#### PH 102, Electromagnetism,

Post Mid Semester

Lecture 12

# Electromagnetic Waves in vacuum

Reflection and Transmission at Oblique Incidence

D. J. Griffiths: 9.3

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#### **Electromagnetic Waves in Matter:**

#### Reflection and Transmission at Normal Incidence:

- Suppose, the xy plane forms the boundary between two linear media.
- A plane wave of frequency  $\omega$ , traveling in the z direction and polarized in the x direction, approaches the interface from the left

#### **Incident Wave:**

$$\tilde{\mathbf{E}}_{I}(z,t) = \tilde{E}_{0_{I}}e^{i(k_{1}z-\omega t)}\,\hat{\mathbf{x}},$$

$$\tilde{\mathbf{B}}_{I}(z,t) = \frac{1}{v_{1}}\tilde{E}_{0_{I}}e^{i(k_{1}z-\omega t)}\,\hat{\mathbf{y}}.$$

$$E_{I}$$

$$E_{I}$$

$$E_{I}$$

$$E_{R}$$

$$E_{R}$$

$$E_{R}$$

$$E_{R}$$
Interface

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$$\frac{\mathbf{Reflected Wave:}}{\tilde{\mathbf{E}}_{R}(z,t) = \tilde{E}_{0_{R}}e^{i(-k_{1}z-\omega t)}\,\hat{\mathbf{x}},$$

$$v_{1}$$

$$\tilde{\mathbf{E}}_{R}$$

$$\tilde{\mathbf{E}}_{R}$$

$$\tilde{\mathbf{E}}_{R}(z,t) = -\frac{1}{v_{1}}\tilde{E}_{0_{R}}e^{i(-k_{1}z-\omega t)}\,\mathbf{y},$$
Interface

Note the minus sign in  $\tilde{\mathbf{B}}_R$ 

$$\tilde{\mathbf{B}}(\mathbf{r},t) = \frac{1}{c} \tilde{E}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)} (\hat{\mathbf{k}} \times \hat{\mathbf{n}})$$

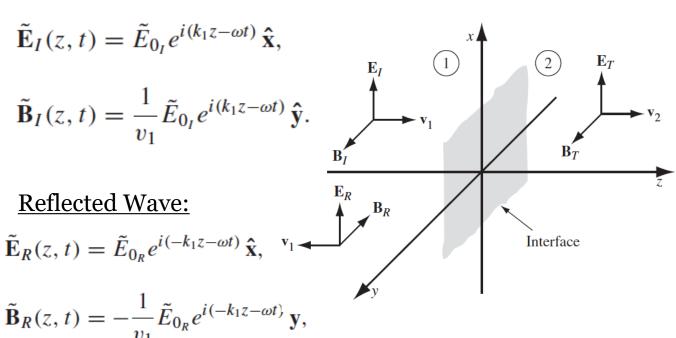
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- A plane wave of frequency  $\omega$ , traveling in the z direction and polarized in the x direction, approaches the interface from the left

#### **Incident Wave:**

#### Transmitted Wave:



$$\mathbf{E}_T(z,t) = E_{0_T} e^{i(\kappa_2 z - \omega t)} \mathbf{x},$$

$$\tilde{\mathbf{E}}_{T}(z,t) = \tilde{E}_{0_{T}} e^{i(k_{2}z - \omega t)} \,\hat{\mathbf{x}},$$

$$\mathbf{v}_{2} \quad \tilde{\mathbf{B}}_{T}(z,t) = \frac{1}{v_{2}} \tilde{E}_{0_{T}} e^{i(k_{2}z - \omega t)} \,\hat{\mathbf{y}},$$

Note the minus sign in  $\tilde{\mathbf{B}}_R$ 

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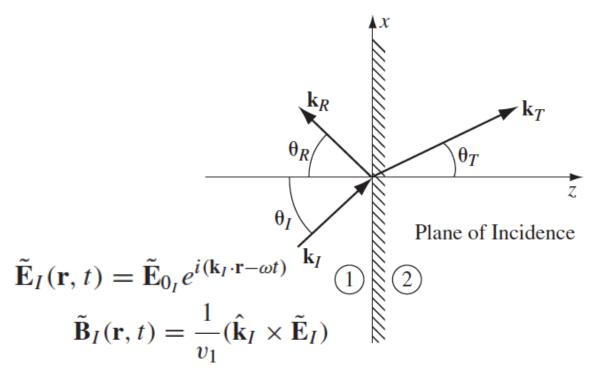
#### **Reflection and Transmission at Oblique Incidence:**

Reflection & Transmission at

Normal Incidence: Incoming wave hits the interface head-on.

