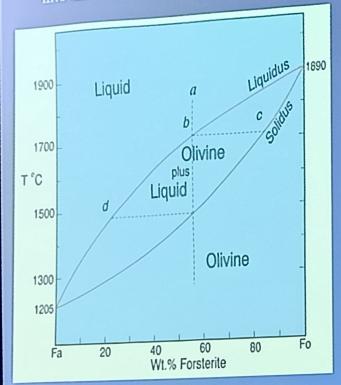
2. If 2 ions have a similar radius and the same valence: the smaller ion is preferentially incorporated into the solid over the liquid



Isobaric T-X phase diagram at atmospheric pressure After Bowen and Shairer (1932), Amer. J. Sci. 5th Ser., 24, 177-213. From Winter (2001) An Introduction to Igneous and Metamorphic Petrology.

smaller ion preferentially -> solid (Mg is smaller than Fe so more Mg in OI than in melt)

- If 2 ions have a similar radius, but different valence: the ion with the higher charge is preferentially incorporated into the solid over the liquid
- Whenever a substitution is possible between two ions with significantly different electro negativities  $(\Delta > 0.1)$ , the ion whose electronegativity is closer to that of the ion it is substituting will be preferentially incorporated

# Goldschmidt's rules originate from a simple ionic model whereby solids (minerals) are viewed as an array of cations and anions with attractive and repulsive forces - CONTROLS LATTICE ENERGY

The concept of lattice energy, U, is a measure of the forces within an ionic crystal

It is a sum of attractive and repulsive forces

We have,

$$U = N_A \left[ -\frac{MZ_1 Z_2 e^2}{4\pi\epsilon_0 r} + \frac{B}{r^n} \right] \quad \& \quad B = \frac{MZ_1 Z_2 e^2 r_0^{n-1}}{4\pi\epsilon_0 n}$$

Substituting the value of B and putting  $r = r_o$ 

$$U_{o} = N_{A} \left[ -\frac{MZ_{1}Z_{2}e^{2}}{4\pi\epsilon_{o}r_{o}} + \frac{1}{r_{o}^{n}} \frac{MZ_{1}Z_{2}e^{2}r_{o}^{n-1}}{4\pi\epsilon_{o}n} \right]$$

$$or, \qquad U_o = N_A \left[ -\frac{MZ_1Z_2e^2}{4\pi\epsilon_o r_o} + \frac{MZ_1Z_2e^2}{4\pi\epsilon_o r_o n} \right]$$

$$U_o = -\frac{N_A M Z_1 Z_2 e^2}{4\pi \epsilon_o r_o} \left(1 - \frac{1}{n}\right) \quad \text{Where,} \quad U_o = \text{lattice energy} \quad \text{Courses-Numericarrying com}$$

# Derivation of Born-Landé equation

Applying the minimization condition,  $\frac{dV(r)}{dr} = 0$ , then  $r = r_0$ 

$$\frac{dU(r)}{dr} = \frac{z^{2}e^{2}}{4\pi\epsilon_{0}r_{0}^{2}}A - \frac{nB}{r_{0}^{n+1}} = 0$$

$$r_{0} = \left(\frac{1\kappa\epsilon_{0}nB}{z^{2}e^{2}A}\right)^{\frac{1}{n-1}}$$

$$B = \frac{z^{2}e^{2}A}{4\pi\epsilon_{0}n}r_{0}^{n-1}$$

$$U(r_{0}) = -\frac{Az^{2}e^{2}}{4\pi\epsilon_{0}r_{0}}\left(1 - \frac{1}{n}\right)$$

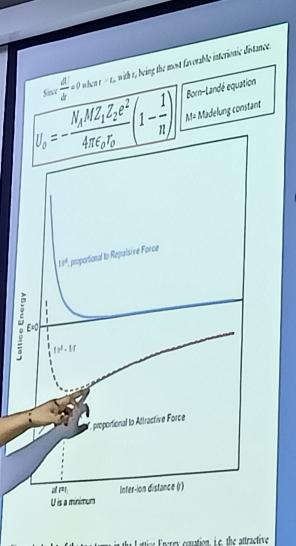
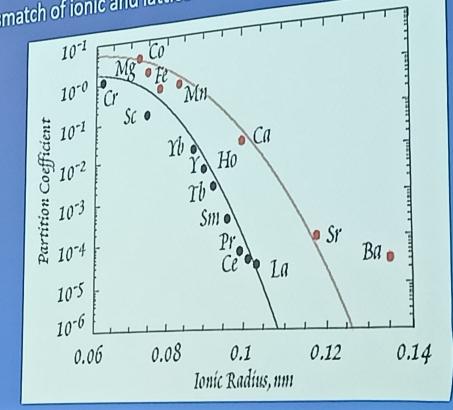


Figure 4: A plot of the two terms in the Lattice Energy equation, i.e. the attractive force varying as  $1i^3$ , showing that there is an interioric distance  $(r_0)$  where the lattice energy is a minimum.

