

## UNIT-II BJT

NPN and PNP Configurations and their characteristics, Early Effect, current Equations, input and output characteristics of CE, CB, CC, h-parameter model, Hybrid - II model, Ebers' moll model.

### 2.1 INTRODUCTION:-

A Bipolar Junction Transistor (BJT) is a three terminal Semiconductor device in which the operation depends on the interaction of both majority and minority carriers and hence the name Bipolar. The BJT is analogous to the vacuum triode and its comparative size is small in size. It is used in amplifier and oscillator circuits and as a switch in digital circuits. It has wide applications in computers, satellites and other modern communication systems.

In Shortly:-

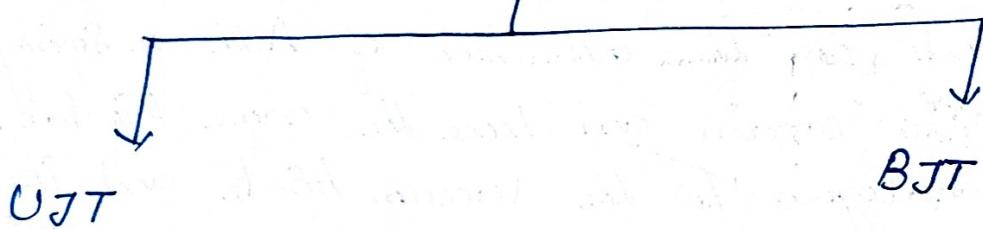
- \* Transistor is a three terminal device : Base, emitter and collector.
- \* It can be operated in three configurations : Common Base (CB), Common Collector (CC), Common Emitter (CE)
- \* According to configurations, it can be used for voltage as well as current amplification.
- \* Amplification in the transistor is achieved by passing input current signal from a region of low resistance to a region of high resistance.

\* This concept of transfer of resistance "Transfer - Resistor" = Transistor.

## 2.2 TYPES OF TRANSISTORS :-

According to the charge carriers of current conduction, Transistor is classified into two types.

Transistors [Based on charge carriers].



### 1. UJT :-

- Unipolar Junction Transistor
- The current conduction is only due to one type of charge carriers. (i.e) majority charge carriers.

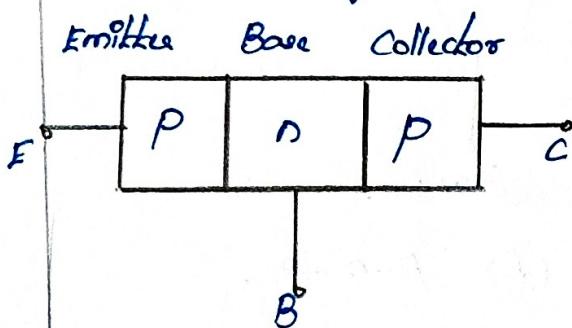
### 2. BJT :-

- Bipolar Junction Transistor.
- The current conduction is due to both type of charge carriers i.e holes and electrons.
- Output current is controlled by input current and hence it is a "Current Controlled Device"

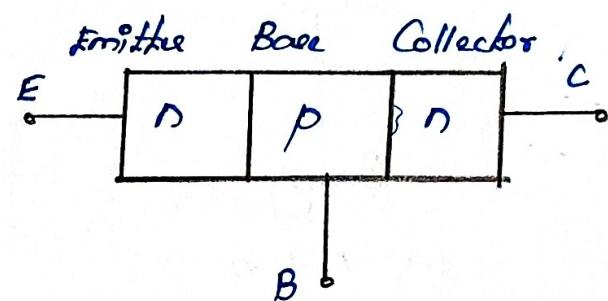
### 2.3 BJT - CONSTRUCTION :-

→ According to the arrangement of materials P, N type materials. BJT can be classified into types of two.

1. NPN type



2. PNP type.



PNP type

NPN type.

→ NPN Transistor is formed by sandwiching a single P-region between two N-regions.

→ PNP Transistor is formed by sandwiching a single N-region between two P-regions.

→ There are three terminals in both NPN and PNP transistors are :-

1) Base

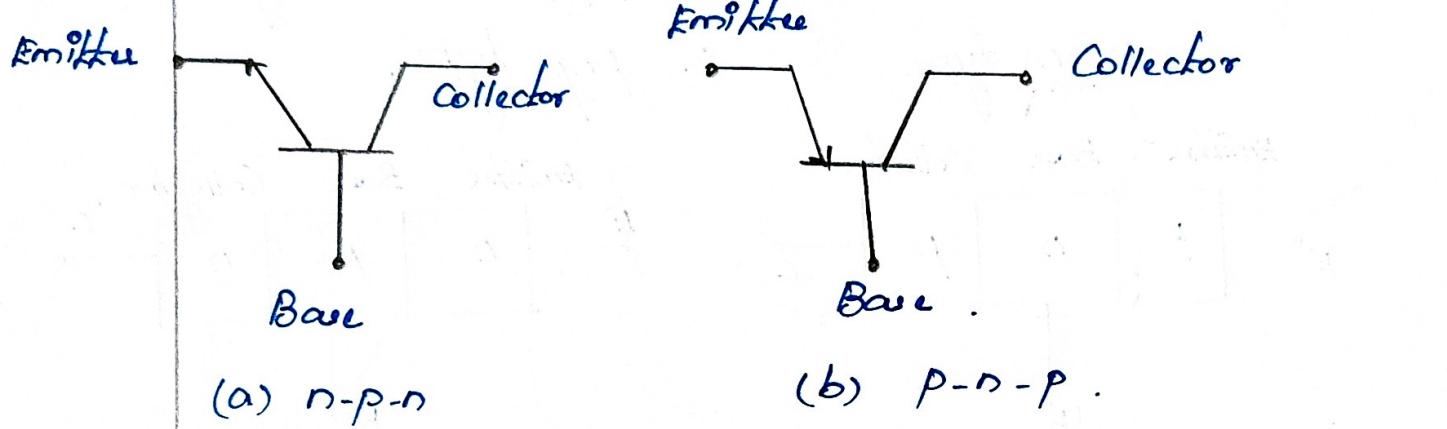
2) Emitter

3) Collector

→ Middle region is base, which is very thin and lightly doped.

→ Emitter and collector regions are heavily doped. But the doping level in emitter is slightly greater than that of collector. So collector is moderately doped.

## 2.3.1 TRANSISTOR SYMBOLS:



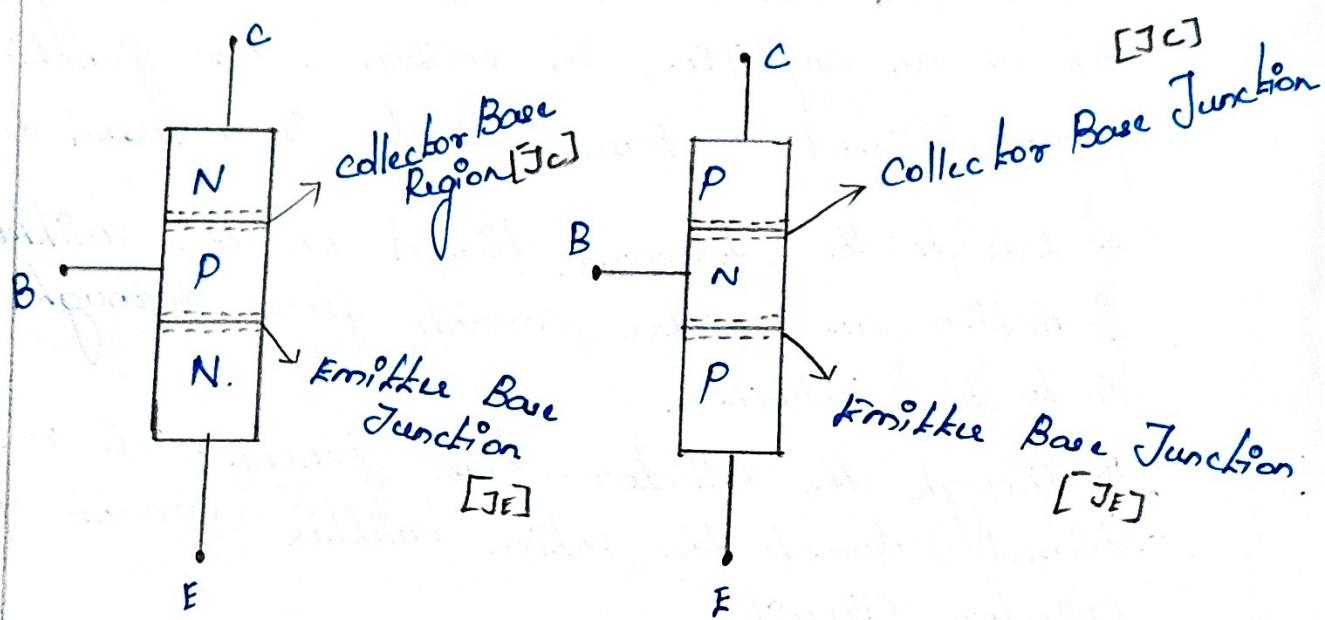
→ The arrow on the emitter indicates the conventional current which is opposite to the direction of electron current in emitter (or) the direction of current flow when the emitter base junction is forward biased.

→ Emitter is heavily doped so that it can inject a large number of charge carriers in to the base.

→ Base is very thin and also lightly doped. It passes most of the injected charge carriers from the emitter in to the collector.

→ collector is moderately doped.

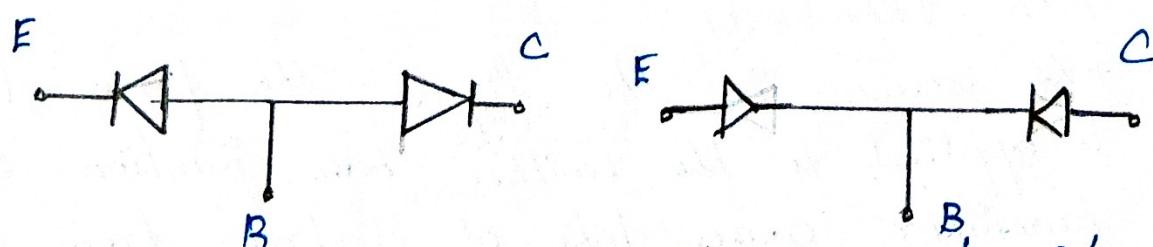
### 2.3.2 JUNCTIONS OF TRANSISTORS :-



- A BJT has two PN Junctions.
- One Junction is between emitter and base is called as emitter base junction (or) Emitter Junction (JE).
- Another Junction is between collector and base is called as collector base junction (or) collector Junction (JC).

### 2.3.3 DIODE EQUIVALENT STRUCTURE OF TRANSISTOR :-

A transistor can be considered as 2 P-N Junction diodes connected as back to back manner.



(a) n-p-n transistor. (b) p-n-p transistor.  
Two-diode transistor analogy.

## 2.3.4 TRANSISTOR BIASING:-

- To bias the transistor in its active region to act as an amplifier, the emitter - base junction is forward biased & Base - collector is reverse biased.
- Due to the forward biased on the emitter base junction an emitter current flows through the base in to the collector.
- Though the collector - base junction is reverse biased almost the entire emitter current flows the collector circuit.

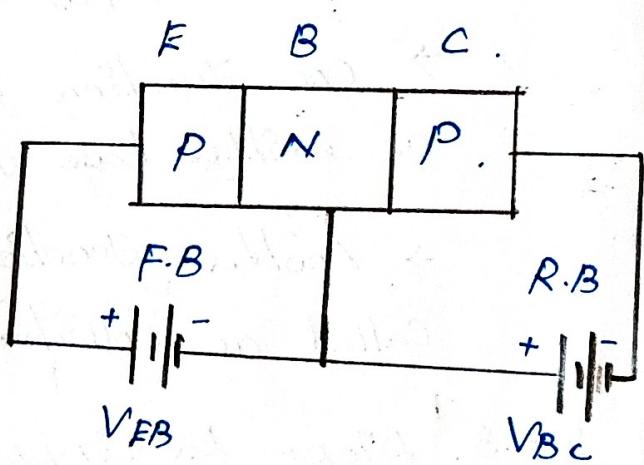
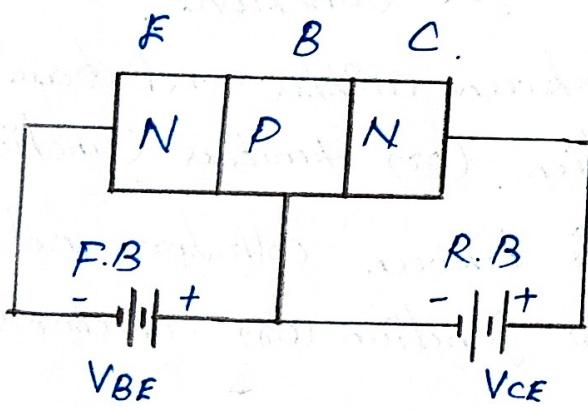


Fig - Transistor biasing (a) NPN Transistor  
(b) PNP Transistor

## 2.3.5 OPERATIONS OF TRANSISTORS:-

### NPN TRANSISTOR:-

- As shown in the figure, the forward bias is applied to the emitter base junction of an NPN transistor causes lots of electrons from emitter region to crossover to the base region.

(A)

→ As the base is lightly doped with p-type impurities, the number of holes in the base region is very small and hence the number of electrons that combines with holes in the p-type base region is also very small.

→ Hence a few electrons combine with holes to constitute a base current  $I_B$ . The remaining electrons (more than 95%) crossover into the collector region to constitute a collector current  $I_E$ .  $I_C$ .

→ Thus the base and collector currents summed up give the emitter current. i.e.

$$I_E = - (I_C + I_B)$$

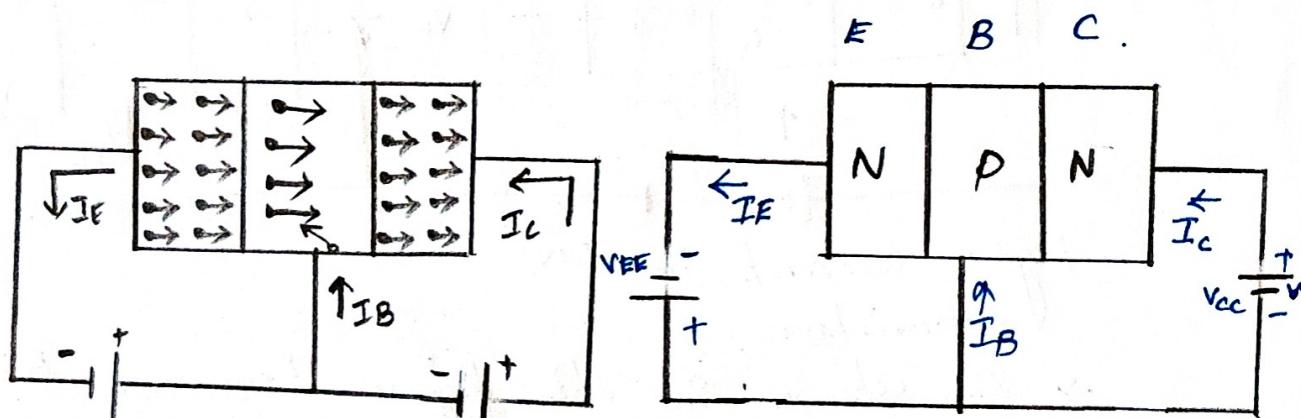


Fig. Current in NPN transistor.

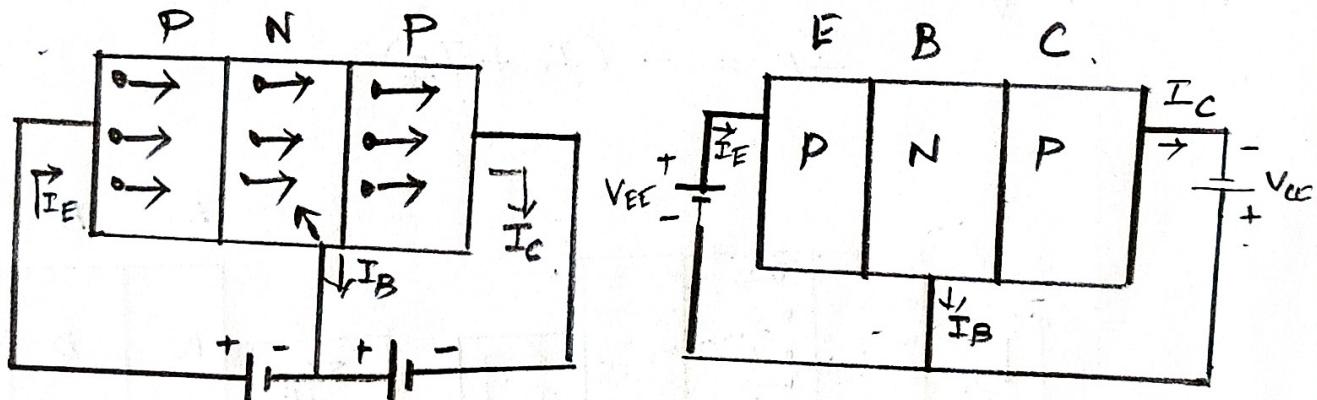
→ In the external circuit of NPN transistor, the magnitude of the emitter current  $I_E$ , the base current  $I_B$  and the collector current  $I_C$  are related by

$$I_E = I_C + I_B$$

$$\therefore I_c = I_{c\text{ majority}} + I_{c\text{ minority}}$$

- $I_{c\text{ minority}} \rightarrow$  minority current component called the leakage current. [ $I_c$  current with emitter terminal open -  $I_{c0}$ ]
- $I_{c\text{ majority}} \rightarrow$  injected collector current due to majority carriers crossing the collector base junction.

### OPERATION OF PNP TRANSISTOR:-



Fig(a) Current in PNP transistor

- As shown in the figure Forward Bias is applied to the Emitter-Base Junction and Reverse Bias is applied to the Collector-Base Junction.
- When Forward Bias is applied to Emitter-Base Junction causes a lot of holes move from emitter region to base region.
- As the base is lightly doped the number of electrons ( $e^-$ ) in the base region is very small.

- Hence a few holes combined with electrons to constitute a base current  $I_B$ .
  - The remaining holes (more than 95%) cross over into the collector region to constitute a collector current  $I_C$ .
  - Thus the collector current and base current when summed up give the emitter current.
- $$\therefore I_E = - (I_C + I_B)$$
- In the external circuit of PNP bipolar Junction transistor, the magnitude of the emitter current  $I_E$ , the base current  $I_B$  and the collector current  $I_C$  are related by
- $$I_E = I_C + I_B.$$

### 2.3.6. OPERATING REGIONS AND BIAS CONDITIONS :-

The transistor can be operated in any of the mode / regions.

Region of Operation	Base-Emitter (B-E) Junction	Base-Collector (B-C) Junction	Application
Saturation	F.B	F.B	BJT as Switch
Cut off	R.B	R.B	BJT as Switch
Forward Active	F.B	R.B	BJT as Amplifier
Inverse active	R.B	F.B	BJT in digital circuits

## 2.4 Types of Configurations:-

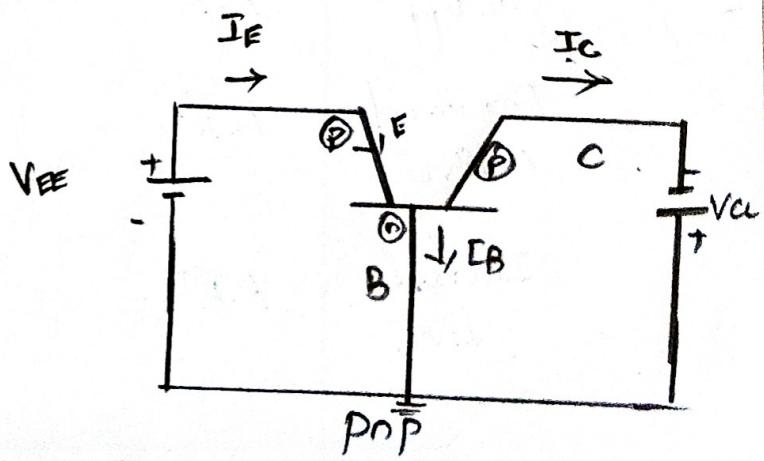
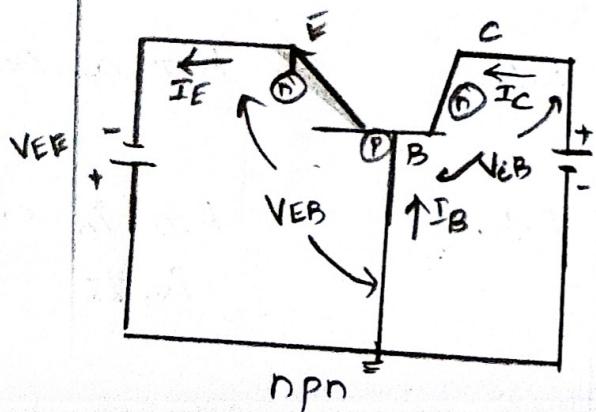
- When a transistor is to be connected in a circuit, one terminal is used as an input terminal, the other terminal is used as an output terminal and third terminal is common to the input and output.
- Depending upon the input, output and common terminal, a transistor can be connected in three configurations.

They are

- Common Base (CB) Configuration
- Common Emitter (CE) Configuration
- Common Collector (CC) Configuration.

### 2.4.1. Common Base (CB) configuration:

- This configuration is also called as grounded base configuration.
- In this configuration emitter is the input terminal, collector is the output terminal and base is the common terminal.



(B)

### 2.4.1.1 Transistor characteristics:-

In general Transistor has input and output characteristics for all the three CB, CC, CE configurations.

Static characteristics of NPN transistor in CB Configurations:-

#### a) Input characteristics:-

→ This curve gives the relationship between input current and input voltage for a given output voltage.

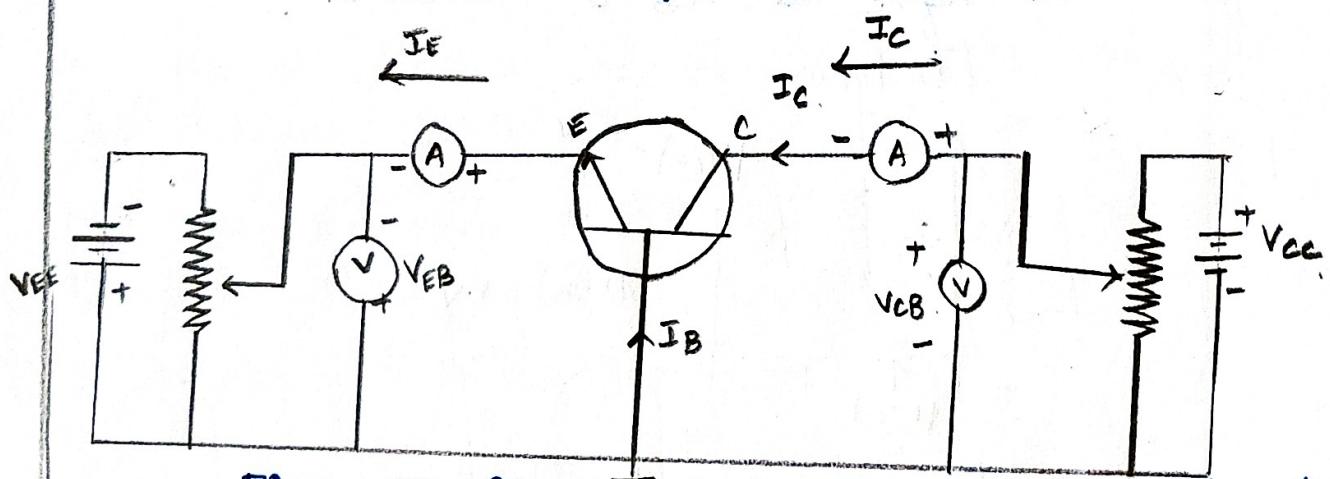


Fig: Circuit to determine CB static characteristics.

→ To determine the input characteristics, the collector current to base voltage ( $V_{CB}$ ) is kept constant at zero, then  $V_{EB}$  is increased in steps and the corresponding emitter current ( $I_E$ ) values are noted.

→ This procedure is repeated for higher fixed values of  $V_{CB}$ .

→ A graph is drawn between  $I_E$  and  $V_{EB}$  at constant  $V_{CB}$ .

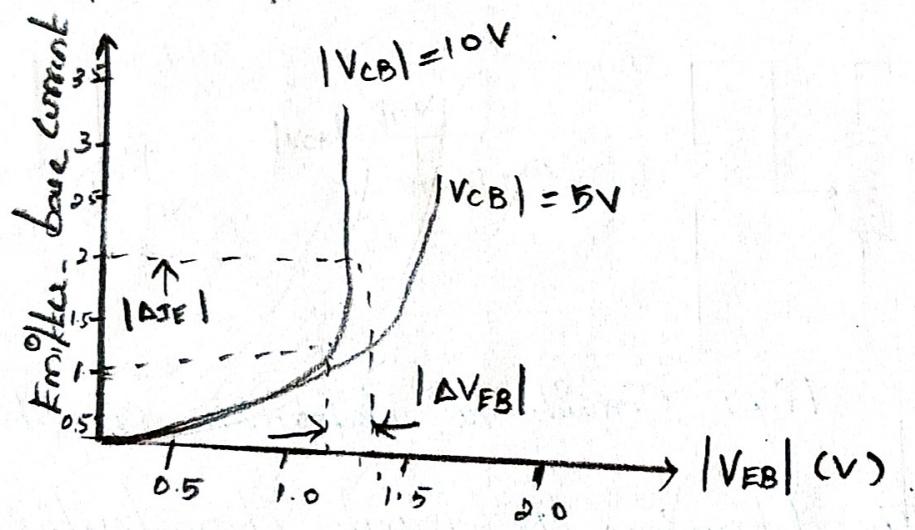
→ when  $V_{CB}$  is zero, emitter-base junction behaves as a forward biased diode. So, that the  $I_E$  increases rapidly with small increase in  $V_{EB}$ . Thus the input resistance ( $r_i$ ) is very small.

→ when  $V_{CB}$  is increased, keeping  $V_{EB}$  constant, the width of the base region will decrease.

→  $I_E$  reduces the chances of recombination of electrons with the holes in the base region.

→ Hence,  $I_E$  current increases, the curve shifts towards left as  $V_{CB}$  is increased.

$|I_E|$  (mA).



Emitter - Base Voltage.

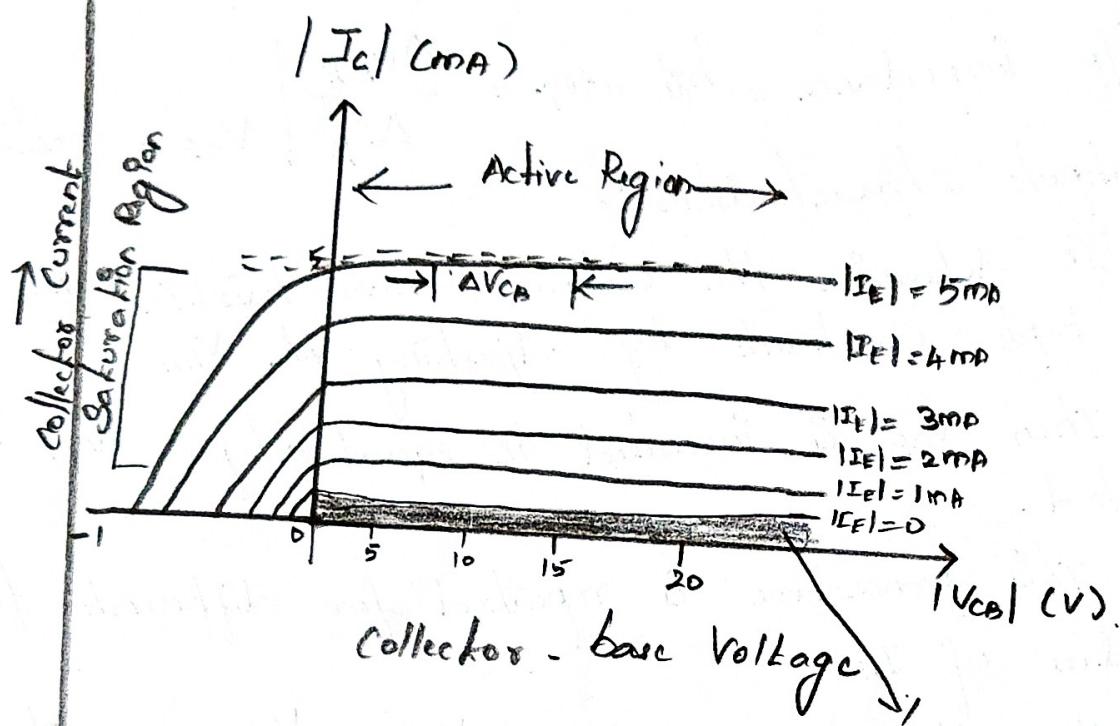
→ For a fixed  $V_{EB}$ ,  $I_E$  increases when  $V_{CB}$  is increased.

→ The dynamic i/p resistance is a ratio of change in emitter-base voltage ( $\Delta V_{EB}$ ) to the resulting change in emitter current ( $\Delta I_E$ ) at constant collector-base voltage ( $V_{CB}$ ).

$$\text{I/P impedance} = h_{ib} = r_o = \frac{\Delta V_{BE}}{\Delta I_B} \quad | \quad V_{CB} = \text{constant}$$

### Output characteristic:

- To determine the output characteristics, the  $I_E$  is kept constant by adjusting the  $V_{EE}$
- Then  $V_{CB}$  is increased in equal steps and  $I_C$  is noted.
- This procedure is repeated for different fixed values of  $I_E$
- Now the curves of  $I_C$  versus  $V_{CB}$  are plotted for constant  $I_E$
- From the characteristics, it is seen that for a constant  $I_E$ ,  $I_C$  is independent of  $V_{CB}$  and the curves are parallel to the axis  $V_{CB}$ .
- $I_C$  flows even when  $V_{CB}$  is equal to zero
- As the Emitter - Base Junction is Forward Biased, the majority carriers is electrons from the emitter are injected into the base region.
- Due to the action of internal potential barrier of the reverse biased collector - Base Junction they flow to the collector region and give rise to  $I_C$  even when  $V_{CB}$  is equal to zero.



- As the collector voltage  $V_{cb}$  is made to increase the reverse bias, the depletion region width between collector and base tends to increase with the result that effective width of the base decreases.
- The dependency of base width on collector to base voltage is known as **Early Effect (or) Base width modulation.**
- For extremely large voltages, the effective base width may be reduced to zero, causing breakdown in the transistor.
- This phenomenon is called **punch through (or) Reach through**.

→ The output characteristic has three regions Active, cut off and saturation.

### a) Active Region :-

→  $J_E \rightarrow F.B$ ,  $J_C \rightarrow R_B$

→  $I_C \approx I_E$  and transistor works as an amplifier  
 $I_C$  is almost constant.

$$\text{dynamic O/P } \left. \frac{\text{change in } V_{CB}}{\text{change in } I_C} \right|_{I_E = \text{constant}}$$

Resistance,  $R_o$

$$R_o = \left. \frac{\Delta V_{CB}}{\Delta I_C} \right|_{I_E = \text{constant}}$$

$$\frac{1}{R_o} = h_{ob} = \text{o/p admittance}$$

→  $I_C$  independent of  $V_{CB}$  and transistor can be said to work as constant-current source.  
This provides very high dynamic o/p resistance.

### b) Saturation Region:-

→  $J_E$  &  $J_C$  both are forward Biased

→  $I_C$  is independent of  $I_E$

→  $I_C$  decrease rapidly as  $V_{CB}$  becomes more negative.

### c) Cut off Region:-

→ The Region below the curve  $I_E = 0$  is known as cut off region, where  $I_C$  is nearly zero and both  $I_E$  &  $I_C$  are reverse biased.

→ DC current gain  $\alpha_{DC}$  (or)  $\alpha$  (or) Large Signal current gain of CB configuration.

$$\therefore \alpha_{DC} = \frac{I_C}{I_E} = \frac{\text{Collector Current}}{\text{Emitter Current}} = \frac{\text{o/p current}}{\text{i/p current}}$$

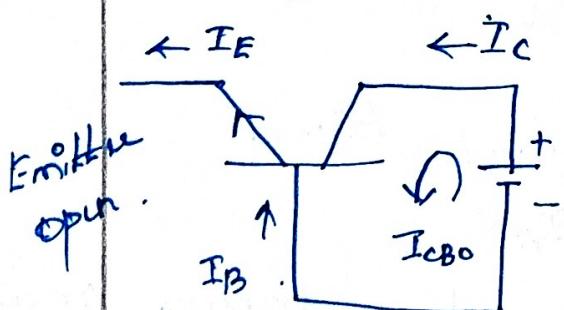
$$\therefore I_C = I_{C\text{majority}} + I_{C\text{BO minority}}$$

$$I_C = \alpha I_E + I_{C\text{BO}}$$

$$I_C = \alpha I_E + I_{C\text{BO}} \quad [I_C \propto I_E]$$

$$\rightarrow kT \cdot k \cdot T$$

$$I_E = I_B + I_C$$



→  $I_{C\text{BO}}$  is order of nA for Si & order of mA for Ge.

↳ Reverse saturation current (negligibly small) or leakage current.

↳  $I_{C\text{BO}}$  is temperature sensitive and it doubles for every  $10^\circ\text{C}$  rise in temperature.

↳  $\approx 0.90$  to  $0.995$   $\text{pk}$  is always  $< 1$ .

→ Thickness of base layer, smaller the values of  $\alpha$ .

→ Ac current gain (or) current amplification factor  
 (or) Common base short ckt current gain (or) small  
 Signal current gain (or)  $h_{fb}$ .

$$(or) \quad L_{ac} = \frac{\text{change in output current}}{\text{forward current gain} \cdot \text{change in i/p current}} = \frac{\Delta I_C}{\Delta I_E} \Big|_{V_{CB} = \text{constant}}$$

→ For all practical purposes, dc current gain  
 is equal to ac current gain ( $\alpha_{dc} \approx \lambda_{ac}$ ).

**CB Transistor parameter (or) Hybrid parameter:-**

(or) **L-parameter:-**

→ The slope of - the CB characteristic will give  
 the following 4 transistor parameters.

a) **Input impedance ( $h_{ib}$ )**.

$$h_{ib} = \frac{\text{change in (i/p) emitter Voltage}}{\text{change in (i/p) emitter current}} \Big|_{V_{CB} = \text{constant}} \quad \begin{array}{l} (\text{o/p}) \\ \text{Collector-} \\ \text{base voltage} \\ V_{CB} = \text{constant} \end{array}$$

$$\Rightarrow h_{ib} = \frac{\Delta V_{EB}}{\Delta I_E} \Big|_{V_{CB} = \text{constant}}$$

→ It is the slope of CB i/p characteristic  $I_E$   
 versus  $V_{EB}$ .

→  $h_{ib}$  value ranges from  $20\Omega$  to  $50\Omega$ .

b) Output admittance ( $h_{ob}$ )

$$h_{ob} = \frac{\text{change in (O/P) collector current}}{\text{change in (O/P) collector voltage}} \quad \left| \begin{array}{l} \text{i/p emitter} \\ \text{current} \\ I_E = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{ob} = \frac{\Delta I_C}{\Delta V_{CB}} \quad \left| \begin{array}{l} I_E = \text{constant} \end{array} \right.$$

$\Rightarrow h_{ob}$  is the slope of  $I_C$  vs  $V_{CB}$ .

$\Rightarrow h_{ob}$  value ranges from 0.1 to 10  $\mu$

c) Forward current gain ( $h_{fb}$ )

$$h_{fb} = \frac{\text{change in (O/P) collector current}}{\text{change in (I/P) emitter current}} \quad \left| \begin{array}{l} \text{(O/P) collector} \\ \text{base voltage} \\ V_{CB} = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{fb} = \frac{\Delta I_C}{\Delta I_E} \quad \left| \begin{array}{l} V_{CB} = \text{constant} \end{array} \right.$$

$\Rightarrow h_{fb}$  is the slope of  $I_C$  vs  $I_E$

$\Rightarrow h_{fb}$  varies from 0.9 to 1.0.

d) Reverse voltage gain ( $h_{rb}$ )

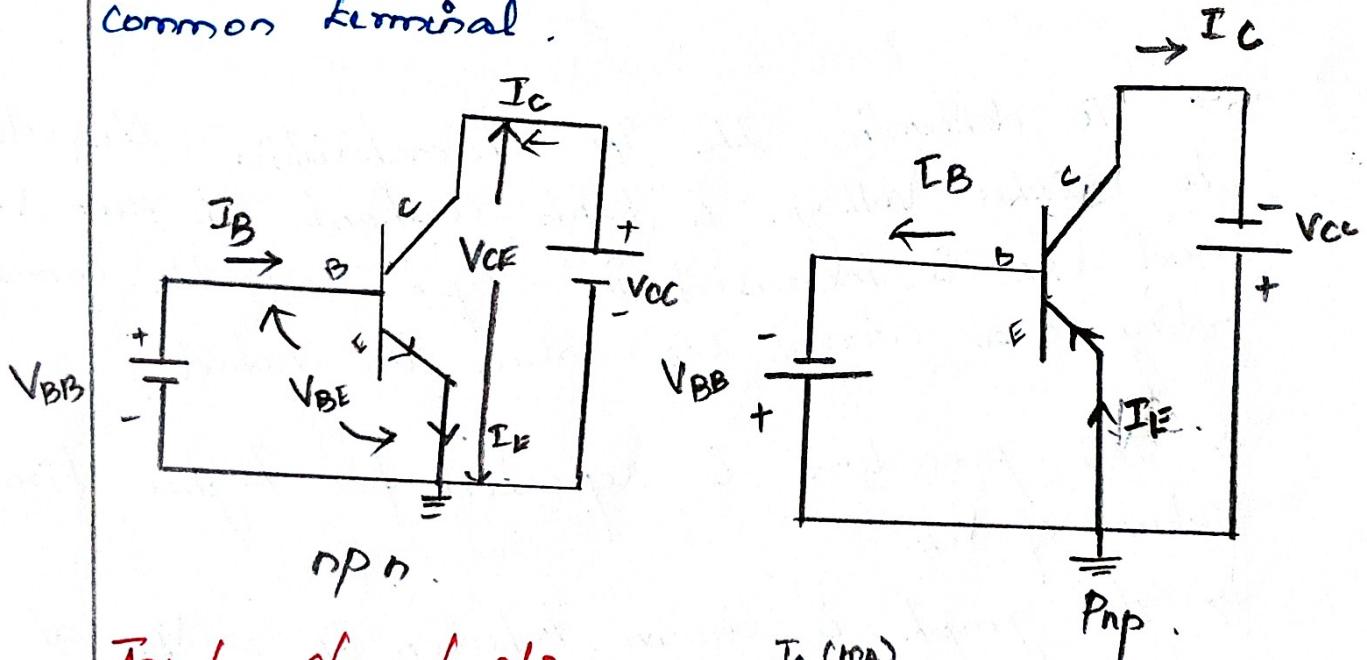
$$h_{rb} = \frac{\text{change in (I/P) emitter voltage}}{\text{change in (O/P) collector voltage}} \quad \left| \begin{array}{l} \text{(I/P) emitter} \\ \text{current} \\ I_E = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{rb} = \frac{\Delta V_{EB}}{\Delta V_{CB}} \quad \left| \begin{array}{l} I_E = \text{constant} \end{array} \right.$$

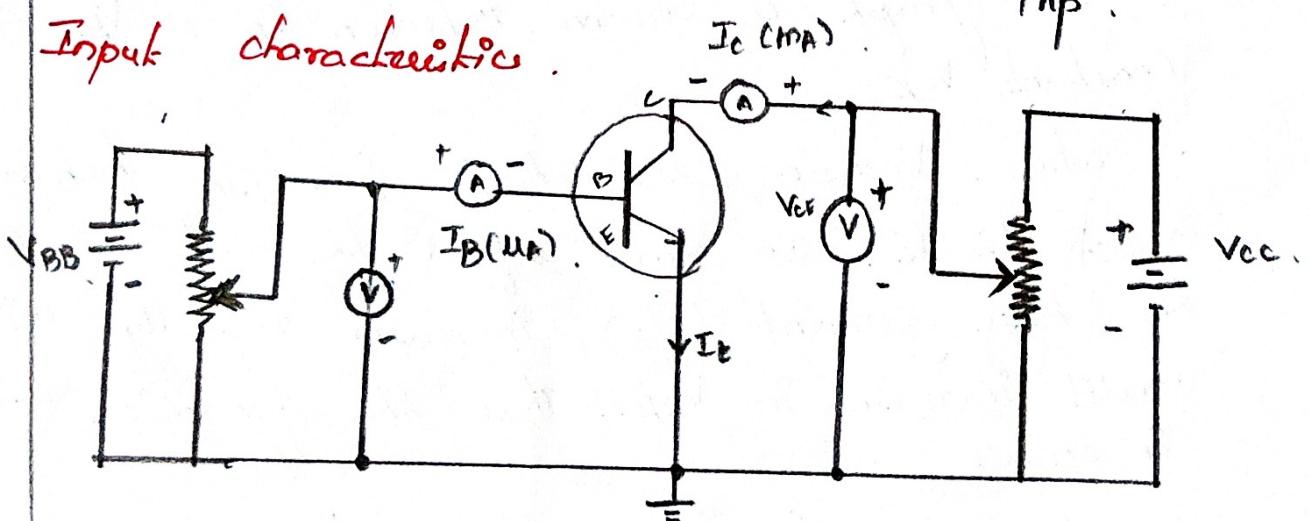
- $\beta$  is the slope of  $V_{EB}$  vs  $V_{CB}$  curve.
- Typical value of  $\beta$  is order of  $10^5$  to  $10^4$ .

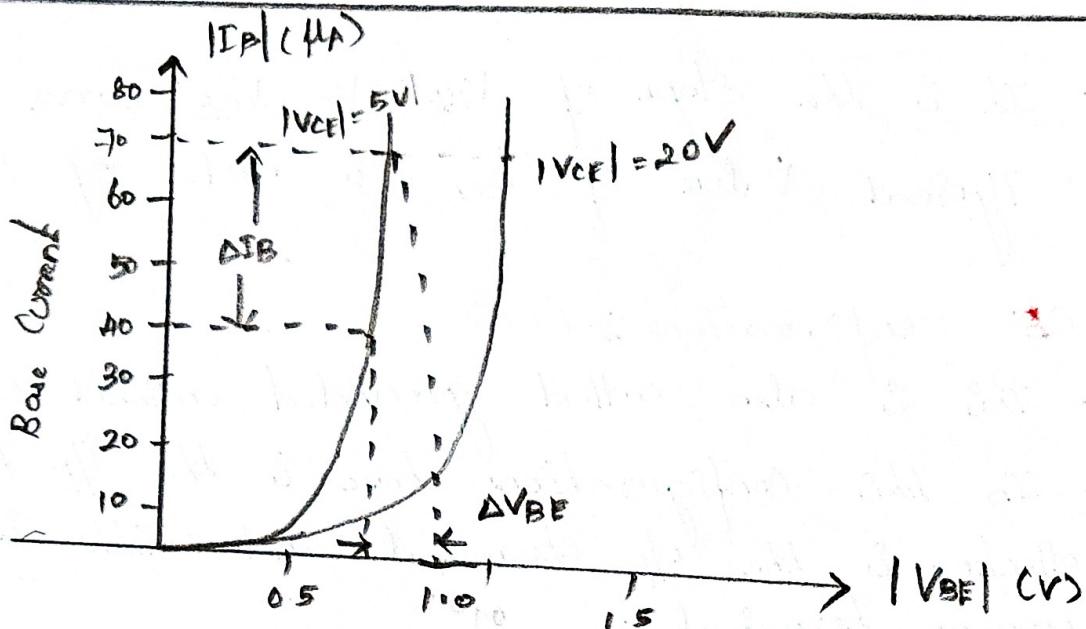
### 2.4.2 CE Configurations :- (CE)

- This is also called grounded emitter configuration.
- In this configuration, base is the input terminal, collector is the output terminal and emitter is the common terminal.



Input characteristics





Base Emitter Voltage.