Oblique incidence: General case, incoming wave meets the boundary @ angle  $\theta_I$ 

Normal Incidence: Oblique incidence,  $\theta_I = 0$ .



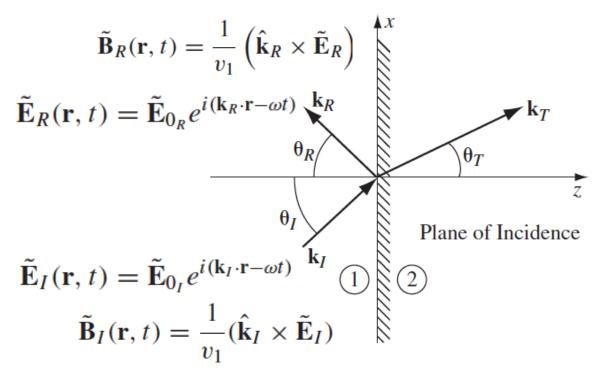
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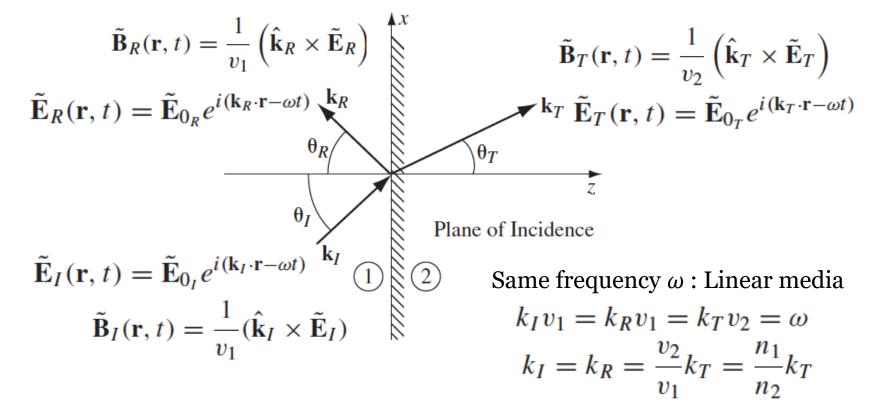
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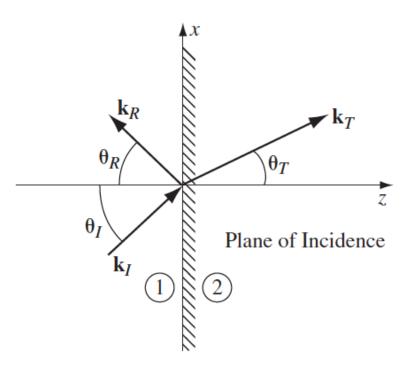
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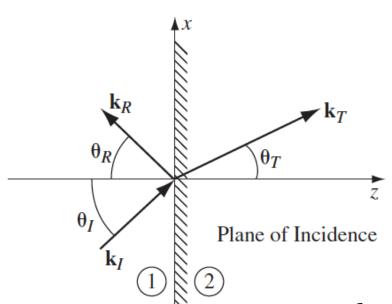
$$\tilde{\mathbf{E}}_I + \tilde{\mathbf{E}}_R \& \tilde{\mathbf{B}}_I + \tilde{\mathbf{B}}_R$$
, joined to  $\tilde{\mathbf{E}}_T + \mathbf{B}_T$  by boundary conditions

(i) 
$$\epsilon_1 E_1^{\perp} = \epsilon_2 E_2^{\perp}$$
, (iii)  $\mathbf{E}_1^{\parallel} = \mathbf{E}_2^{\parallel}$ 

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(ii)  $B_1^{\perp} = B_2^{\perp}$ , (iv)  $\frac{1}{\mu_1} \mathbf{B}_1^{\parallel} = \frac{1}{\mu_2} \mathbf{B}_2^{\parallel}$ .

