

TUTORIAL-5

PRE-TUTORIAL ASSIGNMENT- SOLUTION

Solution-1:

$$V_{BB} = \left(\frac{50}{100 + 50} \right) 15 = 5V, R_B = R_1 \parallel R_2 = 33.33K\Omega$$

This transistor obviously cannot be in saturation because in that case V_E will be 14.9 V which would make $V_B=15.6$ V which certainly cannot happen with a +15V supply!

If the transistor is in the active region –

$$V_{BB} - 0.7 = I_B R_B + (\beta + 1) I_B R_E$$

$$4.3 = I_B (33.33 + 101 \times 5) \Rightarrow I_B = 0.008 \text{ mA}$$

$$I_E = 0.808 \text{ mA} \Rightarrow I_C = 0.8 \text{ mA}$$

$$V_E = 4.04 \text{ V}, V_B = 4.74 \text{ V}$$

Since $V_C = 15 \text{ V}$, $V_{CE} = 10.96 \text{ V}$ and the transistor is confirmed to be in the active region as the B-C junction is reverse biased.

Therefore, Q-Point is $V_{CE}=10.96 \text{ V}$, $I_C=0.8 \text{ mA}$, $I_B=0.008 \text{ mA}$

and
$$r_e = \frac{V_T}{I_E} = 0.032 \text{ K}\Omega$$

Solution-2:

The period of the waveform is $T = 4$ sec. Over a period, the voltage waveform can be written as

$$v(t) = -5t, 0 \leq t < 2 \quad \text{and} \quad v(t) = 10, 2 \leq t < 4$$

The RMS voltage is

$$V_{\text{rms}} = \sqrt{\frac{1}{T} \int_0^T v^2(t) dt} = \sqrt{\frac{1}{4} \left[\int_0^2 (-5t)^2 dt + \int_2^4 10^2 dt \right]} = \sqrt{\frac{1}{4} \left[\frac{25t^3}{3} \Big|_0^2 + 100t \Big|_2^4 \right]} = 8.165 \text{ V}$$

The power absorbed by the resistor = $V_{\text{rms}}^2 / 2 = 33.33 \text{ W}$

TUTORIAL-5: SOLUTIONS

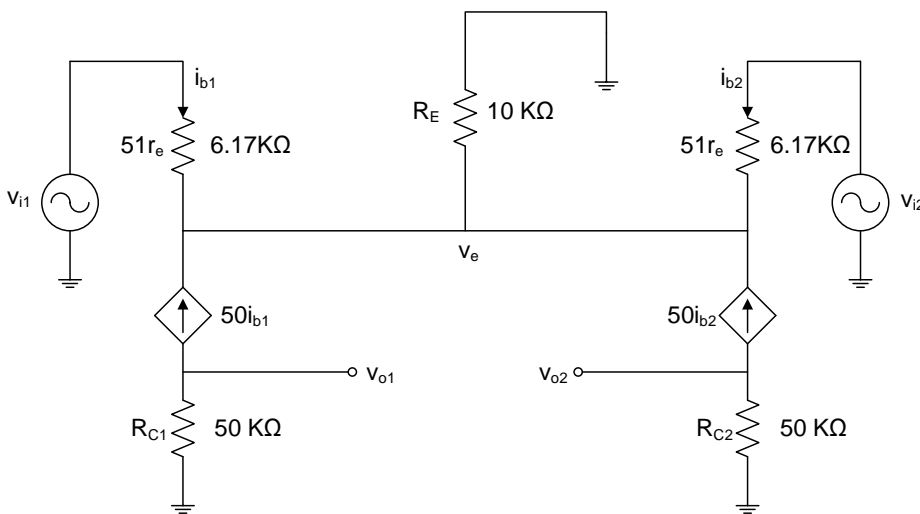
Solution-1:

(a) Since the two transistors are identical, $I_{E1} = I_{E2} = 0.5I_{RE} = 0.5[5-0.7]/10 = 0.215 \text{ mA}$
Therefore, assuming transistors are in the active region, we have

$$\begin{aligned} I_{B1} = I_{B2} &= 0.215/51 = 0.004216 \text{ mA} & \text{and} & & I_{C1} = I_{C2} &= 0.211 \text{ mA} \\ V_{C1} = V_{C2} &= 12 - 0.211(50) = 1.461 \text{ V} & & & V_{B1} = V_{B2} &= 0 \text{ V} \quad V_{E1} = V_{E2} = -0.7 \text{ V} \\ V_{CE1} = V_{CE2} &= 1.461 - (-0.7) = 2.161 \text{ V} \end{aligned}$$

Note that $V_{BC1} = V_{BC2} = -1.461 \text{ V}$ implying that the B-C junction is reverse biased. Since the B-E junction is forward biased, the transistor is operating in the active region.

