

Shape of adhesive fluid controls insect adhesion in air and underwater

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Abstract

Insects like beetles can stick to various surfaces using hairy pads mediated by an oily adhesive fluid. It was previously shown, the pads can even attach underwater, presumably due to an air bubble trapped around the pad. However, the bubble's relative contribution to adhesion via capillary force remains unclear. To investigate the exact role of bubble, in this study, we perform *in-vivo* underwater adhesion measurements of a ladybug pad in the presence and absence of trapped bubble and compare it with adhesion in air. Our experiments reveal that on a hydrophobic substrate, even without a bubble, the pad can show adhesion underwater comparable to that in air. Only on a hydrophilic substrate, a trapped bubble is necessary to aid adhesion underwater. To explain these results, we develop a simple theoretical model to estimate the net adhesion of a hairy pad due to capillary forces. Our results demonstrate that capillary forces in insects are primarily governed by the shape of the adhesive fluid and can help explain its adhesion both in both air and underwater conditions.

1 Introduction

The question of how insects can walk on smooth surfaces against gravity has fascinated scientists for at least the past three centuries^{1,2}. We now know that such animals are able to adhere by using specialized organs on their feet called adhesive pads. These adhesive pads exist in a variety of types depending on the animal, but are generally categorized into: 1) “smooth pads” found in ants³, stick insects⁴, etc. and 2) “hairy pads” seen in flies⁵, geckos⁶ and others. The hairy pads show: 1) compliance to rough surfaces due to their lower effective modulus, 2) angle dependent adhesion due to asymmetric hair geometry and 3) self-cleaning capability⁷, which makes it suitable to adhere to most surfaces reversibly. Many of these insects pads also secrete an adhesive fluid as seen in flies and ants³ (“wet adhesion”), while others such as spiders and geckos rely on their dry hairy pads for attachment (“dry adhesion”). In the “wet adhesion” case, fluid secretion can enforce adhesion through surface tension and viscous forces⁸, on the other hand, “dry adhesion” relies mostly on van der Waals forces⁶.

Terrestrial beetles such as the dock beetle or ladybug have hairy pads consisting of a dense array of hair like structures called setae. The setae tips can be discoidal, spatula or pointed shaped, which are distributed throughout the pad depending on sex or species⁹. Single seta force measurements revealed that discoidal shaped seta shows larger pull-off force than spatula and pointed setae¹⁰, illustrating the role of hair geometry in adhesion. The tip of each seta secretes approximately one femtoliter oily adhesive fluid¹¹. The fluid’s chemical composition is identified as a mixture of mostly long chain hydrocarbons¹² with traces of triglycerides, fatty acids and cholesterol^{13,14}. A recent study by Gernay et. al.¹⁵ based on an elastocapillary model has been able to reasonably predict single seta adhesion forces theoretically, confirming the dominant role of surface tension in the “wet adhesion” of beetles.

While most of the studies on insect adhesion are done under natural conditions in air, insect attachment underwater has been relatively unexplored. Typically, underwater adhesion is complicated to achieve due to the difficulty in displacing the water layer and enable good contact¹⁶. Regardless, a study on leaf beetles¹⁷ has revealed that beetles can attach

well to surfaces underwater. Its hairy pad traps an air bubble underwater, which dewets the surface on contact. It has been hypothesized that a combination of capillary forces due the air bubble and hair contact within the dewetted area results in attachment. However, a detailed investigation of the bubble’s contribution and necessity to adhere to different surfaces is lacking. Geckos are also known to adhere underwater, where its shear adhesion force on hydrophobic substrates are similar in both air and underwater conditions. Interestingly, its adhesion on a fluorinated substrate is even larger underwater than in air¹⁸. This has been partially explained by a thermodynamic work of adhesion model, assuming full displacement of water at the interface, leading to dry contact of hairs with the surface¹⁹.

The goal of this paper is to provide a generalized picture of adhesion in insects using hairy pads secreting a fluid for attachment. First, we perform adhesion measurements of a single constrained pad of a live ladybug beetle in air and underwater conditions on smooth hydrophilic and hydrophobic glass surfaces, with a microscopic observation of the contact process. Second, we develop a simple theoretical model considering capillary forces to predict the net adhesion force of a hairy pad under different conditions. Finally, we discuss key insights gained from our experiments and model as well as possible implications in understanding adhesion in other animals.

2 Experimental

Normal adhesion force measurements on a restrained leg of a live ladybug beetle were performed. We characterize adhesion by the pull-off force during detachment. Measurements were done against smooth glass and fluorinated surfaces to represent hydrophilic and hydrophobic substrates respectively. When no water is present, we labeled the contact type as “*In-Air*”. For the underwater conditions, measurements were done both in the presence and absence of a trapped bubble (“*Underwater: bubble*” and “*Underwater: no bubble*”, respectively) to investigate the bubble’s role in underwater adhesion. Adhesion force for each

of the labeled contact types are compared for both substrates.

2.1 Material and Methods

2.1.1 Insect preparation

Seven-spotted adult ladybug beetles (*Coccinella septempunctata*) purchased from Katz Biotech (Baruth, Germany) were used for adhesion tests. The beetles were housed in a plastic box filled with leaves, twigs and stones under at room temperature and 60-80% relative humidity with daily access to sunlight. The beetles were fed with raisins, honey and water *ad libitum*.

Experiments were done on male beetles. Each leg of the beetle has a pair of hairy pads covered with mostly discoidal shaped setae, capable of strong adhesion. For the test, we only allow the distal-end pad to make contact. The beetle's leg was constrained similar to the method described by Bullock et al⁹. A steel ball fixed with a piece of thick solder wire serves as a rota-table holder to fix the beetle and align its leg (Figure 1). The beetle was first anesthetized using CO₂ sublimating from a piece of dry ice and glued to the steel ball on its back. Its front left leg was carefully fixed to the solder wire using Blue-Tac. Its claws were fixed using epoxy glue to prevent any wiggling. The leg was aligned such that only the distal pad of its leg can make contact. A small piece of non-sticky Teflon tape helped to keep its other legs tucked close to the body to minimize interference during the measurements.

After measurements, the beetle was freed by carefully removing the epoxy glue and Blue-Tac without harming it using a pair of tweezers and set free.

2.1.2 Substrate preparation

Standard 20 mm wide glass coverslips are used as the hydrophilic substrate. Glass was wiped with isopropanol, rinsed in water and dried under nitrogen flow. The surface was then plasma cleaned in oxygen plasma chamber (Diener Electronic Femto) for 10 mins at 120 W. The surface was further rinsed with water and dried under nitrogen flow.

For the hydrophobic substrate, the glass cover slip was coated with a fluorosilane via

chemical vapor deposition (CVD). The glass was first cleaned using IPA and plasma treated as before. 0.2 ml of Trichloro(1H,1H,2H,2H-perfluorooctyl) silane (PFOTS), procured from Sigma Aldrich, was put in a sealed chamber along with the the glass cover slip. The chamber was placed under 100 mbar pressure for 10 mins for the CVD process. The glass substrates were finally annealed at 150°C for 3 hours.

The substrate wettability was characterized by dynamic contact angle measurements performed with a DataPhysics OCA 35 contact angle goniometer using water and n-hexadecane. Advancing and receding contact angles were measured for a maximum drop volume of 10 μ l and with 0.5 μ l/s flow rate. Static contact angles were measured for a 5 μ l drop.

Table 1: Static and dynamic contact angles measurements

Substrate	Liquid	θ_A	θ_R	θ_S
Glass	Water	$63 \pm 5^\circ$	$20 \pm 2^\circ$	$57 \pm 2^\circ$
	n-Hexadecane	$< 10^\circ$	$< 10^\circ$	$< 10^\circ$
PFOTS	Water	$122 \pm 1^\circ$	$93 \pm 2^\circ$	$110 \pm 2^\circ$
	n-Hexadecane	$88 \pm 2^\circ$	$56 \pm 5^\circ$	$72 \pm 2^\circ$

2.1.3 Field desorption mass spectroscopy

Field Desorption Mass Spectrometry (FDMS) measurements of the adhesive fluid secretions were performed using ZAB 2-SE-FPD spectrometer (VG Instruments). A previous study on archanids²⁰ reported that the secreted fluid does not dissolve away in water. To confirm this for the beetle, measurements before and after the immersion of its legs in water were done. The middle leg of an Asian ladybird (*Harmonia axyridis*) was immersed in 50 μ L THF for 20 m and then transferred to the measurement chamber of the FDMS. As a reference, pure THF was used. The second middle leg of the same ladybird was immersed in 100 μ L milli-Q water for 15 minutes, then in THF for 20 minutes and then transferred to the measurement chamber of the FDMS. Molecular composition is extracted from the peak positions of the FDMS data.

2.1.4 Adhesion test

Adhesion measurements were performed on a custom force measurement setup developed in-house (Figure 1). A fiber optic displacement sensor (Philtec D20, PHILTEC, Inc. USA) together with a steel bending beam (spring constant = 68.1 N/m) constitutes the vertical force sensor. Beam deflection was calibrated using 4 different known weights to get the corresponding force. A plastic 3D printed substrate holder was glued to the end of the bending beam. The holder was designed to allow switching from one substrate to another without removing any glue. It also had transparent side walls which allowed us to fill it with water for the underwater experiments. The sensor was mounted on a stage consisting of a X-piezo used for precise lateral movements, XYZ motors for coarse movements and goniometer for adjusting substrate alignment with the optics. Additionally, a separate Z-piezo fixed upright is used for vertical up-down motion, bringing the specimen in contact with the substrate from top. A 3 axis manual micro-manipulator together with a free stainless steel ball allowed good alignment of the beetle's foot to the substrate. A coaxial illuminated tube microscope (Navitar) with 2x objective and a stereo-microscope with 1x objective (Wild Heerbrugg) fit with cameras are used to record the sample contact with the substrate from bottom and side views respectively. Pad contact area was visualized in total reflection mode by the ventral view camera. The data acquisition from the force sensor and cameras together with an appropriate piezo motion steps are synchronized using a custom LABVIEW program. Force data was acquired at a sample rate of 984 Hz, averaged to 512 points per motion step. Videos were recorded at 20 frames per second.

The vertical and lateral piezos were together used to perform approach-retract adhesion tests with the substrate to get the pull-off force. However, instead of a simple down-up motion some additional motion steps were included (Figure 1 b). A 100 μm lateral sliding motion was done after the initial approach step to give a proximal pull to the beetle's leg and thus properly orient its hairs with the substrate⁹. An additional 10 μm compression step (approach) was done to ensure all hairs are loaded in compression and make good contact

with the surface. A short pause (1 s) was introduced to minimize any viscoelastic effects before finally retracting the leg away from the substrate. All approach, retract and lateral slide was done at a speed of $62.5\text{ }\mu\text{m/s}$. Ventral view video recordings were used for contact area extraction while the side view imaging is used only to visually aid orienting the pad with the substrate before a test. Figure 1 shows a typical measurement recording, where force and contact area are plotted as a function of time.

For underwater experiments, 1 ml deionized water was pipetted into the substrate holder. In order to achieve an underwater “wet” contact, the likelihood of bubble trapping between the pad was reduced by degassing the water in a vacuum chamber for 3 hours before use.

Before experiment, the pad was repeatedly brought into contact with the surface 10 times to equilibrate the pad system. 5 force measurements were subsequently performed on a fresh spot of the substrate and averaged for data analysis. Experiments were repeated with 5 individual beetles for each type of contact and substrate. In total, 30 beetles were tested.

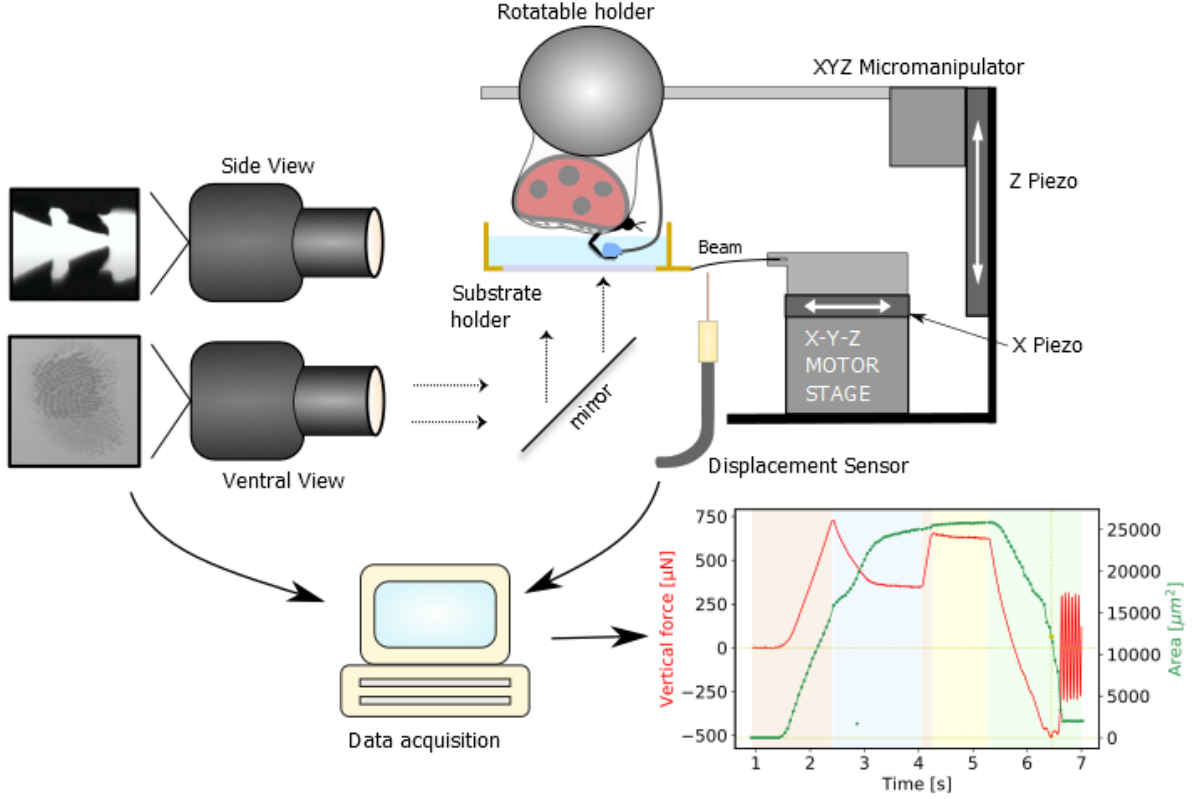


Figure 1: Adhesion test setup. Representative force data and contact area of distal pad is also shown. Shaded regions represent distinct motion steps. Minimum peak value during final retract step is taken as adhesion force.

2.1.5 Data analysis

Extraction of pull-off force from force data, image processing, plotting and statistical analysis were all performed in “Bug”²¹, a tool written in Python using open-source libraries for synchronous analysis of force data and video recordings.

For measurements in air, pull-off force is defined as the minimum negative force during the final retraction step. For underwater measurements, an additional correction needs to be done first. During the piezo motion, contact line of the immersed holder at water surface changes, influencing the force readout due to surface tension. This effect needs to be canceled. So, a background force data is recorded where the submerged beetle makes no

contact with the substrate. The background forces is then subtracted from a typical force data with substrate contact to correct for the external surface tension effects. After this, the pull-off force is calculated from the minima as before.

Data sets are compared for statistical differences using pairwise t-test and their corresponding p-value and CLES effect sizes are reported. Shapiro-Wilk test was done for each data set to verify a normal distribution of its residuals and Levene’s test was done to check for variance homogeneity, to validate the t-test assumptions.

2.2 Results

2.2.1 Field desorption mass spectroscopy

Molecular weights of secreted fluid mixtures extracted from an Asian ladybird (*Harmonia axyridis*) without (left) and with (right) immersion in water are compared (Table 2). Except from two molecular weights (406.8 g/mol and 331.6 g/mol), the chemical fingerprint remained unchanged, indicating stability of the lipid mixture underwater. Probable molecules, corresponding to the resulting molecular weights, include aliphatic hydrocarbons and aldehydes.

Table 2: Molecular weights of adhesive fluid secretion of *Harmonia axyridis* with and without rinsing the beetle’s leg in water. Molecular weights correspond to peaks in the FDMS data.

Without rinsing (g/mol)	After rinsing (g/mol)	Probable compounds
324.5	324.5	C ₂₃ H ₄₈ , C ₂₂ H ₄₄ O
	331.6	C ₂₄ H ₄₄
350.5	350.5	C ₂₅ H ₅₀
352.5	352.5	C ₂₅ H ₅₂ , C ₂₄ H ₄₈ O
378.5	378.5	C ₂₇ H ₅₄
404.6	404.5	C ₂₉ H ₅₆
406.8		C ₂₉ H ₅₈
432.8	432.7	C ₃₁ H ₆₀

2.2.2 Adhesion measurements

Adhesion force for the distal pad of ladybug beetle against glass and PFOTS in air and underwater conditions are compared (Figure 2 and Table 3). In air, there is no significant

difference in the adhesion force between glass and PFOTS substrate ($p = 0.959$). Underwater however, adhesion on a PFOTS surface is significantly larger than on glass when there is no trapped bubble ($p < 0.001$). On PFOTS, there is no significant difference in the adhesion force in air or underwater conditions. But on glass, adhesion in air is significantly larger than underwater in the presence ($p = 0.002$) or absence ($p < 0.011$) of the bubble. At the same, we see that the presence of bubble results in a higher adhesion force than with no bubble (CLES = 0.84), although the difference is not statistically significant ($p = 0.07$).

Table 3: Pairwise statistical comparison of adhesion force for each contact type and substrate. The p-values and Common Language Effect Size (CLES) are obtained from post-hoc pairwise Student t-test between A and B while keeping the third parameter fixed. p-values showing statistically significant difference between A and B are in boldface, where the critical p-value = $0.05/6 = 0.008$, based on Bonferroni’s correction for multiple comparison.

Fixed	A	B	p-value	CLES
In air	PFOTS	Glass	0.959	0.48
Underwater: bubble	PFOTS	Glass	0.011	0.96
Underwater: no bubble	PFOTS	Glass	< 0.001	1.0
PFOTS	In air	Underwater: bubble	0.897	0.48
PFOTS	In air	Underwater: no bubble	0.828	0.48
PFOTS	Underwater: bubble	Underwater: no bubble	0.721	0.44
Glass	In air	Underwater: bubble	0.002	1.0
Glass	In air	Underwater: no bubble	< 0.001	1.0
Glass	Underwater: bubble	Underwater: no bubble	0.07	0.84

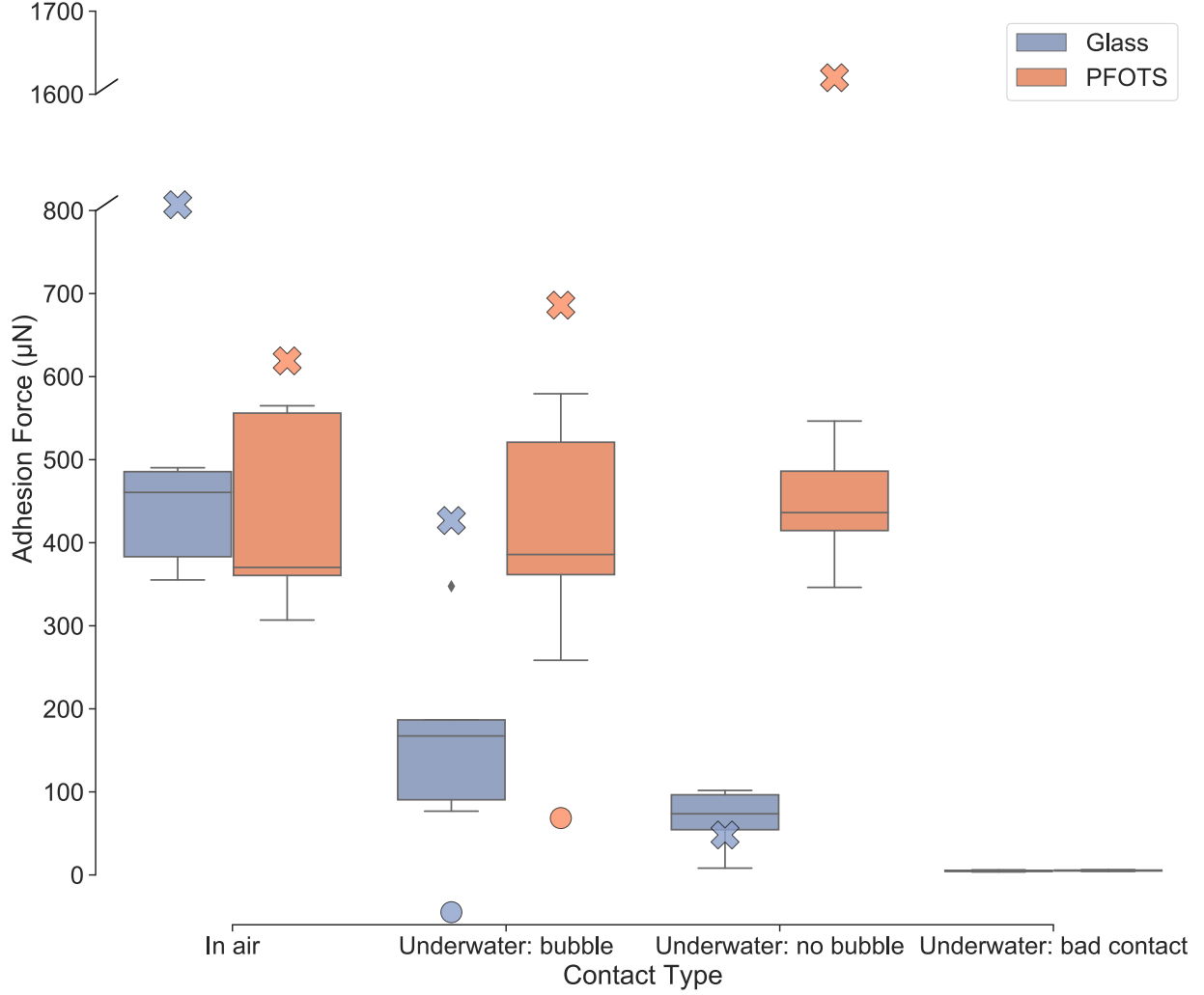


Figure 2: Single leg adhesion force measurements of ladybug beetle on glass and PFOTS substrates in air and underwater conditions. Values represent peak force of a distal pad pulled off from each substrate at $62.5 \mu\text{m/s}$ retraction speed. Three types of contact are seen in underwater experiments and are represented separately: “*bubble*”, “*no bubble*” and “*bad contact*”. Stars represent theoretical predictions of adhesion force calculated from the capillary bridge model, where hair diameter = $4 \mu\text{m}$, pad diameter = $200 \mu\text{m}$, hair height = $40 \mu\text{m}$, $N_{\text{hairs}} = 500$, $V_{\text{fluid}} = 4.2 \text{ fL}$ and $V_{\text{bubble}} = 1.2 \text{ nL}$. Interfacial tension of the adhesive in air and water are assumed to be 24 mN/m and 48 mN/m respectively and water surface tension is 72 mN/m .

Apart from the three predicted contact types, we also observed an additional fourth type of contact which randomly occurs underwater, labeled as “*bad contact*”. In this scenario, the hairs don’t appear to make a perfect contact with the substrate, as seen in the other three contact types. “*Bad contact*” shows no adhesion with either glass or PFOTS substrate.

While it's not completely clear why such a contact occurs, there can be two possible reasons. First, the hairs could get bundled due to a small air meniscus inside the hairs, resulting in ~~its~~ disorientation. Second, the substrate is not dewetted during contact, causing a thin water layer on the surface to prevent adhesion.

3 Theory

3.1 Capillary Bridge Model

We modeled the hairy pad as an array of N cylindrical rods of length L and diameter, D_h fixed to a flat circular base of pad diameter D_p as shown in figure 3. For simplicity, we assume both hairs and the pad to be perfectly rigid. The tip of each cylindrical hair has an adhesive fluid of volume V_f making contact with the substrate. The fluid is assumed to be pinned to the circumference of the hair and forms a capillary bridge of height d with the substrate. In order to model the contact in both air and underwater conditions, we consider three types of contacts as seen in our experiments with the beetle:

1. *In air* - All hairs and fluid bridges are surrounded by air
2. *Underwater: no bubble* - All hairs and fluid bridges are surrounded by water
3. *Underwater: bubble* - A bubble of volume V_b is trapped between the hairs. The bubble is pinned to pad circumference. Liquid bridges forming contact with the substrate within the bubble are surrounded by air while the ones forming contact outside the bubble are surrounded by water.

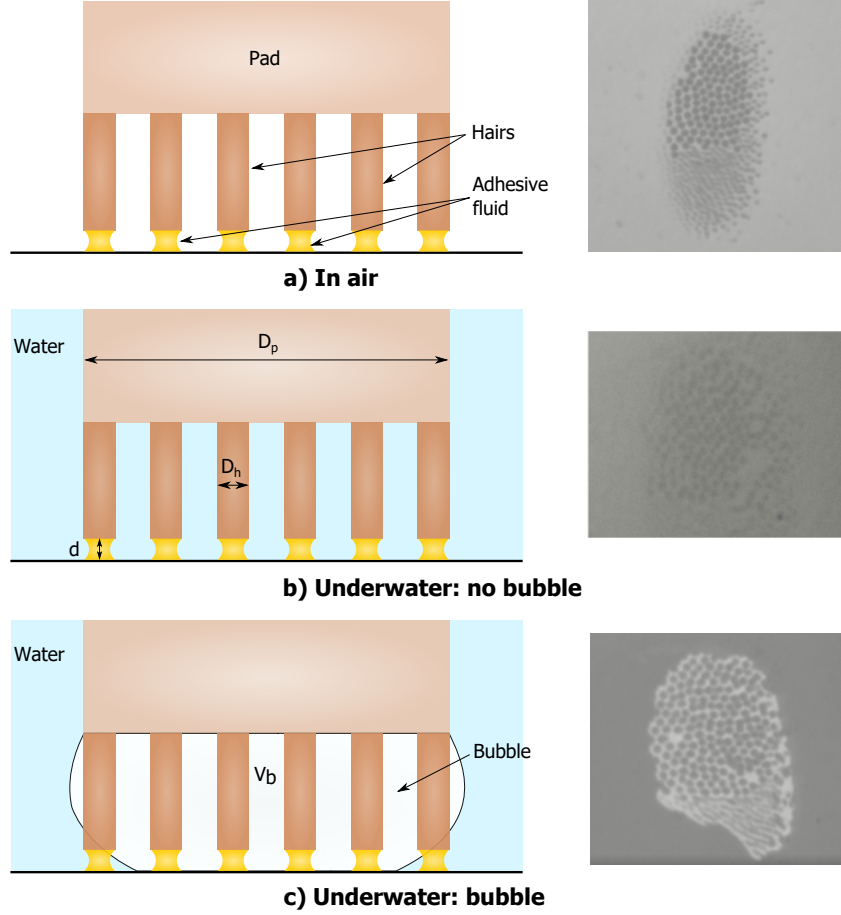


Figure 3: Capillary Bridge Model. The hairy pad system comprises of a cylindrical pad of diameter D_p acting as support for an array N rigid cylindrical hairs with diameters D_h . The tip of each hair carries an adhesive fluid forming a capillary bridge with the substrate. The hairs makes contact with a substrate in three ways: a) *In air*, where the adhesive fluid bridges are surrounded by air; b) *Underwater: no bubble*, where the adhesive fluid bridges are fully surrounded by water; c) *Underwater: bubble*, where part of the adhesive fluid bridges are inside the bubble while others are outside in water. The corresponding contact images of the beetle's pad are shown on the right.

