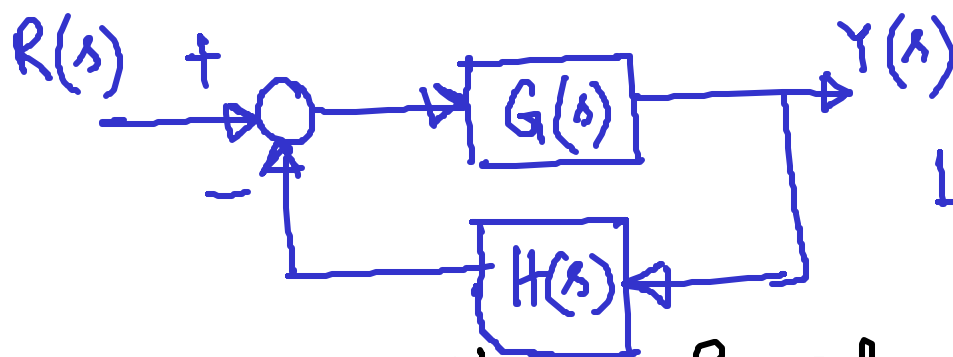


The Nyquist Stability Criterion



$$\text{Loop TF} = \underline{G(s)H(s)} \checkmark$$

- It relates the stability of closed-loop system to the loop TF frequency response and loop TF pole location. \checkmark

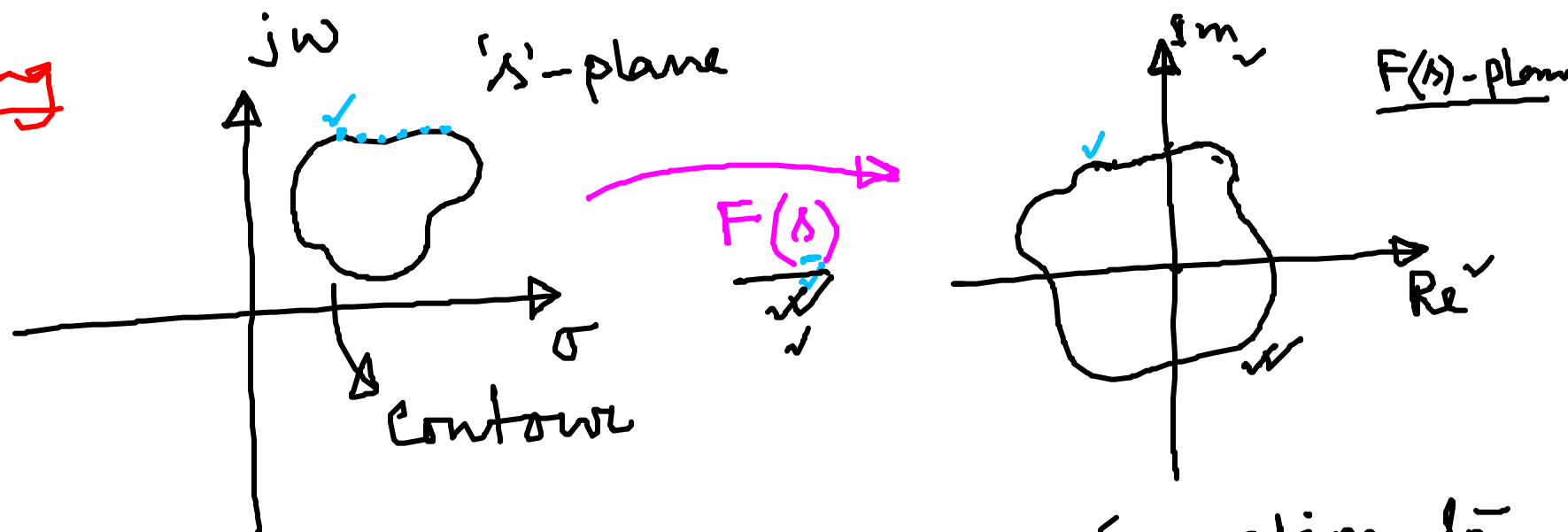
$$\text{Let } G(s) = \frac{N_G}{D_G} \text{ and } H(s) = \frac{N_H}{D_H}.$$

$$\text{Then } G(s)H(s) = \frac{N_G N_H}{\underline{D_G D_H}} \checkmark \text{ and } 1 + G(s)H(s) = \frac{\underline{D_G D_H + N_G N_H}}{\underline{D_G D_H}} \checkmark$$