(b) For both transistors, $r_e = 26/0.215 = 121 \Omega$. Using this, the overall equivalent circuit for AC analysis may be drawn as follows.



$$i_{b1} = \frac{v_{i1} - v_e}{6.17} \quad i_{b2} = \frac{v_{i2} - v_e}{6.17}$$

At the output,

$$v_{o1} = -50i_{b1}R_{C1} = -2500i_{b1} \quad v_{o2} = -50i_{b2}R_{C2} = -2500i_{b2}$$

$$v_{o1} - v_{o2} = -2500(i_{b1} - i_{b2}) = -405.3(v_{i1} - v_{i2})$$

$$\text{Therefore, } A_v = \frac{v_{o1} - v_{o2}}{v_{i1} - v_{i2}} = -405.3$$

Solution-2:

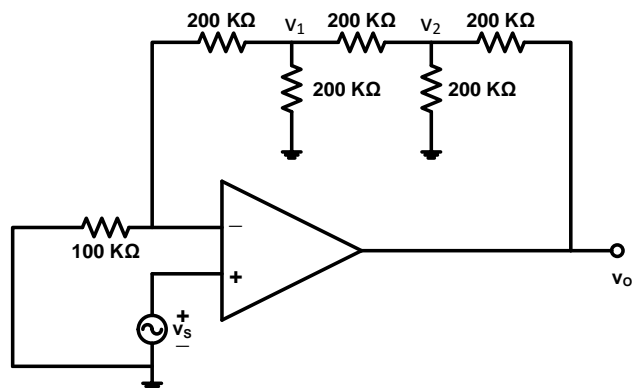
Note that $v_- = v_+ = v_s$

$$\frac{v_1 - v_s}{200} = \frac{v_s}{100} \Rightarrow v_1 = 3v_s$$

$$\frac{v_2 - v_1}{200} = \frac{v_1}{200} + \frac{v_s}{100} \Rightarrow v_2 = 2v_1 + 2v_s = 8v_s$$

$$\frac{v_o - v_2}{200} = \frac{v_2}{200} + \frac{v_2 - v_1}{200} \Rightarrow v_o = 3v_2 - v_1$$

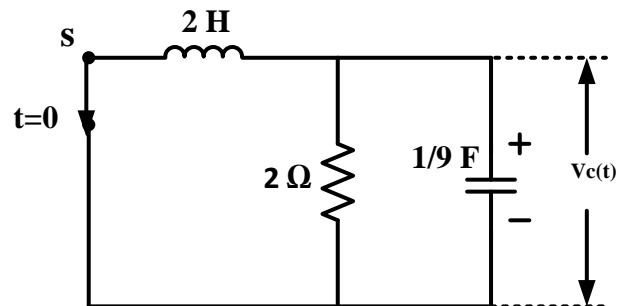
$$\Rightarrow v_o = 21v_s \quad \text{Gain} = A_v = 21$$



Solution-3:

The inductor is short-circuited and capacitor open-circuited in steady state for $t < 0$. Then, using continuity principle $i_L(0^-) = i_L(0^+) = 10$ A and $v_C(0^-) = v_C(0^+) = 20$ V.

When the switch is connected to the position '2', the circuit diagram becomes:



KCL at the top central node yields $v_C(t)/R + C dv_C(t)/dt + i_L = 0$ (1)

Since $v_C(t) = L di_L/dt$, then (1) can be written as

$$(L/R) di_L/dt + LC d^2i_L/dt^2 + i_L = 0 \text{(2)}$$

$$\Rightarrow d^2i_L/dt^2 + 1/(RC) di_L/dt + 1/(LC) i_L = 0 \text{(3)}$$

$$\Rightarrow d^2i_L/dt^2 + 4.5 di_L/dt + 4.5 i_L = 0 \text{(4)}$$

Characteristic equation of (4) gives the distinct real roots

$$r_1 = (-4.5 + \sqrt{(4.5^2 - 4 \times 4.5)})/2 = -1.5 \text{ and } r_2 = (-4.5 - \sqrt{(4.5^2 - 4 \times 4.5)})/2 = -3$$

Since the RLC circuit has no source and the roots are real and distinct, $i_L(t) = A_1 e^{(-1.5t)} + A_2 e^{(-3t)}$ (5)

Using the initial condition $i_L(0^+) = 10$ and (5), we get $A_1 + A_2 = 10$ (6)

Also, $v_C(t) = L di_L(t)/dt = -3A_1 e^{(-1.5t)} - 6A_2 e^{(-3t)}$.

Then, setting $t = 0^+$ in the above expression one gets

$$L di_L(0^+)/dt = -3A_1 - 6A_2 = v_C(0^+) \text{(7)}$$

Using the initial condition $v_C(0^+) = 20$ and (7), we get $-3A_1 - 6A_2 = 20$ (8)

Simultaneous solution of (6) and (8) yields $A_1 = 26.66$ and $A_2 = -16.66$.

Then, expression for $v_C(t)$ becomes

$$v_C(t) = -80 e^{(-1.5t)} + 100 e^{(-3t)} \text{ V (approx.)}$$

Solution-4:

Source in phasor form is $V_s = 100 \angle 53.13^\circ$

Impedance seen by the source = $Z = 3.33 \parallel j1.43 \parallel (-j3.33) = 1.2 + j1.6 = 2 \angle 53.13^\circ$ (approx.)

Source current = $I = V_s/Z = 50 \angle 0^\circ$

$$I_R = V_s/3.33 = 30 \angle 53.13^\circ$$

$$I_L = V_s / (j1.43) = 69.93 \angle -36.87^\circ$$

$$I_C = jV_s/3.33 = 30 \angle 143.13^\circ$$

The current phasor diagram is shown below:

