
NASA-GLENN CHEMICAL EQUILIBRIUM PROGRAM CEA2, MAY 21, 2004
BY BONNIE MCBRIDE AND SANFORD GORDON
REFS: NASA RP-1311, PART I, 1994 AND NASA RP-1311, PART II, 1996

problem case=LMPHR o/f=2,4,6,8,10,
 rocket frozen nfz=1 tcest,k=3800
 p,bar=20,25,30,
react
 oxid=H2O(L) wt=100
 oxid=CH3OH(L) wt=100
 oxid=NH3(L) wt=100
 fuel=Sasoll Wax 6805 wt=100 t,k=298.16
 h,kj/mol=-1179.851 C 40 H 82

WARNING!! Wax NOT RECOGNIZED (INPUT)

WARNING!! LITERAL EXPECTED FOR 6805 (INPUT)

end

OPTIONS: TP=F HP=F SP=F TV=F UV=F SV=F DETN=F SHOCK=F REFL=F INCD=F RKT=T FROZ=T EQL=F IONS=F SIUNIT=T DEBUGF=F SHKDBG=F DETDBG=F TRNSPT=F

TRACE= 0.00E+00 S/R= 0.000000E+00 H/R= 0.000000E+00 U/R= 0.000000E+00

Pc,BAR = 20.000000 25.000000 30.000000

Pc/P =

SUBSONIC AREA RATIOS =

SUPERSONIC AREA RATIOS =

NFZ= 1 Mdot/Ac= 0.000000E+00 Ac/At= 0.000000E+00

REACTANT WT.FRAC (ENERGY/R),K TEMP,K DENSITY
EXPLODED FORMULA

O: H2O(L) 0.333333 0.0000000E+00 0.00 0.0000
H 2.00000 0 1.00000

O: CH3OH(L) 0.333333 0.000000E+00 0.00 0.0000
C 1.00000 H 4.00000 0 1.00000

O: NH3(L) 0.333333 -0.860604E+04 239.72 0.0000
N 1.00000 H 3.00000

F: Sasoll 1.000000 -0.141903E+06 298.16 0.0000
C 40.00000 H 82.00000

SPECIES BEING CONSIDERED IN THIS SYSTEM (CONDENSED PHASE MAY HAVE NAME LISTED SEVERAL TIMES) LAST thermo.inp UPDATE: 9/09/04

