11} - \Delta_{eP1}} \quad (15)$$

$$e'_{11} = \frac{\frac{S_{22t}}{S_{12s}} - e_{33}}{\frac{S_{22t}}{S_{12s}}e_{22} - \Delta_{eP2}} \quad (16)$$

$$e_{10}e_{32} = \left( \frac{S_{21t}}{S_{21s}} - e_{30} \right) (1 - e_{11}e'_{22}) \quad (17)$$

$$e_{23}e_{01} = \left( \frac{S_{12t}}{S_{12s}} - e_{03} \right) (1 - e_{22}e'_{11}) \quad (18)$$

The 12-term calibration method from Agilent [1] does not mention any through standard in its equations, Equations 16 to 18 are slightly modified with respect to [1], the Through and Reflect measurements  $S_{11t}$ ,  $S_{21t}$ ,  $S_{12t}$  and  $S_{22t}$  are compensated with (divided by) the known through standard 3.4.4

### 3.3 3 Port SOLT Calibration

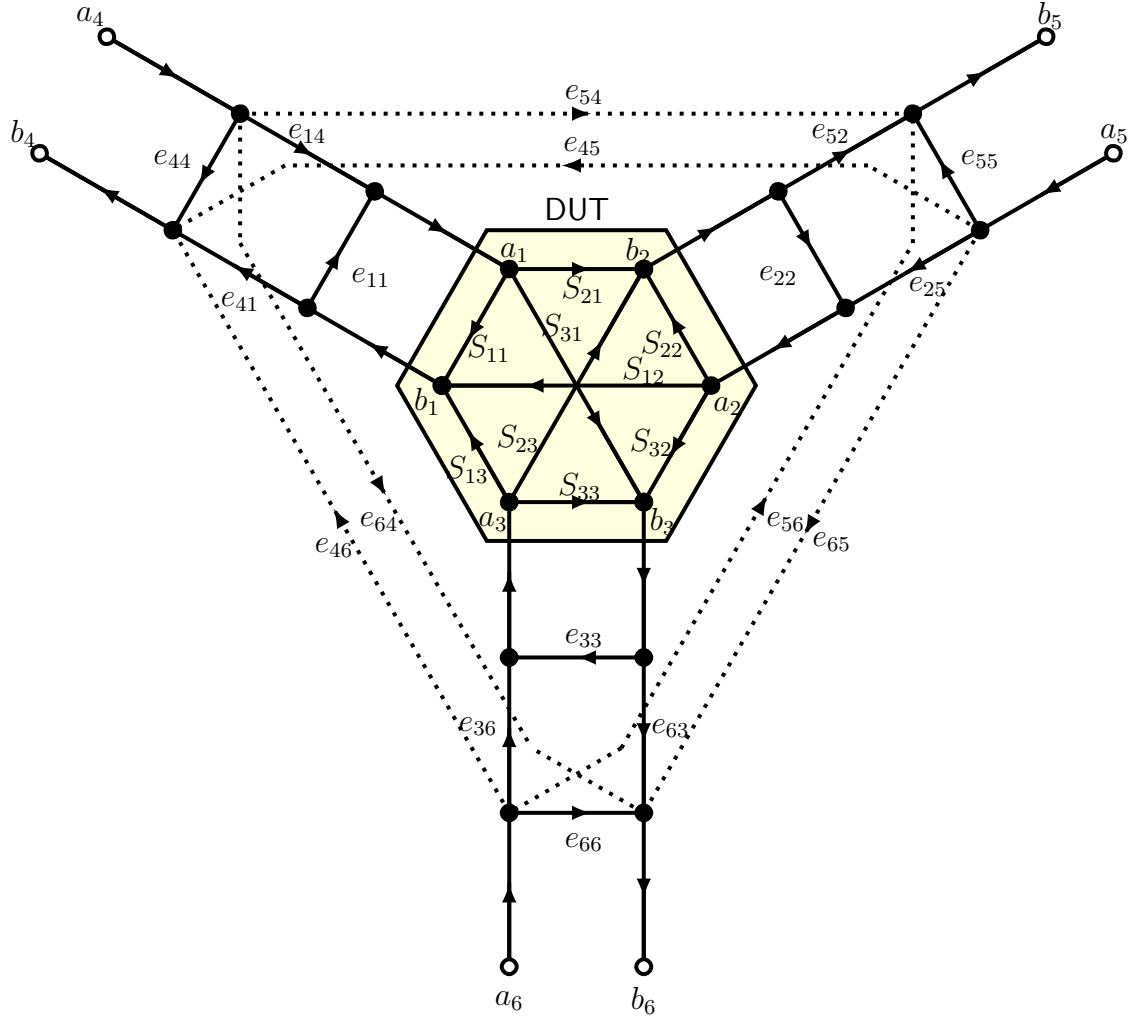


Figure 6: Three port model

$$D = \left[ 1 + \frac{S_{11M} - e_{44}}{e_{14}e_{41}}e_{11} \right] \left[ 1 + \frac{S_{22M} - e_{55}}{e_{25}e_{52}}e_{22} \right] \left[ 1 + \frac{S_{33M} - e_{66}}{e_{36}e_{63}}e_{33} \right] - \frac{S_{21M} - e_{54}}{e_{14}e_{52}} \frac{S_{12M} - e_{45}}{e_{25}e_{41}} e'_{22}e'_{11} - \frac{S_{31M} - e_{64}}{e_{14}e_{63}} \frac{S_{13M} - e_{46}}{e_{36}e_{41}} e'_{33}e'_{11} - \frac{S_{32M} - e_{65}}{e_{25}e_{63}} \frac{S_{23M} - e_{56}}{e_{36}e_{52}} e''_{33}e''_{22} \quad (19)$$

