Chapter 4: Gaits and Cyclic Motion

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Motion planning

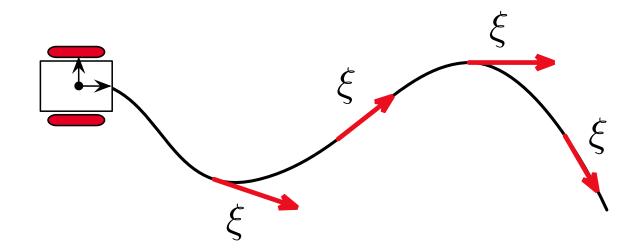
Find shape inputs to move system between two configurations

Motion Planning

Given the local connection, could we just define a path through the world, and then use

$$\dot{r} = \mathbf{A}^{-1}(r)\xi$$

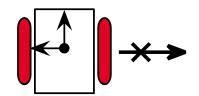
(inverse kinematics with a matrix pseudoinverse) to determine the shape trajectories?



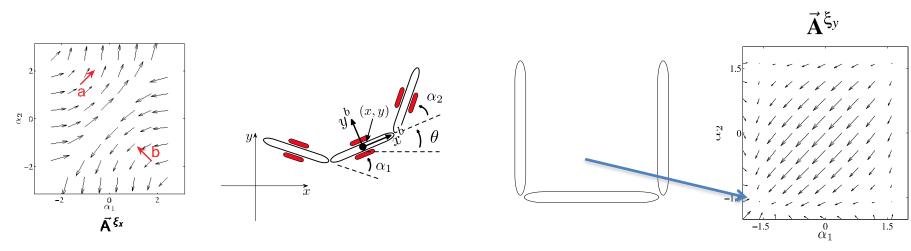
Motion Planning

Inverse kinematics not always sufficient:

1. Constrained directions – only certain paths are admissible



2. Singularities, Sinks, and Joint limits: what's wrong with these



Kinematic snake can't pass through singularities at "C" shapes

Three-link swimmer can't move laterally from this shape

General motion planning needs "look ahead" to workaround these problems

Motion Planning

- Full optimal control requires solving whole path at once (respecting constraints, limits, etc.)
- Maneuver-based planning precalculates short paths that
 - 1. Avoid joint limits and singularities
 - 2. Displace the system in some "useful" manner
 - 3. Can be concatenated together to form a longer motion plan

Gaits

Gaits are cyclic motions in the shape space

Cyclic nature makes them inherently composable

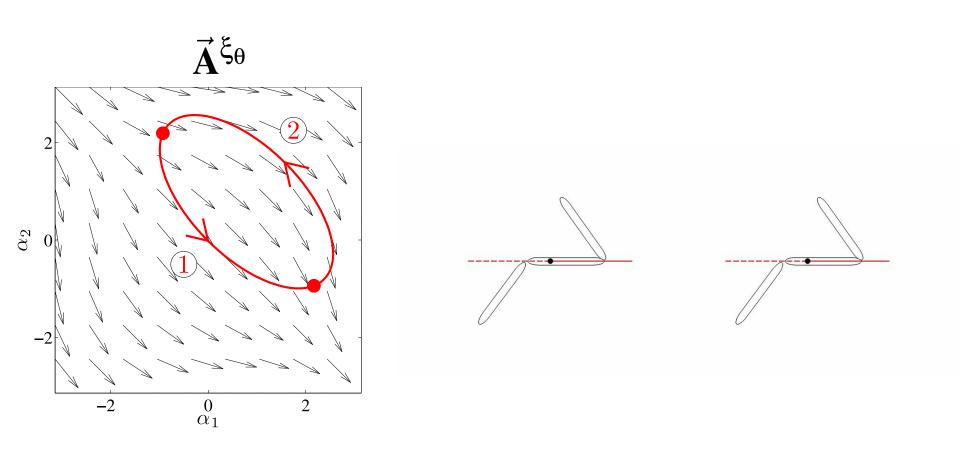
Nonconservativity and Noncommutativity

Kinematic gaits operate on two basic principles:

 Nonconservatvity: System pulls itself forward more than it pushes itself backward each cycle

 Noncommutativity: System rotates during the course of the gait, so forward and backward motions do not directly cancel

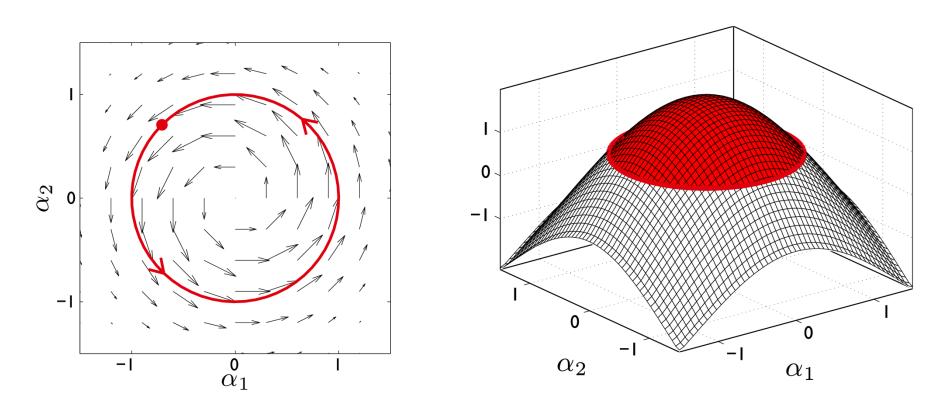
Nonconservativity Example



Gait "flows against" field more than it "flows with" it, and thus has net negative rotation.

Stokes's Theorem

(vector calculus version)



Line integral of a closed path on a vector field is equal to the area integral of the field's *curl*

Curl

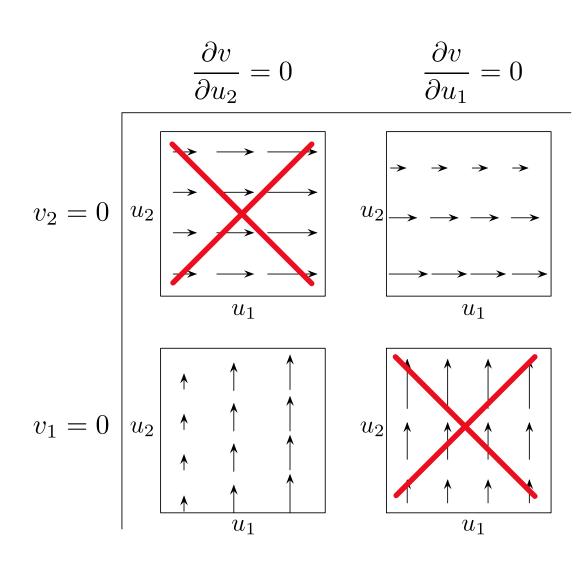
$$\operatorname{curl} V = \frac{\partial v_2}{\partial u_1} - \frac{\partial v_1}{\partial u_2}$$

Curl is sometimes described as "how much the vector field is 'rotating' around a point"

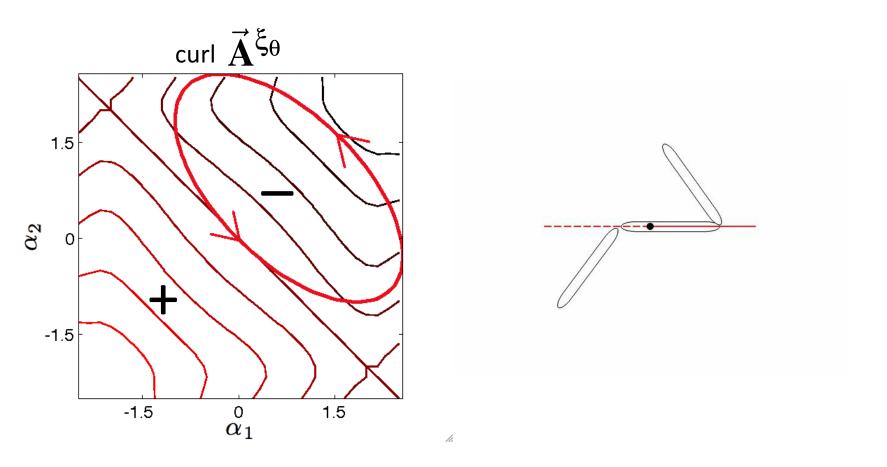
Magnitude also comes in here, so this description can be somewhat confusing

Another way to think of it is "the derivatives of the vector components along orthogonal directions in the space"

Around a cycle, line integrals on top right and bottom left fields will cancel, but those on top left and bottom right will not. Curl measures this non-canceling

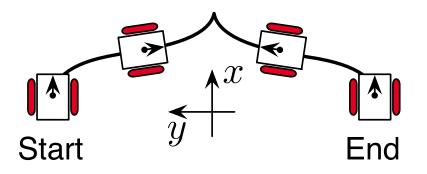


Curl and the Floating Snake

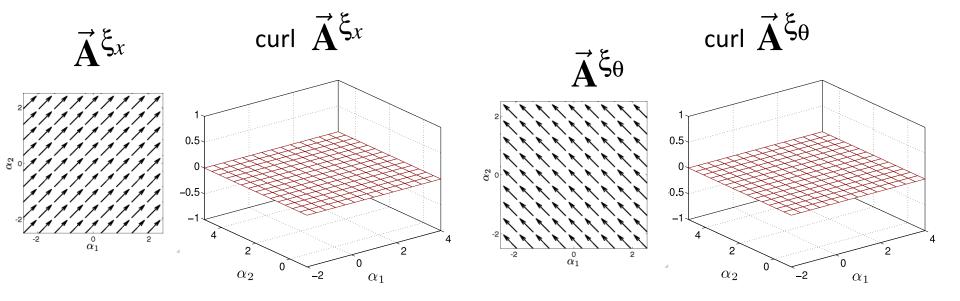


Encircling a region of negative curl means floating snake rotates negatively

Noncommutativity



Car cannot move sideways, but, because translations and rotations do not commute, it can "parallel park" to get a net lateral motion



None of this shows up in the curl

Lie Brackets

Lie bracket measures how vector fields change along each other

Lie bracket

Directional derivative of Y along X

Directional derivative of X along Y

$$[X,Y] = (\nabla Y \cdot X) - (\nabla X \cdot Y)$$

Output of the Lie bracket of two vector fields is a vector field.

At each point, differentially flowing along X, Y, -X, and -Y (in order) is equivalent to differentially flowing along [X,Y]

When we have a Lie group, we can talk about the Lie bracket of two vectors u,v in T_eG as meaning the Lie bracket of their left-invariant fields, evaluated at the origin

$$[u, v] \equiv [T_e L_g u, T_e L_g v]|_{g=\epsilon}$$

When we do this, we are treating T_eG as the *Lie algebra* of the group

Lie bracket on SE(2)

Lie group Lie bracket

$$[u, v] \equiv [T_e L_g u, T_e L_g v]|_{g=\epsilon}$$

SE(2) Lie bracket

$$\begin{bmatrix} \begin{pmatrix} u^{x} \\ u^{y} \\ u^{\theta} \end{pmatrix}, \begin{pmatrix} v^{x} \\ v^{y} \\ v^{\theta} \end{pmatrix} \end{bmatrix} = \begin{pmatrix} v^{\theta}u^{y} - u^{\theta}v^{y} \\ u^{\theta}v^{x} - v^{\theta}u^{x} \\ 0 \end{pmatrix}$$

Lie Bracket and the Car

Turn in place

Differential drive car

$$u = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \qquad v = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \qquad [u, v] = \begin{pmatrix} 0 \\ -1 \\ 0 \end{pmatrix}$$

$$[u,v] = \begin{pmatrix} 0 \\ -1 \\ 0 \end{pmatrix}$$

Drive+, turn+, drive-

$$d[X,\Theta] \downarrow \begin{array}{c} dx^b \\ -dx^b \end{array}$$

Drive forward

$$dx^{b} = \begin{bmatrix} \begin{pmatrix} u^{x} \\ u^{y} \\ u^{\theta} \end{pmatrix}, \begin{pmatrix} v^{x} \\ v^{y} \\ v^{\theta} \end{pmatrix} = \begin{pmatrix} v^{\theta}u^{y} - u^{\theta}v^{y} \\ u^{\theta}v^{x} - v^{\theta}u^{x} \\ 0 \end{pmatrix}$$
This is called (*Lie bracket*) averaging – in

This is called (Lie bracket) averaging – if you alternate between differentially moving forward/backward and rotating cw/ccw, on average you move laterally

Reminder

• <u>Controllability:</u> we have a set of inputs that can move the system in any direction.

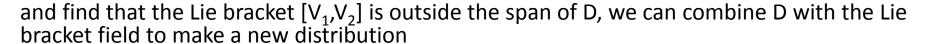
 <u>Distribution</u>: A set of vector fields along which a system can move

Importance of Lie brackets

1. Controlability: Nonholonomically-constrained systems by definition cannot instantaneously move in some directions: their distributions do not span their configuration spaces

If we take a distribution

$$D=\{V_1,V_2\}$$



$$D' = \{V_1, V_2, [V_1, V_2]\}$$

whose span is one dimension higher, and represents the directions the system can move either with a differential control input or with a first order oscillation of the controls. In some cases, we can further expand the distribution with higher-order Lie brackets, e.g.,

$$D'' = \{V_1, V_2, [V_1, V_2], [V_1, [V_1, V_2]]\}$$

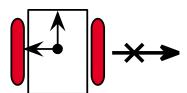
Importance of Lie brackets

Controlability (cont'd)

$$D = \{V_1, V_2\}$$

$$D' = \{V_1, V_2, [V_1, V_2]\}$$

$$D'' = \{V_1, V_2, [V_1, V_2], [V_1, [V_1, V_2]]\}$$



INVOLUTIVE DISTRIBUTION:

If we reach a point where we can't add dimensions by taking more Lie brackets, this is an *involutive distribution*: it describes the full set of directions in which the system can move differentially.

a distribution in which the Lie Bracket of any two elements is in the span of the distribution

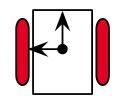
If a system's involutive distribution spans the whole configuration space, then the system is said to be *controllable* – we have a set of inputs that can move the system in any direction. (Note that in general there will be more efficient/effective ways to move the system in non-primary directions, controllability is a proof of existence)

Importance of Lie brackets

2. Relationship to gaits.

$$du \equiv d\alpha_1 + d\alpha_2$$

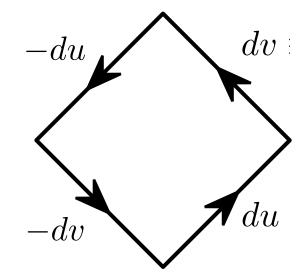
$$dv \equiv -d\alpha_1 + d\alpha_2$$



$$u = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \qquad v = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

are associated with unit shape velocities, and so their Lie bracket corresponds to the motion produced by a differential oscillation in the shape space (i.e. a differential gait)

$$[u,v] = \begin{pmatrix} 0 \\ -1 \\ 0 \end{pmatrix}$$



Lie Brackets and Exponential Maps

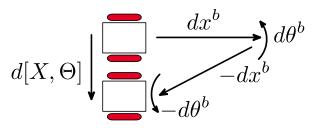
Lie bracket gives us **average** velocity of the system: moving for dt along each of u, v, -u, and -v is equivalent to moving for dt along [u,v]. (note that the total "time" in the cycle is different from the "flow time" along the Lie bracket field).

Note average velocity is a body-frame velocity (a direction and speed) and not a displacement

To get the *displacement* over the cycle, we can exponentiate this velocity:

$$\Delta g = \exp([u, v]dt)$$

Note: still making small angle approximations



Here, [u,v]dt gives the exponential coordinates of the net displacement

we will denote such exponential coordinates as z.

Also note that if we scale u or v, we proportionally increase the displacement

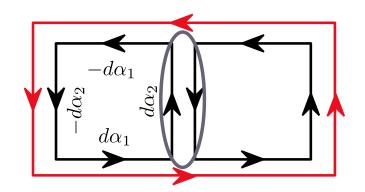
Lie Bracket and Larger Motions

One of the nice things about thinking of Lie bracket motions as differential gaits is that it gives us intuition as to how the system will move over larger gaits: Two differential cycles are equivalent to their combined perimeter if the overlapping edges cancel out.

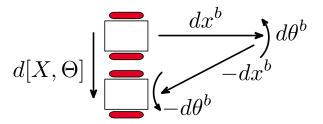
This gives us an area rule: over a larger gait, magnitude of average flow field is the area integral of the Lie bracket over the region enclosed by the gait

This rule is consistent with the Lie bracket as a *bilinear operator* – it scales linearly with *u* and *v*.

$$\begin{bmatrix} \begin{pmatrix} u^{x} \\ u^{y} \\ u^{\theta} \end{pmatrix}, \begin{pmatrix} v^{x} \\ v^{y} \\ v^{\theta} \end{pmatrix} \end{bmatrix} = \begin{pmatrix} v^{\theta}u^{y} - u^{\theta}v^{y} \\ u^{\theta}v^{x} - v^{\theta}u^{x} \\ 0 \end{pmatrix}$$



Example: Increasing forward translation and rotation each linearly increases the lateral translation

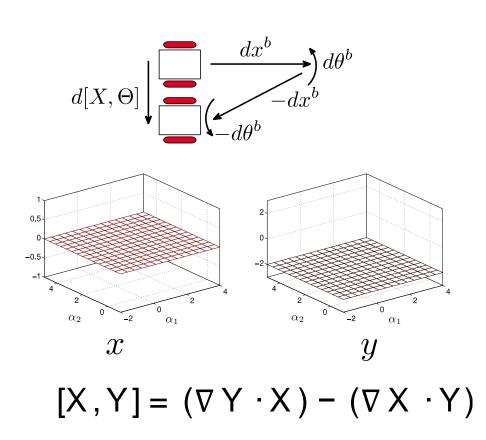


Note that here there is a small-angle condition on this assumption, and we are also assuming that local connection is constant (and thus that input fields are left invariant)

Nonconservativity

$\operatorname{\mathsf{curl}} \vec{\mathbf{A}}^{\xi_\theta}$ -1.5

Noncommutatvity

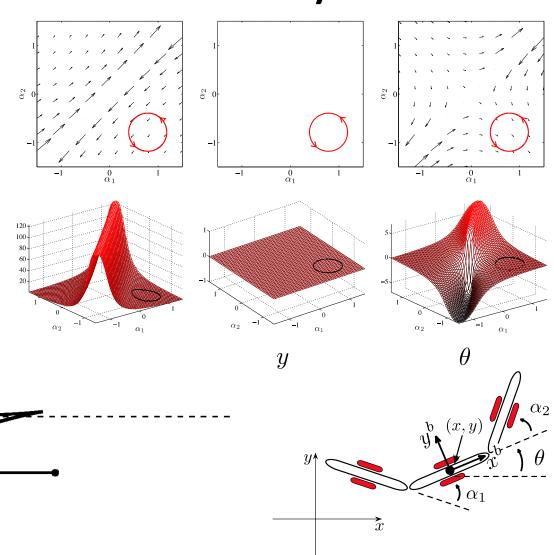


Curl and Lie bracket look very similar. Up next, we combine them into a single concept

Combining Nonconservativity and Noncommutativity

Example: Kinematic snake combines both effects

- curl of the connection vector field means the system moves forward more than backward,
- 2. <u>noncommutativity</u> means it also moves laterally



Combining Nonconservativity and Noncommutativity

Is it legitimate to just add nonconservative and noncommutative elements together?

Yes (as an approximation)

Exponential coordinates (average velocity for normalized time) of net displacement over a cycle are in general

$$z(\phi) = \left(\begin{array}{cc} [A_1,A_2] \text{ is the } \textit{local} \text{ Lie bracket,} \\ \text{as if A did not change with } \textit{r} \end{array} \right)$$

$$z(\phi) = \left(\begin{array}{cc} -\text{dA dr}_1 \text{ dr}_2 + \\ \phi_a \end{array} \right) \left[A_1,A_2 \right] \text{dr}_1 \text{dr}_2 + \text{higher-order terms}$$

d is the *exterior derivative*, which is like the curl, but more technically correct for talking about covectors

Higher order terms are linearizaton error in local Lie bracket, and noncommutativity interacting with nonconservativity

Derivation for this equivalence

Full Lie bracket on the configuration space

$$\left[\begin{pmatrix} \dot{r}_{1} \\ -T_{e}L_{g}A(r)\dot{r}_{1} \end{pmatrix}, \begin{pmatrix} \dot{r}_{2} \\ -T_{e}L_{g}A(r)\dot{r}_{2} \end{pmatrix} \right] = \begin{pmatrix} \left(\frac{\partial \dot{r}_{2}}{\partial r}\dot{r}_{1} - \frac{\partial \dot{r}_{1}}{\partial r}\dot{r}_{2} \right) + \left(\frac{\partial \dot{r}_{2}}{\partial g}\dot{g}_{1} - \frac{\partial \dot{r}_{1}}{\partial g}\dot{g}_{2} \right) \\ \left(\frac{\partial \dot{g}_{2}}{\partial r}\dot{r}_{1} - \frac{\partial \dot{g}_{1}}{\partial r}\dot{r}_{2} \right) + \left(\frac{\partial \dot{g}_{2}}{\partial g}\dot{g}_{1} - \frac{\partial \dot{g}_{1}}{\partial g}\dot{g}_{2} \right) \end{pmatrix}$$

Differential cycle in the shape space is $\vec{r}_1 = [1 \ 0]^T$ and $\vec{r}_2 = [0 \ 1]^T$

Conditions we can apply for these shape inputs:

$$\frac{\partial \dot{\mathbf{r}}_{i}}{\partial \mathbf{r}} = 0$$
 and $\frac{\partial \dot{\mathbf{r}}_{i}}{\partial \mathbf{g}} = 0$

(shape input vector field components are constant)

Top half of full Lie bracket is thus zero, which makes sense: over a cycle in the shape space, there should be no residual change of shape

$$\frac{\partial \dot{r_i}}{\partial r} = 0 \quad \text{and} \quad \frac{\partial \dot{r_i}}{\partial g} = 0 \quad \left| \begin{array}{c} -\frac{\partial \dot{g_i}}{\partial r} \Big|_{(r_0, g_0)} = \frac{\partial T_e L_g A_i(r)}{\partial r} \Big|_{(r_0, g_0)} = \frac{\partial T_e L_g A_i(r)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r} \\ = \frac{\partial T_e L_g A_i(r_0) + T_e L_{g_0}}{\partial r} \frac{\partial A_i(r_0)}{\partial r}$$

$$\left| -\frac{\partial \dot{g}_{i}}{\partial g} \right|_{(r_{0},g_{0})} = \left. \frac{\partial T_{e}L_{g}A_{i}(r)}{\partial g} \right|_{(r_{0},g_{0})} = \left. \frac{\partial T_{e}L_{g}}{\partial g}A_{i}(r_{0}) + T_{e}L_{g_{0}} \frac{\partial A_{i}(r)}{\partial g} \right|_{(r_{0},g_{0})}$$

(A is independent of a)

Derivation, continued

each derivative of \dot{g}_i in the lower-left term of

$$\begin{pmatrix}
\left(\frac{\partial \dot{r}_{2}}{\partial r}\dot{r}_{1} - \frac{\partial \dot{r}_{1}}{\partial r}\dot{r}_{2}\right) + \left(\frac{\partial \dot{r}_{2}}{\partial g}\dot{g}_{1} - \frac{\partial \dot{r}_{1}}{\partial g}\dot{g}_{2}\right) \\
\left(\frac{\partial \dot{g}_{2}}{\partial r}\dot{r}_{1} - \frac{\partial \dot{g}_{1}}{\partial r}\dot{r}_{2}\right) + \left(\frac{\partial \dot{g}_{2}}{\partial g}\dot{g}_{1} - \frac{\partial \dot{g}_{1}}{\partial g}\dot{g}_{2}\right)
\end{pmatrix}$$

is multiplied by the shape velocity

 \vec{r}_j with $i \neq j$, selecting out the jth derivative and giving these terms the form

$$-\frac{\partial \dot{g}_{i}}{\partial r}\dot{r}_{j}\Big|_{(r_{0},q_{0})} = \frac{\partial \dot{g}_{i}}{\partial r^{j}}\Big|_{(r_{0},q_{0})} = T_{e}L_{g_{0}}\frac{\partial A_{i}(r)}{\partial r^{j}} \quad \text{(based condition from last slide)}$$

Derivation, concluded

Collecting all terms gives us

$$\left(T_e L_{go} \left(- \left(\frac{\partial A_2(r)}{\partial r^1} - \frac{\partial A_1(r)}{\partial r^2} \right) + \left(\frac{\partial T_e L_g A_2(r_0)}{\partial g} T_{go} L_g A_1(r_0) - \frac{\partial T_e L_g A_1(r_0)}{\partial g} T_{go} L_g A_2(r_0) \right) \right) \right)$$
 (This is the curl/exterior derivative)
$$\left(\frac{\partial T_e L_g A_2(r_0)}{\partial g} T_e L_g A_1(r_0) - \frac{\partial T_e L_g A_1(r_0)}{\partial g} T_e L_g A_2(r_0) \right)$$
 (Make $g_0 = e$)
$$\left[T_e L_g A_1(r_0), T_e L_g A_2(r_0) \right] = \left[A_1, A_2 \right] (r_0)$$
 (Recognize this as an SE(2) Lie bracket)

Net result: nonconservative and noncommutative terms both appear in total Lie bracket

$$\left[\begin{pmatrix} \dot{r_1} \\ -T_e L_g A(r) \dot{r_1} \end{pmatrix}, \begin{pmatrix} \dot{r_2} \\ -T_e L_g A(r) \dot{r_2} \end{pmatrix}\right] \bigg|_{q_0} = \begin{pmatrix} 0 \\ \left(\underline{-dA + \left[A_1, A_2\right]}\right)(r_0) \end{pmatrix}$$

This is the *curvature form* for the connection, *DA*