g 7/97 *C tpis79 *CH g 4/02 CH2

| 4 /00 | ~ | 11/00 | ~~~~ | 7/00 | 2222 |
|--------|------------------|--------|-----------------|--------|------------------|
| g 4/02 | CH3 | g11/00 | CH2OH | g 7/00 | CH3O |
| g 8/99 | CH4 | g 7/00 | СНЗОН | srd 01 | CH300H |
| g 8/99 | *CN | g12/99 | CNN | tpis79 | *CO |
| g 9/99 | *C02 | tpis91 | COOH | tpis91 | *C2 |
| g 6/01 | C2H | g 1/91 | C2H2, acetylene | g 5/01 | C2H2, vinylidene |
| g 4/02 | CH2CO, ketene | g 3/02 | O (CH) 20 | srd 01 | HO (CO) 2OH |
| g 7/01 | C2H3, vinyl | g 9/00 | CH3CN | g 6/96 | CH3CO, acetyl |
| g 1/00 | C2H4 | g 8/88 | C2H4O,ethylen-o | g 8/88 | CH3CHO, ethanal |
| g 6/00 | СНЗСООН | srd 01 | OHCH2COOH | g 7/00 | C2H5 |
| g 7/00 | C2H6 | g 8/88 | CH3N2CH3 | g 8/88 | С2Н5ОН |
| g 7/00 | CH3OCH3 | srd 01 | CH3O2CH3 | g 7/00 | CCN |
| tpis91 | CNC | srd 01 | OCCN | tpis79 | C2N2 |
| g 8/00 | C20 | tpis79 | *C3 | n 4/98 | C3H3,1-propynl |
| n 4/98 | C3H3,2-propynl | g 2/00 | C3H4,allene | g 1/00 | C3H4, propyne |
| g 5/90 | C3H4,cyclo- | g 3/01 | C3H5,allyl | g 2/00 | C3H6, propylene |
| g 1/00 | C3H6,cyclo- | g 6/01 | C3H6O,propylox | g 6/97 | C3H6O,acetone |
| g 1/02 | C3H6O,propanal | g 7/01 | C3H7,n-propyl | g 9/85 | C3H7,i-propyl |
| g 2/00 | С3Н8 | g 2/00 | C3H8O,1propanol | g 2/00 | C3H8O,2propanol |
| srd 01 | CNCOCN | g 7/88 | C302 | g tpis | *C4 |
| g 7/01 | C4H2,butadiyne | g 8/00 | C4H4,1,3-cyclo- | n10/92 | C4H6,butadiene |
| n10/93 | C4H6,1butyne | n10/93 | C4H6,2butyne | g 8/00 | C4H6,cyclo- |
| n 4/88 | C4H8,1-butene | n 4/88 | C4H8,cis2-buten | n 4/88 | C4H8,tr2-butene |
| n 4/88 | C4H8,isobutene | g 8/00 | C4H8,cyclo- | g10/00 | (CH3COOH) 2 |
| n10/84 | C4H9,n-butyl | n10/84 | C4H9,i-butyl | g 1/93 | C4H9,s-butyl |
| g 1/93 | C4H9,t-butyl | g12/00 | C4H10,n-butane | g 8/00 | C4H10,isobutane |
| g 6/01 | C4N2 | g 8/00 | *C5 | g 5/90 | C5H6,1,3cyclo- |
| g 1/93 | C5H8,cyclo- | n 4/87 | C5H10,1-pentene | g 2/01 | C5H10,cyclo- |
| n10/84 | C5H11,pentyl | g 1/93 | C5H11,t-pentyl | n10/85 | C5H12,n-pentane |
| n10/85 | C5H12,i-pentane | n10/85 | CH3C (CH3) 2CH3 | g 2/93 | C6H2 |
| g11/00 | C6H5,phenyl | g 8/00 | C6H5O,phenoxy | g 8/00 | C6H6 |
| g 8/00 | C6H5OH, phenol | g 1/93 | C6H10,cyclo- | n 4/87 | C6H12,1-hexene |
| g 6/90 | C6H12,cyclo- | n10/83 | C6H13,n-hexyl | g 6/01 | C6H14,n-hexane |
| g 7/01 | C7H7,benzyl | g 1/93 | C7H8 | g12/00 | C7H8O,cresol-mx |
| n 4/87 | C7H14,1-heptene | n10/83 | C7H15,n-heptyl | n10/85 | C7H16,n-heptane |
| n10/85 | C7H16,2-methylh | n 4/89 | C8H8, styrene | n10/86 | C8H10,ethylbenz |
| n 4/87 | C8H16,1-octene | n10/83 | C8H17,n-octyl | n 4/85 | C8H18,n-octane |
| n 4/85 | C8H18,isooctane | n10/83 | C9H19,n-nonyl | g 3/01 | C10H8, naphthale |
| n10/83 | C10H21,n-decyl | g 8/00 | C12H9,o-bipheny | g 8/00 | C12H10,biphenyl |
| g 6/97 | *H | g 6/01 | HCN | g 1/01 | HCO |
| tpis89 | HCCN | g 6/01 | HCCO | g 6/01 | HNC |
| g 7/00 | HNCO | g10/01 | HNO | tpis89 | HNO2 |
| g 5/99 | HNO3 | g 4/02 | HO2 | tpis78 | *H2 |
| g 5/01 | HCHO, formaldehy | g 6/01 | НСООН | g 8/89 | Н2О |
| g 6/99 | H2O2 | g 6/01 | (HCOOH) 2 | g 5/97 | *N |
| g 6/01 | NCO | g 4/99 | *NH | g 3/01 | NH2 |
| tpis89 | NH3 | tpis89 | | tpis89 | *NO |
| g 4/99 | NO2 | j12/64 | | tpis78 | *N2 |
| g 6/01 | NCN | g 5/99 | N2H2 | = | NH2NO2 |
| g 4/99 | N2H4 | q 4/99 | N20 | g 4/99 | N2O3 |
| tpis89 | N2O4 | q 4/99 | N205 | tpis89 | N3 |
| g 4/99 | N3H | g 5/97 | *0 | g 4/02 | *OH |
| tpis89 | *02 | g 8/01 | 03 | n 4/83 | C(gr) |
| n 4/83 | C(gr) | n 4/83 | C(gr) | g11/99 | H2O(cr) |
| g 8/01 | H2O(L) | g 8/01 | H2O(L) | ,,-2 | - (/ |
| J | . , | J -/ - | . , | | |

O/F = 2.000000

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| | | EFFECTIVE FUEL | EFFEC | TIVE OXIDANT | MIXTURE |
|--------------|----------|-----------------|---------|--------------|-----------------|
| ENTHALPY | | h(2)/R | | h(1)/R | h0/R |
| (KG-MOL) (K) | /KG | -0.25201194E+03 | -0.16 | 844346E+03 | -0.19629962E+03 |
| KG-FORM.WT | ./KG | bi(2) | | bi(1) | bOi |
| * H | | 0.14562786E+00 | 0.13 | 733597E+00 | 0.14009993E+00 |
| *0 | | 0.0000000E+00 | 0.28 | 905870E-01 | 0.19270580E-01 |
| *C | | 0.71037979E-01 | 0.10 | 403058E-01 | 0.30614699E-01 |
| *N | | 0.0000000E+00 | 0.19 | 572704E-01 | 0.13048470E-01 |
| POINT ITN | Т | Н | 0 | С | N |
| 1 22 | 1139.750 | -7.809 | -35.284 | -1.055 | -12.332 |
| ADD C(gr) | 1137.635 | -7.733 | -34.919 | -1.715 | -12.340 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 290.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 2.00000 %FUEL= 33.333333 R,EQ.RATIO= 6.812424 PHI,EQ.RATIO=-1.773949