$$S_{11} = \frac{\left( \frac{S_{11M} - e_{44}}{e_{14}e_{41}} \left[ 1 + \frac{S_{22M} - e_{55}}{e_{25}e_{52}}e_{22} \right] \left[ 1 + \frac{S_{33M} - e_{66}}{e_{36}e_{63}}e_{33} \right] - e'_{22} \frac{S_{21M} - e_{54}}{e_{14}e_{52}} \frac{S_{12M} - e_{45}}{e_{25}e_{41}} - e'_{33} \frac{S_{31M} - e_{64}}{e_{14}e_{63}} \frac{S_{13M} - e_{46}}{e_{36}e_{41}} \right)}{D} \quad (20)$$

$$S_{22} = \frac{\left( \frac{S_{22M} - e_{55}}{e_{25}e_{52}} \left[ 1 + \frac{S_{11M} - e_{44}}{e_{14}e_{41}} e_{11} \right] \left[ 1 + \frac{S_{33M} - e_{66}}{e_{36}e_{63}} e_{33} \right] - e'_{11} \frac{S_{12M} - e_{45}}{e_{25}e_{41}} \frac{S_{21M} - e_{54}}{e_{14}e_{52}} - e''_{33} \frac{S_{31M} - e_{64}}{e_{14}e_{62}} \frac{S_{13M} - e_{46}}{e_{26}e_{41}} \right)}{D} \quad (21)$$

$$S_{33} = \frac{\left( \frac{S_{33M} - e_{66}}{e_{36}e_{63}} \left[ 1 + \frac{S_{11M} - e_{44}}{e_{14}e_{41}} e_{11} \right] \left[ 1 + \frac{S_{22M} - e_{55}}{e_{25}e_{52}} e_{22} \right] - e''_{11} \frac{S_{12M} - e_{45}}{e_{25}e_{41}} \frac{S_{21M} - e_{54}}{e_{14}e_{52}} - e''_{22} \frac{S_{21M} - e_{54}}{e_{14}e_{52}} \frac{S_{12M} - e_{45}}{e_{25}e_{41}} \right)}{D} \quad (22)$$

$$S_{21} = \frac{\frac{S_{21M} - e_{54}}{e_{14}e_{52}} \left[ 1 + \frac{S_{22M} - e_{55}}{e_{25}e_{52}} (e_{22} - e'_{22}) \right]}{D} \quad (23)$$