Let $V_f = 4/3\pi s_f^3$ and $V_b = 4/3\pi s_b^3$, where s_f and s_b are the radii of spheres with equivalent volumes. Fluid and bubble radii are assumed to scale proportional to their corresponding pinned contact diameter. We thus define the size parameters $\phi_f = D_f/2s_f$ and $\phi_b = D_b/2s_b$ for the fluid and bubble respectively to conveniently scale their sizes relative to the corresponding hair and pad diameters they are pinned to. The tip of the hairs are at a distance d from the the substrate.

The net adhesion force for case 1 and 2 can be calculated as:

$$F_{net} = Nf \quad (1)$$

Here, f is capillary force by a single fluid bridge at distance d , and N is the total number of hairs

For case 3, the net adhesion force is given by:

$$F_{net} = N_{in}f_{air} + N_{out}f_{water} + f_{bubble} \quad (2)$$

Here, N_{in} and N_{out} are the number of hairs inside and outside the bubble respectively. f_{air} and f_{water} are the capillary forces at distance d of a fluid bridge inside and outside the bubble surrounded by air and water respectively, and f_{bubble} is the capillary force contribution due to the bubble meniscus alone.

The capillary force, f is the sum of two contributions: surface tension and Laplace pressure. Force versus distance for a single capillary bridge is calculated by numerical simulations, described in appendix (A.1) and used to obtain F_{net} as a function of d for each type of contact. The adhesion force of the full hairy pad system is then obtained from the minima of the respective force-distance curves.

We have considered f_{air} and f_{water} to be distinct terms because the capillary force by the adhesive fluid will be different in air and water due to its different contact angles and interfacial tensions. Using the Young-Dupre equations, one can derive the following relation for the contact angle of the adhesive fluid underwater:

$$\cos \theta_{fw} = \frac{\gamma_{fa} \cos \theta_{fa} - \gamma_{wa} \cos \theta_{wa}}{\gamma_{fw}} \quad (3)$$

Here, θ_{fw} and θ_{fa} are the contact angles of the adhesive fluid with the substrate in water and air respectively, θ_{wa} is the contact angle of water with the substrate in air, γ_{fa} is the surface tension of adhesive fluid, γ_{wa} is the surface tension of water and γ_{fw} is the interfacial

tension of adhesive fluid with water.

All lengths were normalized w.r.t. s_f and forces are normalized w.r.t. γ_{fa} . Non dimensional bubble volume, $\hat{V}_b = V_b/s_f^3$

Fixed parameter values used for all model calculations are listed in Table 4. We consider representative hydrophilic and hydrophobic substrates with θ_{fa} and θ_{wa} values corresponding to a typical glass and fluorinated surface respectively. Interfacial tension values are fixed relative to γ_{fa} . We assume the adhesive fluid to be an oil-like substance and thus the interfacial tension ratios γ_{wa}/γ_{fa} and γ_{fw}/γ_{fa} are taken corresponding to typical values of oil and water. Area fraction of hairs relative to the pad defined as $\alpha = ND_h^2/D_p^2$, hair aspect ratio L/D_h and fluid size parameter ϕ_f are fixed to values typical for an insect hairy pad.

First, we calculate force-distance curves for a single pinned liquid capillary bridge. Second, the effect of substrate on the resultant force-distance curve of the hairy pad system is studied for each type of contact. Third, the effect of varying hair diameter on net adhesion is studied by varying D_p/D_h . Finally, ϕ_b is varied to study the effect of bubble volume on the net underwater adhesion.

Table 4: Model parameters

Property	Value
Area fraction, α	0.1
Hair aspect ratio, L/D_h	10
Water surface tension ratio, γ_{wa}/γ_{fa}	3
Fluid-Water interfacial tension ratio, γ_{fw}/γ_{fa}	2
Fluid size parameter, ϕ_f	2
Hydrophilic substrate	$\theta_{fa}=6^\circ$, $\theta_{wa}=24^\circ$
Hydrophobic substrate	$\theta_{fa}=50^\circ$, $\theta_{wa}=120^\circ$

3.2 Results

3.2.1 Capillary force of a pinned liquid bridge

Forces due to a single pinned capillary liquid bridge in contact with a substrate are obtained via simulations (Figure 4). Capillary forces are more attractive for smaller contact angles.

The Laplace pressure contribution to the net adhesion force dominates for contact angles less than 100° (Figure 4b). Interestingly, its contribution to adhesion force is mostly non-repulsive for contact angles greater than 90° . This is because the low volume of fluid and pinned contact line prevents the fluid bridge from having a high positive curvature due to geometric constraints. Only for a contact angle of 150° , the fluid curvature becomes positive, manifested in its slightly repulsive Laplace contribution. Surface tension makes a significant contribution to the net force only for contact angles greater than 70° . For contact angles greater than 150° , the net adhesive force approaches zero. Since Laplace pressure is an indicator of the fluid bridge shape, one can make a general statement that the shape of the fluid bridge primarily determines the strength of its adhesion force for low and high contact angles. High adhesion is thus seen for contact angles less than 70° due to a net negative curvature of the fluid shape, while low adhesion is seen for contact angles greater than 150° due to its net curvature being close to zero.

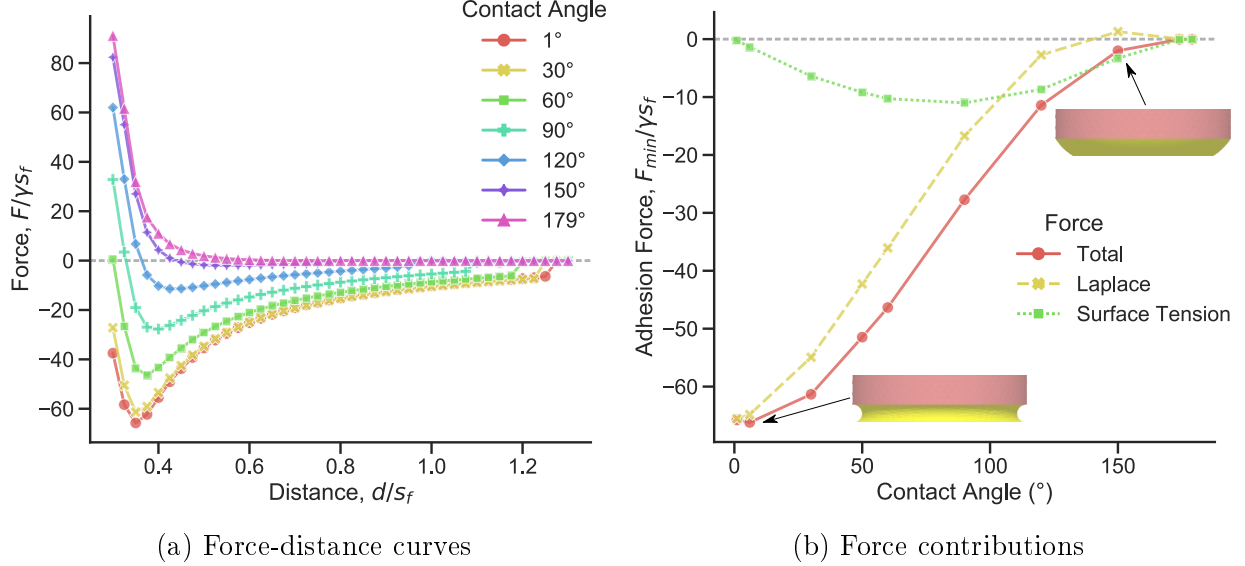


Figure 4: Normalized capillary force of a single liquid meniscus in contact with a substrate and pinned to a circular perimeter on top. Fluid size parameter $\phi_f = 2$. Negative value represents attractive forces. a) Force-distance curves are shown for different contact angles of the liquid with the substrate. b) Adhesion force, calculated from the minima of the corresponding force-distance curve plotted as a function of contact angle with the substrate, shown in red (circles). Laplace and surface tension contributions to the net total adhesion force are shown in yellow (cross) and green (squares) respectively. Simulation snapshots of liquid meniscus corresponding to angles 6° and 150° are depicted.

The force-distance curves show a general trend of being repulsive at small distances (Figure 4 a). This is a result of the pinned contact line constraint. A limited volume is available for the fluid to occupy when the gap distance is small, causing the fluid shape to bulge outward near the pinned contact line. This creates a net positive curvature, resulting in a positive Laplace pressure and thus repulsion.

3.2.2 Capillary Bridge Model: Effect of the substrate

The normalized force-distance curves for a hairy pad system on a hydrophilic and hydrophobic substrate are predicted based on the capillary bridge model (Figure 5). The forces for each type of contact are calculated from equations (1) and (2). Rest of the parameters are kept constant for a direct comparison of the effect of contact type and substrate chemistry.