| | CHAMBER | THROAT |
|----------------|----------|----------|
| Pinf/P | 1.0000 | 1.8064 |
| P, BAR | 20.000 | 11.072 |
| T, K | 1137.64 | 1010.49 |
| RHO, KG/CU M | 2.7492 0 | 1.7134 0 |
| H, KJ/KG | -1632.14 | -2037.94 |
| U, KJ/KG | -2359.63 | -2684.13 |
| G, KJ/KG | -18632.8 | -17138.6 |
| S, KJ/(KG)(K) | 14.9439 | 14.9439 |
| | | |
| M, (1/n) | 13.002 | 13.002 |
| MW, MOL WT | 11.863 | 11.863 |
| Cp, KJ/(KG)(K) | 3.2451 | 3.1374 |
| GAMMAs | 1.2454 | 1.2560 |
| SON VEL, M/SEC | 951.9 | 900.9 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

Ae/At 1.0000 CSTAR, M/SEC 1295.7

| CF | 0.6953 |
|-------------|--------|
| Ivac, M/SEC | 1618.2 |
| Isp, M/SEC | 900.9 |

MOLE FRACTIONS

| CH4 | 0.13546 | *CO | 0.12393 | *C02 | 0.01611 |
|------|---------|-------|---------|------|---------|
| C2H4 | 0.00001 | C2H6 | 0.00002 | HCN | 0.00001 |
| *H2 | 0.48673 | H20 | 0.07246 | NH3 | 0.00054 |
| *N2 | 0.07712 | C(gr) | 0.08762 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1153.327 -7.650 -34.547 -1.737 -12.244

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 362.6 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 2.00000 %FUEL= 33.333333 R,EQ.RATIO= 6.812424 PHI,EQ.RATIO=-1.773949

| | CHAMBER | THROAT |
|---------------|----------|----------|
| Pinf/P | 1.0000 | 1.8044 |
| P, BAR | 25.000 | 13.855 |
| T, K | 1153.33 | 1025.92 |
| RHO, KG/CU M | 3.4148 0 | 2.1275 0 |
| H, KJ/KG | -1632.14 | -2040.05 |
| U, KJ/KG | -2364.25 | -2691.29 |
| G, KJ/KG | -18703.3 | -17225.4 |
| S, KJ/(KG)(K) | 14.8017 | 14.8017 |

| M, (1/n) | 13.098 | 13.098 |
|------------------|--------|--------|
| MW, MOL WT | 12.016 | 12.016 |
| Cp, $KJ/(KG)(K)$ | 3.2554 | 3.1465 |
| GAMMAs | 1.2422 | 1.2527 |
| SON VEL, M/SEC | 953.7 | 903.2 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1301.0 |
| CF | 0.6943 |
| Ivac, M/SEC | 1624.2 |
| Isp, M/SEC | 903.2 |

MOLE FRACTIONS

| CH4 | 0.14363 | *CO | 0.12547 | *CO2 | 0.01609 |
|------|---------|-------|---------|------|---------|
| C2H4 | 0.00001 | C2H6 | 0.00002 | HCN | 0.00001 |
| *H2 | 0.47956 | H20 | 0.07391 | NH3 | 0.00061 |
| *N2 | 0.07809 | C(gr) | 0.08261 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1166.382 -7.582 -34.244 -1.754 -12.165

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 435.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 2.00000 %FUEL= 33.333333 R,EQ.RATIO= 6.812424 PHI,EQ.RATIO=-1.773949

| | CHAMBER | THROAT |
|------------------|----------|---------|
| Pinf/P | | |
| P, BAR | | |
| T, K | | |
| · | | |
| RHO, KG/CU M | | |
| H, KJ/KG | | |
| U, KJ/KG | | |
| G, KJ/KG | | |
| S, KJ/(KG)(K) | 14.6863 | 14.6863 |
| | | |
| M, (1/n) | 13.179 | 13.179 |
| MW, MOL WT | 12.146 | 12.146 |
| Cp, $KJ/(KG)(K)$ | 3.2643 | 3.1545 |
| GAMMAs | | |
| SON VEL, M/SEC | 955.1 | 905.1 |
| MACH NUMBER | | |
| | | |
| PERFORMANCE PAR | RAMETERS | |
| | | |
| Ae/At | | 1.0000 |
| CSTAR, M/SEC | | 1305.3 |
| CF | | 0.6934 |
| Ivac, M/SEC | | 1629.2 |
| Isp, M/SEC | | 905.1 |
| ± * · | | |
| MOLE FRACTIONS | | |
| CIIA | 0 15055 | +00 |
| CH4 | 0.15055 | ^ |

| CH4 | 0.15055 | *CO | 0.12674 | *CO2 | 0.01610 |
|------|---------|-------|---------|------|---------|
| C2H4 | 0.00001 | C2H6 | 0.00003 | HCN | 0.00001 |
| *H2 | 0.47348 | H20 | 0.07513 | NH3 | 0.00067 |
| *N2 | 0.07890 | C(gr) | 0.07837 | | |