$$S_{12} = \frac{\frac{S_{12M} - e_{45}}{e_{25}e_{41}} \left[ 1 + \frac{S_{11M} - e_{44}}{e_{14}e_{41}} (e_{11} - e'_{11}) \right]}{D} \quad (24)$$

$$S_{31} = \frac{\frac{S_{31M} - e_{64}}{e_{14}e_{63}} \left[ 1 + \frac{S_{33M} - e_{66}}{e_{36}e_{63}} (e_{33} - e'_{33}) \right]}{D} \quad (25)$$

$$S_{13} = \frac{\frac{S_{13M} - e_{46}}{e_{36}e_{41}} \left[ 1 + \frac{S_{11M} - e_{44}}{e_{14}e_{41}} (e_{11} - e''_{11}) \right]}{D} \quad (26)$$

$$S_{32} = \frac{\frac{S_{32M} - e_{65}}{e_{25}e_{63}} \left[ 1 + \frac{S_{33M} - e_{66}}{e_{36}e_{63}} (e_{33} - e''_{33}) \right]}{D} \quad (27)$$

$$S_{23} = \frac{\frac{S_{23M} - e_{56}}{e_{36}e_{52}} \left[ 1 + \frac{S_{22M} - e_{55}}{e_{25}e_{52}} (e_{22} - e''_{22}) \right]}{D} \quad (28)$$

- $e_{44}$ : Port 1 directivity
- $e_{55}$ : Port 2 directivity
- $e_{66}$ : Port 3 directivity
- $e_{11}$ : Port 1 match
- $e'_{11}$ : Port 1 match seen from port 2
- $e''_{11}$ : Port 1 match seen from port 3
- $e_{22}$ : Port 2 match
- $e'_{22}$ : Port 2 match seen from port 1
- $e''_{22}$ : Port 2 match seen from port 3
- $e_{33}$ : Port 3 match
- $e'_{33}$ : Port 3 match seen from port 1
- $e''_{33}$ : Port 3 match seen from port 2
- $e_{14}e_{41}$ : Port 1 reflection tracking
- $e_{25}e_{52}$ : Port 2 reflection tracking
- $e_{36}e_{63}$ : Port 3 reflection tracking
- $e_{14}e_{52}$ : P1 to P2 transmission tracking
- $e_{25}e_{41}$ : P2 to P1 transmission tracking
- $e_{14}e_{63}$ : P1 to P3 transmission tracking
- $e_{36}e_{41}$ : P3 to P1 transmission tracking
- $e_{36}e_{52}$ : P2 to P3 transmission tracking
- $e_{25}e_{63}$ : P3 to P2 transmission tracking
- $e_{54}$ : P1 to P2 transmission leakage
- $e_{45}$ : P2 to P1 transmission leakage
- $e_{64}$ : P1 to P3 transmission leakage
- $e_{46}$ : P3 to P1 transmission leakage
- $e_{65}$ : P2 to P3 transmission leakage
- $e_{56}$ : P3 to P2 transmission leakage

### 3.3.1 obtaining the error coefficients for 3 port SOLT Calibration

The 3 port Through - Isolation calibration depends on the SOL calibration, this calibration has to be done first.  $e_{44}$ ,  $e_{11}$  and  $\Delta_{eP1}$  are obtained from the measurements in 3.1.1,  $e_{55}$ ,  $e_{22}$  and  $\Delta_{eP2}$  use the same equations but with Short / Open / Load measurements taken from port 2,  $e_{66}$ ,  $e_{33}$  and  $\Delta_{eP3}$  use the same equations but with Short / Open / Load measurements taken from port 3.