These all share the generic structure at z = o.

() 
$$\exp[i(\mathbf{k_{I}}\cdot\mathbf{r}-\omega t) + ()\exp[i(\mathbf{k_{R}}\cdot\mathbf{r}-\omega t)]$$
  
= ()  $\exp[i(\mathbf{k_{T}}\cdot\mathbf{r}-\omega t)$ 



$$\tilde{\mathbf{E}}_I + \tilde{\mathbf{E}}_R \& \tilde{\mathbf{B}}_I + \tilde{\mathbf{B}}_R$$
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These all share the generic structure at z = o.

$$() \exp[i (\mathbf{k_{I} \cdot r} - \omega t) + () \exp[i (\mathbf{k_{R} \cdot r} - \omega t)]]$$

$$= () \exp[i (\mathbf{k_{T} \cdot r} - \omega t)]$$

- x, y & t dependence is confined to the exponents
- The boundary conditions hold at *all* points on the plane, and for *all* times,
  - Thus the exponential factors must be equal

$$\mathbf{k}_I \cdot \mathbf{r} = \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}$$
, when  $z = 0$ ,

$$\mathbf{k}_I \cdot \mathbf{r} = \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}$$
, when  $z = 0$ ,

and for all x and all y.

$$x(k_I)_x + y(k_I)_y = x(k_R)_x + y(k_R)_y = x(k_T)_x + y(k_T)_y$$

Holds: only if the components are separately equal,

For 
$$x = 0$$
, we get,

while 
$$y = 0$$
, gives

$$(k_{\rm I})_{\rm y} = (k_{\rm R})_{\rm y} = (k_{\rm T})_{\rm y},$$

$$(k_{\rm I})_{x} = (k_{R})_{x} = (k_{T})_{x},$$

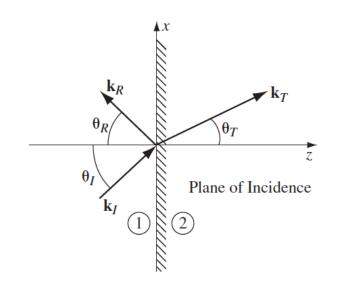
$$\mathbf{k}_I \cdot \mathbf{r} = \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}$$
, when  $z = 0$ ,

Holds: only if the components are separately equal,

$$(k_{\rm I})_{\rm y} = (k_{\rm R})_{\rm y} = (k_{\rm T})_{\rm y}$$

One can orient the axes such that  $\mathbf{k}_{I}$  lies in the xz plane (i.e.  $(k_{I})_{v} = 0$ );

 $\mathbf{k}_{\mathbf{R}}$  and  $\mathbf{k}_{\mathbf{T}}$  also lies in the same plane  $((k_{\mathbf{I}})_{\mathbf{y}} = (k_{\mathbf{R}})_{\mathbf{y}} = (k_{\mathbf{T}})_{\mathbf{y}} = \mathbf{0}).$ 



**First Law:** The incident, reflected, and transmitted wave vectors form a plane (plane of incidence), which also includes the normal to the surface (here, z axis).

$$\mathbf{k}_I \cdot \mathbf{r} = \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}$$
, when  $z = 0$ ,

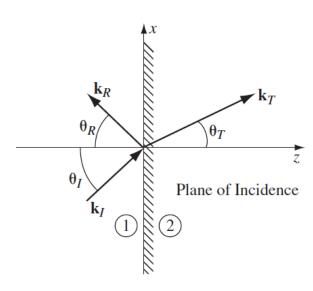
Holds: only if the components are separately equal,

$$(k_{\rm I})_{x} = (k_{R})_{x} = (k_{T})_{x}$$

Now,  $k_I \sin \theta_I = k_R \sin \theta_R = k_T \sin \theta_T$ ,

 $\theta_I$ ,  $\theta_R \& \theta_T$ , are the angle of incidence, reflection & transmission (refraction) respectively. and measured with respect to the normal..

$$k_I \sin \theta_I = k_R \sin \theta_R$$



$$k_I = k_R = \frac{v_2}{v_1} k_T = \frac{n_1}{n_2} k_T$$

**Second Law:** The angle of incidence is equal to the angle reflection,

$$\theta_{I} = \theta_{R}$$
. (law of reflection)

$$\mathbf{k}_I \cdot \mathbf{r} = \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}$$
, when  $z = 0$ ,

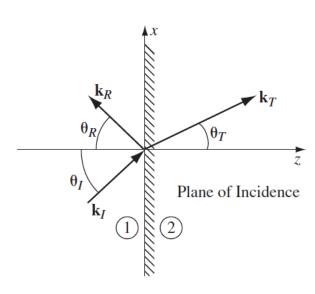
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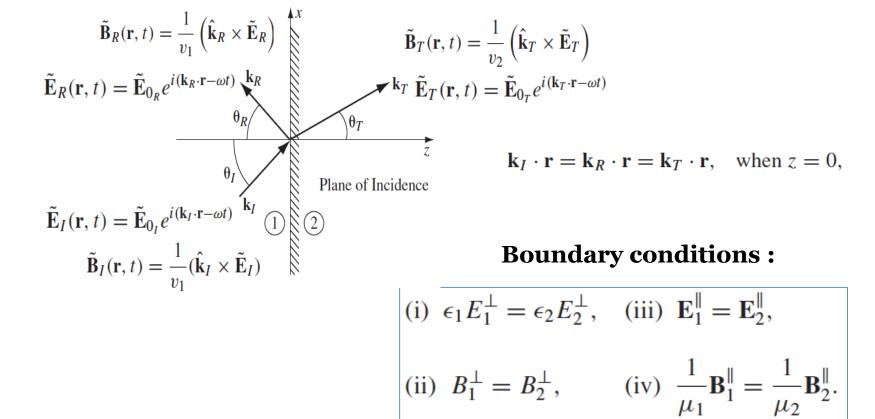
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$$k_R \sin \theta_R = k_T \sin \theta_T$$

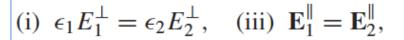


$$k_I = k_R = \frac{v_2}{v_1} k_T = \frac{n_1}{n_2} k_T$$

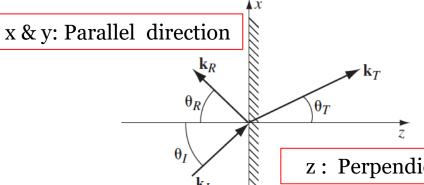
Third Law: 
$$\frac{\sin \theta_T}{\sin \theta_I} = \frac{n_1}{n_2}$$
. (law of refraction/Snell's Law)



It is only Amplitudes + Exponentials cancelled,



(ii) 
$$B_1^{\perp} = B_2^{\perp}$$
, (iv)  $\frac{1}{\mu_1} \mathbf{B}_1^{\parallel} = \frac{1}{\mu_2} \mathbf{B}_2^{\parallel}$ .



z : Perpendicular direction

#### **Boundary conditions:**

(i) 
$$\epsilon_1 \left( \tilde{\mathbf{E}}_{0_I} + \tilde{\mathbf{E}}_{0_R} \right)_{\tau} = \epsilon_2 \left( \tilde{\mathbf{E}}_{0_T} \right)_{\tau}$$
 (iii)  $\left( \tilde{\mathbf{E}}_{0_I} + \tilde{\mathbf{E}}_{0_R} \right)_{x,y} = \left( \tilde{\mathbf{E}}_{0_T} \right)_{x,y}$ 

(ii) 
$$\left(\tilde{\mathbf{B}}_{0_I} + \tilde{\mathbf{B}}_{0_R}\right)_z = \left(\tilde{\mathbf{B}}_{0_T}\right)_z$$
 (iv)  $\frac{1}{\mu_1} \left(\tilde{\mathbf{B}}_{0_I} + \tilde{\mathbf{B}}_{0_R}\right)_{x,y} = \frac{1}{\mu_2} \left(\tilde{\mathbf{B}}_{0_T}\right)_{x,y}$ 

Here,  $\tilde{\mathbf{B}}_0 = (1/v)\hat{\mathbf{k}} \times \tilde{\mathbf{E}}_0$  and (iii)/(iv) are pairs of eqs, for x & y component.

