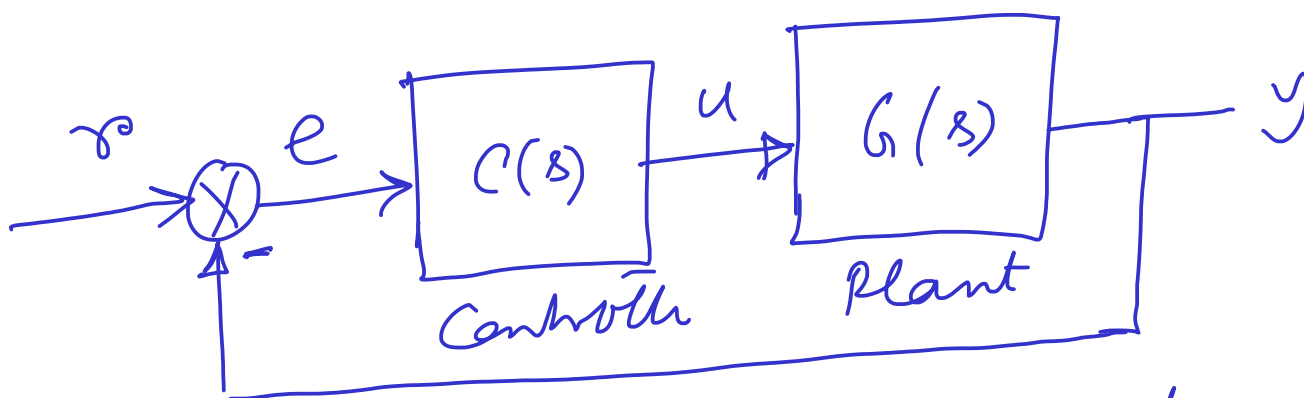


Lecture - 7

Designing lag, lead & lag-lead controllers

specifications

- Steady-state error constraints
(e.g. proportional error constraint (k_p)
velocity error constraint (k_v), etc)
- phase margin (PM)
- gain cross-over freq (ω_{cf})



$$C(s) = K H(s) \quad \text{--- Cascaded Controller}$$

K - Static gain used to meet
S.S error constraints

$H(s)$ → Normalized lag, lead
or lag-lead controller
(used to meet PM & g.c.f
specifications).

To meet S.S specifications:

$$e_{ss} = \frac{1}{1 + K_p} \rightarrow \text{for step i/p}$$

$$= \frac{1}{K_v} \rightarrow \text{for ramp input}$$

Where

$$K_p = \lim_{s \rightarrow 0} L(s) = \lim_{s \rightarrow 0} G(s) \cdot K H(s)$$

$$= \lim_{s \rightarrow 0} K G(s) \left[\because H(0) = 1 \right]$$

$$K_v = \lim_{s \rightarrow 0} s L(s) = \lim_{s \rightarrow 0} K s G(s)$$

To meet PM & g.c.f

- From given PM specification, determine the phase of the compensated system at g.c.f as $-180^\circ + \text{PM} = \phi_{\text{com}}$

- Determine the phase of the uncompensated system at the given ω_{uc} , say ϕ_{uc} .
- Determine the gain (in dB) of the uncompensated system at the given ω_{uc} .
- If $\phi_{com} > \phi_{uc}$ & M_{uc} is -ve in dB, then use lead controller with $\phi_c = \phi_{com} - \phi_{uc}$ & $M_c = -M_{uc}$.
- If $\phi_{com} < \phi_{uc}$ & M_{uc} is +ve in dB, then use lag controller where $\phi_c = \phi_{com} - \phi_{uc}$, $M_c = -M_{uc}$.
- If $\phi_{com} > \phi_{uc}$ but M_{uc} is +ve then use lag-lead controller with $M_c = -M_{uc}$, $\phi_c = \phi_{com} - \phi_{uc}$.

Note: If ω_c is not mentioned, then the following are important:

- $\omega_c > \omega_{uc}$, use lead controller such that M_c is +ve & ϕ_c is positive.
- $\omega_c < \omega_{uc}$, use lag controller such that M_c & ϕ_c are negative.