- $e_{44}$ ,  $e_{55}$  and  $e_{66}$  are obtained from equation 5
- $e_{11}$ ,  $e_{22}$  and  $e_{33}$  are obtained from equation 6
- $\Delta_{eP1}$ ,  $\Delta_{eP2}$  and  $\Delta_{eP3}$  are obtained from equation 7

$$(e_{14}e_{41}) = -\Delta_{eP1} + e_{11}e_{44} \quad (29)$$

$$(e_{25}e_{52}) = -\Delta_{eP2} + e_{22}e_{55} \quad (30)$$

$$(e_{36}e_{63}) = -\Delta_{eP3} + e_{33}e_{66} \quad (31)$$

For the next set of equations, we determine 5 sets of 3-port s-parameter matrices, as described in 3.2.1.

The 3 port isolation measurement file is created with the measurement cables connected to a 50 $\Omega$  load. From this file the following error terms are obtained:

- $e_{54} = S_{21i}$ , this is the P1 to P2 isolation
- $e_{45} = S_{12i}$ , this is the P2 to P1 isolation
- $e_{64} = S_{31i}$ , this is the P1 to P3 isolation
- $e_{46} = S_{13i}$ , this is the P3 to P1 isolation
- $e_{65} = S_{32i}$ , this is the P2 to P3 isolation
- $e_{56} = S_{23i}$ , this is the P3 to P2 isolation

$e'_{22}$  and  $e''_{22}$  is in fact the same error term as  $e_{22}$ , but it is seen from port 1 or port 3 respectively, for that reason we use a different calculation. Instead we use the SOL calibration method to de-embed the reflection measured at the through measurement  $S_{11t}$ , normalized to the standard  $S_{21s}$ . The same is true for  $e'_{11}$ ,  $e''_{11}$ ,  $e'_{33}$  and  $e''_{33}$ .

$$e'_{11} = \frac{\frac{S_{22t}}{S_{12s}} - e_{55}}{\frac{S_{22t}}{S_{12s}} e_{22} - \Delta_{eP2}} \quad (32)$$

$$e''_{11} = \frac{\frac{S_{33t}}{S_{13s}} - e_{66}}{\frac{S_{33t}}{S_{13s}} e_{22} - \Delta_{eP3}} \quad (33)$$

$$e'_{22} = \frac{\frac{S_{11t}}{S_{21s}} - e_{44}}{\frac{S_{11t}}{S_{21s}} e_{11} - \Delta_{eP1}} \quad (34)$$

$$e''_{22} = \frac{\frac{S_{33t}}{S_{23s}} - e_{66}}{\frac{S_{33t}}{S_{23s}} e_{33} - \Delta_{eP3}} \quad (35)$$

$$e'_{33} = \frac{\frac{S_{11t}}{S_{31s}} - e_{44}}{\frac{S_{11t}}{S_{31s}} e_{11} - \Delta_{eP1}} \quad (36)$$

$$e''_{33} = \frac{\frac{S_{22t}}{S_{32s}} - e_{55}}{\frac{S_{22t}}{S_{32s}} e_{22} - \Delta_{eP2}} \quad (37)$$

$$e_{14}e_{52} = \left( \frac{S_{21t}}{S_{21s}} - e_{54} \right) (1 - e_{11}e'_{22}) \quad (38)$$

$$e_{25}e_{41} = \left( \frac{S_{12t}}{S_{12s}} - e_{45} \right) (1 - e_{22}e'_{11}) \quad (39)$$

$$e_{14}e_{63} = \left( \frac{S_{31t}}{S_{31s}} - e_{64} \right) (1 - e_{11}e'_{33}) \quad (40)$$

$$e_{36}e_{41} = \left( \frac{S_{13t}}{S_{13s}} - e_{46} \right) (1 - e_{33}e'_{11}) \quad (41)$$

$$e_{25}e_{63} = \left( \frac{S_{32t}}{S_{32s}} - e_{65} \right) (1 - e_{22}e'_{33}) \quad (42)$$

$$e_{36}e_{52} = \left( \frac{S_{23t}}{S_{23s}} - e_{56} \right) (1 - e_{33}e'_{22}) \quad (43)$$



### 3.4 Calibration Standards

The calibrations used in 3.1 and 3.2 contain measurements of known standards, but apart from the measured trace we also need to know what the actual standard looks like. In order to use the standard in the calibration methods, we need to know the  $\Gamma$  (S-Parameter) of the standard.

#### 3.4.1 Short

The short standard like other standards is never  $0\Omega$ , instead it usually has a series inductance that can be frequency dependent. The connector of the standard can also have electrical loss and an electrical length. The parameters of the Short standard in DeEmbed are:

- $L_0$ : Constant series inductance.
- $L_1 \cdot f$ : Series inductance with linear frequency dependency
- $L_2 \cdot f^2$ : Series inductance with quadratic frequency dependency
- $L_3 \cdot f^3$ : Series inductance with cubic frequency dependency
- Loss(dB): Connector or trace loss of the standard
- Loss(dB/Hz): Frequency dependent connector or trace loss of the standard
- Length (m): Electrical (not physical) length of the connector / trace towards the standard.

$\Gamma_{sp}$  is calculated in 3 steps, first the complex impedance of the inductive part is calculated:

$$Z_{sp} = i2\pi f(L_0 + L_1f + L_2f^2 + L_3f^3) \quad (44)$$

Convert  $Z_{sp}$  into  $\Gamma_{sp}$  with equation 45.

$$\Gamma = \frac{\frac{Z}{50\Omega} - 1}{\frac{Z}{50\Omega} + 1} \quad (45)$$

At last we apply electrical length and loss:

$$\Gamma_{sp} = \Gamma_{sp} e^{2\pi length \cdot f \cdot c^{-1}} 10^{\frac{-Loss_{dB}}{20}} 10^{\frac{-Loss_{dB}Hzf}{20}} \quad (46)$$

where  $c$  is the speed of light (299792458)

#### 3.4.2 Open

The open standard like other standards is never  $\infty\Omega$ , instead it usually has a capacitance that can be frequency dependent. The connector of the standard can also have electrical loss and an electrical length. The parameters of the Open standard in DeEmbed are:

- $C_0$ : Constant series capacitance.
- $C_1 \cdot f$ : Series capacitance with linear frequency dependency
- $C_2 \cdot f^2$ : Series capacitance with quadratic frequency dependency
- $C_3 \cdot f^3$ : Series capacitance with cubic frequency dependency
- Loss(dB): Connector or trace loss of the standard
- Loss(dB/Hz): Frequency dependent connector or trace loss of the standard
- Length (m): Electrical (not physical) length of the connector / trace towards the standard.

$\Gamma_{op}$  is calculated in 3 steps, first the complex impedance of the capacitive part is calculated:

$$Z_{op} = \frac{-i}{2\pi f(C_0 + C_1f + C_2f^2 + C_3f^3)} \quad (47)$$

Convert  $Z_{op}$  into  $\Gamma_{op}$  with equation 45. At last we apply electrical length and loss:

$$\Gamma_{op} = \Gamma_{op} e^{2\pi length \cdot f \cdot c^{-1}} 10^{\frac{-Loss_{dB}}{20}} 10^{\frac{-Loss_{dBHz}f}{20}} \quad (48)$$

where  $c$  is the speed of light (299792458)

### 3.4.3 Load

The load standard in DeEmbed can be defined as a perfect resistance ( $R_l$ ) with a series inductance ( $L_l$ ).

$$Z_{lp} = R_l + 2\pi f \cdot L_l \quad (49)$$

Convert  $Z_{lp}$  into  $\Gamma_{lp}$  with equation 45.

### 3.4.4 Through

The through standard is only a connector between the two cables, we define the standard with only length and loss:

- Loss(dB): Connector or trace loss of the standard
- Loss(dB/Hz): Frequency dependent connector or trace loss of the standard
- Length (m): Electrical (not physical) length of the connector / trace towards the standard.

$$\Gamma_{th} = 1 \cdot e^{2\pi length \cdot f \cdot c^{-1}} 10^{\frac{-Loss_{dB}}{20}} 10^{\frac{-Loss_{dBHz}f}{20}} \quad (50)$$

## References

- [1] Network Analyzer Error Models and Calibration Methods, Doug Rytting - Agilent Technologies  
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