Basic rules for sketching the mot bours

1. No. of branches: The number of branches of the number of closed-loop poles.

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Ex.
$$1 + \frac{(3+2)}{(3+3)(3+4)} = 0$$

ch.
$$eq^{2}$$
: $(5+3)(5+4)+(5+2)=0$

$$(5+2)=0$$
No. of chied-log pres = 2

when k=0, S=-3 and S=-4 are two mosts of the Ch.

$$\frac{1}{1} + \frac{3}{1} + \frac{2}{1} = 0$$

$$\frac{1}{1} + \frac{2}{1} = 0$$

$$1 + \frac{2}{1} + \frac{2}{1} = 0$$

$$1 + \frac{3}{1} + \frac{4}{1} = 0$$

When k-100, s=-2 is a mot of the ear.

K-100, s=0 is a most of the ear.

2. Symmetry: The roof locus is symmetrical about the real-axis since the polynomial is a real co-efficient polynomial. 3 40°+140° 0° 1 3. Real-aris regment: [K 4(5) H(5) = (2K+1) 180° JWA 's'-plane = 180° www.w - Repultant Contribution of complex pole and/or z'ero is 360°/0°. On the real-axis, for k)o, the noof locus exists to the left of an odd number of real axis finite open. list poles and/or finite
open-ling zerrs. The roof locus approaches straight lines as asymptilis as the locus approaches infinity, 4. Centroid and The real-axis intercept T = I finite poles - Etimite zems (no. of finite poles) (no of finite
zerrs)

Angle of asymptoles 2 Symptones $\frac{1}{2}$ (2xH) \sqrt{N} $\sqrt{$ It is needed when some zerrs are at infinity. $\frac{k}{(5+2)(5+4)(5+6)} = kG(5)H(5)$ G(s) = No. of finite ples = 3 (-2, -4, -6)No. of fimili Zem = 0 $\sigma = (-2 - 4 - 6) - (0) = -\frac{12}{3} = -4$ $\theta = \frac{180^{\circ}}{3-0} = 60^{\circ}, 180^{\circ}, 300^{\circ}$ (s'-plane)

5. Real-axis breakaway or break-in points:

$$1 + k (9) H(5) = 0. \text{ if } k = -\frac{1}{9(5) H(5)} \text{ if } k = -\frac{1}{9(5) H(5)} \text{ if } k = -\frac{1}{9(5) H(5)} \text{ if } k = 0.$$

Calculate $\frac{dk}{ds}$ and $\frac{dk}{ds} = 0$.

$$= \frac{1}{9(5) H(5)} \text{ if } k = 0.$$

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6. The jw-axis crossing: The Roult-Hurwitz criterion is used to find the jw-axis crossing point and the corresponding gain K. 5+35+2+4(5-85+15)=0 5 (KH) + 5 (3-8K) + (2+15K) = D 7 S (KH) (2+15K) S (3-8K) + 3-8K = 0 S (2+15K) + 8 = 3 = 4Anciliary eans $4(5) = \frac{11}{8}x^{2} + \frac{61}{8} = 0$ 7. Angle of departure and Anival: When complex conjugate pole and/or zero pole and/or zero exist, we need to find angle of departure or avrival.

kG(s) H(s) = k(s+2)Ex jw (3+3) (3+33+2) ~ ろ1,2 = -1±1 * A point -> [K4(5) HCs) = (2KH) (80) -01+02-90°-0 = 180° Centraid $T = (-3 - 1 + 1 - 1 - 1) - (-2) = \frac{3}{3} = -1.5$ Angle of asymptotis $\theta = \frac{180^{\circ}}{2} = 90^{\circ}, 270^{\circ}$ $\theta_1 = tan \left(\frac{1}{2}\right) \quad \theta_2 = tan \left(\frac{1}{2}\right)$ $-\theta = 180^{\circ} + 90^{\circ} + \theta_1 - \theta_2 = 270^{\circ} + 26.55^{\circ} - 45^{\circ}$ = 251.6° $\theta = -251.6^{\circ} = 108.4^{\circ}$

D1,2 = 2 ± 4) (Zerrs) K(120) EX R(s) + -0,-02+90+0=180° -ton (4/6) -45°+90°+0 -33-69°-45°+90+0 0 = 168. C9° Angle of avoival $k = -\frac{(5^{2} + 60 + 8)}{(5^{2} - 40 + 20)}$ $\frac{dK}{ds} = 0$, $5\tilde{N} - 12N - 76 = 0$ b_{1,2} = (-2.86) 5.28 $1 + \kappa \frac{(\sqrt{3} - 4s + 20)}{\sqrt{3} + 6s + 8} = 0$ 5+60+8+KN-1K0+20K=0

$$\int_{0}^{3} (x+1) + (6-4k) n + (8+20k) = 0$$

$$\int_{0}^{3} (x+1)^{3} (8+20k) + k = 0$$

$$\int_{0}^{3} (6-4k) + k = 0$$

$$\int_{0}^{3} (8+20k) + k = 6/4 = 1.5$$

$$\int_{0}^{3} (8+20k) + k = 6/4 = 1.5$$

$$\int_{0}^{3} (8+20k) + k = 0$$

Roof sensitivity (pole sensitivity)

The valio of the fractional change in a closed-loop pile to the fractional change in a system parameter. $S = \frac{8s/s}{8v/v} = \frac{k}{s} \frac{ss}{sv} \times \frac{v}{s} \frac{\Delta s}{\Delta v} = \frac{k}{s} \frac{ss}{sv} \times \frac{v}{s} \frac{\Delta s}{\Delta v} = \frac{s}{s} \frac{s}{s} \frac{s}{s} \frac{s}{s} = \frac{s}{s} \frac{s}{s} \frac{s}{s} = \frac{s}{s} \frac{s}{s} \frac{s}{s} \frac{s}{s} = \frac{s}{s} \frac{s}{s} \frac{s}{s} \frac{s}{s} = \frac{s}{s} \frac{s}{$

= 40= 254K

Let ch. en? be

$$3 + 100 + 1 = 0$$

$$3 + 10 = 0$$

$$3 + 10 = 0$$

$$\frac{dn}{dk} = -\frac{1}{2h+10} \times \frac{1}{2h+10} \times \frac$$

Closed-loop TF = KG(5) 1- K G(s) H(s) Poles of closed-loop system satisfy 1-KG(S)H(S)=0. \Rightarrow KG(s) Hes) = 1.=1/2KT = 1/K360° x=0, ±1, ±2 $\sqrt{\frac{k G(s) Hes}{k}} = \frac{[k340^{\circ}] k^{2} O, \pm 1, \cdots N}{\sqrt{\frac{k}{N}}}$ 1. No. of brancher: No Change
2. Symmetry: No Change 3. Real-axis segment: On the real-axis, the roof voeus exists to the left of an EVEN/numbere of real-axis, finite open hop zenos. 4. Starting and ending: No change 5. Centrid and angle of asymptolis: J: No Change 10 0 of finite pres) - (no finite zens)

(no of finite pres) - (no finite zens)

If we consider $K < 0 \cdot V - \omega < K < 0$