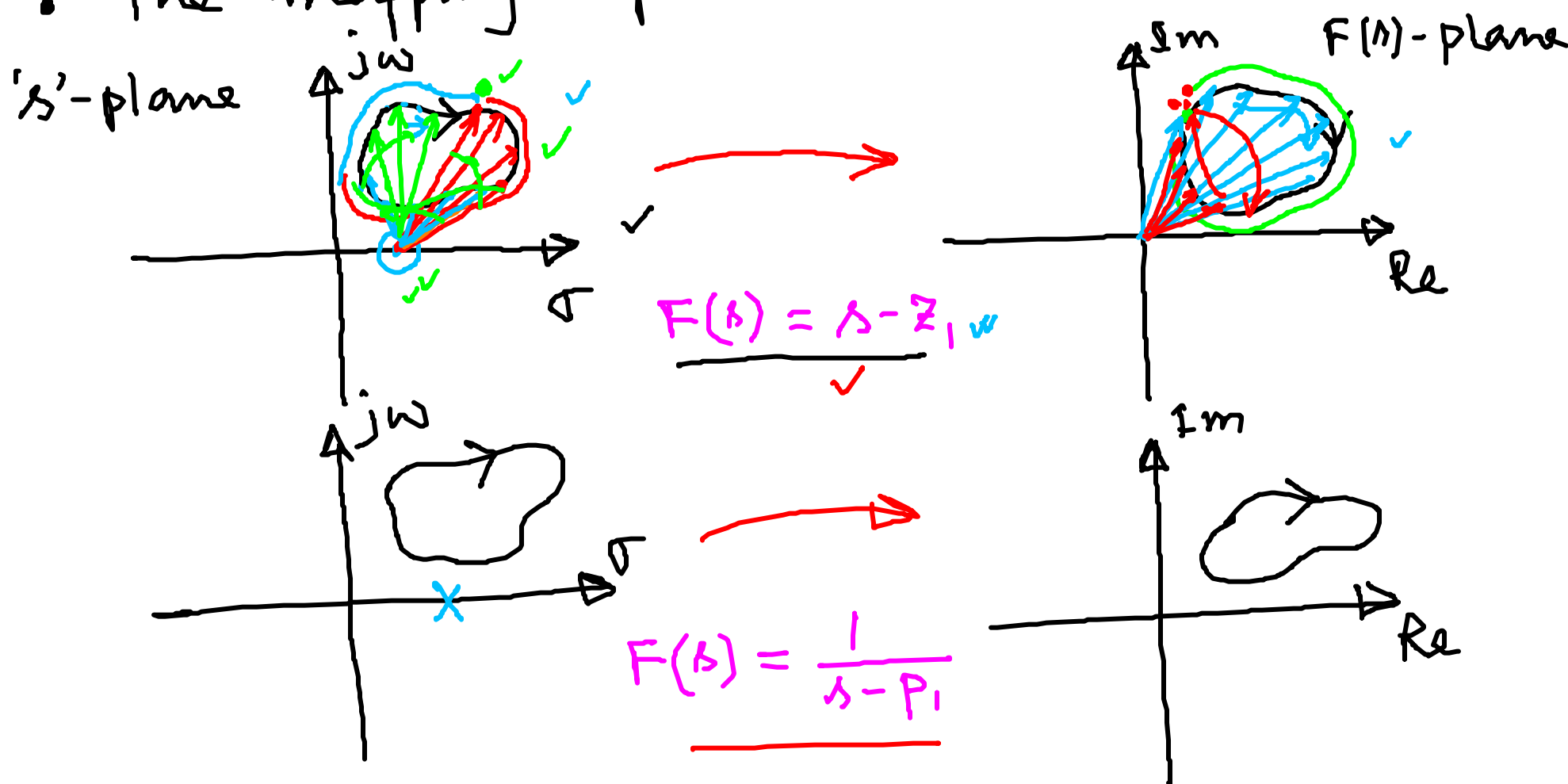
$$\text{The } \underline{\text{closed-loop TF}} = \frac{G(s)}{1 + G(s)H(s)} = \frac{N_G D_H}{\underline{D_G D_H + N_G N_H}} \checkmark$$

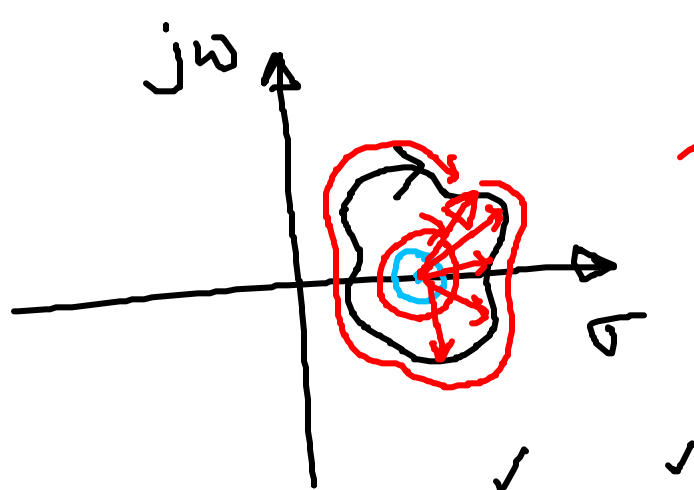
- Poles of $G(s)H(s)$ are same as the poles of $1 + G(s)H(s)$. \checkmark
- Zeros of $1 + G(s)H(s)$ are same as the poles of closed-loop system. \checkmark

Mapping



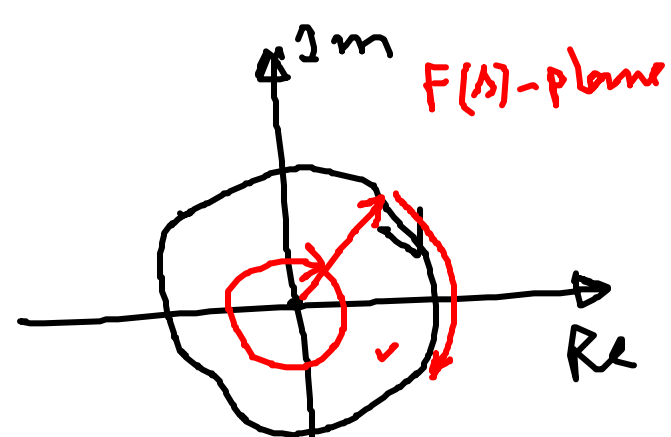
- A Contour is mapped through a function to another contour in $F(s)$ -plane.
- The mapping depends on $F(s)$.