On the hydrophilic substrate ($\theta_{wa} = 24^\circ$), contact in air shows the highest attractive forces.

Underwater: no bubble contact shows close to no adhesion while *underwater: bubble* contact shows moderate adhesion. In contrast, for a hydrophobic substrate ($\theta_{wa} = 120^\circ$), the highest attractive forces are seen for *underwater: no bubble* contact, much larger than adhesion *in air*. Even *underwater: bubble* contact has slightly higher adhesion than *in air*. Note that the contact area is fixed by keeping the area fraction α (Table 4) and pad/hair size (D_p/D_h) constant. All curves correspond to the same total hair contact area. The above effects can thus be attributed solely to how the the capillary force changes for each type of contact.

On a hydrophilic substrate, the contact angle of the oily adhesive fluid is 6° (Table 4) when surrounded by air and 150° when surrounded by water, as calculated from equation (3). This results in the capillary bridge shape having a net negative and slightly positive curvatures respectively (Figure 8). Since Laplace contribution controls capillary force at such extreme contact angles (see section 3.2.1), the fluid bridges show strong adhesion in air while underwater, they show little to no adhesion.

On a hydrophobic substrate however, the contact angles of the fluid in air and water are 50° and 1° respectively. In both cases, the contact angles are low, resulting in a net attractive force in both types of contact. Additionally, the interfacial tension of the oily fluid underwater (γ_{fw}) is twice that of in air (γ_{fa}). Thus, we see higher attractive force in a *underwater: no bubble* contact when compared to contact *in air*.

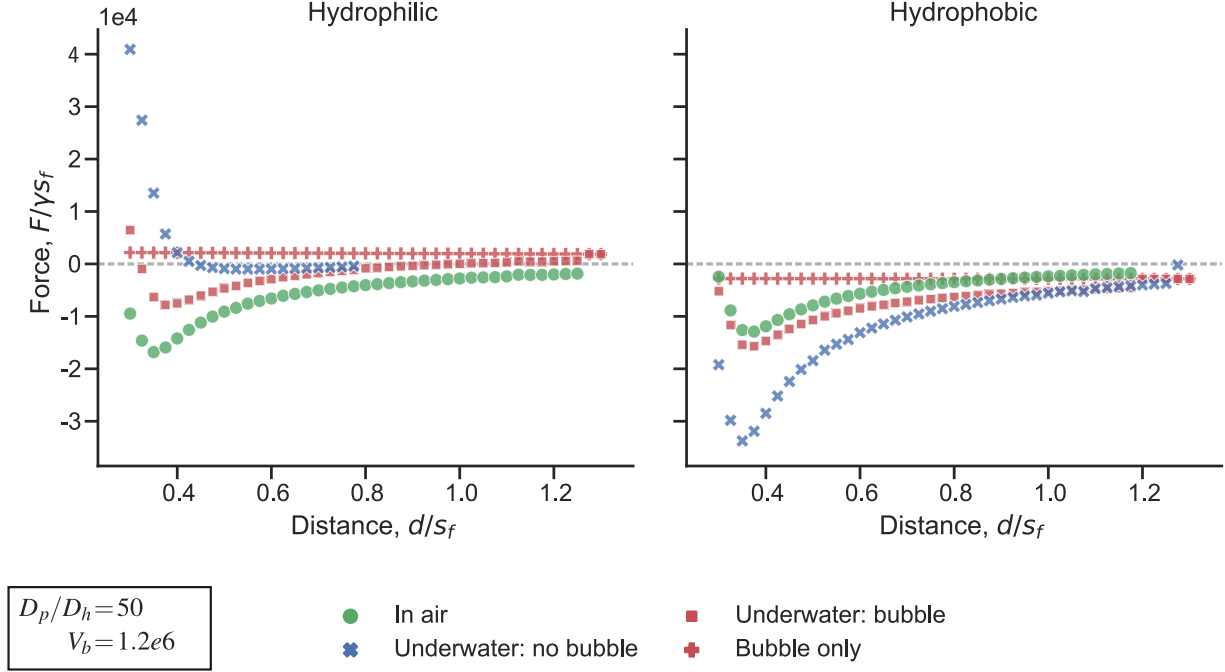


Figure 5: Theoretical force-distance curves of a hairy pad system on a hydrophilic (left) and hydrophobic (right) substrate in air and underwater conditions. A negative value represents attractive force. Normalized forces are calculated from the capillary bridge model, with model parameters listed in Table 4. The bubble's contribution to the net force for an *underwater: bubble* contact is denoted by plus symbols. Pad to hair diameter ratio (D_p/D_h) and bubble volume are kept fixed.

The net force in the *underwater: bubble* contact mainly depends on the proportion of hairs inside the bubble surrounded by air or outside the bubble surrounded by water (see equation (2)). For the given bubble volume, only part of the hairs are inside the bubble for the hydrophilic substrate while all the hairs are inside the bubble for the hydrophobic substrate. Therefore, its force curve lies in between *in air* and *underwater: no bubble* contact on a hydrophilic substrate, and closely follows that *in air* for a hydrophobic substrate.

The contribution of capillary force created by the bubble is negligible for both hydrophilic and hydrophobic substrates (Figure 5). Its contribution even is slightly repulsive on the hydrophilic substrate due to the positive curvature of the bubble, and slightly attractive on the hydrophobic substrate due to its negative curvature. The small contribution is manifested by a small downward shift in the *underwater: bubble* contact force curve on hydrophobic

substrate. Here, all the hairs are trapped inside the bubble and thus its slightly higher adhesion relative to air contact is due to the small additional contribution of the bubble.

3.2.3 Capillary Bridge Model: Effect of hair diameter

The effect of changing hair diameter, D_h to the net adhesion force is compared for hydrophilic and hydrophobic substrates (Figure 6). Here, the pad diameter, total hair contact area and bubble volume are constant since D_p , α and ϕ_b are fixed. The radius corresponding to the fluid volume is assumed to scale proportional to the hair diameter ~~it is pinned~~ to ($\phi_f = 2$).

Adhesion force increases with decreasing D_h for both hydrophilic and hydrophobic substrates in all contact types. This is consistent with the “contact splitting” theory which predicts higher adhesion when the contact is split into many small contacts points²². Reducing the hair diameter results in two competing effects: 1) capillary force due to a single fluid bridge decreases due to its smaller size and “self-similar” scaling assumption, which decreases the net force, and 2) total number of fluid bridges, N increases since the total hair contact area is assumed to be fixed, which increases the net force. The net effect results in higher adhesion force as D_h decreases.

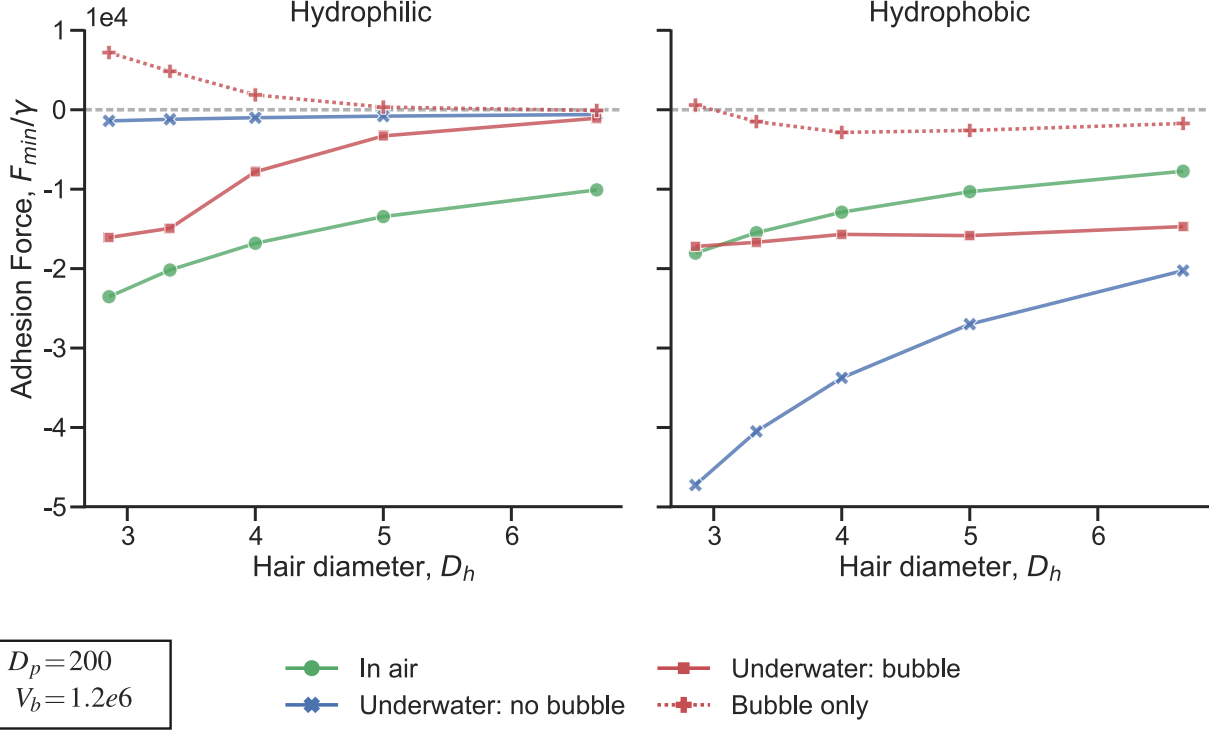


Figure 6: Normalized adhesion force of a hairy pad system on a hydrophilic (left) and hydrophobic (right) substrate as a function of hair diameter (D_h), calculated from the capillary bridge model. Negative value represents attractive force. The bubble's contribution to the net force for an *underwater: bubble* contact is denoted by plus symbols. Pad diameter and bubble volume are kept fixed. Adhesion forces are calculated from the minima of the respective force-distance curves. Length in arbitrary units.