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PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

O/F = 4.000000

| | EFFECTIVE FUEL | EFFECTIVE OXIDANT | MIXTURE |
|----------------|-----------------|-------------------|-----------------|
| ENTHALPY | h(2)/R | h(1)/R | h0/R |
| (KG-MOL)(K)/KG | -0.25201194E+03 | -0.16844346E+03 | -0.18515716E+03 |
| KG-FORM.WT./KG | bi(2) | bi(1) | bOi |
| * H | 0.14562786E+00 | 0.13733597E+00 | 0.13899435E+00 |

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| *0 | | | 0.0000000E+00 | 0.28 | 905870E-01 | 0.23124696E | E-01 |
|--------|------|-----------------|----------------|---------|------------|-------------|------|
| *C | | | 0.71037979E-01 | 0.10 | 403058E-01 | 0.22530042 | E-01 |
| *N | | | 0.0000000E+00 | 0.19 | 572704E-01 | 0.15658164 | E-01 |
| POINT | ITN | Т | Н | 0 | С | N | |
| 1 | 4 | 1190.307 | -7.779 | -34.158 | -1.787 | -12.364 | |
| REMOVE | E C(| gr) 1193.955 | -7.761 | -33.919 | -2.100 | -12.371 | |
| | | | | | | | |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 290.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.000000 | -1179851.000 | 298.160 |

O/F= 4.00000 %FUEL= 20.000000 R,EQ.RATIO= 4.953893 PHI,EQ.RATIO=-0.886974

| Pinf/P P, BAR T, K RHO, KG/CU M | 20.000 1193.95 2.3444 0 | 1.8338 10.906 1040.03 1.4676 0 |
|---|---|--|
| H, KJ/KG U, KJ/KG G, KJ/KG S, KJ/(KG)(K) | | |
| M, (1/n) MW, MOL WT Cp, KJ/(KG)(K) GAMMAS SON VEL,M/SEC MACH NUMBER | 11.636 11.636 3.1916 1.2884 1048.4 0.000 | 11.636 11.636 3.0885 1.3010 983.3 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1386.0 |
| CF | 0.7094 |
| Ivac, M/SEC | 1739.0 |
| Isp, M/SEC | 983.3 |

MOLE FRACTIONS

| CH4 | 0.08070 | *CO | 0.16599 | *C02 | 0.01544 |
|------|---------|-----|---------|------|---------|
| C2H6 | 0.00001 | HCN | 0.00001 | *H2 | 0.57428 |
| H20 | 0.07221 | NH3 | 0.00052 | *N2 | 0.09084 |

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PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

| POINT | ITN | T | Н | 0 | С | N |
|-------|-----|----------|--------|---------|--------|---------|
| 1 | 3 | 1211.059 | -7.673 | -33.530 | -2.159 | -12.277 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 362.6 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.000000 | -1179851.000 | 298.160 |

O/F= 4.00000 %FUEL= 20.000000 R,EQ.RATIO= 4.953893 PHI,EQ.RATIO=-0.886974

| CHAMBER | THROAT |
|----------|--|
| 1.0000 | 1.8317 |
| 25.000 | 13.648 |
| 1211.06 | 1056.50 |
| 2.9057 0 | 1.8183 0 |
| -1539.49 | -2026.46 |
| -2399.88 | -2777.04 |
| -20971.9 | -18978.9 |
| 16.0458 | 16.0458 |
| | |
| 11.703 | 11.703 |
| 11.703 | 11.703 |
| 3.2023 | 3.0981 |
| 1.2851 | 1.2976 |
| 1051.5 | 986.9 |
| 0.000 | 1.000 |
| | 25.000 1211.06 2.9057 0 -1539.49 -2399.88 -20971.9 16.0458 11.703 11.703 3.2023 1.2851 1051.5 |

PERFORMANCE PARAMETERS

Ae/At 1.0000
CSTAR, M/SEC 1393.2
CF 0.7084
Ivac, M/SEC 1747.4
Isp, M/SEC 986.9

MOLE FRACTIONS

| CH4 | 0.08399 | *CO | 0.16423 | *CO2 | 0.01541 |
|------|---------|------|---------|------|---------|
| C2H4 | 0.00001 | C2H6 | 0.00001 | HCN | 0.00002 |
| *H2 | 0.56884 | H20 | 0.07558 | NH3 | 0.00059 |
| *N12 | 0 09132 | | | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1225.339 -7.602 -33.215 -2.207 -12.200

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 435.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | N ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 4.00000 %FUEL= 20.000000 R,EQ.RATIO= 4.953893 PHI,EQ.RATIO=-0.886974