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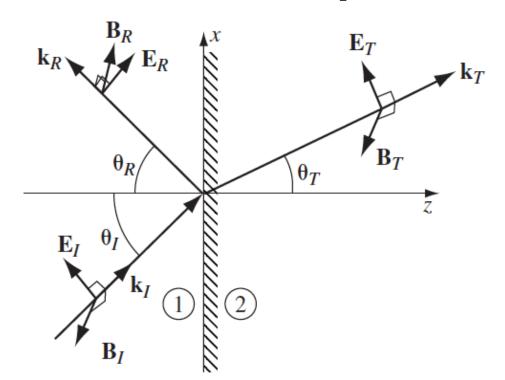
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#### Polarization of the incident wave is parallel to the plane of incidence ( $E_I$ confined in xz plane)

The reflected and transmitted waves are also polarized in this plane



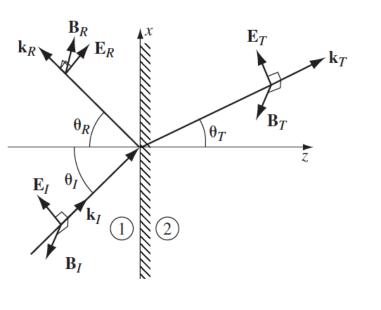
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(i) 
$$\epsilon_1 \left( -\tilde{E}_{0_I} \sin \theta_I + \tilde{E}_{0_R} \sin \theta_R \right) = \epsilon_2 \left( -\tilde{E}_{0_T} \sin \theta_T \right)$$

(ii) No z-component for 
$$\boldsymbol{B}$$

(iii) 
$$\tilde{E}_{0_I} \cos \theta_I + \tilde{E}_{0_R} \cos \theta_R = \tilde{E}_{0_T} \cos \theta_T$$
 No y-comp

(iv) 
$$\frac{1}{\mu_1 v_1} \left( \tilde{E}_{0_I} - \tilde{E}_{0_R} \right) = \frac{1}{\mu_2 v_2} \tilde{E}_{0_T}$$
 No x-comp

# **Boundary** conditions:

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 $\tilde{E}_{0_I} - \tilde{E}_{0_R} = \beta \tilde{E}_{0_T}$ 

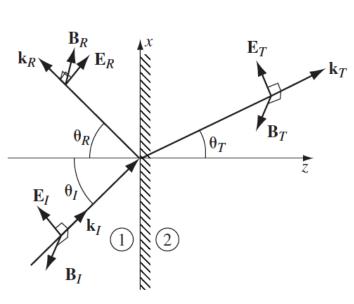
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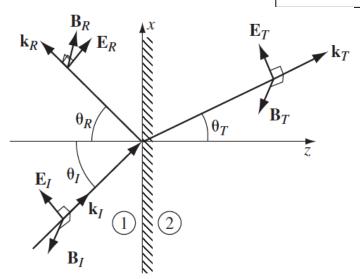
$$\beta \equiv \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1}$$

(iii) 
$$\tilde{E}_{0_I} \cos \theta_I + \tilde{E}_{0_R} \cos \theta_R = \tilde{E}_{0_T} \cos \theta_T$$

$$\tilde{E}_{0_I} + \tilde{E}_{0_R} = \alpha \tilde{E}_{0_T}$$
  $\alpha \equiv \frac{\cos \theta_T}{\cos \theta_I}$ 

(iv) 
$$\frac{1}{\mu_1 v_1} \left( \tilde{E}_{0_I} - \tilde{E}_{0_R} \right) = \frac{1}{\mu_2 v_2} \tilde{E}_{0_T}$$
  
 $\tilde{E}_{0_I} - \tilde{E}_{0_R} = \beta \tilde{E}_{0_T}$ 





$$\tilde{E}_{0_I} - \tilde{E}_{0_R} = \beta \tilde{E}_{0_T} \qquad \qquad \tilde{E}_{0_I} + \tilde{E}_{0_R} = \alpha \tilde{E}_{0_T}$$

$$\tilde{E}_{0_I} + \tilde{E}_{0_R} = \alpha \tilde{E}_{0_T}$$

$$\tilde{E}_{0_R} = \left(\frac{\alpha - \beta}{\alpha + \beta}\right) \tilde{E}_{0_I}, \quad \tilde{E}_{0_T} = \left(\frac{2}{\alpha + \beta}\right) \tilde{E}_{0_I}.$$

**Fresnel's equations**, for the case of polarization in the plane of incidence.

- Transmitted wave is in phase with the incident one.
- Reflected wave is either in phase,  $\alpha > \beta$  or 180° out of phase, if  $\alpha < \beta$ .
- $\cos \theta_T$ Amplitudes of the transmitted & reflected waves depend on the  $\theta_I$ , as  $\alpha \equiv$  $\cos \theta_I$

$$\alpha = \frac{\sqrt{1 - \sin^2 \theta_T}}{\cos \theta_I} = \frac{\sqrt{1 - [(n_1/n_2)\sin \theta_I]^2}}{\cos \theta_I}.$$

Normal incidence ( $\theta_I = 0$ ),  $\alpha = 1$ .

Grazing incidence ( $\theta_I = 90^{\circ}$ ),  $\alpha$  diverges, the wave is totally reflected.

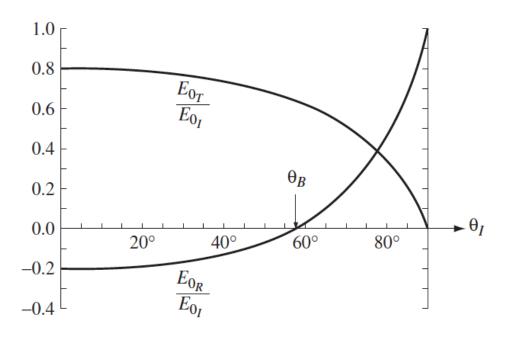
#### **Brewster's Angle:**

$$\tilde{E}_{0_R} = \left(\frac{\alpha - \beta}{\alpha + \beta}\right) \tilde{E}_{0_I}$$

Intermediate angle,  $\theta_B$  (Brewster's angle ).

Reflected wave is completely extinguished,  $\alpha = \beta$ , or  $\sin^2 \theta_B = \frac{1 - \beta^2}{(n_1/n_2)^2 - \beta^2}$ .

For 
$$\mu_1 \cong \mu_2$$
, so  $\beta \cong n_2/n_1$ ,  $\sin^2 \theta_B \cong \beta^2/(1+\beta^2)$ ,  $\tan \theta_B \cong \frac{n_2}{n_1}$ 



Transmitted and reflected amplitudes as functions of  $\theta_I$ , for light incident on glass (n<sub>2</sub>=1. 5) from air (n<sub>1</sub>=1)

-ve ratio: 180 degree out of phase, Absolute value for amplitude

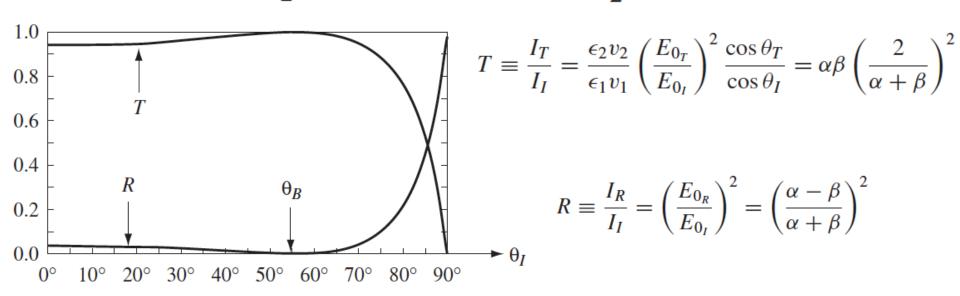
The power per unit area striking the **interface** is **S.z**̂.