Similar to the trend in Figure 5, contact in air shows the highest adhesion force for the hydrophilic substrate for all hair diameters, while on the hydrophobic substrate, *underwater: no bubble* contact shows highest adhesion. *Underwater: bubble* contact shows intermediate adhesion between *in air* and *underwater: no bubble* contact types.

The bubble's contribution gets repulsive as hair diameter decreases for both substrates (Figure 6). Since the aspect ratio L/D_h is fixed (Table 4), decreasing the hair diameter also decreases its length. The bubble has less space available between the pad and the substrate, resulting in it bulging outwards near the pinned contact line on top. Thus, bubble contribution gets repulsive as hair diameter decreases if bubble volume is kept constant.

3.2.4 Capillary Bridge Model: Effect of bubble volume

The effect of varying bubble volume (non-dimensionalized as \hat{V}_b) on the net adhesion force of the *underwater: bubble* contact for hydrophilic and hydrophobic substrates are compared (Figure 7). From section 3.2.2, we know that on the hydrophilic substrate, fluid bridges outside the bubble has negligible contribution due to its positive curvature. Thus, decreasing \hat{V}_b decreases adhesion force due to the larger proportion of hairs outside the bubble. In contrast, on the hydrophobic substrate, fluid bridges outside the bubble have stronger contribution to the net capillary force due to the low contact angle and high interfacial tension in water. Thus, adhesion force increases for a hydrophobic substrate as the bubble size decreases.

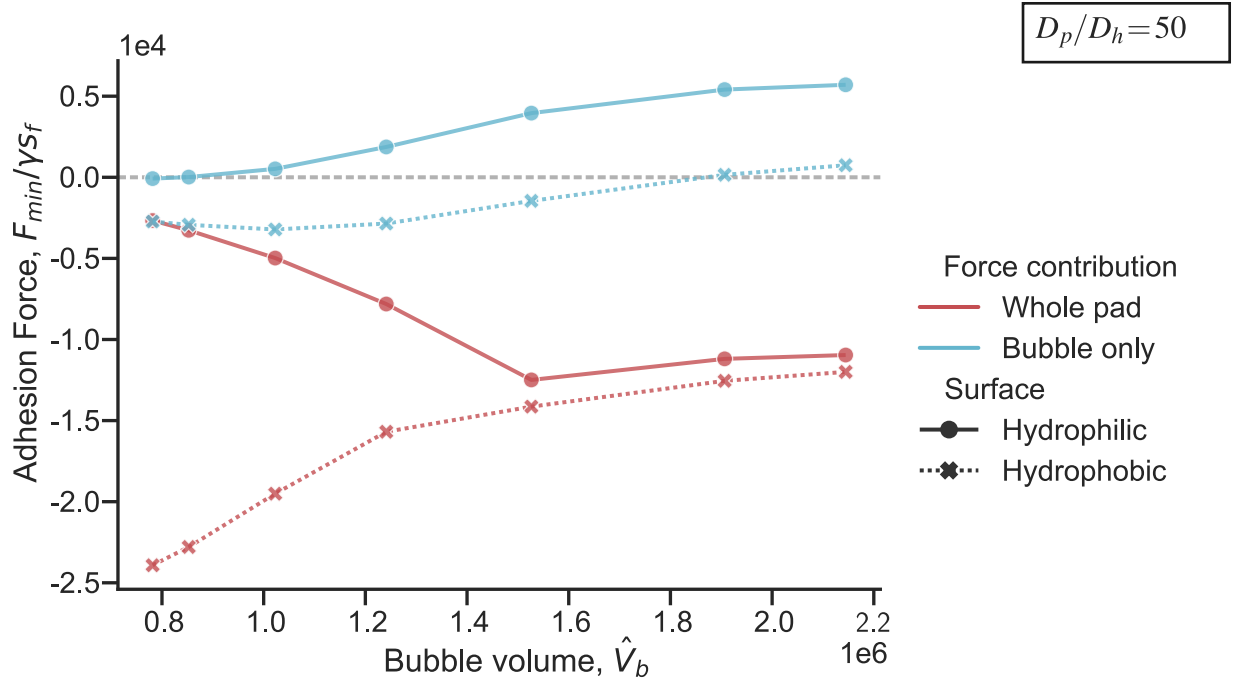


Figure 7: Normalized adhesion force of a hairy pad system as a function of bubble volume (\hat{V}_b) for *underwater: bubble* contact type. Negative value represents attractive force. Here, pad to hair size ratio (D_p/D_h) is kept fixed. Adhesion forces are calculated from minima of the respective force-distance curves.

The contribution of the bubble to the net adhesion force is small regardless of its size. We see that a smaller \hat{V}_b results in increased attraction by the bubble in both types of substrates. For larger values of \hat{V}_b , force trend for the whole pad mostly follows that of the

bubble, because the bubble in this case is big enough to entrap all hairs inside it. Thus, the force contribution due to the fluid bridges remains unchanged while the bubble’s contribution increases slightly as \hat{V}_b increases. Once the bubble becomes small enough and part of the fluid bridges make contact in water, the force trend changes with a steep decrease (increase) in adhesion force on hydrophilic (hydrophobic) substrate. In all cases, the bubble’s adhesion force is much smaller when compared to the whole pad.

To summarize, on a hydrophilic substrate, a trapped air bubble in the adhesive pad can promote adhesion when its large enough to enclose most of the hairs. This allows the hairs to make contact in an air environment. This is because wet hairs underwater show no adhesion due to the fluid’s large contact angle and the only way to achieve adhesion is by maintaining the hairs in the air environment provided by the bubble. On a hydrophobic substrate, however, a smaller or no bubble enhances adhesion, as the bubble has little effect on improving adhesion force. Here, hairs making a contact underwater without a trapped bubble show stronger adhesion than in air due to the fluid’s smaller contact angle and higher interfacial tension. In either case, the bubble by itself hardly contributes to the net force. Despite its large size, the bubble fails to overcome the combined contribution of the much smaller fluid bridges to the total force.

4 Discussion

Our experiments demonstrate, for the first time, that the ladybug beetle can attach underwater to a hydrophobic substrate even without a bubble trapped around its hairs. A previous study¹⁷ had hypothesized that a bubble is necessary for underwater attachment in beetles. This is, however, only true for hydrophilic substrates, where a trapped bubble can facilitate underwater adhesion due to the hairs making contact in a dewetted environment. For a hydrophobic substrate, the adhesion is similar regardless of whether the contact occurs in air or underwater conditions, with or without a trapped bubble. Our theoretical calcu-

lations also show that the bubble by itself has a negligible capillary contribution to the net adhesion of the pad underwater. Direct force measurement of a single similarly sized bubble making contact with a hydrophobic substrate shows a maximum adhesion less than 50 μN , which further validates that the bubble’s contribution is insignificant (see SI).

Predictions of adhesion force from the capillary bridge model follow the experimental results (Figure 2). In underwater conditions without a trapped bubble, adhesion on a hydrophobic substrate is significantly larger than on a hydrophilic substrate. This is explained by the different oil contact angles and its interfacial tension values for both substrates in air and underwater, which ~~influences~~ the capillary adhesive force in each case (Figure 8). However, the measurements don’t show the predicted ~ 2.6 times increase in underwater adhesion relative to that in air on the hydrophobic PFOTS surface. This discrepancy could be due to our assumptions of the oily fluid’s interfacial properties. If we choose $\gamma_{\text{fa}}=30$ mN/m and $\gamma_{\text{wa}}=40$ mN/m, the corresponding increase in adhesion will be ~ 1.7 , closer to our experimental value of ~ 1 . Direct measurement of the fluid’s interfacial properties is thus essential to better predict the insect’s adhesion, and will be a subject of future study. Further, due to surface inhomogeneities, ~~all~~ the hairs might ~~not~~ be able to completely drain the water layer on the surface, in order for the fluid to make a direct contact with the substrate. This can further reduce underwater adhesion, in comparison to our theoretical predictions which assumes a perfect contact.