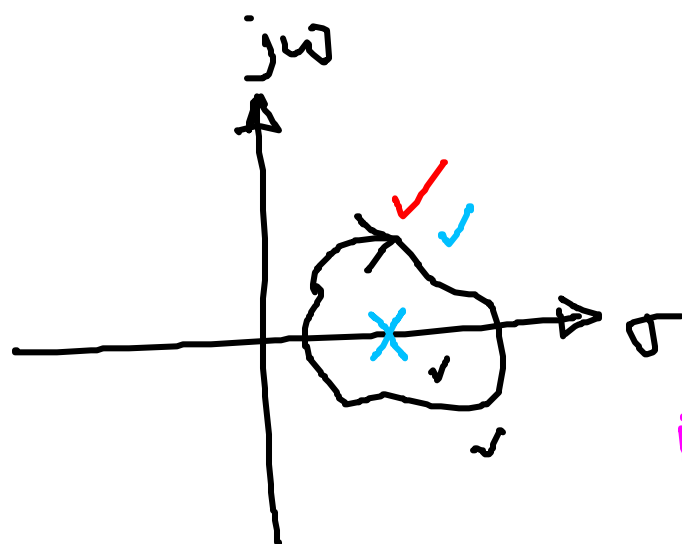


$$F(s) = s - z_1$$

✓
✓

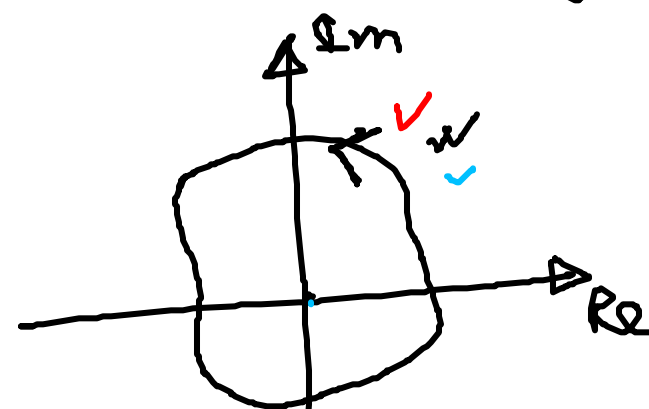


Rotation is same
and encircles origin.