CHAMBER THROAT
Pinf/P 1.0000 1.8300
P, BAR 30.000 16.393
T, K 1225.34 1070.29

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| RHO, KG/CU M | 3.4628 0 | 2.1664 0 |
|----------------|----------|----------|
| H, KJ/KG | -1539.49 | -2029.35 |
| U, KJ/KG | -2405.84 | -2786.08 |
| G, KJ/KG | -21042.7 | -19064.7 |
| S, KJ/(KG)(K) | 15.9166 | 15.9166 |
| | | |
| M, (1/n) | 11.760 | 11.760 |
| MW, MOL WT | 11.760 | 11.760 |
| Cp, KJ/(KG)(K) | 3.2113 | 3.1062 |
| GAMMAs | 1.2823 | 1.2947 |
| SON VEL, M/SEC | 1054.0 | 989.8 |
| MACH NUMBER | 0.000 | 1.000 |
| | | |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1399.1 |
| CF | 0.7075 |
| Ivac, M/SEC | 1754.3 |
| Isp, M/SEC | 989.8 |

MOLE FRACTIONS

| CH4 | 0.08677 | *CO | 0.16274 | *C02 | 0.01538 |
|------|---------|------|---------|------|---------|
| C2H4 | 0.00001 | C2H6 | 0.00001 | HCN | 0.00002 |
| *H2 | 0.56425 | H2O | 0.07844 | NH3 | 0.00066 |
| *N2 | 0.09173 | | | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

O/F = 6.000000

| ENTHALPY (KG-MOL) (| K)/KG | EFFECTIVE FUEL h(2)/R -0.25201194E+03 | | TIVE OXIDANT h(1)/R 844346E+03 | MIXTURE h0/R -0.18038182E+03 |
|------------------------|----------|---|---------|--------------------------------------|------------------------------------|
| KG-FORM.W | T./KG | bi(2) | | bi(1) | bOi |
| * H | | 0.14562786E+00 | 0.13 | 733597E+00 | 0.13852052E+00 |
| *0 | | 0.0000000E+00 | 0.28 | 905870E-01 | 0.24776460E-01 |
| *C | | 0.71037979E-01 | 0.10 | 403058E-01 | 0.19065190E-01 |
| *N | | 0.0000000E+00 | 0.19 | 572704E-01 | 0.16776604E-01 |
| POINT ITN | T | Н | 0 | С | N |
| 1 5 | 1234.653 | -7.776 | -33.031 | -2.754 | -12.407 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 290.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 6.00000 %FUEL= 14.285714 R,EQ.RATIO= 4.334382 PHI,EQ.RATIO=-0.591316

| | CHAMPED | munoam |
|----------------|----------|----------|
| | CHAMBER | THROAT |
| Pinf/P | 1.0000 | 1.8456 |
| P, BAR | 20.000 | 10.837 |
| T, K | 1234.65 | 1066.43 |
| RHO, KG/CU M | 2.1645 0 | 1.3578 0 |
| H, KJ/KG | -1499.79 | -2026.70 |
| U, KJ/KG | -2423.78 | -2824.81 |
| G, KJ/KG | -22134.8 | -19850.2 |
| S, KJ/(KG)(K) | 16.7132 | 16.7132 |
| | | |
| M, (1/n) | 11.110 | 11.110 |
| MW, MOL WT | 11.110 | 11.110 |
| Cp, KJ/(KG)(K) | 3.1800 | 3.0841 |
| GAMMAs | 1.3078 | 1.3204 |
| SON VEL, M/SEC | 1099.3 | 1026.6 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1434.9 |
| CF | 0.7154 |
| Ivac, M/SEC | 1804.0 |
| Isp, M/SEC | 1026.6 |

MOLE FRACTIONS

| CH4 | 0.03699 | *CO | 0.15990 | *CO2 | 0.01491 |
|-----|---------|------|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.60921 | H20 | 0.08555 |
| MH3 | 0 00048 | *N12 | 0 09295 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

| POINT | ITN | T | Н | 0 | С | N |
|-------|-----|----------|--------|---------|--------|---------|
| 1 | 3 | 1251.607 | -7.687 | -32.677 | -2.789 | -12.313 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 362.6 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | I ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 6.00000 %FUEL= 14.285714 R,EQ.RATIO= 4.334382 PHI,EQ.RATIO=-0.591316

| | CHAMBER | THROAT |
|------------------|----------|----------|
| Pinf/P | 1.0000 | 1.8436 |
| P, BAR | 25.000 | 13.561 |
| T, K | 1251.61 | 1082.65 |
| RHO, KG/CU M | 2.6835 0 | 1.6827 0 |
| H, KJ/KG | -1499.79 | -2030.48 |
| U, KJ/KG | -2431.42 | -2836.34 |
| G, KJ/KG | -22209.7 | -19944.6 |
| S, KJ/(KG)(K) | 16.5466 | 16.5466 |
| | | |
| M, (1/n) | 11.170 | 11.170 |
| MW, MOL WT | 11.170 | 11.170 |
| Cp, $KJ/(KG)(K)$ | 3.1892 | 3.0919 |
| GAMMAs | 1.3045 | 1.3171 |
| SON VEL, M/SEC | 1102.4 | 1030.2 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1442.1 |
| CF | 0.7144 |
| Ivac, M/SEC | 1812.5 |
| Isp, M/SEC | 1030.2 |