- use lag-lead for a lead if M_c is -ve but ϕ_c is +ve

Example : $G(s) = \frac{1}{s(s+5)(s+10)}$

Design a suitable controller to meet the following specifications

a) $K_v = 10$, b) $PM = 45^\circ$
 (choose suitable g.l.f ω_c)

Soln To determine servo gain K

$$K_v = \lim_{s \rightarrow 0} s K G(s)$$

$$\Rightarrow K_v = \frac{K}{50}$$

$$\Rightarrow K = 50 K_v$$

$$\Rightarrow \boxed{K = 500}$$

choice of suitable g.l.f ω_c

Freq response data (for $K_G(s) \rightarrow$ un
compensated
loop TF)

| ω (rad/s) | ϕ_{uc} (degree) | M_{uc} (dB) | ω rad/s | ϕ_{uc} (deg) | M_{uc} (dB) |
|---------------------|-------------------------|---------------|-------------------|----------------------|---------------|
| 1 | -107.02 | 19.79 | 4 | -150.46 | 5.166 |
| 1.5 | -115.21 | 16.01 | 6 | -171.16 | 0.772 |
| 2 | -123.11 | 13.164 | 8 | -186.65 | -5.725 |
| 2.5 | -130.6 | 10.81 | 9 | -192.93 | -7.935 |
| 3.0 | -136.6 | 8.75 | 10 | -198.43 | -10 |

For lead Control:

Compensated syst: phase needed at
desired ω_c is $\phi_{com} = -180^\circ + PM = -180^\circ + 45^\circ$
 $\Rightarrow \phi_{com} = -135^\circ$

From the table $\phi_{com} > \phi_{uc}$
 $\& m_{uc} = -ve$ for the range

$8 \leq \omega \leq 10 \Rightarrow \omega_c$ should be
 chosen from 8 to 10 rad/s for lead
 control design

Let $\omega_c = 8 \text{ rad/s}$

Then $\phi_c = -135^\circ - (-186.65^\circ)$

$\Rightarrow \phi_c = 51.65^\circ$

$\& M_c = 5.725 \text{ dB}$

The lead controller becomes

$$H(s) = \frac{12.725(s + 4.78)}{s + 60.82}$$

(check it)

For lag controller design:

From freq response data,

$\phi_{uc} > \phi_{com}$ & $M_{uc} = +ve$

for ω $1 \leq \omega \leq 2.5$. Thus

here ω_c should lie in between

$1 \text{ to } 2.5 \text{ rad/s.}$

Let $\omega_c = 2 \text{ rad/sec.}$

Then $\phi_c = \phi_{com} - \phi_{uc}$

$$\Rightarrow \phi_c = -135 - (-123.11) \quad (\text{phase lag})$$

$$= 11.89^\circ$$

$$M_c = -M_{uc} = -13.164 \text{ dB}$$

Then the lag controller becomes

$$H(s) = \frac{0.2124 (s + 0.543)}{s + 0.1153}$$

(check it)

For lag-lead controller:

Here $3 \leq \omega_c \leq 6 \text{ rad/s}$

[since in this range M_{uc} is +ve but $\phi_{uc} < \phi_{com}$

Let $\omega_c = 4 \text{ rad/s}$

Then $\phi_c = -135^\circ - (-150.46^\circ)$

$$\Rightarrow \phi_c = 15.46^\circ$$

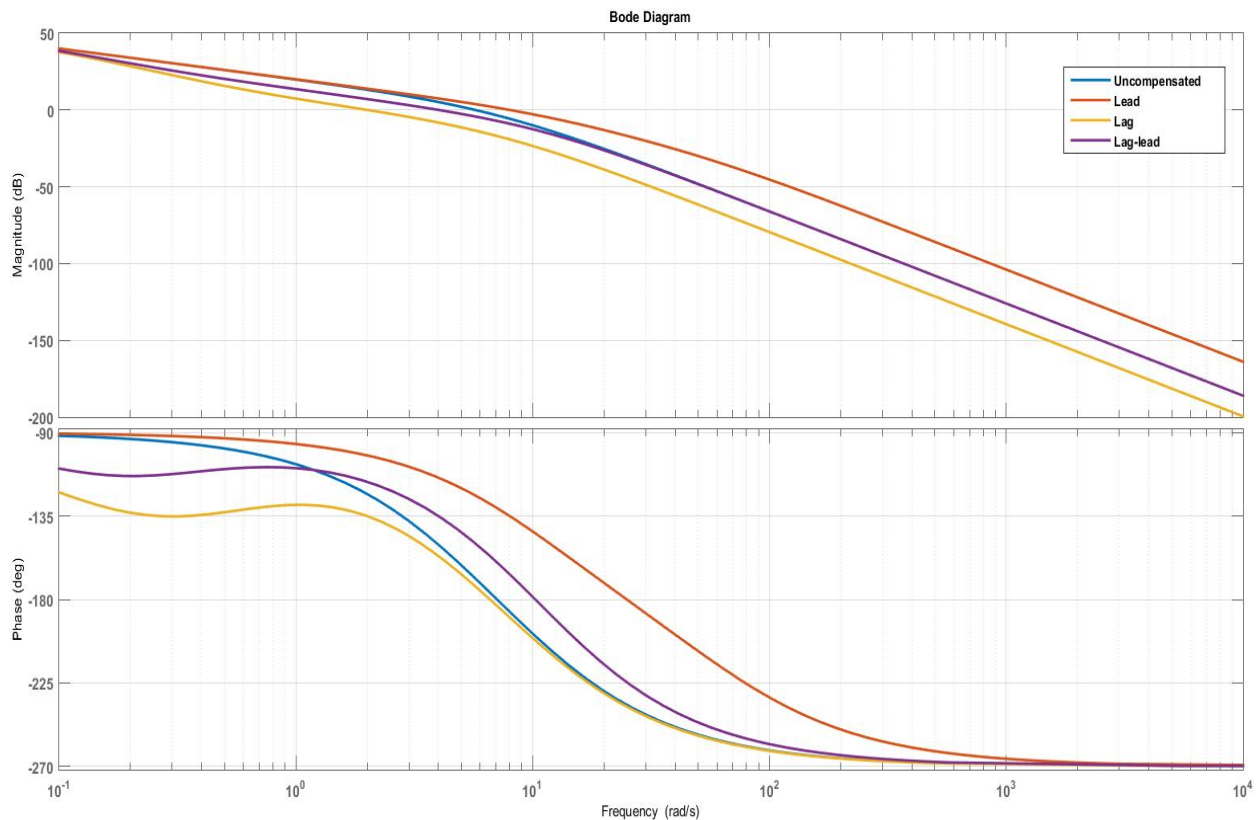
$$M_c = -M_{uc} = -5.166 \text{ dB}$$

Then with $\phi_2 = 2^\circ$, one obtains the lag-lead controller

$$H(s) = \frac{(s + 5.36236)(s + 0.26331)}{(s + 11.44735)(s + 0.1233)}$$

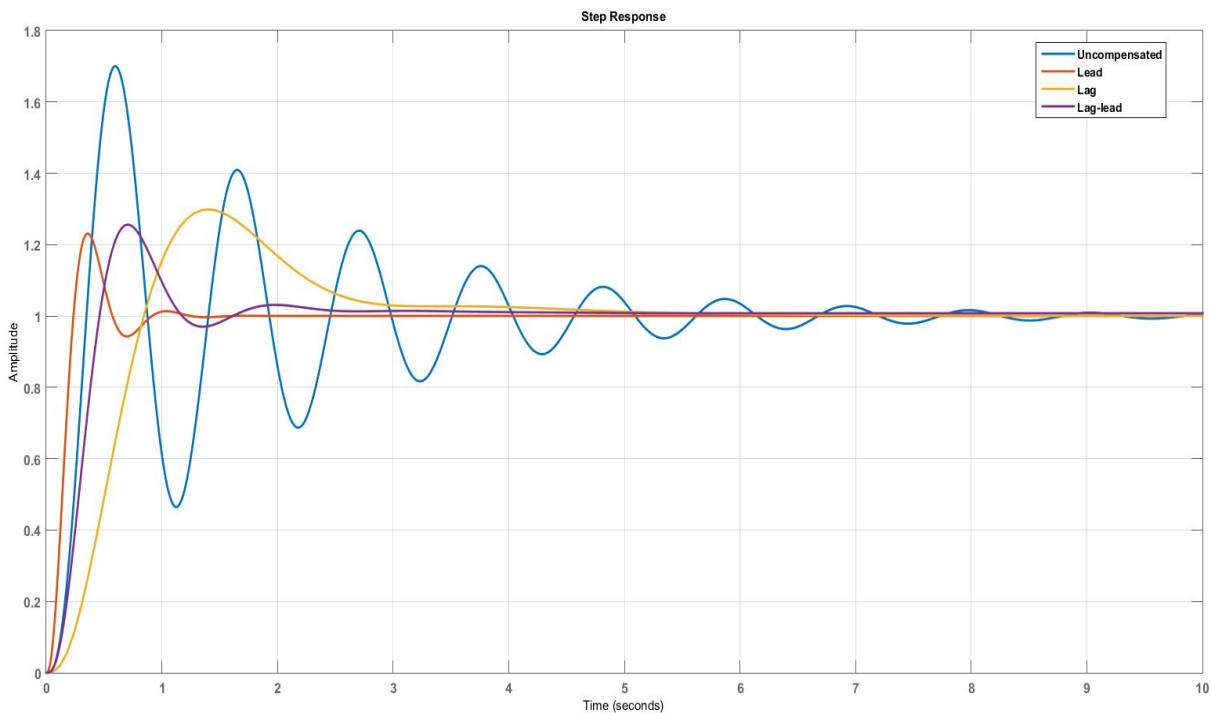
(check it)

Bode-plot



- with lead control dB and Phase curves get shifted up
- - - - lag - - - dB & Phase lower
- lag-lead control a compromise is made.

Time response



- uncompensated response is oscillatory
- with lead control system is fast
- - - - lag - - - becomes slow
- - - - lag-lead - - - response is traded-off.