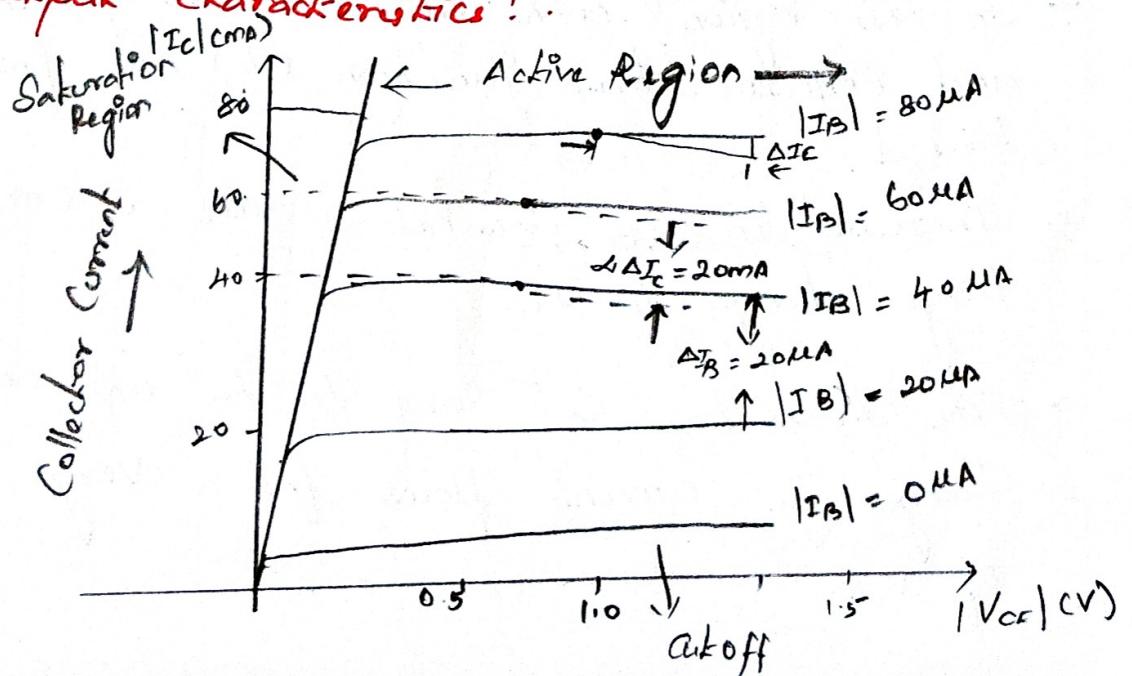
- To determine the  $I_B$  characteristic, the collector-to-emitter voltage is kept constant at zero volt and  $V_{BE}$  is increased in steps and the corresponding base current ( $I_B$ ) values are noted.
- This procedure is repeated for higher fixed values of  $V_{CE}$ .
- The graph is drawn between  $I_B$  &  $V_{BE}$  at constant  $V_{CE}$ .
- When  $V_{CE} = 0$ , the E-B junction behaves as a P-N diode. So that, after the cut-in voltage, the base current ( $I_B$ ) increases rapidly with small increase in  $V_{BE}$ . Thus the dynamic resistance is small.
- When  $V_{CE}$  is increased (i.e.) R.B at collector-emitter junction is increased the width of the depletion region at the R.B collector-emitter junction will increase.

- Hence the effective width of base will decrease.
- So, it reduces the chance of recombination of electrons in the emitter with the hole in base region.
- ∵ Base current ( $I_B$ ) decreases. The curve shift towards right as  $V_{CE}$  increases. For a fixed value of  $V_{BE}$ ,  $I_B$  decreases as  $V_{CE}$  is increased.
- The dynamic i/p resistance & ratio of change in base-emitter voltage ( $\Delta V_{BE}$ ) to the resulting change in base current ( $\Delta I_B$ ) at constant collector-emitter voltage ( $V_{CE}$ ).

$$\text{i/p impedance} = h_{ie} = \gamma_0 = \frac{\Delta V_{BE}}{\Delta I_B} \quad |V_{CE} = \text{Constant.}$$

- The value of  $\gamma_0$  in CE configuration is greater than the value of  $\gamma_0$  in CB configuration.

### Output Characteristics:



- To determine the output characteristics,  $I_B$  is kept constant by adjusting  $V_{BE}$
  - Then  $V_{CE}$  is increased in equal steps and  $I_C$  is noted.
  - $I_C$  reaches to a saturation value when  $V_{CE}$  is about 1V
  - When  $V_{CE}$  is increased further,  $I_C$  is slightly increase and  $I_B$  decrease.
  - When  $I_B$  is zero, a small  $I_C$  current exists. This is called leakage current. ( $I_{CEO}$ )
  - For all practical purpose,  $I_C$  is zero when  $I_B = 0$ . Under this conditions the transistor is said to be cut off.
  - The op characteristics may be divided into three regions: Saturation, Active and cutoff.
- a) **Saturation Region:**
- In this region both emitter-base junction ( $J_E$ ) and collector-base junction ( $J_C$ ) are forward biased.
  - Increase in  $I_B$  does not cause a corresponding large change in  $I_C$ .
  - The transistor is said to be 'on' condition i.e. Large  $I_C$  current flows for a very low value of  $V_{CE}$ .

### b) Cut off Region:-

- The region below the curve for  $I_B = 0$  is called as cut off Region. In this region both  $J_E, J_C$  are Reverse biased.
- $J_C$  becomes almost zero and  $V_{CE}$  almost equals to  $V_{CC}$ .
- The Transistor is said to be in OFF condition.

### c) Active Region:-

- In this region,  $J_E \propto I_B$  and  $J_C \propto R_B$
- The central region where curves are uniform in Spacing and Slope is called active region.
- In this Transistor is to be used as Linear amplifier, it should be operated in active region.

$$\text{dynamic o/p resistance, } R_o = \frac{\text{change in } V_{CE}}{\text{change in } I_C} \quad \left| \begin{array}{l} \text{I}_B = \text{constant} \\ \text{I}_C = \text{constant} \end{array} \right.$$

$$\Rightarrow R_o = \frac{\Delta V_{CE}}{\Delta I_C} \quad \left| \begin{array}{l} \text{I}_B = \text{constant} \\ \text{I}_C = \text{constant} \end{array} \right.$$

$$\frac{1}{R_o} = h_{oE} = \text{o/p admittance.}$$

$\text{DC current gain } \beta_{dc}$  (or)  $\beta$  (or) Large Signal current gain of CE Configuration.

$$\beta_{dc} = \frac{I_C}{I_B} = \frac{\text{Collector Current}}{\text{Base Current}}$$

AC current gain (or) current amplification factor  $\beta$  (or)  
 Small signal current gain (or)  $h_{fe}$  (or) forward current  
 gain.

$$\beta_{ac} = \frac{\text{change in o/p current}}{\text{change in i/p current}} = \frac{\Delta I_c}{\Delta I_B} \quad | \quad V_{CE} = \text{constant.}$$

Relationship between  $\alpha, \beta$ :

h.f.k. T

$$\alpha = \frac{\Delta I_c}{\Delta I_E} \quad — \textcircled{1}$$

$$\beta = \frac{\Delta I_c}{\Delta I_B} \quad — \textcircled{2}$$

$$\Delta I_E = \Delta I_B + \Delta I_c \quad — \textcircled{3}$$

from  $\textcircled{3}$

$$\Delta I_B = \Delta I_E - \Delta I_c \quad — \textcircled{4}$$

Sub eqn  $\textcircled{3}$  in  $\textcircled{1}$

$$\Delta I_E = \Delta I_B + \Delta I_c \text{ in } \textcircled{1}$$

$$\alpha = \frac{\Delta I_c}{\Delta I_B + \Delta I_c}$$

$\therefore$  Numerator and Denominator divided by  $I_B$

$$\alpha = \frac{\Delta I_c / \Delta I_B}{1 + \Delta I_c / \Delta I_B} \Rightarrow$$

where  $\Delta I_c / \Delta I_B = \beta$

$$\boxed{\alpha = \frac{\beta}{1 + \beta}}$$

111ly sub ④ in ②

$$\Delta I_E - \Delta I_C = \Delta I_B \text{ in } ②$$

$$\beta = \frac{\Delta I_C}{\Delta I_E - \Delta I_C}$$

∴ Numerator and denominator divided by  $\Delta I_E$

$$\beta = \frac{\Delta I_C / \Delta I_E}{\frac{\Delta E - \Delta I_C}{\Delta I_E}} = \frac{\Delta I_C / \Delta I_E}{1 - \frac{\Delta I_C}{\Delta I_E}}$$

$$\boxed{\beta = \frac{\alpha}{1-\alpha}}$$

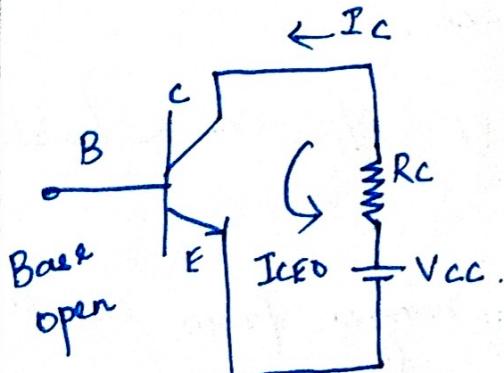
$$\text{where } \alpha = \Delta I_C / \Delta I_E$$

Leakage current:

→ when the base is open, a leakage current flows from emitter to collector terminal. It is denoted by  $I_{CEO}$ .

$$\boxed{I_{CEO} = I_{CBO} + \beta I_{EBO} = (1+\beta) I_{CBO}}$$

∴ Total collector current  $I_C = \beta I_B + I_{CEO}$



$$I_C = \beta I_B + (1+\beta) I_{CBO}$$

∴  $I_{CEO} \rightarrow$   
 $\downarrow 0 \rightarrow$  Base open  
 $CR \rightarrow$  collector to emitter  
 Leakage current (or)  
 Reverse saturation current.

Transistor parameters (or) CE hybrid parameters:-  
(h-parameter):

→ The slope of the CE characteristic will give the following 4 transistor parameters.

a) Input Impedance ( $h_{ie}$ )

$$h_{ie} = \frac{\text{change in (I/p) base voltage}}{\text{change in (I/p) base current}} \quad \left| \begin{array}{l} (\text{O/p}) \text{ collector} \\ \text{Voltage} \\ V_{CE} = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{ie} = \frac{\Delta V_{BE}}{\Delta I_B} \quad \left| \begin{array}{l} V_{CE} = \text{constant} \end{array} \right.$$

→ It is the slope of CE I/p characteristic  $I_B$  vs  $V_{BE}$ .

→  $h_{ie}$  ranges from 500 to 2000  $\Omega$

b) Output admittance ( $h_{oe}$ )

$$h_{oe} = \frac{\text{change in (O/p) collector current}}{\text{change in (O/p) collector Voltage}} \quad \left| \begin{array}{l} (\text{I/p}) \text{ base} \\ \text{current,} \\ I_B = \text{constant.} \end{array} \right.$$

$$\Rightarrow h_{oe} = \frac{\Delta I_C}{\Delta V_{CE}} \quad \left| \begin{array}{l} I_B = \text{constant.} \end{array} \right.$$

→ It is the slope of CE O/p characteristic  $I_C$  vs  $V_{CE}$ .

→ Typical values of  $h_{oe}$  range from 0.1 to 10  $mS$

c) Forward current gain ( $h_{fe}$ ):

$$h_{fe} = \frac{\text{change in (O/p) collector current}}{\text{change in (I/p) base current}} \quad \left| \begin{array}{l} (\text{O/p}) \text{ collector} \\ \text{voltage} \\ V_{CE} = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{fe} = \frac{\Delta I_C}{\Delta I_B} \quad \left| \begin{array}{l} V_{CE} = \text{constant} \end{array} \right.$$

$\rightarrow I_k$  & the slope of  $I_C$  vs  $I_B$  curve.

$\rightarrow$  Typical value of  $h_{fe}$  varies from 20 to 200

d) Reverse Voltage gain ( $h_{re}$ ):

$$h_{re} = \frac{\text{change in (I/p) base voltage}}{\text{change in (O/p) collector voltage}} \quad \left| \begin{array}{l} I_B = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{re} = \frac{\Delta V_{BE}}{\Delta V_{CE}} \quad \left| \begin{array}{l} I_B = \text{constant} \end{array} \right.$$

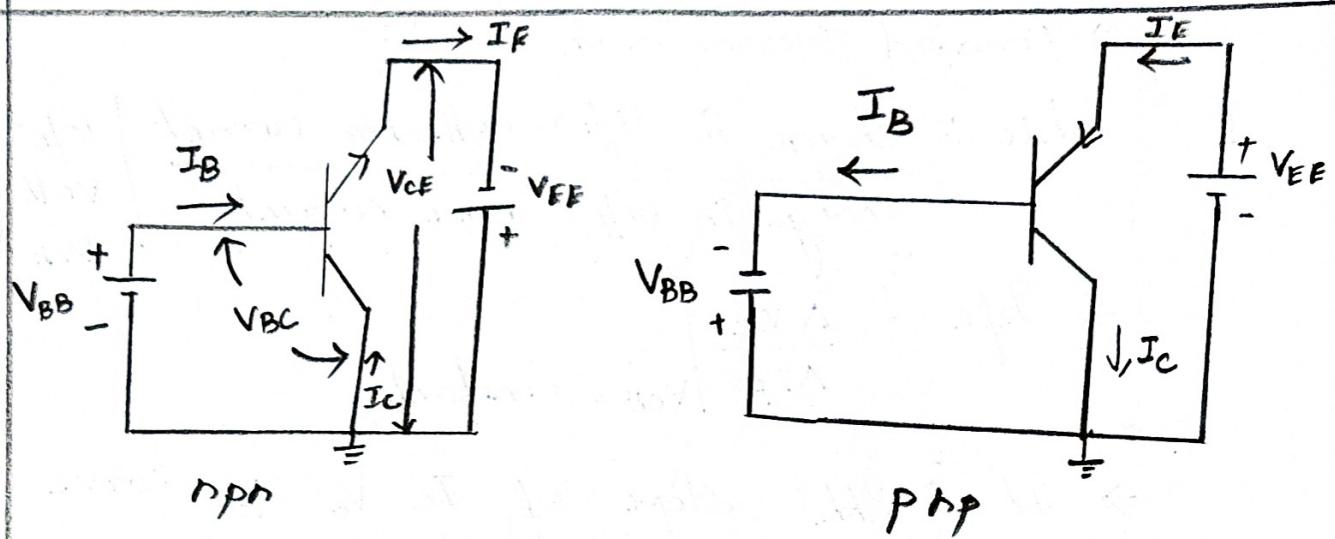
$\rightarrow I_k$  & the slope of  $V_{BE}$  vs  $V_{CE}$  curve

$\rightarrow$  Typical value of  $h_{re}$  is the order of  $10^{-5}$  to  $10^4$ .

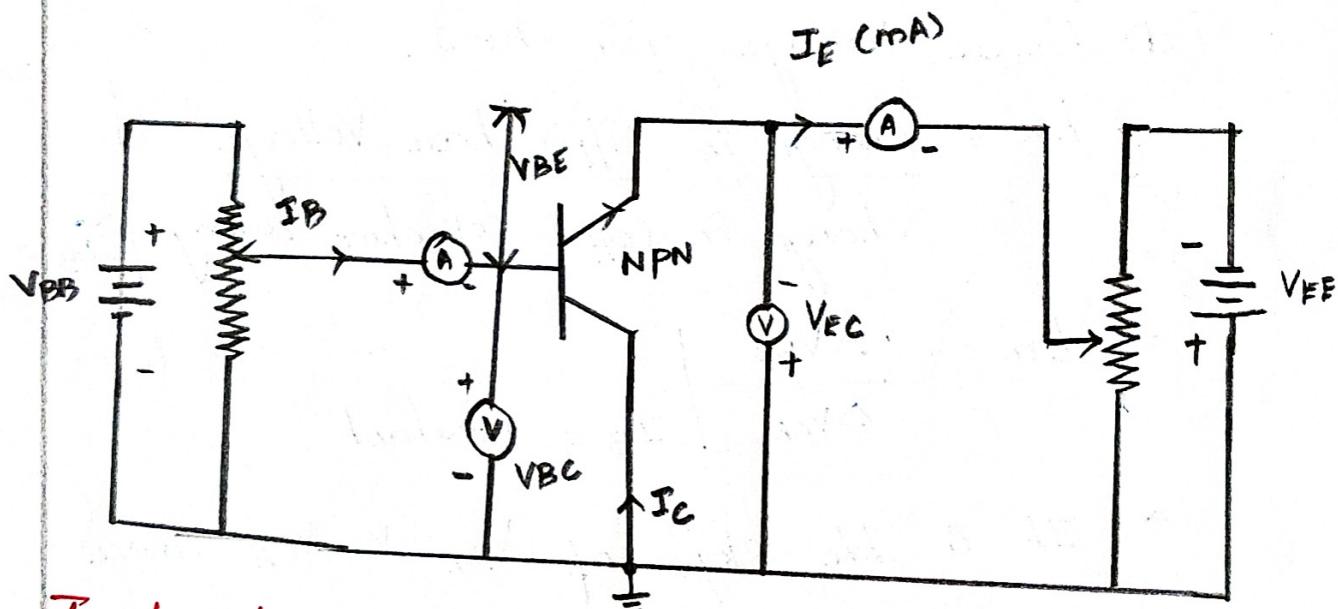
2.4.3. CC Configuration:

$\rightarrow$  This is also called grounded collector configuration

$\rightarrow$  In this configuration, base is the input terminal, emitter is the o/p terminal, collector is the common terminal.

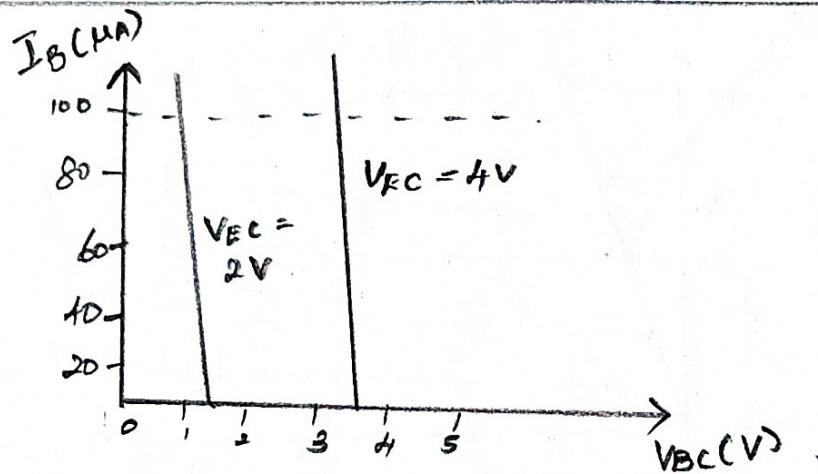


Transistor characteristics :-



Input characteristics :-

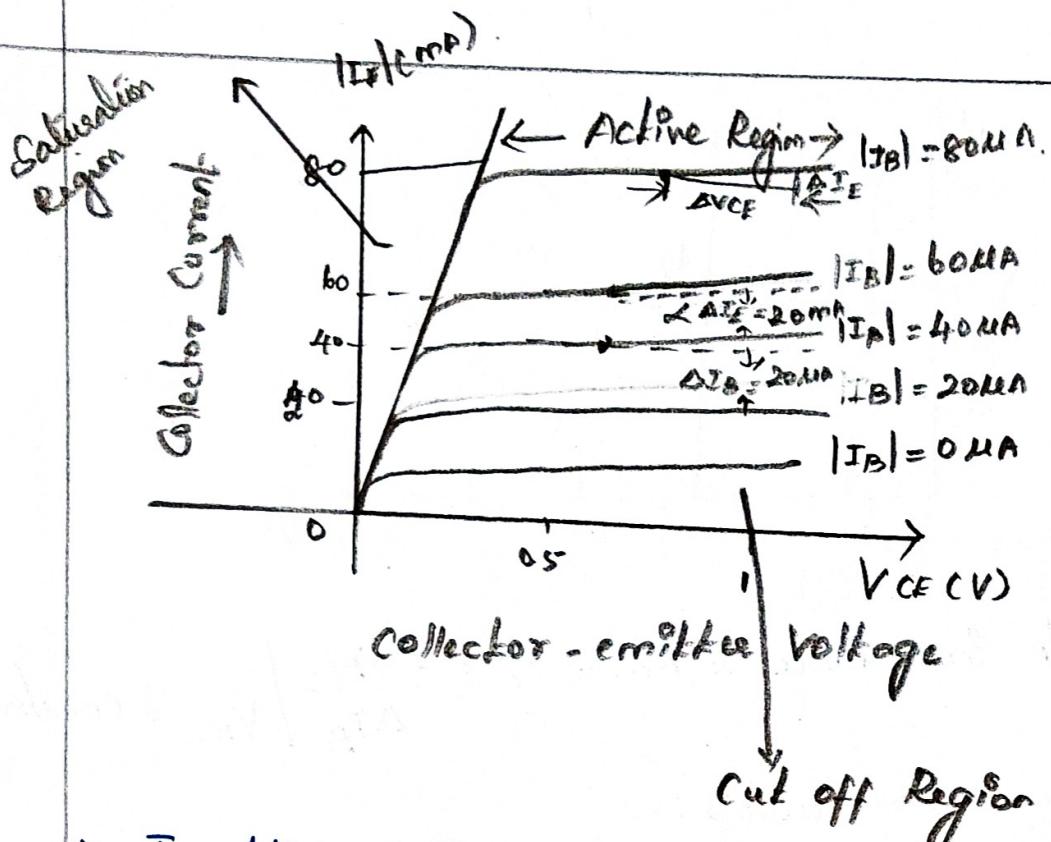
- To determine the I/p characteristics,  $V_{EC}$  is kept constant and  $V_{BC}$  is increased in equal steps and the corresponding increase in  $I_B$  is noted.
- This procedure is repeated for higher fixed values of  $V_{EC}$ .
- The graph is drawn between  $I_B$  &  $V_{BC}$  at constant  $V_{EC}$ .



→ i/p impedance =  $R_{ic} = \infty = \frac{\Delta V_{BC}}{\Delta I_B}$  /  $V_{CE}$  = constant.

### Output characteristics:-

- To determine the o/p characteristics,  $I_B$  is kept constant and  $V_{CE}$  is increased in equal steps and the corresponding  $I_E$  is noted.
- This procedure is repeated for different fixed values of  $I_B$ .
- Graph is drawn between  $I_E$  vs  $V_{CE}$  at constant  $I_B$ .
- $I_C$  is approximately equal to  $I_E$ , the cc o/p characteristics are practically similar to those of ce o/p characteristics.



- In this configuration, i/p is applied between base and collector and o/p is taken from emitter and collector.
- The cc configuration is also known as Emitter follower configurations.
- The o/p resistance  $R_o = \frac{\text{change in } V_{EC}}{\text{change in } I_E} \quad | I_B = \text{constant}$

$$R_o = \frac{\Delta V_{EC}}{\Delta I_E} \quad | I_B = \text{constant}.$$

Transistor parameters (or) cc hybrid parameters (or) h-parameters.

- The slope of the cc characteristics will give 4 transistor parameters.

Transistor parameters (or) CC hybrid parameters (or) h-parameters.

The slope of the CC characteristics will give the following 4 transistor parameters.

a) Input Impedance ( $h_{ic}$ )

$$h_{ic} = \frac{\text{change in (i/p) base voltage}}{\text{change in (i/p) base current}} \quad \left| \begin{array}{l} \text{o/p collector} \\ \text{voltage} \\ V_{EC} = \text{constant} \end{array} \right.$$

$$\Rightarrow h_{ic} = \frac{\Delta V_{BC}}{\Delta I_B} \quad \left| \begin{array}{l} V_{EC} = \text{constant} \end{array} \right.$$

$\rightarrow$  It is the slope of CC i/p characteristic  $I_B$  vs  $V_{BC}$ .

b) Output Admittance ( $h_{oc}$ )

$$h_{oc} = \frac{\text{change in (o/p) emitter current}}{\text{change in (o/p) collector voltage}} \quad \left| \begin{array}{l} \text{i/p base} \\ \text{current} \\ I_B = \text{constant} \end{array} \right.$$

$$h_{oc} = \frac{\Delta I_E}{\Delta V_{EC}} \quad \left| \begin{array}{l} I_B = \text{constant} \end{array} \right.$$

$\rightarrow$  It is the slope of CC o/p characteristics  $\frac{I_E}{V_{EC}}$

c) Forward Current gain ( $h_{fc}$ )

$$h_{fc} = \frac{\text{change in (o/p) emitter current}}{\text{change in (i/p) base current}} \quad \left| \begin{array}{l} \text{o/p collector} \\ \text{voltage} \\ V_{CE} = \text{constant} \end{array} \right.$$

$$h_{fc} = \frac{\Delta I_E}{\Delta I_B} \quad | \quad V_{CE} = \text{constant}$$

$\Rightarrow h_{fc}$  is the slope of  $I_C$  vs  $I_B$  curve.

d) Reverse Voltage gain ( $h_{rc}$ )

$$h_{rc} = \frac{\text{change in (i/p) base voltage}}{\text{change in (o/p) emitter voltage}} \quad | \quad \begin{matrix} (\text{i/p}) \text{ base} \\ (\text{o/p}) \text{ emitter} \end{matrix} \quad \begin{matrix} \text{current} \\ I_B = \text{constant} \end{matrix}$$

$$h_{rc} = \frac{\Delta V_{BC}}{\Delta V_{EC}} \quad | \quad I_B = \text{constant}$$

$\Rightarrow$  Slope of  $V_{BC}$  vs  $V_{EC}$  curve.

DC current gain  $H_{dc}$  (or) (or) Large signal current gain of CC configuration.

$$\gamma = \frac{I_E}{I_B} = \frac{\text{emitter current}}{\text{Base current}}$$

AC current gain  $\gamma_{ac}$  (or) current amplification factor  $\gamma$  (or) Small signal current gain (or)  $h_{fc}$  (or) forward gain

$$\gamma_{ac} = \frac{\text{change in o/p current}}{\text{change in i/p current}} \quad | \quad V_{CE} = \text{constant}$$

$$= \frac{\Delta I_E}{\Delta I_B} \quad | \quad V_{CE} = \text{constant}$$

Relationship b/w  $\alpha$ ,  $\beta$  and  $\gamma$

$$\gamma = \frac{I_E}{I_B} - ①$$

N.K.T

$$I_E = I_B + I_C$$

$$\therefore I_B = I_E - I_C - ②$$

Sub ② in ①

$$\gamma = \frac{I_E}{I_E - I_C} - ③$$

$\therefore$  numerator and denominator by  $I_E$

$$\gamma = \frac{I_E/I_E}{I_E/I_E - I_C/I_E} - ④$$

$$= \frac{1}{1 - I_C/I_E}$$

$$\boxed{\gamma = \frac{1}{1 - \alpha}} - ⑤$$

$$\left[ \because \alpha = \frac{I_C}{I_E} \right]$$

$$\left[ \because \alpha = \frac{\beta}{1+\beta} \right]$$

Sub  $\alpha = \beta/(1+\beta)$  in ⑤

$$\gamma = \frac{1}{1 - \beta/(1+\beta)} = \frac{1}{1+\beta - \beta} = \frac{1}{1+\beta}$$

$$\boxed{\gamma = 1+\beta}$$

Note: - CE configuration is most widely used in amplifier circuits

- 1) provides both voltage gain and current gain
- 2) provides high power gain
- 3) can be cascaded efficiently

Comparison of CB, CF and CC configurations:-

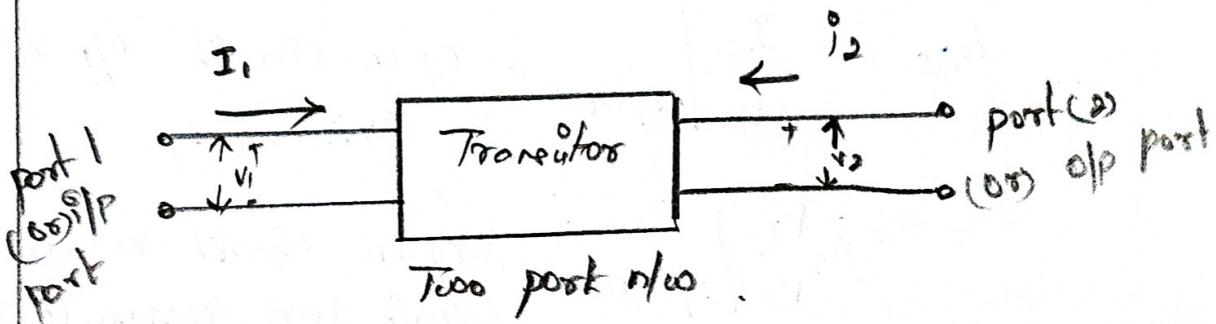
S.No	Characteristic	CB Config	CF Config	CC Config
1.	I/p Resistance ( $R_i$ )	Very Low ( $20\Omega$ )	Low ( $1k\Omega$ )	High ( $500k\Omega$ )
2.	O/p Resistance ( $R_o$ )	Very High ( $1M\Omega$ )	High ( $40k\Omega$ )	Low ( $50k\Omega$ )
3.	I/p Current	$I_E$	$I_B$	$I_B$
4.	O/p Current	$I_C$	$I_C$	$I_E$
5.	Input Voltage applied between emitter & base	Emitter & base	Base & Emitter	Base & Collector .
6.	Leakage current	Small	Large	Large .
7.	O/p Voltage taken between collector & base	Collector & base	Collector & emitter	Emitter & Collector .
8.	Current Amplification factor	$\alpha = \frac{I_C}{I_E}$	$\beta = \frac{I_C}{I_B}$	$\gamma = \frac{I_E}{I_B}$

S.No	Characteristics	CB Config	CE Config	CC Config.
9.	Current gain ( $A_i$ )	Less than unity	High (20 to few hundred)	High (20 to few hundreds)
10.	Voltage gain ( $A_v$ )	Medium	Medium	Less than unity
11.	Application	As a i/p stage of multistage amplifier and for high freq -ency applications.	Provides both voltage and current gains greater than unity and hence it is widely used in audio signal amplification.	For impedance matching.

### Reach through (or) punch through

- According to Early effect, the depletion region width of junction  $J_c$  increases with increased collector - junction voltage. Hence width of the base will be reduced or reached to zero.
- It affects both i/p and o/p characteristics of a transistor.
- If it is possible to raise the punch through concentration voltage by increasing the doping in the base but this automatically reduces the emitter efficiency.

- punch through takes place at a fixed voltage b/w collector and base and is not dependent on circuit configuration, where as
- Multiplication takes place at different voltages depending upon the circuit configuration.
- The voltage limit of a particular transistor is determined by either of the two types of break down which occurs at lower voltage.
- A transistor can be treated as a 2-pot network
- The terminal behaviour of any 2-pot n/w can be specified by the terminal voltages  $V_1$  &  $V_2$  at ports 1 & 2 respectively.
- Currents  $I_1, I_2$  entering ports 1 & 2 respectively.
- Out of 4 variables  $V_1, V_2, I_1, I_2$ , two can be selected as independent variable ( $I_1, V_2$ ) and the remaining two ( $V_1, I_2$ ) can be expressed in terms of these independent variables.



- The h-parameter representation is widely used in modelling of transistors.
- Hence both short circuit and open circuit terminal conditions are used.

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$\therefore V_1 = h_{11} I_1 + h_{12} V_2$$

$h_{11}, h_{12}, h_{21}, h_{22}$  are hybrid parameters.

$$I_2 = h_{21} I_1 + h_{22} V_2$$

when  $V_2 = 0$ , (i.e) with open o/p port short Circuited.

$$\therefore h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0} = \text{short circuit i/p impedance.}$$

[unit -Ω]

$$h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0} = \text{short circuit Forward current gain (or) Forward transistor ratio.}$$

when  $I_1 = 0$ , i.e. with i/p port open circuited.

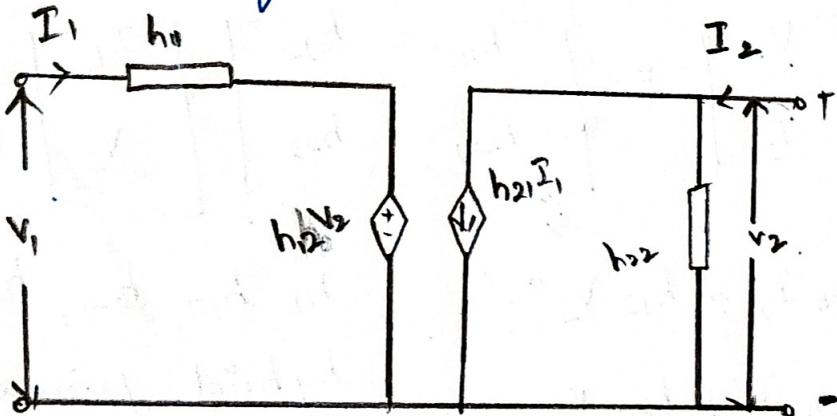
$$h_{22} = \left. \frac{I_2}{V_2} \right|_{I_1=0} = \text{open circuit o/p admittance}$$

(unit - v)

$$h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0} = \text{open circuit reverse Voltage}$$

gain (or) reverse transfer  
ratio.

→ As the dimension ( $A, V, \text{ dimensionless}$ ) are not a like as they are hybrid in nature, these parameters are called hybrid parameters.



Equivalent Circuit of h-parameter model

→  $h_{12} V_2$  is the Voltage controlled Source and  $h_{21} I_1$  is the Current Controlled Source.

→ The alternative Subscript notations recommended by IEEE commonly used are

$$i = II = \text{i/p}$$

$$o = 22 = \text{o/p}$$

$$f = 21 = \text{forward transfer}$$

$$r = 12 = \text{reverse transfer}$$

→ Second Subscript to designate the type of configuration 'e' for CE, 'b' for CB and 'c' for CC.

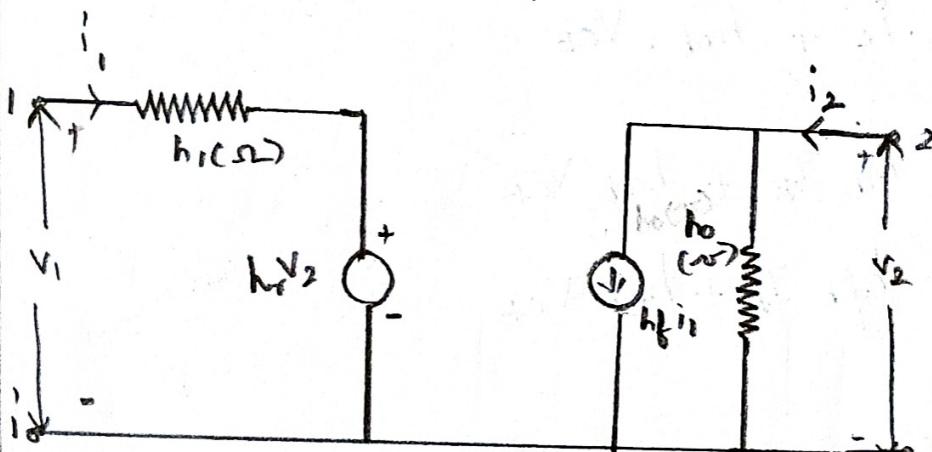
Ex:

$h_{ie} = h_{11e}$  = short ckt o/p impedance

$h_{oe} = h_{22e}$  = open ckt o/p admittance

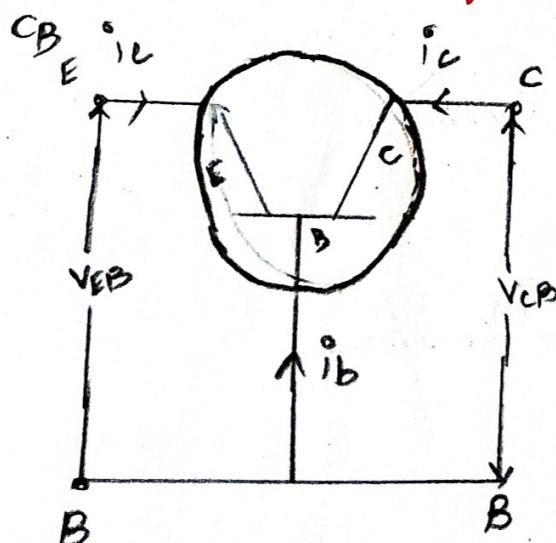
$h_{fe} = h_{21e}$  = short ckt forward current gain

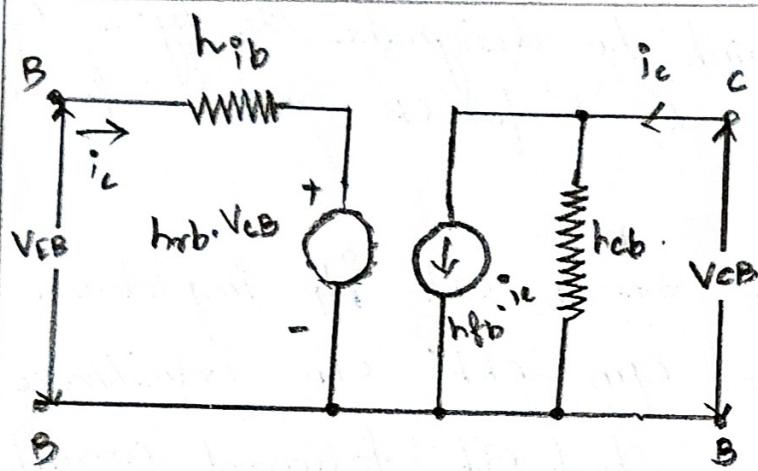
$h_{re} = h_{12e}$  = open ckt reverse voltage gain.



H-parameter model for two port network

a) H-parameter model for CB configurations:





$$V_{BE} = h_{ib} \cdot i_C + h_{re} \cdot V_{CB}$$

$$i_C = h_{fb} \cdot i_C + h_{re} \cdot V_{CB}$$

$$\Rightarrow V_{BE} = h_{ib} I_E + h_{re} V_{CB}$$

$$I_C = h_{fb} I_E + h_{re} V_{CB}$$

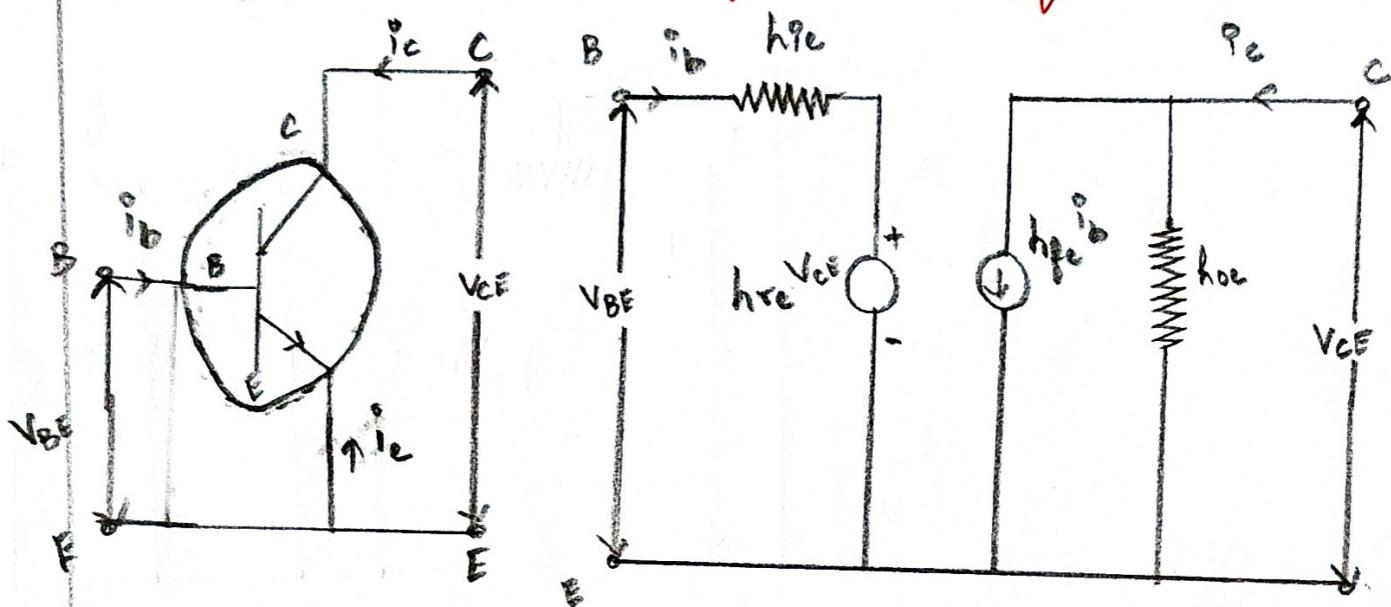
$$h_{ib} = \frac{V_{BE}}{I_E} \quad | \quad V_{CB} = \text{constant}$$

$$h_{re} = \frac{V_{BE}}{V_{CB}} \quad | \quad I_E = \text{constant}$$

$$h_{fb} = \frac{I_C}{I_E} \quad | \quad V_{CB} = \text{constant}$$

$$h_{re} = \frac{I_C}{V_{CB}} \quad | \quad I_E = \text{constant}$$

b) h-parameter model for CE configurations:



$$V_{BE} = h_{ie} I_B + h_{re} V_{CE}$$

$$I_C = h_{fe} I_B + h_{oe} V_{CE}$$

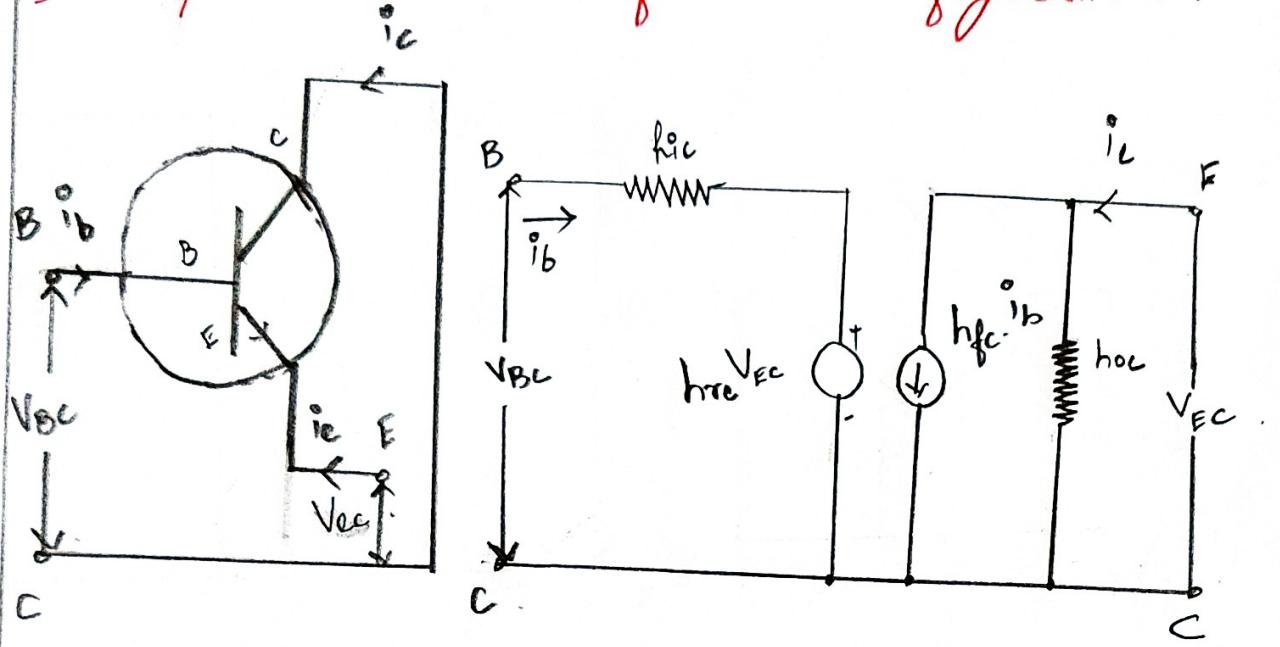
$$\text{Input Impedance } h_{ie} = \frac{V_{BE}}{I_B} \quad | \quad V_{CE} = \text{constant}$$

$$\text{Output Admittance } h_{oe} = \frac{I_C}{V_{CE}} \quad | \quad I_B = \text{constant}$$

$$\text{Reverse Voltage gain } h_{re} = \frac{V_{BE}}{V_{CE}} \quad | \quad I_B = \text{constant}$$

$$\text{Forward Current gain } h_{fe} = \frac{I_C}{I_B} \quad | \quad V_{CE} = \text{constant}$$

Q) h-parameter model for cc. configuration.



$$V_{BC} = h_{ic}^{\circ} I_B + h_{re} V_{EC}$$

$$I_F = h_{fc} I_B + h_{oc} V_{EC}$$

Input impedance

$$h_{ic}^{\circ} = \frac{V_{BC}}{I_B} \quad | \quad V_{EC} = \text{constant}$$

Output Admittance

$$h_{oc} = \frac{I_F}{V_{EC}} \quad | \quad I_B = \text{constant}$$

forward current gain

$$h_{fc} = \frac{I_F}{I_B} \quad | \quad V_{EC} = \text{constant}$$

Reverse Voltage gain

$$h_{re} = \frac{V_{BC}}{V_{EC}} \quad | \quad I_B = \text{constant}$$

Typical h-parameter Value for a transistor.

Parameter	CB	CF	CC
$h_i$	$22 \Omega$	$1,100 \Omega$	$1,100 \Omega$
$h_{re}$	$2.5 \times 10^{-4}$	$2.5 \times 10^{-4}$	1
$h_{fe}$	- 0.98	50	- 51
$h_o$	$0.49 \mu A/V$	$25 \mu A/V$	$25 \mu A/V$

### h parameter Conversion table

CF to CB conversion formulae	CF to CC conversion formulae
$h_{ib}^o = \frac{h_{ie}}{1 + h_{fe}}$	$h_{ic}^o = h_{ie}$
$h_{rb}^o = \frac{h_{ie} h_{oe}}{1 + h_{fe}} - h_{re}$	$h_{rc}^o = 1 - h_{re} \approx 1$
$h_{fb}^o = \frac{-h_{fe}}{1 + h_{fe}}$	$h_{fc}^o = -(1 + h_{fe})$
$h_{ob}^o = \frac{h_{oe}}{1 + h_{fe}}$	$h_{oc}^o = h_{oe}$