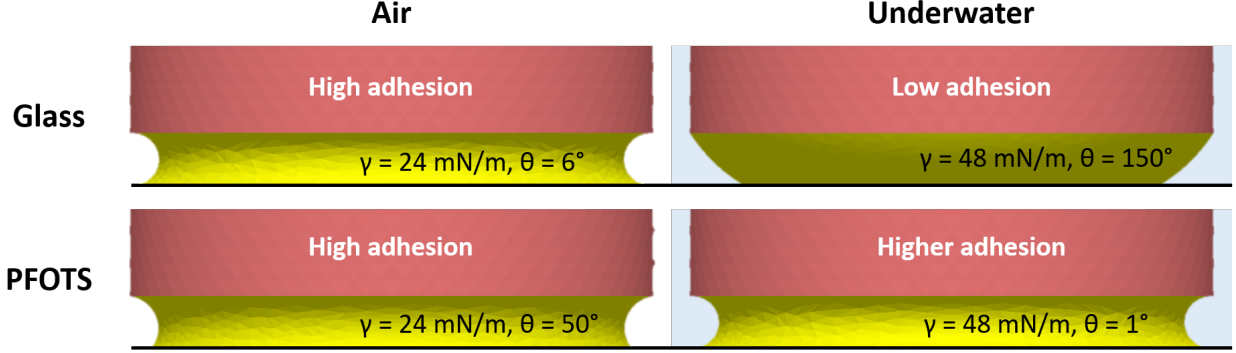


Figure 8: Simulation snapshots of oil capillary meniscus in contact with glass and PFOTS in air and underwater conditions. The corresponding interfacial tension, γ , and contact angle, θ , used to predict the ladybug’s adhesion are labeled for each case.

In the model, we assume that all the hairs detach simultaneously to give a theoretical maximum achievable adhesion force. Our experimental conditions, however, differ from such assumptions. The pad always makes contact with the substrate at a random orientation, which is difficult to control precisely. During detachment, the pad typically peels off from its proximal to distal end rather than detach simultaneously. Our model also assumes the hairs to be of similar geometry, unlike the beetle’s pad which has a distribution of flat or pointed tipped hairs. Thus, it’s not surprising that the model overestimates the adhesion forces. The predictions are however in the same order of magnitude as experiments, and the qualitative trend is consistent for both hydrophilic and hydrophobic substrates in air and underwater.

Our study provides further validation that capillary forces by the adhesive fluid control insect adhesion and van der Waals contribution, if any, must be negligible. Further, the same capillary forces can even enable adhesion underwater depending on the substrate chemistry. Underwater without a trapped bubble, the pad adheres strongly to a hydrophobic substrate, but poorly to a hydrophilic substrate, even though it shows similarly strong adhesion to both substrates in air. This behavior can only be explained by capillary forces. Our preliminary FDMS results further provides validation to our assumption that the adhesive fluid can form capillary bridges with the substrate underwater, instead of getting washed away (Table 2).

The findings can also be extended to other animals relying on oily adhesive fluids for adhesion. Ants for example show similar adhesion on hydrophobic substrates under wet and dry conditions²³, similar to what we see in a ladybug. Recent adhesion experiments on geckos reveal that they can attach well to fluoropolymer substrates underwater while they show little adhesion to the same substrate in air^{18,19}. Geckos are thought to rely on van der Waals forces via dry contact with the substrate⁶, although recent observations of phospholipid footprints left behind walking geckos²⁴ could change that picture. Since geckos adhere poorly to PTFE (surface energy ~ 20 mN/m) one can speculate that the phospholipid material has a higher surface energy, and consequently makes a higher contact angle with PTFE in air. Let us assume the phospholipid substance to be a fluid similar to oil with $\gamma_{fa}=30$ mN/m and $\gamma_{fw}=42$ mN/m such that its contact angle with PTFE is 80° . Equation 3 then gives us an underwater contact angle of 70° for the phospholipid fluid. Thus, the capillary bridge model can predict a higher adhesion underwater than in air with PTFE due to its lower contact angle and higher interfacial energy underwater. Based on similar assumptions, we predict the net adhesion force for a gecko on different substrates (Figure 9). The adhesion force predictions are in good qualitative agreement with the whole animal experimental shear force values reported for the gecko, with the trend of higher adhesion in air than underwater for glass, similar adhesion in air and underwater for PMMA/OTS-SAM and lower adhesion in air than underwater for PTFE. We, thus, propose that the underwater experiments performed on geckos^{18,19} ~~are an indirect proof of~~ capillary contribution to gecko adhesion in this scenario. We suggest performing single seta adhesion force tests similar to Autumn et. al.⁶ using a hydrophilic and fluorinated probe in air and underwater conditions to validate the role of capillary contributions to gecko adhesion.

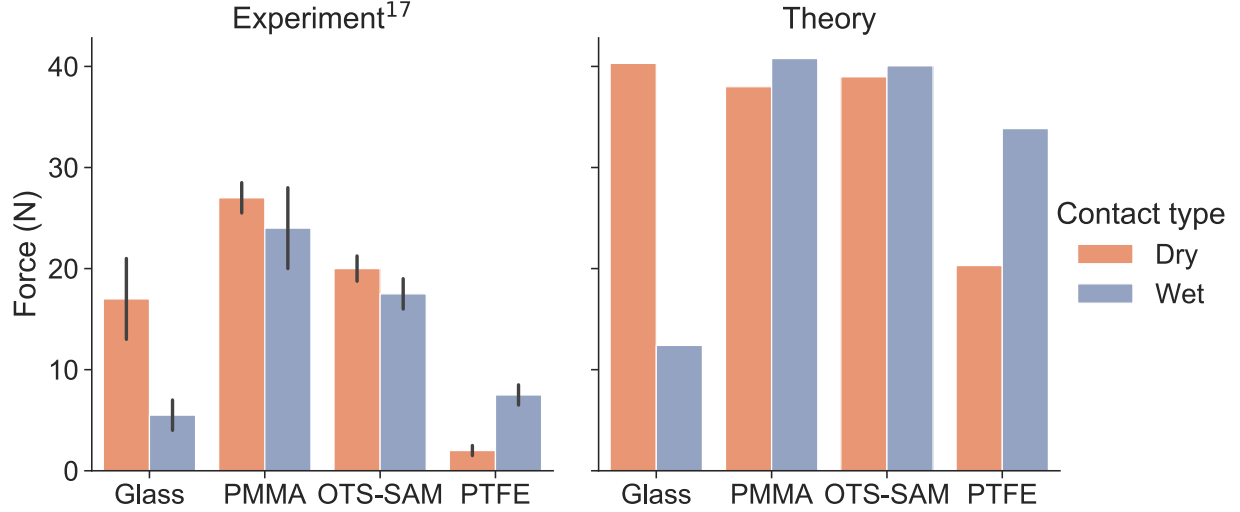


Figure 9: Whole animal adhesion force of geckos on various substrates. Experimental shear adhesion values are reproduced from Stark et. al.¹⁸. Normal adhesion forces for each gecko toe are theoretically estimated from the capillary bridge model, with hair diameter = 400 nm, toe diameter = 4 mm, adhesive fluid volume = 4.19×10^{-3} fL and 10% hair coverage. “Underwater:Wet” contact is assumed for “Wet” contact. Net adhesion force is calculated by assuming 5 toes on each leg and 4 legs in total on a gecko. Interfacial tension of phospholipid layer (PL) in air and water are assumed to be 30 mN/m and 42 mN/m respectively. PL contact angles with glass, PMMA, OTS-SAM and PTFE are assumed to be 6°, 10°, 20° and 80° respectively. The corresponding water contact angles are 50°, 85°, 94° and 97° respectively, as reported in Stark et. al.¹⁸.

We have so far limited our analysis to only smooth substrates. Insects in the real world, however, interacts with rough substrates very often. Previous studies²⁵ have shown that substrate roughness is a more dominant parameter than substrate chemistry in controlling insect adhesion. Future work will explore how roughness can impact the net capillary force as predicted by our model. Our study can have potential applications in the design of bio-inspired materials to achieve adhesion via capillary bridges. Bubble can possibly be used to control underwater adhesion by changing the relative proportion of the arrays inside and outside the bubble. A suitable choice of adhesive fluid can be made tailored to the substrate and environment of application for optimal adhesion performance. Future studies on insect adhesion should characterize oleophilicity rather than hydrophilicity of a substrate, since oil contact angle primarily controls its adhesion to the substrate.

5 Conclusions

Our study illustrates that ladybug relies primarily on its oily adhesive fluid secretion to achieve adhesion in both air and underwater conditions. We show that the beetles can attach underwater on a hydrophobic substrate even without a trapped air bubble within its hairy pad, although it loses this ability on a hydrophilic substrate. The different contact angle and interfacial tension manifested by the adhesive fluid in air and underwater conditions explain this observation. Theoretical calculations suggest that the bubble itself has a negligible capillary contribution to the total force. The trapped bubble can promote adhesion only on a hydrophilic substrate by providing an air medium to the adhesive fluid bridges inside it. Insect adhesion is correlated directly to the shape of the adhesive fluid bridge on a given substrate and medium, which is a result of the small fluid volume and its contact angle with the substrate. A similar argument also explains previously reported measurements in geckos¹⁸, which highlights the possibility of capillary contributions to gecko adhesion.

6 Acknowledgement

We are grateful to Eduard Arzt and Renè Hensel for fruitful discussions. The project was funded by Deutsche Forschungsgemeinschaft.

