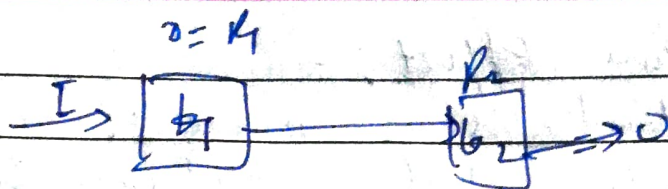


Q6 =



full scale error of Inst 1

$$= \frac{k_1 R_1 \alpha n_1}{100}$$

But if input is not FS,

$$\text{Error} = \frac{k_1 I_{fs}}{100}$$

So, we have 4 case here.

Taking  $(n_1, n_2), (x, y), (y_1, n_2) \& (y_1, y_2)$ .

Case I  $(n_1, n_2)$

$$O = k_2 \left( k_1 I + \frac{k_1 R_1 n_1}{100} \right) + \frac{k_2 R_2 n_2}{100}$$

$$O = k_2 k_1 I + \frac{k_1 k_2 R_1 n_1}{100} + \frac{k_2 R_2 n_2}{100}$$

$$\text{Error} = \frac{k_1 k_2 R_1 n_1}{100} + \frac{k_2 R_2 n_2}{100}$$

Case II ( $x_1, y_2$ )

$$0 = b_2 \left( b_1 I + \frac{b_1 R_1 x_1}{100} \right) + \frac{b_2 y_2}{100} \left( b_1 I + \frac{b_1 R_1 x_1}{100} \right)$$

$$0 = b_2 b_1 I + \frac{b_1 b_2 R_1 x_1}{100} + \frac{b_2 b_1 y_2 I}{100} + \frac{b_2 b_1 R_1 x_1 y_2}{10000}$$

Error  $\frac{b_1 b_2 (R_1 x_1 + y_2 I)}{100}$  Ignored

Case III ( $y_1, x_2$ )

$$\text{Error} = \frac{b_1 b_2 I y_1 + b_1 R_2 x_2}{100}$$

Case IV ( )

$$0 = b_2 \left( b_1 I + \frac{b_1 I y_1}{100} \right) + \frac{b_2 y_2}{100} \left( b_1 I + \frac{b_1 I y_1}{100} \right)$$

$$\text{Error} = \frac{b_1 b_2 I y_1}{100} + \frac{b_1 b_2 I y_2}{100}$$



Q20

Given:-

Rated Input ( $I$ ) = 2kWOutput Sensitivity w.r.t Input ( $K$ ) = 2mV/V of excitationRepeatability error ( $E_1$ ) =  $\pm 0.05\%$  of rated o/p (PS)Reversibility error ( $E_2$ ) =  $\pm 0.5\%$  of rated o/pNon-linearity ( $N$ ) =  $\pm 0.25\%$  of rated o/pDeviation of zero signal ( $E_3$ ) =Modifying input  $\pm 0.05\%$  of rated o/p.  
Sensitivity = $\pm 0.26\%$  of o/p/°C→ Modifying input here is dependent of or Temp  $\propto T = T_m$ in the worst case  $T = 100^\circ\text{C}$ → Similarly, interfering input is also temp  $E = I_2$ Sensitivity ( $K_2$ ) =  $\pm 0.15\%$  of rated o/p/°C

(a) From here Net of p can be divided into sections =

Nominal Excitation  $(O_L) =$

$$\begin{aligned} & (kI + \gamma) \\ & = (2mV \times I + \gamma) \quad \text{no value} \\ & = 2mI \end{aligned}$$

$$\text{Errors} = (\pm 0.05\% + 0.5\% + 0.05\%) \times (2mI)$$

$$= 1.2 \times 10^{-5} I$$

$$\begin{aligned} \text{Non-linearity} &= \pm 0.25\% \times 2mI \\ &= 0.5 \times 10^{-5} I \end{aligned}$$

$$\text{Interfering output} = kT_2 IT$$

$$\begin{aligned} &= \frac{0.18 \times 2mI \times T}{10} \\ &= \frac{0.36}{10} \times 10^{-5} TI \end{aligned}$$

$$\text{Till now total output} = \left( 2mI + 1.2 \times 10^{-5} I \right) + 0.36 \times 10^{-5} IT$$

Modifying output =

( $\pm 0.25\%$  of Netm-o/p)

$$= 0.25 \times 10^{-2}$$

$$\frac{0.36 \times TI \times (2m + 1.2 \times 10^{-5} + 9.6 \times 10^{-2} T)}{10}$$



So, net output =

$$\begin{aligned} & (2 \times 10^{-3} + 1.7 \times 10^{-5} + 3.6 \times 10^{-5} T) I \\ & + 3.6 \times 10^{-5} I T (2 \times 10^{-3} + 1.7 \times 10^{-5} + 3.6 \times 10^{-5} T) \end{aligned}$$

(b).  $O(I_T) = (2 \times 10^{-3} + 1.7 \times 10^{-5} + 3.6 \times 10^{-5} T) \% \text{ of FS O/P}$   
 $\pm (3.6 \times 10^{-2} T) \% \text{ of Measured O/P.}$   
 Here ideal output =  $2 \times 10^{-3} \text{ V/V FS.}$

then error band

$$\begin{aligned} & = 0.2035 \% \text{ of FS/O/P} \\ & \pm 1.8 \% \text{ of Measured O/P} \end{aligned}$$

(c).  $I = 10 \text{ V, Measured O/P} = 10 \text{ mV.}$

$$\begin{aligned} \text{FS O/P} &= k I \cdot e \alpha \\ &= 2 \text{ mV/V} \times 10 \\ &= 20 \text{ mV.} \end{aligned}$$

from above Equation.

⊕



(d)

Temperature Effect:-

As load cells are made of either stainless steel or tool steel then temperature changes will influence the accuracy.

CREEP Effects:-

this is the change of load cell signal that occurs under load.

Repeatability:-

When a load is repeatedly applied to a load cell, the output may vary slightly.