SOLUTIONS

Solution of pre-tutorial:

For the same source, the impedance of LHS figure is $Z_1 = 4+j2\omega$,

whereas that of RHS is either $Z_2 = j8\omega L/(8+j\omega L)$ or $Z_2 = 8/(j8\omega C + 1)$.

The circuits are equivalent to each order when the source is subjected to the same impedance i.e. $Z_1 = Z_2$. In the case of an inductor, $4+j2\omega = j8\omega L/(8+j\omega L)$(1)

Cross-multiplication of (1) yields $j8\omega L = 32-2\omega^2 L + j(16\omega + 4\omega L)...$ (2)

Equating real and imaginary part of (2) gives $\omega = 2 \text{ rad/s}$ and L = 4 H.

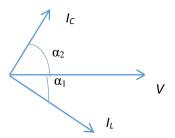
In the case of a capacitor, $4+j2\omega = 8/(j8\omega C+1))....(3)$

Solution of (3) yields a negative value for C.

Therefore, the equivalent circuit will have a sinusoidal source with $\omega = 2$ rad/s and the 8 Ω resistor in parallel with the inductor of 4 H.

Solution of problem 2:

Approximate Phasor diagram can be given as follows:



 $\alpha_1 = \tan^{-1}(\omega L/R_1)$ and $\alpha_2 = \tan^{-1}(1/(\omega R_2 C))$

For the two currents to be in quadrature, $\alpha_1 + \alpha_2 = \pi/2 = \tan^{-1}(\omega L/R_1) + \tan^{-1}(1/(\omega R_2C)) = \pi/2$ (1)

- $\Rightarrow \tan[\tan^{-1}(\omega L/R_1) + \tan^{-1}(1/(\omega R_2 C))] = \tan(\pi/2)$
- $\Rightarrow [(\omega L/R_1) + 1/(\omega R_2 C)] / [1-L/(R_1 R_2 C)] = 1/0$ (2)

Cross-mutiplication and further simplification of (2) gives the condition: $R_1 R_2 = L/C$.

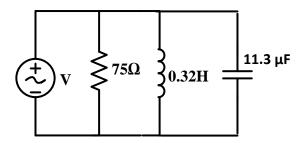
Solution of problem 3:

Given, $\mathbf{V} = 240\sqrt{2} \angle 0^0 = V_m \angle \theta$ and $\mathbf{Z} = (75 \parallel j32\pi) = 48 + j36 = 60 \angle 36.87^0$ (approx.) Then, $\mathbf{I} = \mathbf{V}/\mathbf{Z} = 4\sqrt{2} \angle -36.87^0 = I_m \angle \phi$ and $(\theta - \phi) = 36.87^0$. The power factor is $cos(\theta-\phi) = cos(36.87^{\circ}) = 0.8$ lagging (as the pf angle is +ve)

(1) Real power = P = $(\frac{1}{2})$ V_m I_m cos(θ - ϕ) = $(\frac{1}{2})$ 240 $\sqrt{2}$ x 4 $\sqrt{2}$ x cos(36.87°) = 768 W Also, using RMS values of voltage and current, $P = V_{rms} \times I_{rms} \times \cos(36.87^{\circ}) = 240 \times 4 \times 0.8 = 768 \text{ W}$ Also, $P = V_{rms}^2/R = 240^2/75 = 768 \text{ W}$

(2) Reactive power = Q =
$$V_{rms}^2$$
 / $X_L = V_{rms} x I_{rms} x sin(36.87^0) = 576 VAR$ (Note: $X_L = 100 \Omega$, approx)
Also, reactive power = $P tan(\theta - \phi) = 576 VAR$

In the following circuit, a capacitor of C=11.3 µF is connected in parallel with the source.



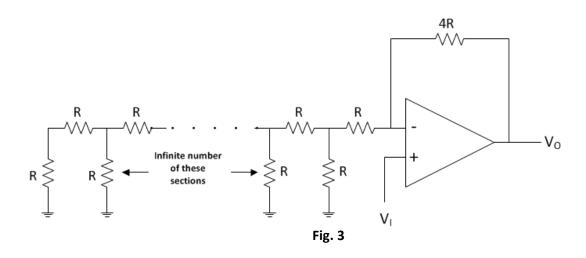
Reactive power of the capacitor, $Qc = -V_{rms}^2/Xc = -204.04 \text{ VAR}$

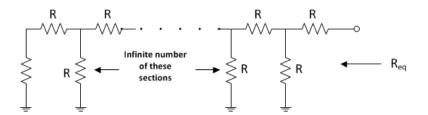
Net reactive power experienced by the source = 576 - 204.04 = 371.96 VAR Net real power experienced by the source = 768 W Using the power triangle,

$$\tan (\theta - \phi) = 371.96/768$$
 => $(\theta - \phi) = 25.842^0$ (pf angle is positive)

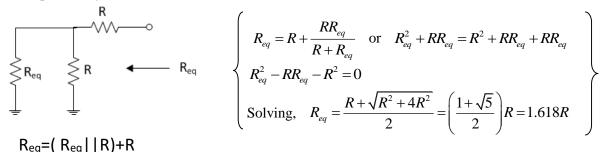
Therefore, power factor = $cos(25.842^{\circ}) = 0.9$ lagging

Solution of problem 4:





or, equivalently



$$\frac{V_I}{R_{ea}} = \frac{V_O - V_I}{4R}$$

$$\frac{V_O}{V_V} = 1 + \frac{4R}{R_{co}} = 1 + \frac{4}{1.618} = 3.472$$
 A_V=3.47

Solution of problem 5:

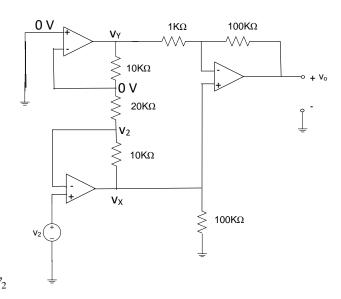
We can solve this circuit directly but it would be interesting to consider an unusual way of solving it through superposition.

Setting v_1 =0 (i.e. grounding that source), the circuit becomes as shown.

$$\frac{v_x - v_2}{10} = \frac{v_2}{20} \implies v_x = 1.5v_2$$

$$\frac{v_y}{10} = -\frac{v_2}{20} \implies v_y = -0.5v_2$$

$$v_o(for \ v_1 = 0) = -100v_y + (1+100)v_x = 201.5v_2$$



Now setting v_2 =0 (i.e. grounding that source), the circuit becomes as shown

$$\frac{v_x}{10} = -\frac{v_1}{20} \qquad \Rightarrow \quad v_x = -0.5v_1$$

$$\frac{v_y - v_1}{10} = \frac{v_1}{20} \implies v_y = 1.5v_1$$

$$v_o = -100v_y + (1+100)v_x = -200.5v_1$$

Combining the two, we get –

$$v_o = -200.5v_1 + 201.5v_2$$