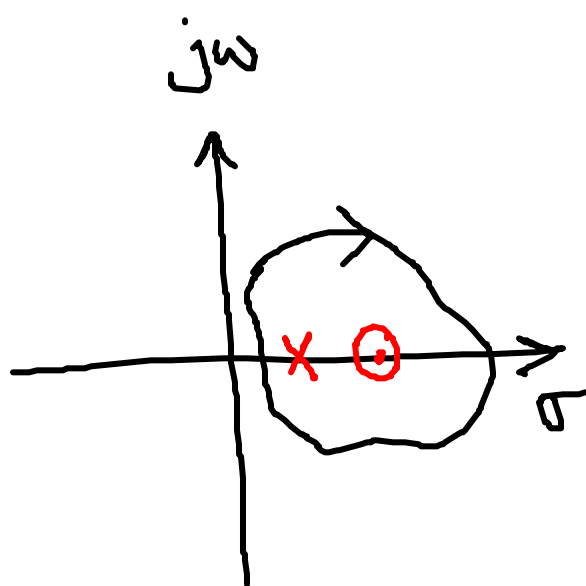


$$F(s) = \frac{1}{s - p_1}$$

✓
-w

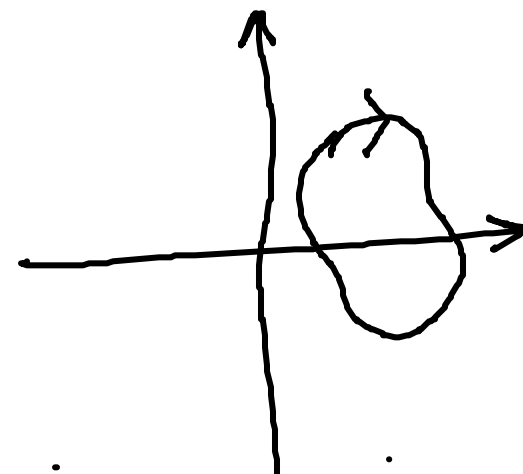


Rotation is reverse
and encircles origin

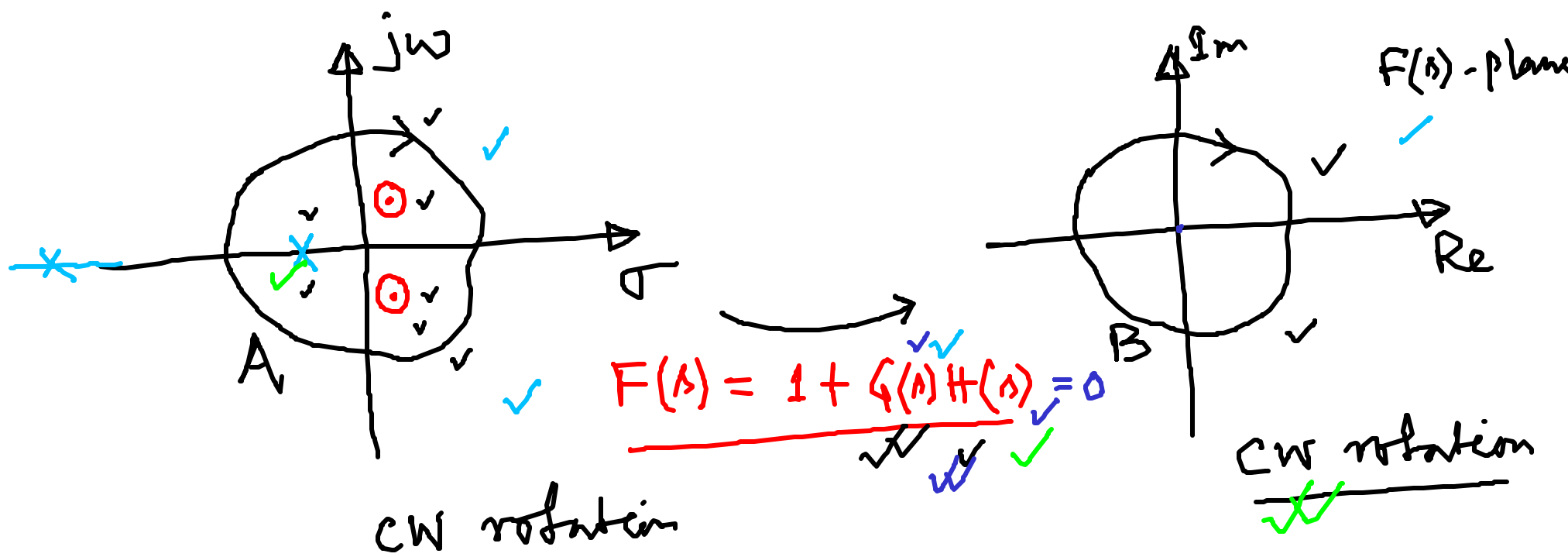


$$F(s) = \frac{s - z_1}{s - p_1}$$

✓
✓



Rotation remains same
and doesn't encircle origin



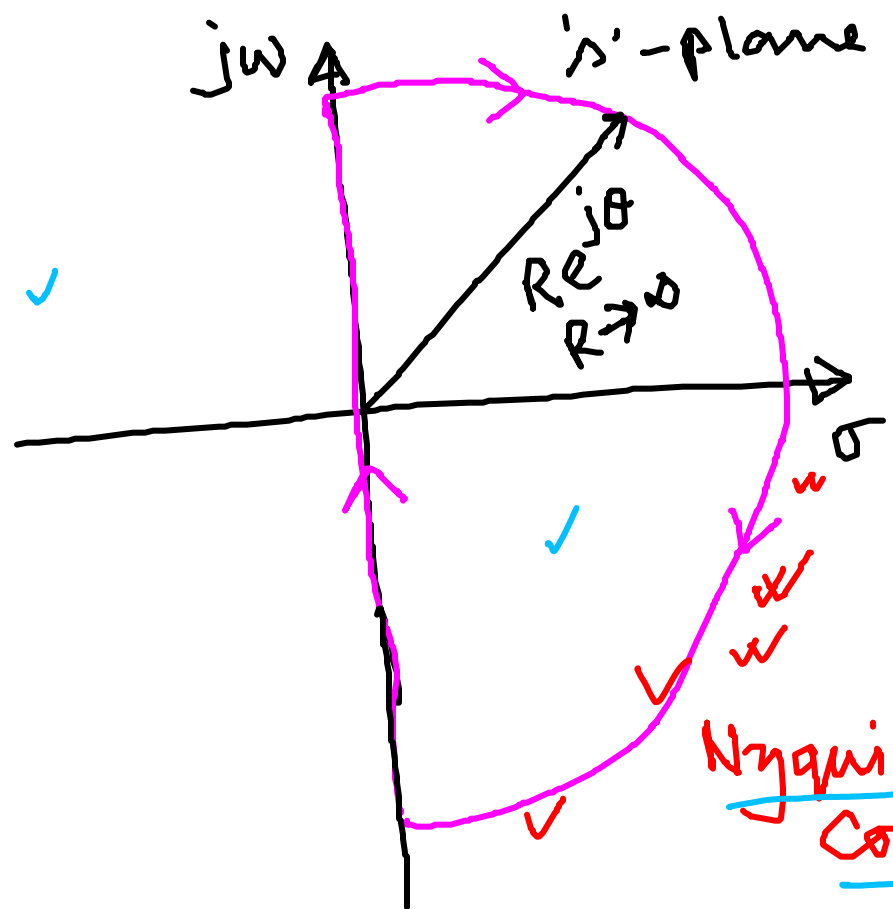
$$N = P - Z = -1$$

N = The number of CCW rotation of Contour B about the origin.

P = The number of poles of $1 + G(s)H(s)$ inside the contour A.

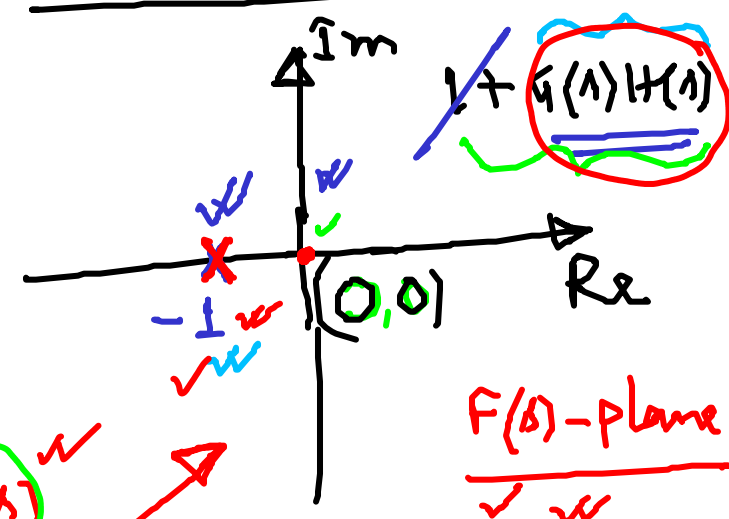
Z = The number of zeros of $1 + G(s)H(s)$ inside the contour A.

This is known as 'Principle of argument'



$$N = P - Z \quad \text{from principle of argument.}$$

Mapping via $G(s)H(s)$



Nyquist Contour.

$$F(s) = \frac{G(s)H(s)}{1 + G(s)H(s)}$$

$$N = P - Z$$

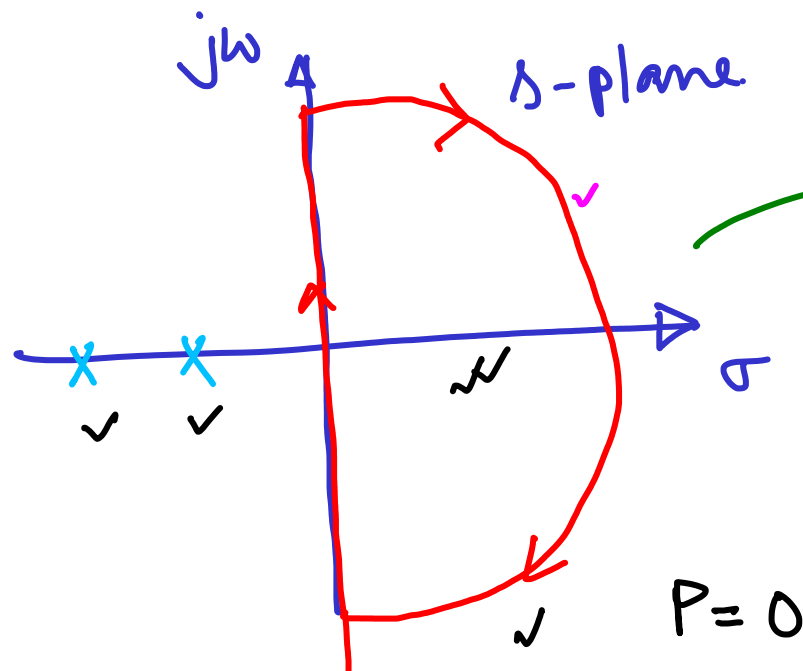
$$\Rightarrow Z = P - N \quad \leftarrow \text{CCW rotation enclosing } -1+j0.$$