MOLE FRACTIONS

| CH4 | 0.03987 | *CO | 0.15826 | *C02 | 0.01481 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.60420 | H20 | 0.08888 |
| NH3 | 0.00055 | *N2 | 0.09342 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

| POINT | ITN | T | Н | 0 | С | N |
|-------|-----|----------|--------|---------|--------|---------|
| 1 | 3 | 1265.828 | -7.615 | -32.387 | -2.819 | -12.236 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 435.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 6.00000 %FUEL= 14.285714 R,EQ.RATIO= 4.334382 PHI,EQ.RATIO=-0.591316

| | CHAMBER | THROAT |
|------------------|----------|----------|
| Pinf/P | 1.0000 | 1.8419 |
| P, BAR | 30.000 | 16.288 |
| T, K | 1265.83 | 1096.28 |
| RHO, KG/CU M | 3.1986 0 | 2.0052 0 |
| H, KJ/KG | -1499.79 | -2033.57 |
| U, KJ/KG | -2437.70 | -2845.86 |
| G, KJ/KG | -22273.6 | -20024.9 |
| S, $KJ/(KG)(K)$ | 16.4112 | 16.4112 |
| | | |
| $M_{,}$ (1/n) | 11.221 | 11.221 |
| MW, MOL WT | 11.221 | 11.221 |
| Cp, $KJ/(KG)(K)$ | 3.1970 | 3.0987 |
| GAMMAs | 1.3017 | 1.3143 |
| SON VEL, M/SEC | 1104.9 | 1033.2 |

MACH NUMBER 0.000 1.000

PERFORMANCE PARAMETERS

Ae/At 1.0000
CSTAR, M/SEC 1448.0
CF 0.7135
Ivac, M/SEC 1819.4
Isp, M/SEC 1033.2

MOLE FRACTIONS

* THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

O/F = 8.000000

| | | EFFECTIVE FUEL | EFFEC: | TIVE OXIDANT | MIXTURE | |
|--------------|----------|-----------------|---------|--------------|----------------|----|
| ENTHALPY | | h(2)/R | l | n(1)/R | h0/R | |
| (KG-MOL) (K) | /KG | -0.25201194E+03 | -0.168 | 844346E+03 | -0.17772885E+0 | 03 |
| KG-FORM.WT. | ./KG | bi(2) | | bi(1) | bOi | |
| * H | | 0.14562786E+00 | 0.13 | 733597E+00 | 0.13825729E+0 | 00 |
| *0 | | 0.0000000E+00 | 0.289 | 905870E-01 | 0.25694107E-0 | 01 |
| *C | | 0.71037979E-01 | 0.104 | 403058E-01 | 0.17140272E-0 | 01 |
| *N | | 0.0000000E+00 | 0.195 | 572704E-01 | 0.17397959E-0 | 01 |
| POINT ITN | Т | Н | 0 | С | N | |
| 1 4 | 1274.629 | -7.809 | -32.225 | -3.344 | -12.444 | |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 290.1 PSIA CASE = LMPHR

REACTANT WT FRACTION ENERGY TEMP

| | | (SEE NOTE) | KJ/KG-MOL | K |
|---------|----------|------------|--------------|---------|
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 8.00000 %FUEL= 11.111111 R,EQ.RATIO= 4.024627 PHI,EQ.RATIO=-0.443487

| | CHAMBER | THROAT |
|------------------|----------|----------|
| Pinf/P | 1.0000 | 1.8505 |
| P, BAR | 20.000 | 10.808 |
| T, K | 1274.63 | 1097.10 |
| RHO, KG/CU M | 2.0560 0 | 1.2908 0 |
| H, KJ/KG | -1477.73 | -2033.90 |
| U, KJ/KG | -2450.47 | -2871.16 |
| G, KJ/KG | -23119.3 | -20661.3 |
| S, KJ/(KG)(K) | 16.9787 | 16.9787 |
| | | |
| M, (1/n) | 10.895 | 10.895 |
| MW, MOL WT | 10.895 | 10.895 |
| Cp, $KJ/(KG)(K)$ | 3.1792 | 3.0860 |
| GAMMAs | 1.3159 | 1.3285 |
| SON VEL, M/SEC | 1131.4 | 1054.7 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.00000 |
|--------------|---------|
| CSTAR, M/SEC | 1469.1 |
| CF | 0.7179 |
| Ivac, M/SEC | 1848.5 |
| Isp, M/SEC | 1054.7 |

MOLE FRACTIONS

| CH4 | 0.01712 | *CO | 0.15522 | *CO2 | 0.01439 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.62235 | H20 | 0.09593 |
| инз | 0 00042 | *N2 | 0 09456 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1289.865 -7.717 -31.928 -3.340 -12.348