PO F11

- Mineral-melt partition coefficients for series of isovalence on cations show near-parabolic smooth dependence on the cations of isovalence on the cations show near-parabolic smooth dependence on the cations of isovalence or isoval
- Curves for elements having different ionic charge tend to be parallel to each other for the same mineral—melt with increasing
- system
   Reflects increasing lattice strain
   mismatch of ionic and lattice site size



# Onuma curves explained through

Lattice strain model: The lattice strain model assumes that the principal energetic term controlling the incorporation of a misfit cation into a lattice site is the elastic strain energy, MG required to displace the surrounding atoms. The expression representing this strain energy is:

$$\Delta G_{\text{strain}} = 4\pi \text{EN}_A \left[ \frac{r_0}{2} (r_i - r_0)^2 + \frac{1}{3} (r_i - r_0)^3 \right]$$
 (1)

where  $r_0$  is the radius of the crystallographic site,  $r_i$  is the radius of the substituent cation,  $N_A$  is Avogadro's number and E is the Young's modulus of the site. Blundy and Wood (1994) assumed  $\Delta G_{strain}$  to be the dominant energy term determining mineral-melt partitioning and linked the partition coefficient for element i,  $D_i$ , to  $\Delta G_{strain}$  as follows

$$D_{i} = D_{0} * \exp \left( \frac{-4\pi E N_{A} \left[ \frac{r_{0}}{2} (r_{i} - r_{0})^{2} + \frac{1}{3} (r_{i} - r_{0})^{3} \right]}{RT} \right)$$
(2)

where D<sub>0</sub> is the partition coefficient for an element with ideal radius  $r_0$ . We have fitted equation (2) to all REE data reported Also lattice energy is at a minimum in a system of spherical ions when each ion is surrounded by as many ions of opposite charge as possible

This increases the attractive forces relative to the repulsive forces, thereby lowering the lattice energy

Use of Ionic radii to predict coordination number of cations in silicate Cation coordination number (CN) for silicate minerals is the number of oxygen anions surrounding

a cation

If we assume that 1) cations and anions are rigid spheres, and 2) ionic radii are constant, the concept of radius ratio (Pauling's

i.e. (cation ionic radii)/ (oxygen ionic radii) can be used to predict cation coordination number

Radius ratio	Anion arrangement around cation	Cation coordination number		Example
<0.155 0.155 to 0.225	Linear  Corners of equilateral triangle	2		B <sub>2</sub> CO <sub>3</sub>
0.225 to 0.414	Corners of tetrahedron	4		ZnS, CuCl
0.414 to 0.732	Octahedral	6		NaCl, MgO
0.732-1.0	Cubic			CsCl
>1	Midpoint of cube edges	12 packing)	(close	

Major element	Substituting trace element
Si	Ge, P
Ti Carlos	V
Al	Ga
Fe Company of the Com	Cr, Co, Ni
Mg	Cr, Co, Ni
Ca	Sr, Eu, REE
Na	Eu
(	Rb, Ba, Sr, Eu

We now know that Goldschmidt's Rules are not rigorously correct: (1) We have learnt that for a given structural site in a mineral, there is an optimal jonic

- radius and ions that are too large or too small are less readily incorporated into the (2) Highly charged ions not always preferentially incorporated into solids, e.g., there
- (3) Partitioning involves two phases, and in solid-melt partitioning, the effects of melt composition cannot be ignored; Goldschmidt's Rules consider only the crystal phase
- (4) In fluids, the partitioning of trace elements is often controlled complexation/chelation characteristics of the cation. This is primarily controlled by F11 the electronic configuration and not the ionic charge and radius

# Trace element fractionation during partial melting and crystallization

# . Batch Melting

Melt continuously reacts & equilibrates with the solid residue at the site of melting until mechanical conditions allow it to escape as a single 'batch' of magma

Batch melting can be modal and non modal

Minerals melt in the proportion in which they exist in the rock

Minerals melt in a proportion different from that of their mode in the rock

# **Batch melting equation-derivation**

C<sub>L</sub> =concentration of element in melt

C<sub>0</sub> = starting concentration of element in un-melted source

 $C_s$  = concentration of element in un-melted residue

F = weight fraction of melt produced (wt. of melt/wt. of melt + wt. of residual rock)

For closed system equilibrium melting, simple mass balance between the phases yields:

$$C_O = F * C_L + (1-F) * C_S$$

Since 
$$D_{RS} = C_S / C_L$$

So, 
$$C_S = D_{RS} * C_L$$

Substituting C<sub>s</sub> in the mass balance equation gives:

$$C_0 = F * C_L + (1-F) * D_{RS} * C_L$$

$$C_{o} = C_{L} [F + (1-F) * D_{RS}]$$

$$C_L / C_O = 1/[F + (1-F) * D_{RS}]$$

$$C_L / C_O = 1 / [F + D_{RS} - F^* D_{RS}]$$

$$C_L / C_O = 1 / [F^*(1-D_{RS}) + D_{RS}]$$

$$C_S / C_O = D_{RS} / [D_{RS} + F (1 - D_{RS})]$$
  $D_{RS} \rightarrow \text{bulk partition co-efficient of residual solid}$ 

$$\frac{C_{L}}{C_{O}} = \frac{1}{D_{RS}(1-F)+F}$$