A Appendix

A.1 Simulation method: Single capillary bridge

Capillary force due to a single adhesive fluid or bubble meniscus (“capillary bridge”) is calculated by performing simulations in Surface Evolver²⁶, similar to the method described in De Souza et. al.²⁷. A simple cubic geometry mimicking the capillary bridge of constant volume V is defined as the initial condition with an interfacial tension γ with the surrounding medium. Interfacial tension of the capillary bridge with the substrate is given by $\gamma\cos\theta$,

where θ is the corresponding contact angle inside the bridge. For the case of a bubble meniscus, θ is defined w.r.t. the surrounding water since θ can also then characterize the substrate wettability. The capillary bridge spans a gap distance d between the top face and the substrate. The boundary conditions are set corresponding to a pinned contact line of diameter D on the top face and constant interfacial tension with the substrate on the bottom. All lengths are normalized relative to length $s = (3V/4\pi)^{1/3}$. An appropriate geometry refinement routine is chosen to evolve the capillary bridge shape to its minimum energy state. The normalized total capillary force, $F=f/\gamma s$, is the sum of the Laplace pressure and surface tension contributions, where:

$$f = f_{laplace} + f_{surface\ tension} = \Delta P_{laplace} A_{bottom} + 2\pi R_{bottom} \gamma \sin \theta \quad (A.1)$$

Here, $\Delta P_{laplace}$ which is the Laplace pressure of the equilibrium capillary bridge, A_{bottom} which is the contact area of the capillary bridge with the substrate at bottom and R_{bottom} which is the corresponding radius of contact are all obtained from the simulation output for the equilibrium surface.

The gap distance d is varied by fixed steps and the capillary force is calculated each time to obtain force-distance curves for a particular choice of D and θ .

A.2 Single capillary bridge: Effect of volume

Surface Evolver simulations showing the effect of volume on the maximum capillary force of a single fluid bridge.

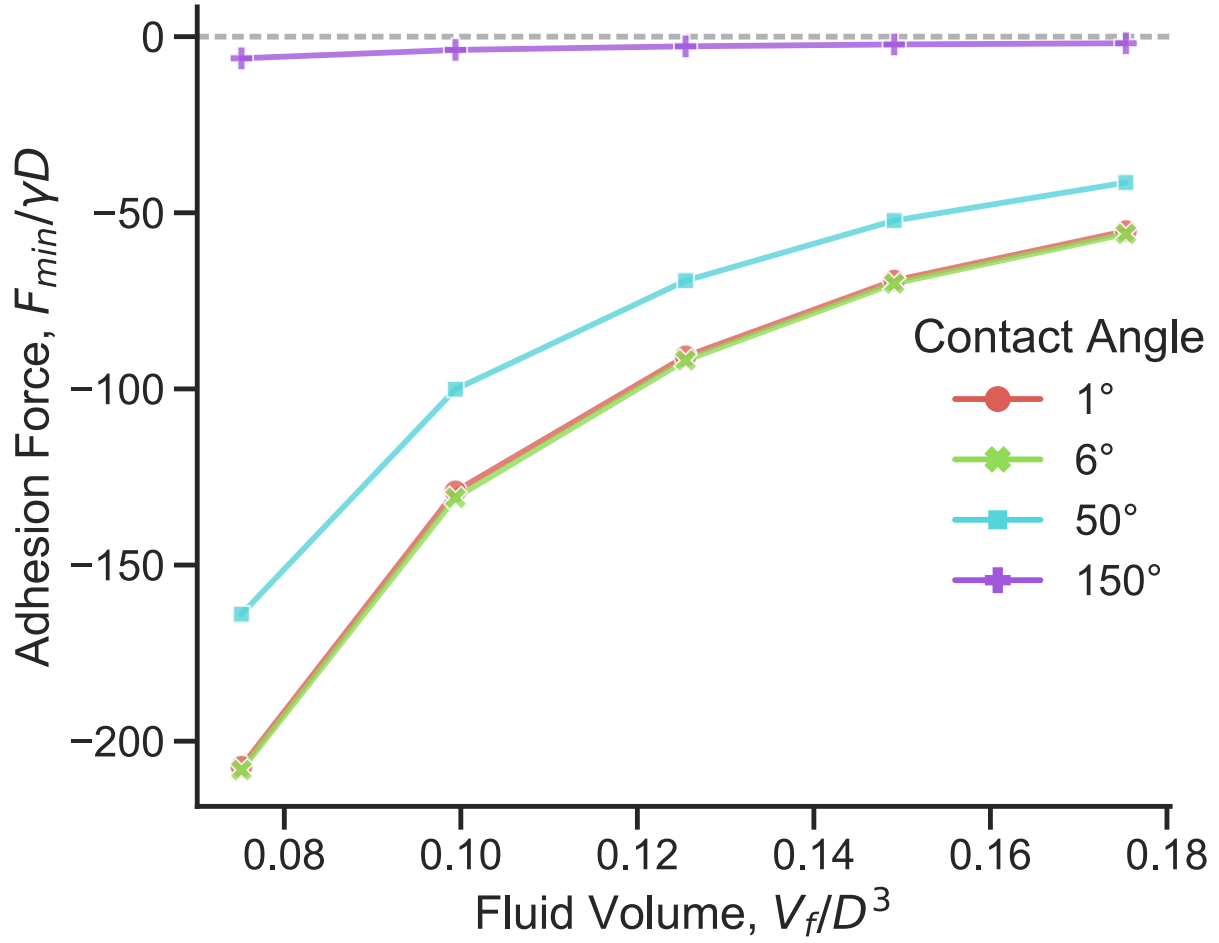


Figure A.1: Normalized maximum capillary force for a single bridge as a function of fluid volume

A.3 Capillary Bridge Model: Effect of hair diameter at constant fluid volume

Here, instead of scaling of fluid volume relative to the hair diameter, we now assume a fixed total fluid volume distributed equally among the N hairs. Hair diameter is varied while keeping the total hair contact area constant. Length is in arbitrary units. Forces increase at a much smaller rate on decreasing diameter when compared to the case with self-similar scaling of fluid volume.

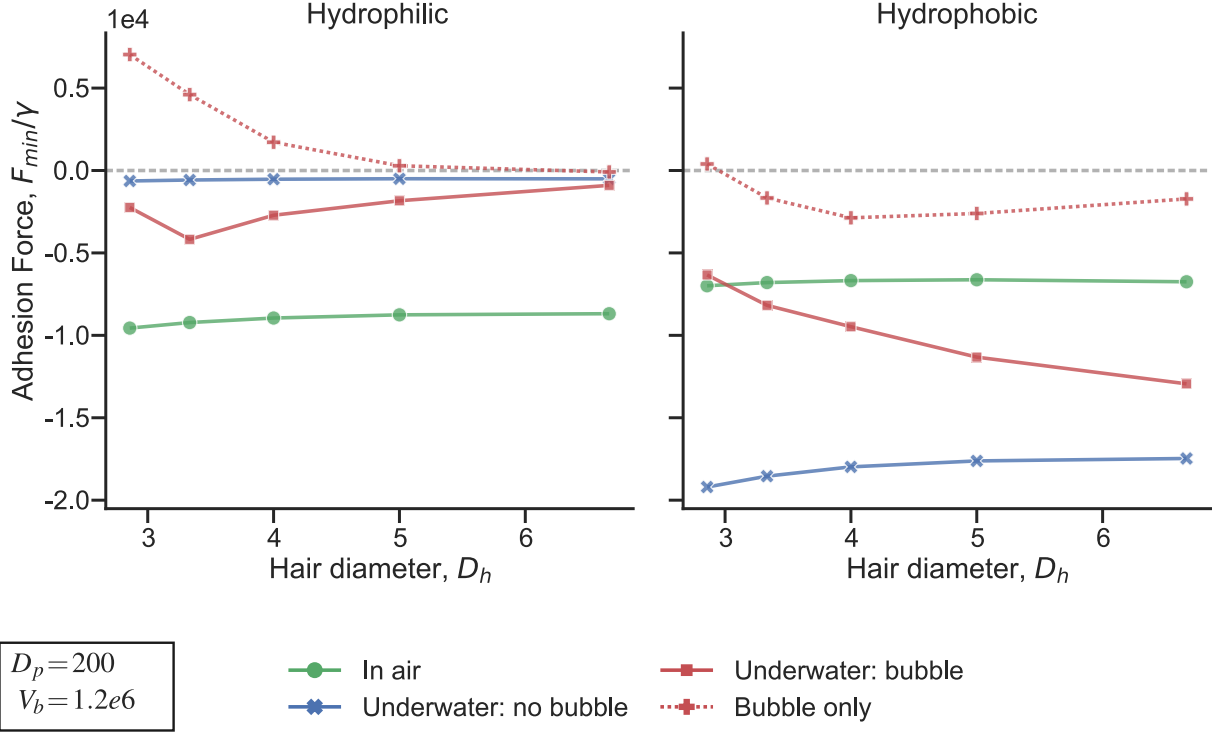


Figure A.2: Normalized adhesion force of hairy pad system on a hydrophilic (left) and hydrophobic (right) substrate as a function of hair diameter (D_h), calculated from Capillary Bridge Model. Negative value represents attractive force. The bubble's contribution to the net force for an *underwater: bubble* contact is denoted by plus symbols. Bubble volume (V_b), pad diameter ($D_p = 200$) and total adhesive fluid volume ($NV_f = 2000$) are kept fixed. Adhesion forces are calculated from minima of the respective force-distance curves.

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