Thus the incident intensity is,  $I_I = \frac{1}{2} \epsilon_1 v_1 E_{0_I}^2 \cos \theta_I$ 

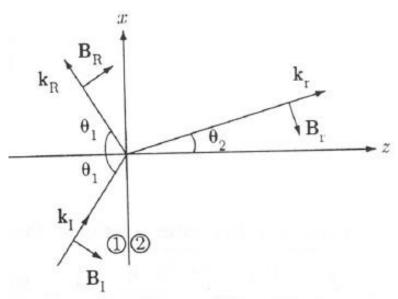
@ Interface, giving the cosθ

The reflected and transmitted intensities are

$$I_R = \frac{1}{2} \epsilon_1 v_1 E_{0_R}^2 \cos \theta_R$$
 and  $I_T = \frac{1}{2} \epsilon_2 v_2 E_{0_T}^2 \cos \theta_T$ 



**Problem 9.17** Analyze the case of polarization *perpendicular* to the plane of incidence (i.e. electric fields in the y direction, in Fig. 9.15). Impose the boundary conditions (Eq. 9.101), and obtain the Fresnel equations for  $\tilde{E}_{0_R}$  and  $\tilde{E}_{0_T}$ . Sketch  $(\tilde{E}_{0_R}/\tilde{E}_{0_I})$  and  $(\tilde{E}_{0_T}/\tilde{E}_{0_I})$  as functions of  $\theta_I$ , for the case  $\beta = n_2/n_1 = 1.5$ . (Note that for this  $\beta$  the reflected wave is *always* 180° out of phase.) Show that there is no Brewster's angle for *any*  $n_1$  and  $n_2$ :  $\tilde{E}_{0_R}$  is *never* zero (unless, of course,  $n_1 = n_2$  and  $\mu_1 = \mu_2$ , in which case the two media are optically indistinguishable). Confirm that your Fresnel equations reduce to the proper forms at normal incidence. Compute the reflection and transmission coefficients, and check that they add up to 1.



(i) 
$$\epsilon_1 E_1^{\perp} = \epsilon_2 E_2^{\perp}$$
, (iii)  $\mathbf{E}_1^{\parallel} = \mathbf{E}_2^{\parallel}$ ,

(ii) 
$$B_1^{\perp} = B_2^{\perp}$$
, (iv)  $\frac{1}{\mu_1} \mathbf{B}_1^{\parallel} = \frac{1}{\mu_2} \mathbf{B}_2^{\parallel}$ .

$$\tilde{\mathbf{E}}_{R} = \tilde{E}_{0_{R}} e^{i(\mathbf{k}_{R} \cdot \mathbf{r} - \omega t)} \hat{\mathbf{y}},$$

$$\tilde{\mathbf{B}}_{R} = \frac{1}{v_{1}} \tilde{E}_{0_{R}} e^{i(\mathbf{k}_{R} \cdot \mathbf{r} - \omega t)} (\cos \theta_{1} \hat{\mathbf{x}} + \sin \theta_{1} \hat{\mathbf{z}});$$

$$\tilde{\mathbf{E}}_{T} = \tilde{E}_{0_{T}} e^{i(\mathbf{k}_{T} \cdot \mathbf{r} - \omega t)} \hat{\mathbf{y}},$$

$$\tilde{\mathbf{B}}_{T} = \frac{1}{v_{2}} \tilde{E}_{0_{T}} e^{i(\mathbf{k}_{T} \cdot \mathbf{r} - \omega t)} (-\cos \theta_{2} \hat{\mathbf{x}} + \sin \theta_{2} \hat{\mathbf{z}})$$

$$\begin{split} \tilde{\mathbf{E}}_{I} &= \tilde{E}_{0_{I}} e^{i(\mathbf{k}_{I} \cdot \mathbf{r} - \omega t)} \hat{\mathbf{y}}, \\ \tilde{\mathbf{B}}_{I} &= \frac{1}{v_{1}} \tilde{E}_{0_{I}} e^{i(\mathbf{k}_{I} \cdot \mathbf{r} - \omega t)} (-\cos \theta_{1} \, \hat{\mathbf{x}} + \sin \theta_{1} \, \hat{\mathbf{z}}); \end{split}$$

$$ilde{\mathbf{B}}_{I} = rac{1}{m} ilde{E}_{0_{I}} e^{i(\mathbf{k}_{I}\cdot\mathbf{r}-\omega t)} (-\cos heta_{1}\,\hat{\mathbf{x}}+\sin heta_{1}\,\hat{\mathbf{z}})$$

$$\frac{\sin \theta_2}{\sin \theta_1} = \frac{v_2}{v_1}.$$
 [Note:  $\mathbf{k}_I \cdot \mathbf{r} - \omega t = \mathbf{k}_R \cdot \mathbf{r} - \omega t = \mathbf{k}_T \cdot \mathbf{r} - \omega t$ , at  $z = 0$ ]