No of poles of loop TF ($G(s)H(s)$) enclosed by the Nyquist Contour

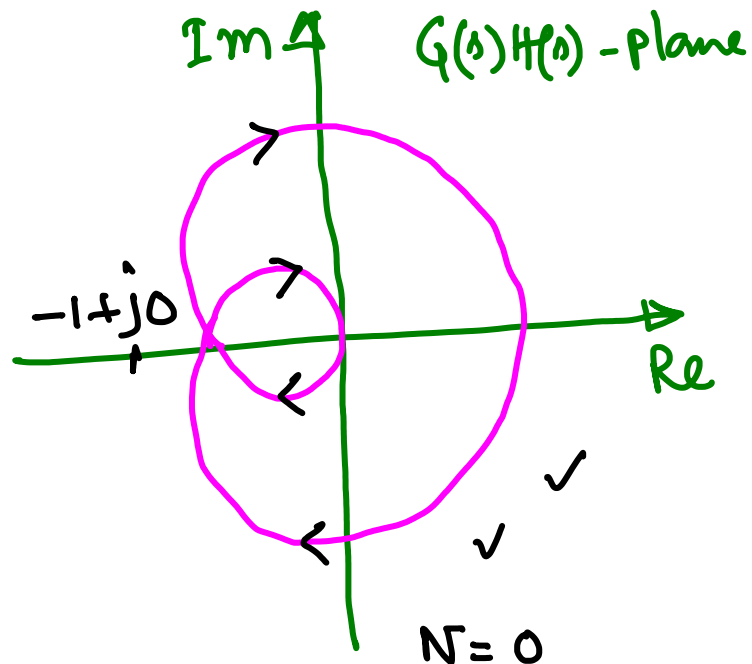
No of closed-loop poles enclosed by the Nyquist Contour.

The closed-loop system is stable if the number of encirclement about $-1+j0$ in CCW direction is equal to the number of loop TF poles in RHP.

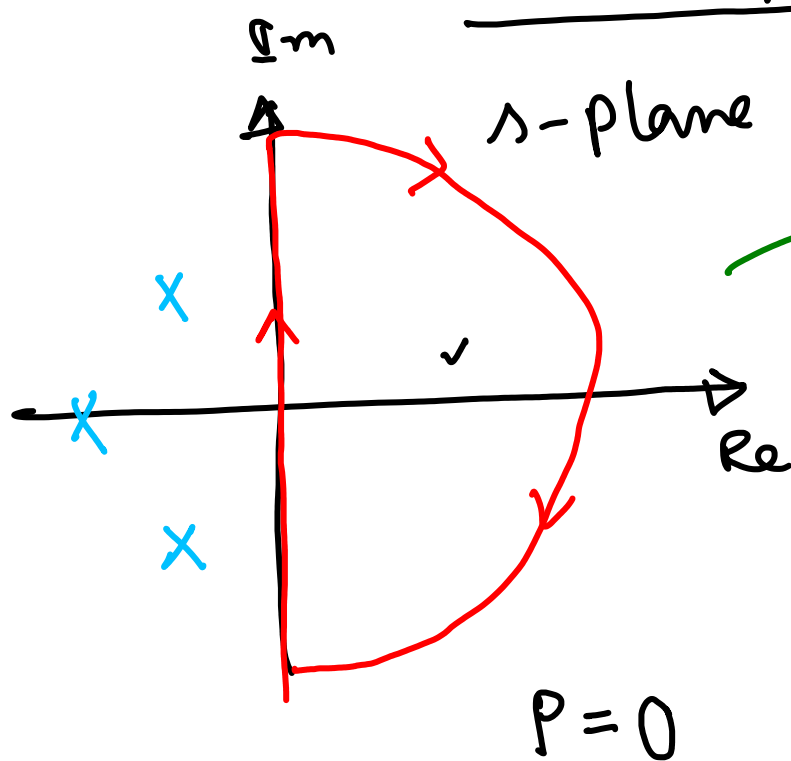
Ex



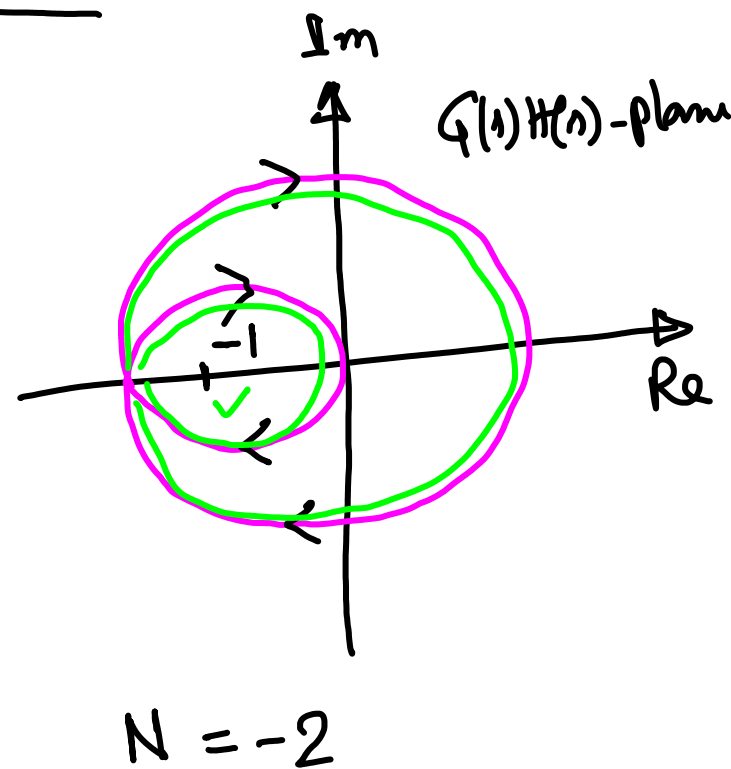
$G(s)H(s)$



$Z = P - N = 0 - 0 = 0$
Closed-loop system Stable.