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 362.6 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | I ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 8.00000 %FUEL= 11.111111 R,EQ.RATIO= 4.024627 PHI,EQ.RATIO=-0.443487

| | CHAMBER | THROAT |
|----------------|----------|----------|
| Pinf/P | 1.0000 | 1.8487 |
| P, BAR | 25.000 | 13.523 |
| T, K | 1289.87 | 1111.66 |
| RHO, KG/CU M | 2.5519 0 | 1.6016 0 |
| H, KJ/KG | -1477.73 | -2037.33 |
| U, KJ/KG | -2457.41 | -2881.66 |
| G, KJ/KG | -23158.8 | -20723.0 |
| S, KJ/(KG)(K) | 16.8088 | 16.8088 |
| | | |
| $M_{,}$ (1/n) | 10.947 | 10.947 |
| MW, MOL WT | 10.947 | 10.947 |
| Cp, KJ/(KG)(K) | 3.1870 | 3.0926 |
| GAMMAs | 1.3129 | 1.3255 |
| SON VEL, M/SEC | 1134.1 | 1057.9 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1475.5 |
| CF | 0.7170 |
| Ivac, M/SEC | 1856.0 |
| Isp, M/SEC | 1057.9 |
| | |

MOLE FRACTIONS

| CH4 | 0.01955 | *CO | 0.15378 | *C02 | 0.01428 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.61798 | H2O | 0.09893 |
| NH3 | 0.00049 | *N2 | 0.09498 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

| POINT | ITN | T | H | 0 | С | N |
|-------|-----|----------|--------|---------|--------|---------|
| 1 | 3 | 1302.868 | -7.643 | -31.679 | -3.341 | -12.269 |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 435.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 8.00000 %FUEL= 11.111111 R,EQ.RATIO= 4.024627 PHI,EQ.RATIO=-0.443487

| | CHAMBER | THROAT |
|----------------|----------|----------|
| Pinf/P | 1.0000 | 1.8472 |
| P, BAR | 30.000 | 16.241 |
| T, K | 1302.87 | 1124.11 |
| RHO, KG/CU M | 3.0441 0 | 1.9101 0 |
| H, KJ/KG | -1477.73 | -2040.19 |
| U, KJ/KG | -2463.23 | -2890.48 |
| G, KJ/KG | -23197.4 | -20779.8 |
| S, KJ/(KG)(K) | 16.6706 | 16.6706 |
| | | |
| M, (1/n) | 10.992 | 10.992 |
| MW, MOL WT | 10.992 | 10.992 |
| Cp, KJ/(KG)(K) | 3.1938 | 3.0984 |
| GAMMAs | 1.3103 | 1.3230 |
| SON VEL, M/SEC | 1136.4 | 1060.6 |
| MACH NUMBER | 0.000 | 1.000 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1480.9 |
| CF | 0.7162 |
| Ivac, M/SEC | 1862.3 |
| Isp, M/SEC | 1060.6 |

MOLE FRACTIONS

| CH4 | 0.02166 | *CO | 0.15253 | *CO2 | 0.01420 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00002 | *H2 | 0.61421 | H20 | 0.10150 |
| NH3 | 0.00055 | *N2 | 0.09534 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

O/F = 10.000000

| | | EFFECTIVE FUEL | EFFEC: | TIVE OXIDANT | MIXTURE | |
|----------|----------|-----------------|---------|--------------|----------------|-----|
| ENTHALPY | | h(2)/R | l | n(1)/R | h0/R | |
| (KG-MOL) | (K)/KG | -0.25201194E+03 | -0.168 | 344346E+03 | -0.17604060E+0 |)3 |
| KG-FORM. | WT./KG | bi(2) | | bi(1) | b0i | |
| * H | | 0.14562786E+00 | 0.13 | 733597E+00 | 0.13808978E+0 | 0 (|
| *0 | | 0.0000000E+00 | 0.289 | 905870E-01 | 0.26278064E-0 |)1 |
| *C | | 0.71037979E-01 | 0.104 | 403058E-01 | 0.15915324E-0 |)1 |
| *N | | 0.0000000E+00 | 0.195 | 572704E-01 | 0.17793368E-0 |)1 |
| POINT IT | N T | Н | 0 | С | N | |
| 1 4 | 1317.779 | -7.853 | -31.412 | -3.943 | -12.485 | |

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 290.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.0000000 | -1179851.000 | 298.160 |

O/F= 10.00000 %FUEL= 9.090909 R,EQ.RATIO= 3.838774 PHI,EQ.RATIO=-0.354790

| | | CHAMBER | THROAT |
|-----|------|---------|---------|
| Piı | nf/P | 1.0000 | 1.8518 |
| P, | BAR | 20.000 | 10.801 |
| Τ, | K | 1317.78 | 1133.27 |

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| RHO, KG/CU M H, KJ/KG U, KJ/KG G, KJ/KG S, KJ/(KG)(K) | 1.9751 0 -1463.69 -2476.27 -24046.9 17.1374 | -2043.02 -2913.82 -21464.2 |
|---|---|----------------------------------|
| M, (1/n) MW, MOL WT Cp, KJ/(KG)(K) GAMMAS SON VEL,M/SEC MACH NUMBER | 10.821 10.821 3.1859 1.3179 1155.2 0.000 | 10.821 3.0930 1.3306 |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1498.1 |
| CF | 0.7185 |
| Ivac, M/SEC | 1885.4 |
| Isp, M/SEC | 1076.4 |