## **Boundary** conditions:

(i) Trivial

(ii) & (iii) 
$$ilde{E}_{0_I} + ilde{E}_{0_R} = ilde{E}_{0_T}$$

(iv) 
$$\tilde{E}_{0_I} - \tilde{E}_{0_R} = \alpha \beta \tilde{E}_{0_T}$$

$$\alpha \equiv \frac{\cos \theta_2}{\cos \theta_1}; \ \beta \equiv \frac{\mu_1 v_1}{\mu_2 v_2}$$

$$\tilde{E}_{0_T} = \left(\frac{2}{1 + \alpha\beta}\right) \tilde{E}_{0_I}$$

In phase,  $\alpha\beta > o$ 

$$E_{0_T} = \left(\frac{2}{1 + \alpha\beta}\right) E_{0_I}$$

$$\tilde{E}_{0_R} = \left(\frac{1 - \alpha\beta}{1 + \alpha\beta}\right) \tilde{E}_{0_I}$$

in phase for  $\alpha\beta < 1$ 

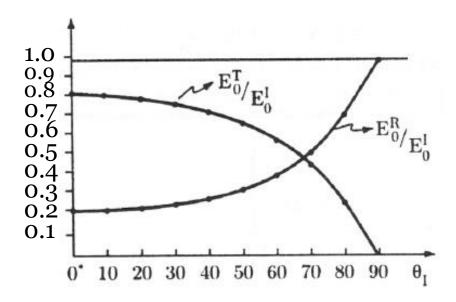
$$E_{0_R} = \left| \frac{1 - \alpha \beta}{1 + \alpha \beta} \right| E_{0_I}$$

Fresnel equations for polarization perpendicular to the plane of incidence.

Now,

$$\alpha\beta = \beta \frac{\sqrt{1 - \sin^2 \theta / \beta^2}}{\cos \theta} = \frac{\sqrt{\beta^2 - \sin^2 \theta}}{\cos \theta}$$
,  $\theta$  is the angle of incidence!

$$\beta = 1.5, \ \alpha\beta = \frac{\sqrt{2.25 - \sin^2 \theta}}{\cos \theta}$$



Brewster's angle:  $E_{0_R} = 0$  would mean that  $\alpha\beta = 1$ 

$$\alpha = \frac{\sqrt{1 - (v_2/v_1)^2 \sin^2 \theta}}{\cos \theta} = \frac{1}{\beta} = \frac{\mu_2 v_2}{\mu_1 v_1}$$

or, 
$$1 - \left(\frac{v_2}{v_1}\right)^2 \sin^2 \theta = \left(\frac{\mu_2 v_2}{\mu_1 v_1}\right)^2 \cos^2 \theta$$

or, 
$$1 = \left(\frac{v_2}{v_1}\right)^2 \left[\sin^2\theta + (\mu_2/\mu_1)^2 \cos^2\theta\right]$$

$$\mu_1 pprox \mu_2$$
 , would mean  $1 pprox (v_2/v_1)^2$ 

i.e. optically indistinguishable media!

[find angle if  $\mu$ 's are not same]

#### Fresnel's equations:

$$E_{0_T} = \left(\frac{2}{1 + \alpha\beta}\right) E_{0_I} \quad E_{0_R} = \left|\frac{1 - \alpha\beta}{1 + \alpha\beta}\right| E_{0_I}$$

At normal incidence,  $\alpha = 1$ ,

$$E_{0_T} = \left(\frac{2}{1+\beta}\right) E_{0_I} \qquad E_{0_R} = \left|\frac{1-\beta}{1+\beta}\right| E_{0_I}$$

The reflection and transmission coefficients:

$$R = \left(\frac{E_{0_R}}{E_{0_I}}\right)^2 = \left(\frac{1 - \alpha\beta}{1 + \alpha\beta}\right)^2$$

$$R + T = 1$$

$$T = \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \alpha \left(\frac{E_{0_T}}{E_{0_T}}\right)^2 = \alpha\beta \left(\frac{2}{1 + \alpha\beta}\right)^2$$