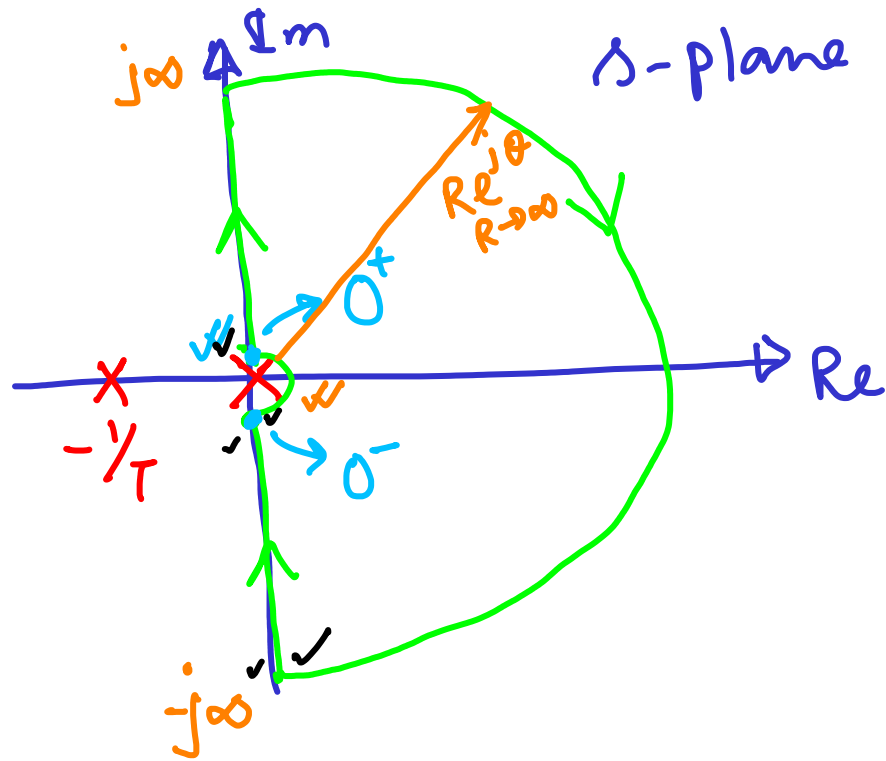
$G(s)H(s)$



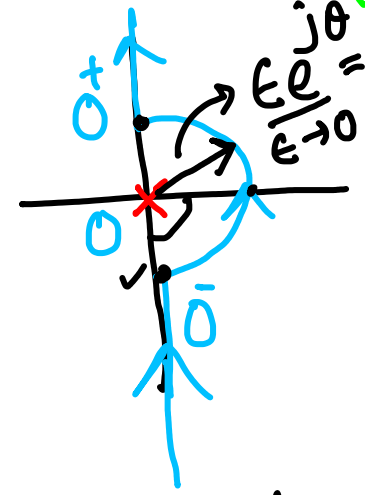
$Z = P - N$
 $= 0 - (-2) = 2$ (Two poles are in RHP)

The closed-loop system is unstable.

When $G(s)H(s)$ has poles and/or zeros on the jw-axis

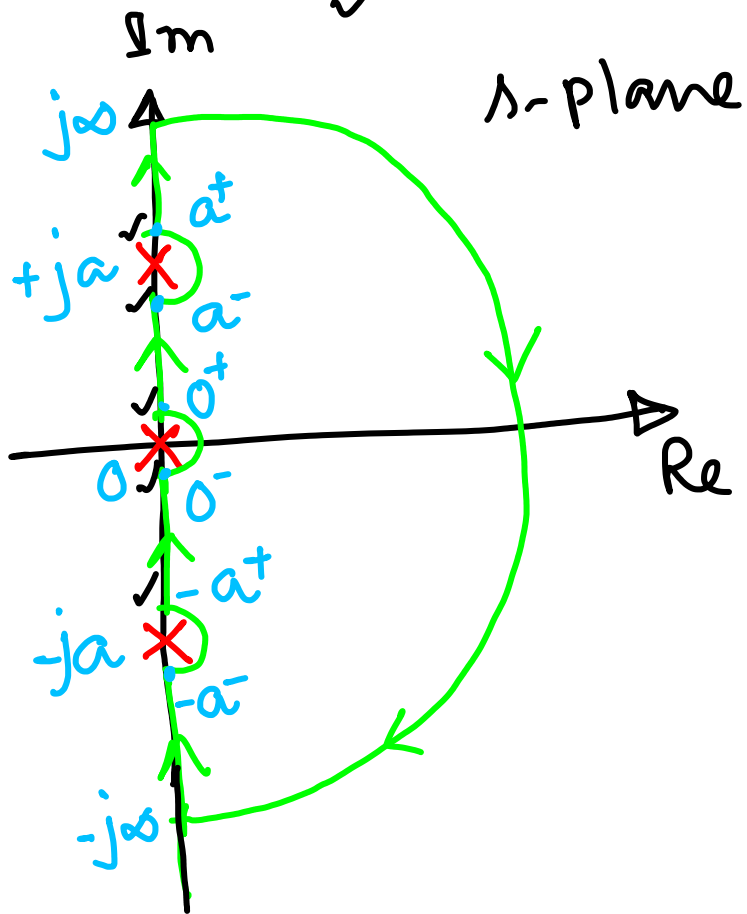


$$GH(n) = \frac{1}{n(n+1)}$$



$\epsilon \rightarrow 0$ and
 θ varies as
 -90° to 0 to 90°

$$\frac{-\infty \quad b^- \quad 0 \quad b^- \quad 0^+ \quad b^- \quad \infty}{-}$$

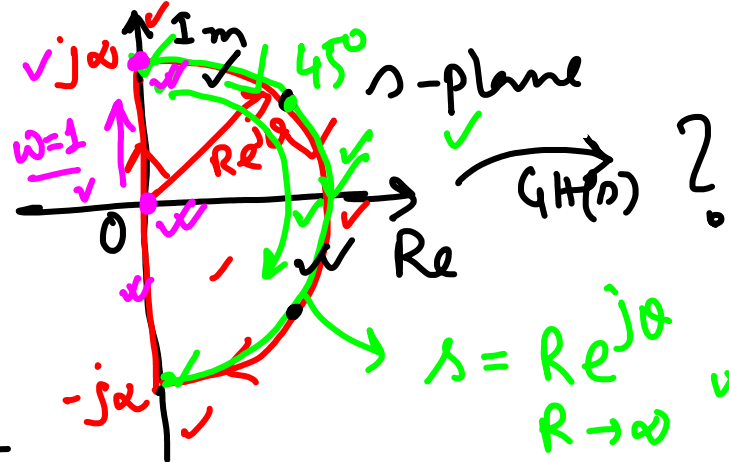


Variation of ω

$$- \cancel{\omega} b^- - \bar{a} b^- - a^+ b^- \bar{0}$$
$$b^- 0^+ b^- \bar{a} b^- a^+ b^-$$
$$\quad \quad \quad \infty.$$

Ex

$$G(s)H(s) = \frac{1}{s^2 + 0.8s + 1}$$



$$G(j\omega)H(j\omega) = \frac{1}{-\omega^2 + j0.8\omega + 1}$$

$$= \frac{(1 - \omega^2) - j0.8\omega}{(1 - \omega^2)^2 + 0.64\omega^2} = \frac{1 - \omega^2}{(1 - \omega^2)^2 + 0.64\omega^2} - j \frac{0.8\omega}{(1 - \omega^2)^2 + 0.64\omega^2}$$

$$\lim_{\omega \rightarrow 0} G_H(j\omega) = \underline{1} \angle 0^\circ \checkmark$$

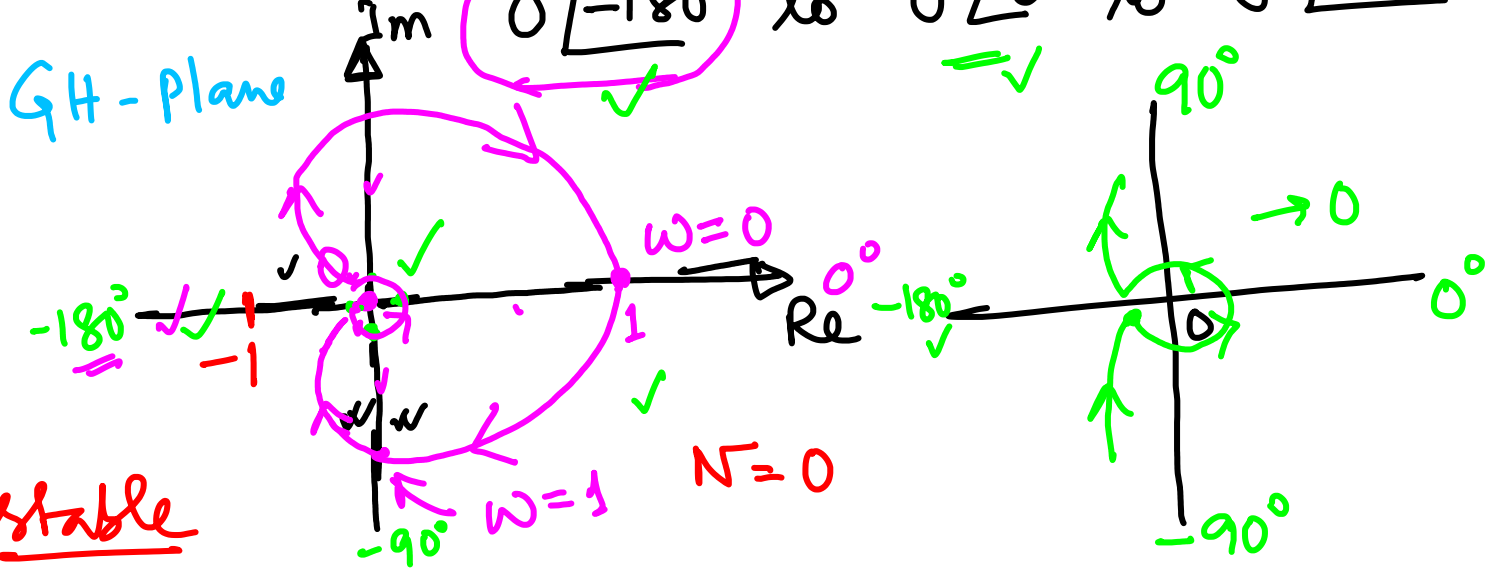
$$\lim_{\omega \rightarrow \infty} G_H(j\omega) = 0 \quad \checkmark \checkmark$$

$\lim_{R \rightarrow \infty} GH(R e^{j\theta}) = \frac{1}{R^2 e^{j2\theta} + 0.8 R e^{j\theta} + 1} = 0 \angle -2\theta$

$G_H\text{-Plane}$

m

$0 \angle -180^\circ$, $0 \angle 90^\circ$, $0 \angle 0^\circ$, $0 \angle 180^\circ$.



$$Z = P - N$$
$$= 0 - 0 = 0$$

stable

Ex $G_H(s) = \frac{1}{s(s+1)}$

$$G_H(j\omega) = \frac{1}{-\omega^2 + j\omega}$$

$$= \frac{-\omega^2 - j\omega}{\omega^4 + \omega^2} = -\frac{\omega^2}{\omega^4 + \omega^2} - j \frac{\omega}{\omega^4 + \omega^2}$$

$$= -\frac{1}{\omega^2 + 1} - j \frac{1}{\omega(\omega^2 + 1)}$$

$-1 - j\omega$

$$G_H(\epsilon e^{j\theta}) = \lim_{\epsilon \rightarrow 0} \frac{1}{\epsilon e^{j\theta}(\epsilon e^{j\theta} + 1)} = \lim_{\epsilon \rightarrow 0} G_H(\epsilon e^{j\theta}) = \infty \angle -\theta$$

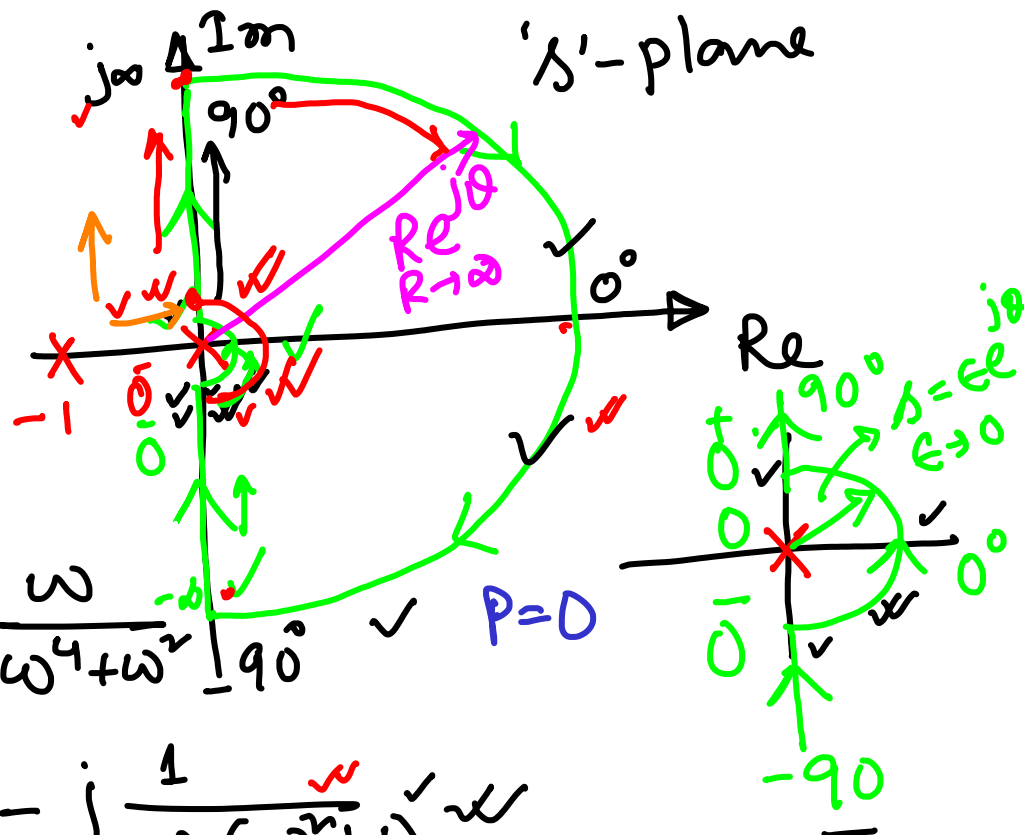
$$\propto \angle 90^\circ \quad \text{to} \quad \propto \angle 0^\circ \quad \text{to} \quad \propto \angle -90^\circ$$

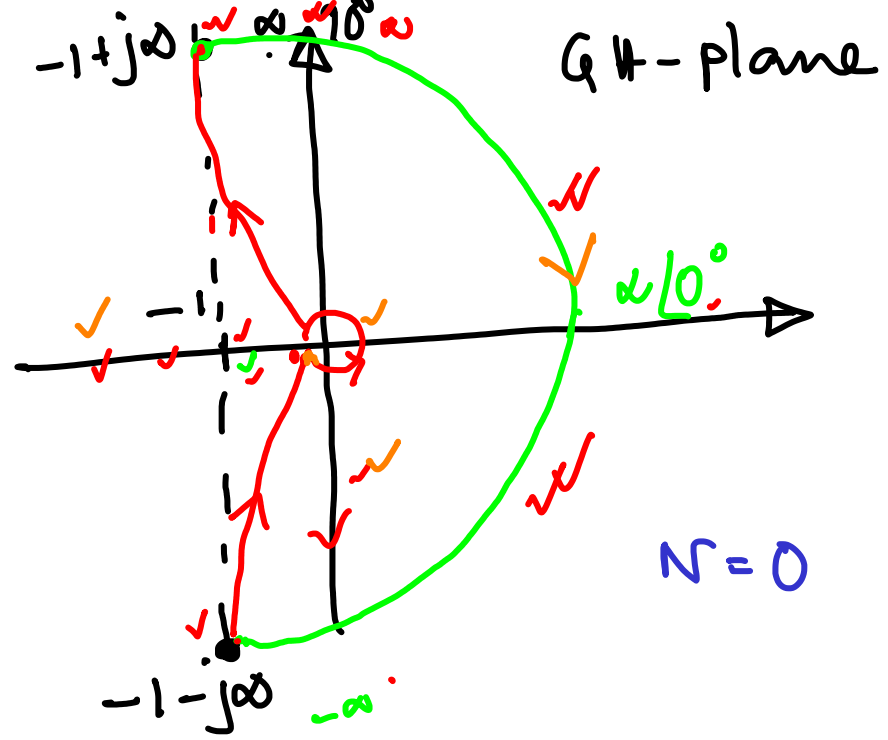
$\lim_{\omega \rightarrow \infty} G_H(j\omega) = 0$

$$G_H(R e^{j\theta}) = \frac{1}{R e^{j\theta}(R e^{j\theta} + 1)}$$

$$\lim_{R \rightarrow \infty} G_H(R e^{j\theta}) = 0 \angle -2\theta$$

$$0 \angle -180^\circ \quad \text{to} \quad 0 \angle 0^\circ \quad \text{to} \quad 0 \angle 180^\circ$$





$Z = 0$
(stable).
✓