MOLE FRACTIONS

| CH4 | 0.00761 | *CO | 0.15070 | *C02 | 0.01390 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.62550 | H20 | 0.10585 |
| NH3 | 0.00036 | *N2 | 0.09608 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1329.614 -7.756 -31.196 -3.880 -12.385

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 362.6 PSIA CASE = LMPHR

REACTANT WT FRACTION ENERGY TEMP (SEE NOTE) KJ/KG-MOL K

| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
|---------|----------|-----------|--------------|---------|
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.000000 | -1179851.000 | 298.160 |

O/F= 10.00000 %FUEL= 9.090909 R,EQ.RATIO= 3.838774 PHI,EQ.RATIO=-0.354790

| | CHAMBER | THROAT |
|---------------------|----------|----------|
| Pinf/P | 1.0000 | 1.8503 |
| P, BAR | 25.000 | 13.511 |
| T, K | 1329.61 | 1144.60 |
| RHO, KG/CU M | 2.4560 0 | 1.5419 0 |
| H, KJ/KG | -1463.69 | -2045.63 |
| U, KJ/KG | -2481.60 | -2921.90 |
| G, KJ/KG | -24022.2 | -21465.2 |
| S, $KJ/(KG)(K)$ | 16.9662 | 16.9662 |
| | | |
| M_{\bullet} (1/n) | 10.861 | 10.861 |
| MW, MOL WT | 10.861 | 10.861 |
| Cp, $KJ/(KG)(K)$ | 3.1919 | 3.0981 |
| GAMMAs | 1.3155 | 1.3282 |
| SON VEL, M/SEC | 1157.2 | 1078.8 |
| MACH NUMBER | 0.000 | 1.000 |
| | | |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1502.9 |
| CF | 0.7178 |
| Ivac, M/SEC | 1891.1 |
| Isp, M/SEC | 1078.8 |

MOLE FRACTIONS

| CH4 | 0.00945 | *CO | 0.14957 | *CO2 | 0.01381 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.62213 | H20 | 0.10820 |
| NH3 | 0.00042 | *N2 | 0.09641 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

POINT ITN T H O C N

1 3 1340.206 -7.679 -31.006 -3.840 -12.304

THEORETICAL ROCKET PERFORMANCE ASSUMING FROZEN COMPOSITION

Pin = 435.1 PSIA CASE = LMPHR

| | REACTANT | WT FRACTION | ENERGY | TEMP |
|---------|----------|-------------|--------------|---------|
| | | (SEE NOTE) | KJ/KG-MOL | K |
| OXIDANT | H2O(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | CH3OH(L) | 0.3333333 | 0.000 | 0.000 |
| OXIDANT | NH3(L) | 0.3333333 | -71555.000 | 239.720 |
| FUEL | Sasoll | 1.000000 | -1179851.000 | 298.160 |

O/F= 10.00000 %FUEL= 9.090909 R,EQ.RATIO= 3.838774 PHI,EQ.RATIO=-0.354790

| | CHAMBER | THROAT |
|------------------|----------|----------|
| Pinf/P | 1.0000 | 1.8491 |
| P, BAR | 30.000 | 16.224 |
| T, K | 1340.21 | 1154.76 |
| RHO, KG/CU M | 2.9337 0 | 1.8413 0 |
| H, KJ/KG | -1463.69 | -2047.92 |
| U, KJ/KG | -2486.30 | -2929.04 |
| G, KJ/KG | -24015.2 | -21479.0 |
| S, KJ/(KG)(K) | 16.8269 | 16.8269 |
| | | |
| M, (1/n) | 10.897 | 10.897 |
| MW, MOL WT | 10.897 | 10.897 |
| Cp, $KJ/(KG)(K)$ | 3.1973 | 3.1027 |
| GAMMAs | 1.3135 | 1.3261 |
| SON VEL, M/SEC | 1158.9 | 1081.0 |
| MACH NUMBER | 0.000 | 1.000 |
| | | |

PERFORMANCE PARAMETERS

| Ae/At | 1.0000 |
|--------------|--------|
| CSTAR, M/SEC | 1507.2 |
| CF | 0.7172 |
| Ivac, M/SEC | 1896.1 |
| Isp, M/SEC | 1081.0 |

MOLE FRACTIONS

| CH4 | 0.01112 | *CO | 0.14855 | *C02 | 0.01374 |
|-----|---------|-----|---------|------|---------|
| HCN | 0.00001 | *H2 | 0.61909 | H2O | 0.11031 |
| NH3 | 0.00048 | *N2 | 0.09670 | | |

^{*} THERMODYNAMIC PROPERTIES FITTED TO 20000.K

PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 5.000000E-06 FOR ALL ASSIGNED CONDITIONS

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS