Wave aberration function and transverse ray aberrations

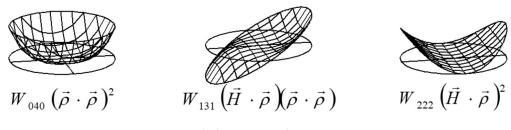
OPTI 517

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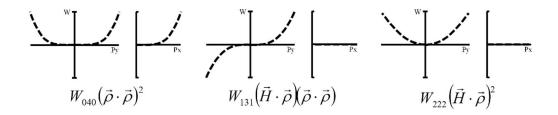
The aberration function for spherical, coma, and astigmatism aberrations is

$$W\left(\vec{H},\vec{\rho}\right) = W_{040} \left(\vec{\rho} \cdot \vec{\rho}\right)^2 + W_{131} \left(\vec{H} \cdot \vec{\rho}\right) \left(\vec{\rho} \cdot \vec{\rho}\right) + W_{222} \left(\vec{H} \cdot \vec{\rho}\right)^2.$$

Graphically the wavefront deformation for these aberrations is



and the wave fans are

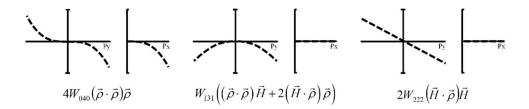


The transverse ray aberration is

$$\vec{\varepsilon} = \overline{y}_i \Delta \vec{H} = -\frac{\overline{y}_i}{\mathcal{K}} \vec{\nabla}_{\rho} W (\vec{H}, \vec{\rho}) = \frac{1}{n'u'} \vec{\nabla}_{\rho} W (\vec{H}, \vec{\rho}).$$

For the case of spherical aberration, coma, and astigmatism we have

$$\begin{split} \vec{\varepsilon} &= \frac{1}{n'u'} \vec{\nabla}_{\rho} W \left(\vec{H}, \vec{\rho} \right) = \frac{1}{n'u'} \frac{\delta}{\delta \vec{\rho}} \left(W_{040} \left(\vec{\rho} \cdot \vec{\rho} \right)^2 + W_{131} \left(\vec{H} \cdot \vec{\rho} \right) (\vec{\rho} \cdot \vec{\rho}) + W_{222} \left(\vec{H} \cdot \vec{\rho} \right)^2 \right) \\ &= \frac{1}{n'u'} \left(4W_{040} \left(\vec{\rho} \cdot \vec{\rho} \right) \vec{\rho} + W_{131} \left(\vec{\rho} \cdot \vec{\rho} \right) \vec{H} + 2W_{131} \left(\vec{H} \cdot \vec{\rho} \right) \vec{\rho} + 2W_{222} \left(\vec{H} \cdot \vec{\rho} \right) \vec{H} \right) \end{split}$$

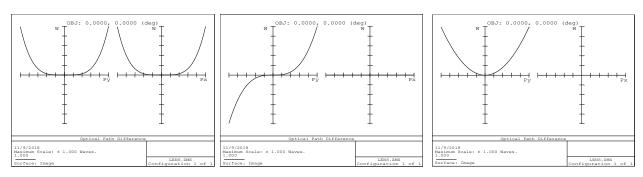


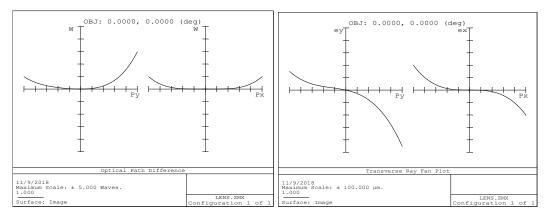
In the meridional plane $\phi = 0$, at full field H = 1, and at full aperture $\rho = 1$ we have

$$\varepsilon_y = \frac{1}{n'u'} (4W_{040} + 3W_{131} + 2W_{222}).$$

Assume the system is f/10, λ =0.0005 mm, n'=1, W_{040} =1 λ , W_{131} =1 λ , and W_{222} =1 λ then

$$\varepsilon_y = -20(4+3+2)\lambda = -180\lambda = -0.09mm$$





Combined Wavefront deformation and transverse ray aberration

Alternatively the transverse ray aberration is

$$\begin{split} & \varepsilon_{y} = \frac{1}{n'u'} \frac{\delta}{\delta \rho_{y}} W \left(\vec{H}, \vec{\rho} \right) = \frac{1}{n'u'} \frac{\delta}{\delta \rho_{y}} \left(W_{040} \left(\vec{\rho} \cdot \vec{\rho} \right)^{2} + W_{131} \left(\vec{H} \cdot \vec{\rho} \right) \left(\vec{\rho} \cdot \vec{\rho} \right) + W_{222} \left(\vec{H} \cdot \vec{\rho} \right)^{2} \right) \\ & = \frac{1}{n'u'} \frac{\delta}{\delta \rho_{y}} \left(W_{040} \left(\rho_{x}^{2} + \rho_{y}^{2} \right)^{2} + W_{131} \left(H_{x} \rho_{x} + H_{y} \rho_{y} \right) \left(\rho_{x}^{2} + \rho_{y}^{2} \right) + W_{222} \left(H_{x} \rho_{x} + H_{y} \rho_{y} \right)^{2} \right) \\ & = \frac{1}{n'u'} \left(4W_{040} \left(\rho_{x}^{2} + \rho_{y}^{2} \right) \rho_{y} + W_{131} \left(\rho_{x}^{2} + \rho_{y}^{2} \right) H_{y} + 2W_{131} \left(H_{x} \rho_{x} + H_{y} \rho_{y} \right) \rho_{y} + 2W_{222} \left(H_{x} \rho_{x} + H_{y} \rho_{y} \right) H_{y} \right) \end{split}$$

And similarly for

$$\varepsilon_{x} = \frac{1}{n'u'} \frac{\delta}{\delta \rho_{x}} W(\vec{H}, \vec{\rho}).$$