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WIEN

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¹ 1 Cathodic Ray Tube Basics

² This section features a quick explanation what a CRT is and what it's main components
³ are, followed by a more detailed description on how these components are implemented
⁴ in the CRT Heerlen D14-363GY, which was used in this project. It ends with a
⁵ description of the important characteristics of the CRT and the requirement the theory
⁶ poses on them.

⁷ 1.1 Underlying Physics

⁸ Wikipedia states: “The cathode-ray tube (CRT) is a vacuum tube that contains one
⁹ or more electron guns and a phosphorescent screen and is used to display images. It
¹⁰ modulates, accelerates, and deflects electron beam(s) onto the screen to create the
¹¹ images.”

¹² There are three vital components to accomplish this feat: the electron gun, the
¹³ electron lens and the deflection plates.

¹⁴ The electron gun extracts electrons from a cathode material, accelerates them onto
¹⁵ a perforated anode and thereby produces a free electron beam (see fig. 1.1). One
¹⁶ important characteristic in the selection of a cathode material is a low work function.
¹⁷ The work function denotes the amount of energy needed to extract one electron from
¹⁸ the material. There are two ways to overcome this energy barrier in an electron gun,
¹⁹ one can either overcompensate it by applying a strong electric field (“field emission”,
²⁰ “cold cathode”, fig. 1.2b or one can heat the material until some electrons have enough
²¹ thermal energy to overcome the energy barrier (“thermal emission”, “hot cathode”,
²² fig. 1.2a. For our CRT, only thermal emission is relevant, more detail on this will be
²³ added later along with the description of our cathode’s design.

²⁴ The cathode itself is housed in a so-called Wehnelt cylinder, as the name suggests
²⁵ it is a conducting cylinder, which is set to a slightly more negative potential than the
²⁶ cathode itself. This part implements two features, firstly it condenses the emitted
²⁷ electrons, leading to a smaller spot size, i.e. making the cathode a more point-like
²⁸ electron source. Secondly it enables us to regulate the beam current, the more negative
²⁹ the Wehnelt potential is, the less electrons are emitted by the electron gun. As we

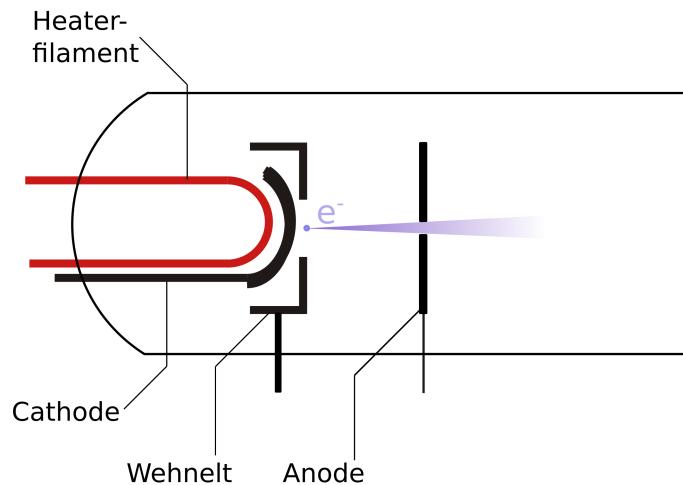
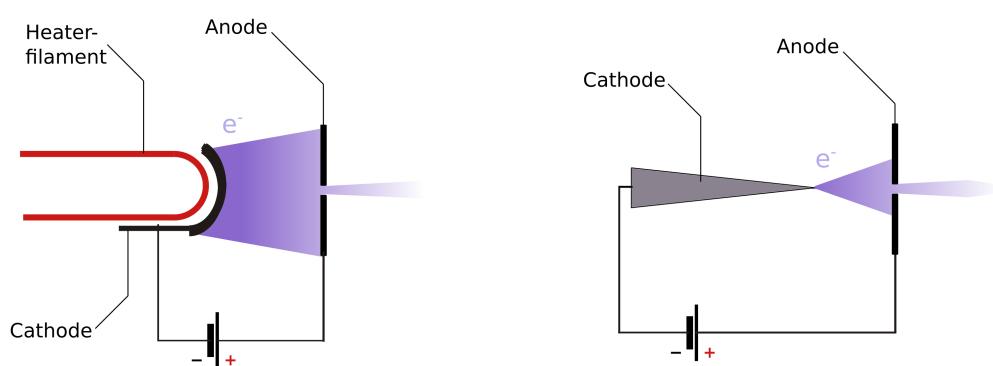


Figure 1.1: Schematic of an electron gun



(a) Schematic of a hot cathode

(b) Schematic of field emission cathode

Figure 1.2: Cathode types

¹ make the Wehnelt potential more positive, the beam current increases and continues
² to rise even after it is more positive than the cathode itself. However the spot size
³ reduction is lost in the process, along with the ability to properly focus the beam with
⁴ electron optics.

⁵ The electrons that leave the electron gun are still divergent and need to be focused.
⁶ For our 2 keV electrons it is still possible to use an electrostatic lens. Cylindrically
⁷ symmetrical pieces of conductor, like rings and tubes, can be set to an electrical
⁸ potential and act as a lens for the electrons. By combining several of them, one can
⁹ (theoretically) engineer an electro-optical system with any combination of desired focal
¹⁰ lengths f_1 and f_2 . The field of this system is simply governed by Laplace's equation in
¹¹ cylindrical coordinates:

$$0 = \frac{1}{r} \frac{\partial \phi}{\partial r} + \frac{\partial^2 \phi}{\partial r^2} + \frac{\partial^2 \phi}{\partial z^2} \quad (1.1)$$

¹³ If we take the axis of the beam to be the z-axis, the position of the focal point in the
¹⁴ x-y-plane can be shifted using the two pairs of deflection plates, one for the x- and one
¹⁵ for the y-direction. The deflection is achieved by applying a voltage between the two
¹⁶ parallel plates. (see: fig. 1.3) By starting with an electron with kinetic energy $e \cdot U_0$
¹⁷ which is accelerated in x-direction by a constant force $e \cdot U_x/d$ over the extent of the
¹⁸ plates L , the deflection angle is approximately [Demtroeder3]:

$$\delta \approx \tan(\delta) \approx \frac{U_x \cdot L}{2U_0 \cdot d} \quad (1.2)$$

²⁰ For the measures of our CRT ($L \approx 10$ cm, $d \approx 1$ cm, $U_0 \approx 2$ kV and distance to
²¹ screen ≈ 20 cm) this amounts to a deflection coefficient of around 20 V cm^{-1} , which is
²² quite consistent with the value given in the CRT's manual.

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stimmen?

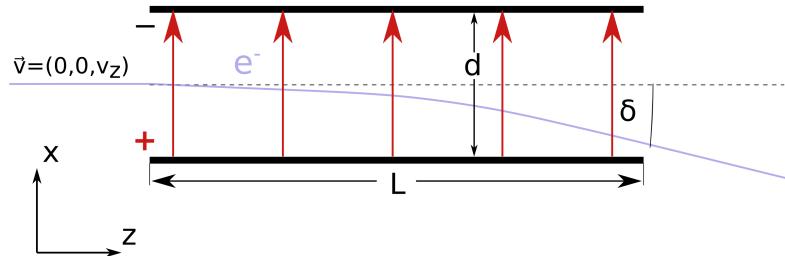


Figure 1.3: Deflection of an electron beam in a constant electrical field

1.2 Implementation in the Heerlen D14-363GY

This section describes how the mechanisms described above are implemented in the CRT that was used in this project: the PDS/CRT Heerlen D14-363GY. Figure 1.4a shows an image of said CRT, fig. 1.4b shows a schematic depiction. The cathode is not visible, as it is fixed inside the Wehnelt cylinder (1), just a few millimeters from the exit of the wehnelt cylinder the electrons pass through the perforated anode (2) they gain their full final kinetic energy over this short distance. The electrons that go through the perforation and enter the electrostatic lens, have 2 keV and therefore move at a speed of approximately $0.08 c$. The electrostatic lenses are realized using three conducting rings (3), that are set to the same potential but have varying radii: Each consecutive ring has a smaller radius than the previous one.

Between the electrostatic lens and the deflection plates, there is another aperture (4), which is internally connected to the anode and is thereby kept at the same potential. In our Setup, the deflection plates are not simply parallel but are shaped like funnels (5,7), between the two pairs of deflection plates, we have the final aperture (6), this ones potential can be regulated separately (usually it's on the same potential as the anode)

It is connected to the glass envelope of the CRT to prevent the glass from charging up and distorting the image. Finally the beam hits the phosphorous-coated screen which fluoresces on electron impact.

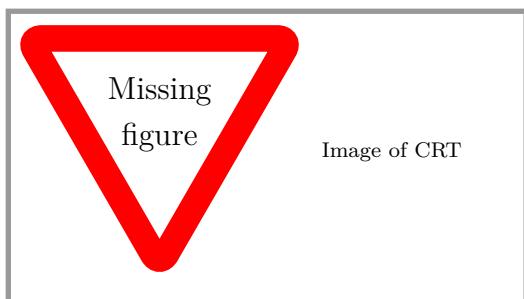
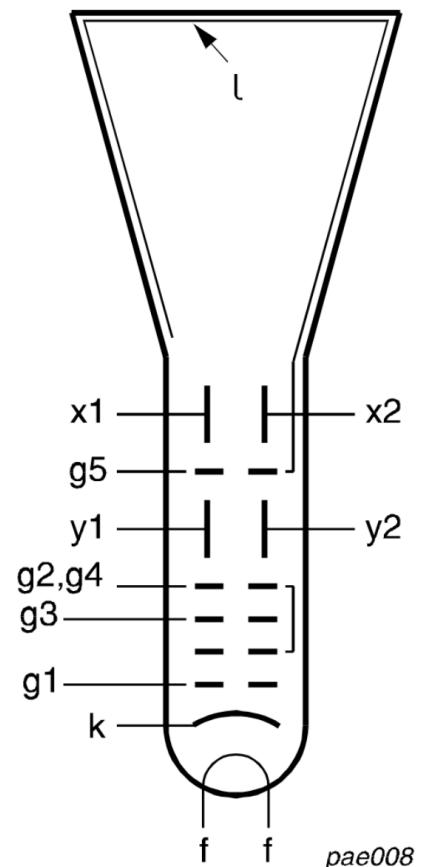


Image of CRT

(a) Image picture of the Heerlen D14-363GY



(b) Schematic of the CRT from [D14363GY123-manual]

Figure 1.4

1.2.1 The Cathode

As already mentioned, we are using a hot cathode, where the electrons are excited thermally until some of them acquire enough energy to leave the material. Compared to cold cathodes, which work by field emission, this leads to a broader energy distribution. In fields like electron microscopy, where a high resolution is the goal, this is undesirable, as it leads to some degree of chromatic aberration in the electron optics, for our purposes, this should not be a problem. On the other hand, hot cathodes normally allow for higher current densities, which is very important to us. The electron current from this kind of emission is described by [Whitaker]:

$$I = A \cdot T^2 \cdot e^{-b/T} \quad (1.3)$$

Where b is proportional to the work function of the material, T is temperature and A is a material-dependent constant. It is clear from this formula, that a low work function and a high melting point are important characteristics for a good cathode material.

The cathode from one of our Heerlen D14-363GY-tubes has been removed and examined with EDX (Energy-dispersive X-ray Spectroscopy). Nickel, barium, and strontium have been found, which suggests that it is a metal oxide cathode with barium-, strontium-, and possibly aluminum-oxide. This type of cathode is very common in low power electron tubes.

The “Power Vacuum Tubes Handbook” [Whitaker] describes a typical oxide cathode as a coating of barium and strontium oxides on a structure made from nickel alloys. Nickel is chosen for its strength and toughness, which it retains even at high temperatures. These cathodes are normally made by coating a case structure with a mixture of barium and strontium carbonates (typically 60 % Ba and 40 % Sr), suspended in a binder material and then baking the structure, causing the carbonates to be reduced to oxides.

These metal oxide cathodes normally operate at 700 °C to 820 °C and are capable of average emission densities of 100 mA cm⁻² to 500 mA cm⁻². Still higher peak emissions are possible for shorter periods of time, as already mentioned, one of the advantages of this type of cathode is its high emission current capability compared to cathodes made from other materials. Downsides to this cathode type are its greater susceptibility to so-called oxygen poisoning and to ion bombardment. The literature therefore recommends to avoid prolonged exposure to oxygen. Oxygen poisoning is the process in which oxygen adsorbs onto the cathode and increases its work function, effectively reducing its ability to emit electrons. Also the material from the oxide cathode will

¹ evaporate during the tube's lifetime and will travel to other parts of the tube, adsorbing
² to electron optics parts and turning them into additional emitters. The literature
³ (also from [Whitaker]) therefore also advises against exceeding the design value for
⁴ the heater voltage, as this reduces the lifetime of the cathode significantly. (However
⁵ during the course of our project, we did drive the cathode with higher heater voltages
⁶ on various occasions in order to increase the available beam current.)

⁷ 1.2.2 Cathode Layout

⁸ Figure 1.5 shows how metal oxide cathodes for CRTs typically look, the depiction agrees
⁹ very well with the layout of our cathode. On the image we see the cathode cylinder,
¹⁰ which corresponds to the nickel support structure mentioned above. It is shaped into a
¹¹ cup, i.e. the cylinder is hollow and open on one side, where the heater filament (shaped
¹² into a heater coil) is inserted. The oxide disk, from where the electrons are emitted,
¹³ is baked onto the top of the cathode cylinder. The cathode cylinder is mounted on
¹⁴ an isolating support structure and inserted into the Wehnelt cylinder, which is called
¹⁵ "grid cup" in the drawing.

1 Cathodic Ray Tube Basics

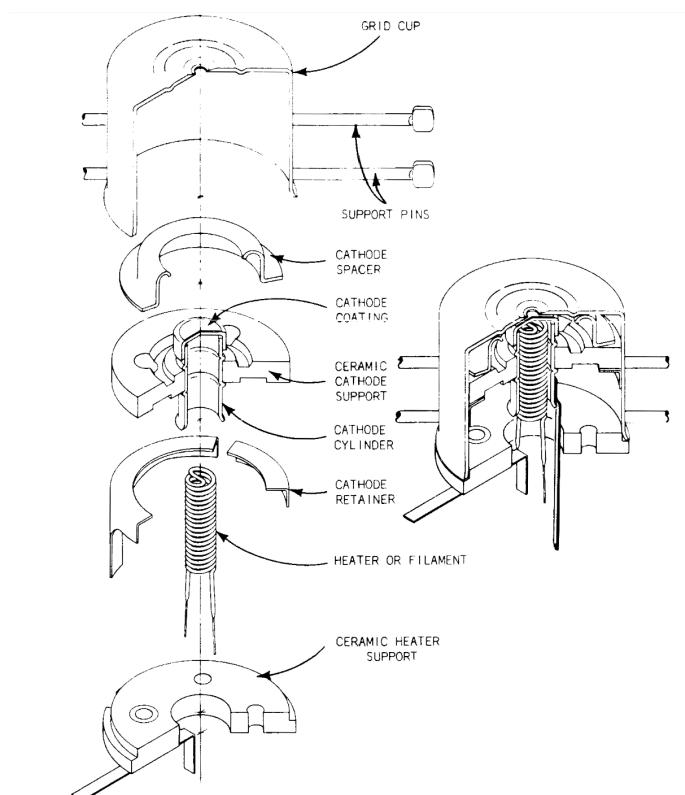


Figure 1.5: Schematic of the layout of a typical CRT-cathode from [deVere69]

¹ 2 Cicero Word Generator

² This chapter describes the installation and initial setup of Cicero Word Generator[**keshet2013distribution**]
³ on a PC running Windows 10 with analog and digital cards from National Instruments
⁴ (NI). The code is freely available on Github[**akeshet:Github**]. This chapter contains
⁵ only differences, problems, and possible solutions encountered when Cicero was installed
⁶ for the PC ‘Fritz Fantom’ which will be used for the QuaK experiment. It is therefore
⁷ advised to use the technical and user manual[**akeshet:manual**] in conjunction. The
⁸ titles in this chapter and font style with Courier and Boldface was mirrored to fit
⁹ the manual.

¹⁰ 2.1 Installation of National Instruments drivers

¹¹ Before setting up the Cicero Word Generator, it is necessary to install the newest .NET
¹² Framework[**microsoft:download.net**] from Microsoft. For the first installation of NI
¹³ drivers, NI-DAQmx (version 9.3), NI-VISA (newest version), and NI-4888.2 (newest
¹⁴ version) should be downloaded from the National Instruments website[**ni:drivers**].
¹⁵ When installing the NI drivers it is possible to get an ‘Runtime Error!’. In this case it
¹⁶ is necessary to set the Regional format settings of Windows 10 to ‘English (United
¹⁷ States)’[**ni:runtimerror**].

¹⁸ 2.2 Installation of National Instruments Cards

¹⁹ After installation of the necessary drivers, the physical cards can be inserted into the
²⁰ PCIe slots on the motherboard. On ‘Fritz Fantom’ the digital card (NI PCIe-6537B)
²¹ was installed in PCIe bus 3 while the analog cards (NI PCIe-6738) were installed in
²² PCIe bus 4 and 5.

2.3 Configuring Atticus

After installation of the NI cards, Atticus should be launched for the first time and closed without changing any settings. After this, the NI-DAQmx drivers should be updated to the newest version. If version 9.3 was not used when launching Atticus in this step, it could result in an error. After this, “Configuring Atticus” on the user manual can be followed. The **Server Name** was set to ‘Fritz_Phantom’. **Dev1** to **Dev3** were set in the same ascending order as the physical installation on the motherboard.

2.3.1 Configure hardware timing / synchronization

For synchronization, a **Shared Sample Clock** was used with **Dev1** being the master card. The settings are summarized in table 2.1 and table 2.2. For **Dev3** ‘SampleClockExternalSource’ should be set to ‘/Dev3/RTSI7’. The ‘SampleClockRate’ is set to 350 kHz since this is the fastest rate with all 32 analog channels active. It is possible to raise this to 1 MHz by only using 8 channels (1 channel per bank).

Table 2.1: Settings for **Dev1**.

Setting	Value
MasterTimebaseSource	
MySampleClockSource	DerivedFromMaster
SampleClockRate	350000
UsingVariabletimebase	False
SoftTriggerLast	True
StartTriggerType	SoftwareTrigger

Table 2.2: Settings for **Dev2**.

Setting	Value
MasterTimebaseSource	
MySampleClockSource	External
SampleClockExternalSource	/Dev2/RTSI7
SampleClockRate	350000
UsingVariabletimebase	False
SoftTriggerLast	False
StartTriggerType	SoftwareTrigger

1 2.4 Configuration and Basic Usage of Cicero

2 After setting up the Atticus server, Cicero can be configured. In step 3.c. it is necessary
3 to write the full IP address and not ‘localhost’. Once step 6 is finished, Cicero should
4 run without any problems.

5 2.5 Saving of Settings and Sequences

6 The ‘SettingsData’ of the Server Atticus are saved in C:\Users\confetti\Documents
7 \Cicero_Atticus\Cicero\SettingsData while the ‘SequenceData’ of Cicero are saved in
8 C:\Users\confetti\Documents\Cicero_Atticus\Cicero\SequenceData.

9 2.6 Sequence length limit

10 The duration of a sequence is limited to $2^{32}/(16 * 32 * 350 \text{ kHz}) = 23.967 \text{ s}$ coming
11 from a 32-bit application, 16 bit per channel, 32 channels in a NI PCIe-6738 card, and
12 350 kHz clock rate.

3 Electron beam setup

1

3.1 Charatarization of a working CRT

2

HAMEG HM507 oscilloscopes [HM507-manual] were used for testing purposes. These contain a D14-363GY/123[D14363GY123-manual] CRT hereinafter abbreviated as 'D14', 'tube', or 'CRT'. Although the HM507 has only a bandwidth of 0 MHz to 50 MHz, which is not sufficient for the hyperfine splitting frequency of 461.7 MHz of ^{39}K , it was used nevertheless because of its simple construction and availability. A schematic view of the device is shown in fig. 3.1 with the back pin arrangement in fig. 3.2.

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The voltages and currents of the necessary pins to drive the CRT were measured using a 2.5 kV probe with an attenuation ratio of and are summarized in table 3.1. It was not possible to measure pin g3 directly. Therefore a HVPS (section 3.2) was used to set a voltage and the beam diameter was observed. The best focus was achieved with the voltage mentioned in the table. The voltage offset of x-, and y-plates was not possible to measure directly, since it varies with time to draw the necessary image on the phosphor screen. The given values in table 3.1 are the mean of the minimum and maximum measured voltage. The deflection coefficient is summarized in table 3.2.

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10model number

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3 Electron beam setup

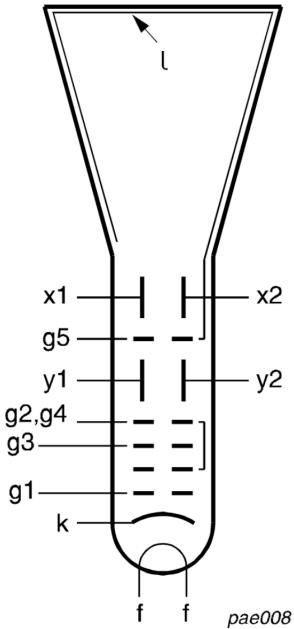


Figure 3.1: Electrode configuration (from [D14363GY123-manual])

how to cite figure

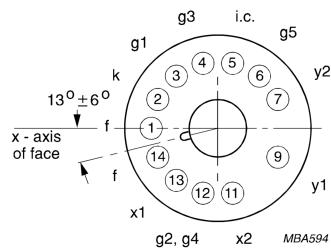


Figure 3.2: Pin arrangement, bottom view (from [D14363GY123-manual])

how to cite figure

3 Electron beam setup

Table 3.1: D14-363GY/123 CRT pin measurements

current empty or '-' symbol

number	pin	voltage/V	current/ μ A
1	f	-1.99×10^3	86.6×10^3
2	k	-2.00	-7.6
3	g1	-2.03	0
4	g3	-1.813×10^3	
5	i.c.	71.7	0.1
6	g5	64.0	7.2
7	y2	78	
9	y1	78	
11	x2	96	-
12	g2, g4	71.0	0
13	x1	96	-
14	f	-1.97×10^3	-86.2×10^3

Table 3.2: D14-363GY/123 deflection coefficient (from [D14363GY123-manual])

how to cite source

horizontal	M_x	19 V/cm
vertical	M_y	11.5 V/cm

¹ 3.2 High Voltage Power Supply HVPS

² To produce high dc voltages to drive the CRT, four HCP 14-6500 power supplies [fug-hcp-manual]
³ were used. They were named ‘HVPS 1’ to ‘HVPS 4’ and can provide up to ± 6.5 kV and
⁴ 2 mA. To connect the output to the CRT pins, BNC cables were refitted with a save
⁵ high voltage (SHV) connector on one side while on the other end the BNC connector
⁶ was kept (fig. 3.3). A 6 kV probe was used to obtain the breakdown voltage, which is
⁷ around 3 kV caused by the coaxial cable which was not built to sustain high voltages.

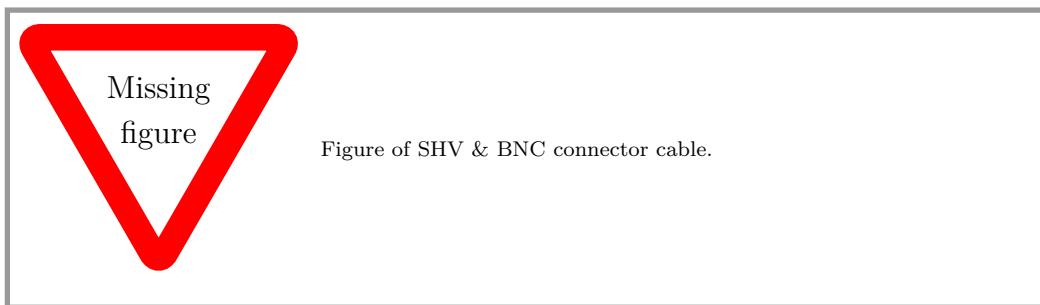


Figure 3.3: Coaxial cable with SHV and BNC connector.

⁸ 3.2.1 Ripple measurement

⁹ Each power supply was measured for its ripple with a set voltage of 2 kV. A 2.5 kV
¹⁰ probe (attenuation ratio)was connected to an oscilloscope set to ac coupling with a
¹¹ timescale of 1 ms. To get the electronic noise of the oscilloscope itself, the probe was
¹² shorted and the noise measured. A picture of a measurement is shown in fig. 3.4 with
¹³ the values summarized in table 3.3.

find name of bi
yellow probe

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find exact value

100:1 or 1:100

Table 3.3: HVPS ripple

device	ripple/mV
short	116
HVPS 1	136
HVPS 2	138
HVPS 3	194
HVPS 4	204

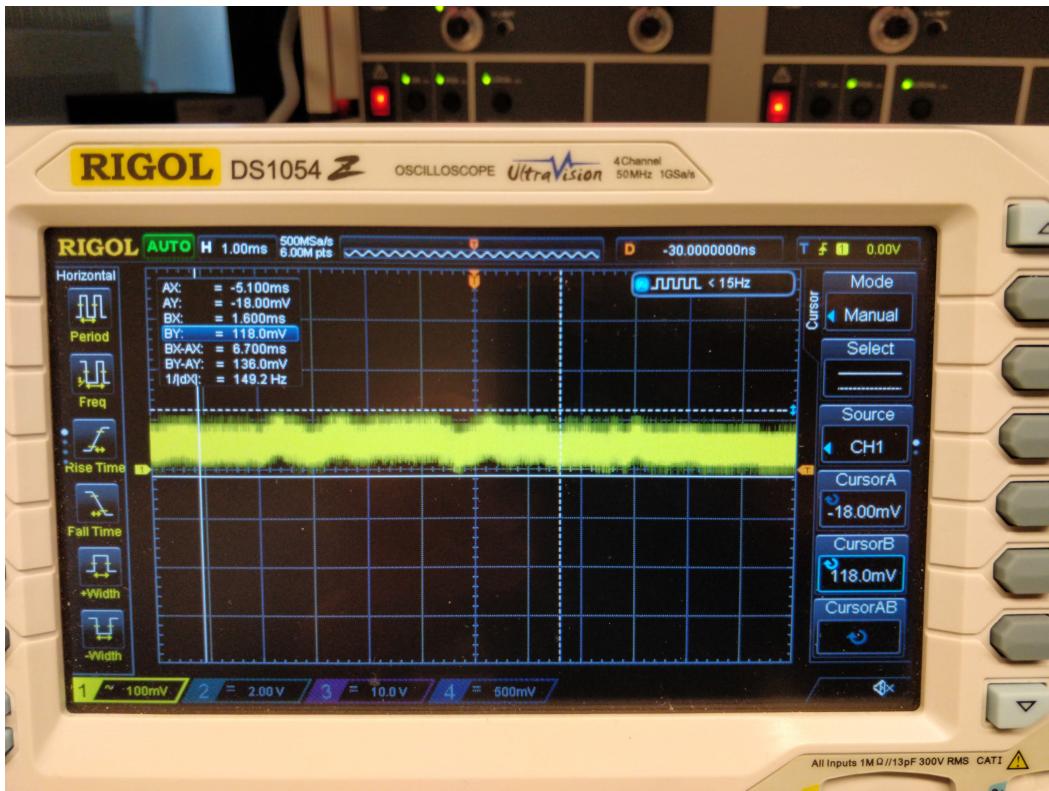


Figure 3.4: Measurement of HVPS ripple.

3.3 CRT wiring

A schematic of the supplied power is shown in fig. 3.5. A small ac or dc voltage is necessary to drive the heater filament f. This part of the setup is explained in section 3.4.

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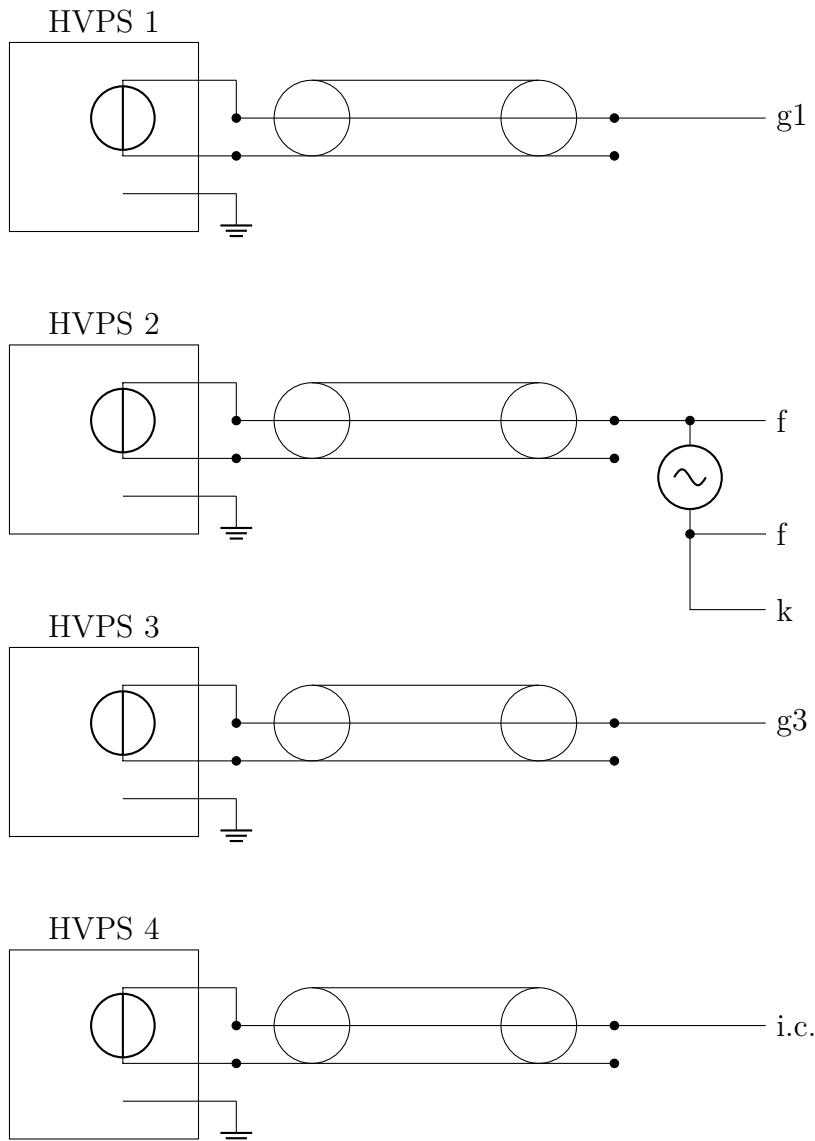


Figure 3.5: Schematics of supplying CRT pins with power.

¹ 3.4 Heater

- ² The heater provides an adjustable ac voltage, which is used to regulate the temperature
³ of the cathode. In the cold state, the heater filament has a an electrical resistitance
⁴ of approximately 15Ω , when the filament is hot, this value rises to 90Ω . The normal
⁵ heater voltage for the D14-363GY/123 during operation is 6.0 V to 6.6 V according to
⁶ [[D14363GY123-manual](#)]. Our ac-power supply (figure 3.6 shows its circuit diagram)

3 Electron beam setup

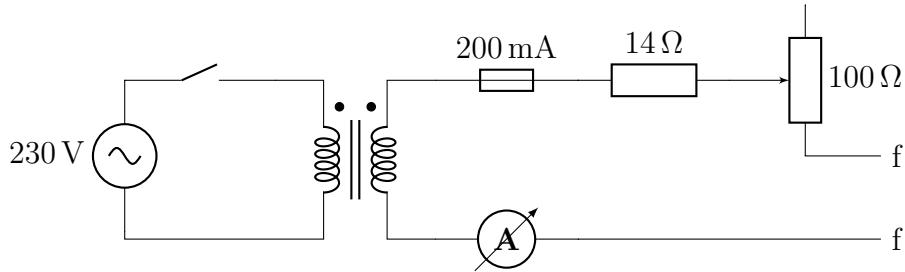


Figure 3.6: Circuit diagram of filament power supply.

check if really 14Ω or if it even exists

consists of an isolation transformer (from grid voltage to 12 V), its primary and secondary circuits are isolated up to 4 kV [DS44231-DataSheet]. The power supply has two banana plug sockets to connect to the heater filament. It is connected to the transformer in series with a 100Ω potentiometer. Using the full resistance, there is a voltage of approximately 5.7 V applied to the heater filament, by lowering the resistance this value can go up to nearly the full voltage of the transformer. The current running through the filament is measured with an integrated amperemeter [ACA-20PC-manual] that measures currents up to two 2 A with mA accuracy.

At the beginning of operation it is recommendable to set the maximum resistance and slowly increase the current to the desired value once the filament is heated up. As the resistance of the cold filament is significantly lower, high onset currents could otherwise damage it.

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¹ 4 CRT handling

² 4.1 Opening CRTs

³ In order to hit the ^{39}K cloud with an electron beam, it is necessary to cut open the
⁴ CRT. This section explains the different methods which were tried and which resulted
⁵ in clean and easy cuts. All slices were made in a glove box filled with nitrogen gas
⁶ (fig. 4.1) to avoid oxygen poisoning of the cathode.

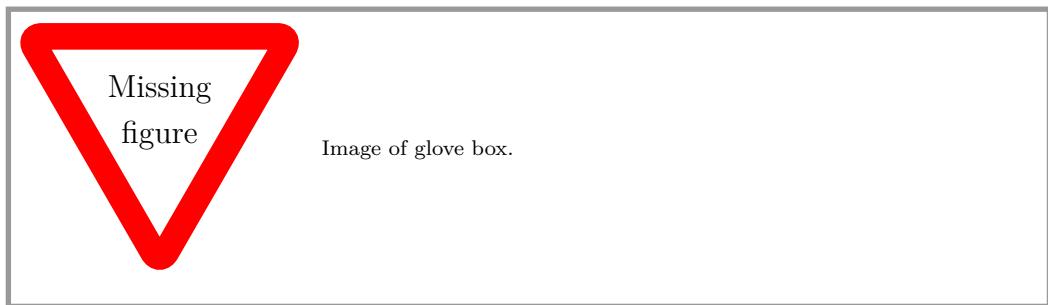


Figure 4.1: Glovebox filled with nitrogen gas to open CRTs.

⁷ 4.1.1 Rotary tool

⁸ First, a small hole was drilled in the center of the CRT pins to pressurize the CRT
⁹ with nitrogen. Then a diamond wheel attached to a rotary tool was used to cut the
¹⁰ glass. This method was tried twice, but did not work well, as the method produced a
¹¹ lot of glass dust, which adhered to the electron optics. Another obstacle is the plastic
¹² box, since it is not fully transparent and therefore made more difficult to see inside.

¹³ 4.1.2 Wire cutting

¹⁴ Higher success was achieved by cutting the glass with a heated wire. Two wires were
¹⁵ put through the glove box, each ending in a ring terminal. A small height adjustable
¹⁶ stage was built out of optical table parts (fig. 4.2) in which the CRT was put vertically

and looped by an 0.25 mm steel wire (Fe 70/Cr 25/Al 5). It is important to keep a small gap in the loop to avoid an electrical short. Therefore two notches were made in which the wire was fixed.

The assembly was put inside the glove box which was subsequently filled with nitrogen. A current of approximately 2 A to 2.5 A was used to heat the thin wire which resulted in a breaking point inside the CRT glass. This method does not require a CRT pressurization before the cut. In order to not destroy a device by mistake, this procedure can first be tested on drinking glasses.

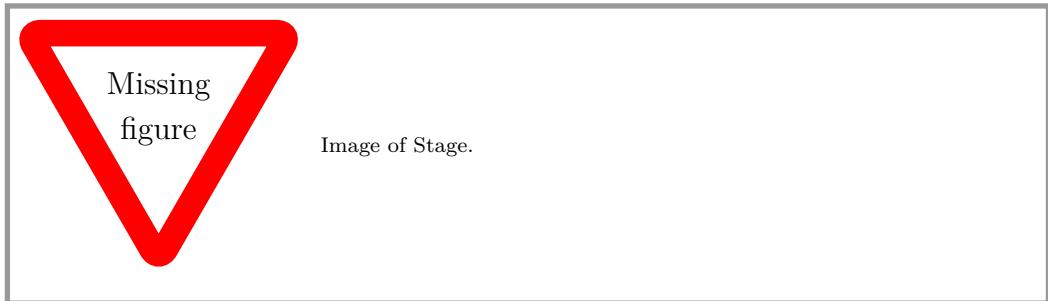


Figure 4.2: Stage to cut CRT with wire.

4.2 Oxygen poisoning

As mentioned in it is paramount to avoid contact of the cathode with oxygen. Therefore tests with a broken CRT were made to test on how well it can be isolated from air.

The first experiment consisted of filling a drinking glass put upside-down with helium and putting a lighter after a set amount of time. If the fire goes off, it means that oxygen did not get inside. This was tested successfully from 0.5 min to 10 min.

Next, plastic wrap was put on top of the glass filled with nitrogen by a rubber band. The glass was put with the open side up from 3 min to 10 min after which it was turned upside down and the foil was removed. A lighter was put inside and the flame went out again.

To improve the sensitivity, a He leak tester was used. For the first two tests, one plastic foil and one rubber band were used, for the third test three foils and two rubber bands, and for the last test an aluminum foil was hot glued on the CRT to seal it. The measurement locations are shown in fig. 4.3. As shown in table 4.1 using rubber band and clear foil results in the highest leakage while the glue seals much better (glue avg). But care needs to be taken in order ensure that the whole CRT is sealed since even a

4 CRT handling

- ¹ small leak can result in a rate around an order of magnitude above the background
- ² (glue max).

Table 4.1: He leak test.

location	leak rate/(10 ⁻⁵ mbar l/s)
1 plastic foil, 1 rubber band	
background	8
plastic foil	20
He gas cylinder	200
1 plastic foil, 1 rubber band	
background	7
plastic foil	20
rubber band	40
3 foils, 2 rubber bands	
background	20
plastic foil	30
rubber band	70
1 aluminum foil, hot glue	
background	6
glue avg	7
glue max	60
aluminum foil	8

4 CRT handling



(a) plastic foil



(b) rubber band



(c) glue



(d) aluminum

Figure 4.3: Measurement locations of He leakage.

¹ 5 Vacuum test chamber

² ignore from here

³ 2020-08-30 leak rate 2020-09-27 set voltages 2020-09-30 first successful external run

⁴ 2020-10-07 spot vs pressure 2020-10-22 current measurement aluminum foil 2020-11-05

⁵ forgot to turn off filament heating 2020-11-14 assemble chamber with copper rings

⁶ to here

⁷ In order to be able to fit the CRT screen, CF160 flanges were chosen for the test
⁸ chamber. At one point during testing, major changes were made which will be explained
⁹ in section 5.2.

¹⁰ 5.1 First iteration

¹¹ A 3D render of the chamber is shown in (fig. 5.1). Without a CRT installed, it
¹² was possible to reach a pressure of 6.8×10^{-7} mbar, while with one the lowest was
¹³ 2.0×10^{-6} mbar.

¹⁴ 5.1.1 Parts

¹⁵ The center piece consists of a 6-way cross with view ports at the front and bottom.
¹⁶ A valve was installed at the back in order to flood the chamber with nitrogen when
¹⁷ installing a new CRT to avoid oxygen poisoning. On the right side, a HiCube 300 Eco
¹⁸ turbo pump was installed and on the left side a wobble stick was attached with a wire.
¹⁹ A nipple fitting was installed at the top with a 5 port cluster flange, each being of length
²⁰ type CF63.

²¹ In the middle port, a VSH vacuum transducer was installed to measure pressure.
²² This needs a 24 V dc power supply. On the left, a 19 pin connector was installed to
²³ supply the necessary voltages to the CRT. Two flanges were equipped with four BNC
²⁴ feedthroughs each. One of them was used to connect do the x-, and y-plates, while the
²⁵ other connected to the wobble stick and aluminum foil at the CRT screen. Further
²⁶ explanation will be given in . The last port was capped off by a blank flange.
ref ch:Beam ch
terization, incl
picture there

5 Vacuum test chamber

For the inside wires, stranded copper cables were used. The chamber was sealed by
1
rubber gaskets.
2



Figure 5.1: 3D rendering of test chamber.

5.1.2 CRT mounting mechanism

Two M8 rods of length ~~were drilled into the cluster flange. On each, a L-piece was~~ rod length?
5
6
installed between two nuts and they were connected by a hose clamp. Two of these
were used to secure the CRT inside the nipple facing the cross (fig. 5.2).
7

5.1.3 Leak test

Before inserting a CRT, a leak test was performed. First, the chamber was set to a
8
pressure of 10^{-5} mbar after which the pump was turned off. The pressure was measured
9
once a minute for a duration 3 h. This is shown in fig. 5.3.
10

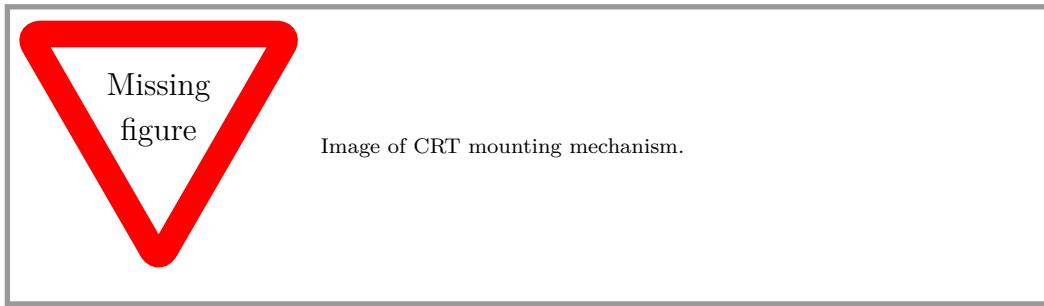


Figure 5.2: Image of CRT mounting mechanism.

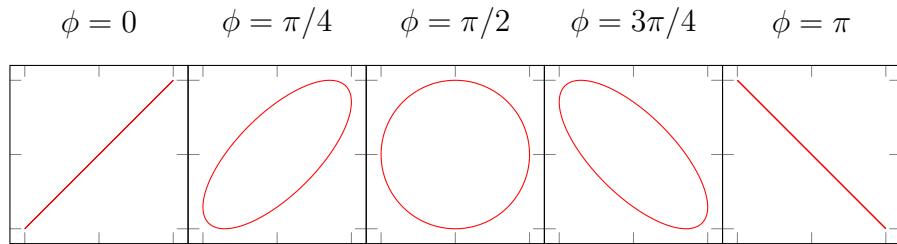


Figure 5.3: Leak rate of test chamber after turning off pump.

¹ 5.2 Second iteration

² At one point during experimentation, major changes were made to the chamber. Thanks
³ to these, it was possible to reach a pressure of 1.2×10^{-7} mbar.

⁴ 5.2.1 Changes

⁵ First, every rubber gasket was changed to a copper one for a better seal, except at the
⁶ cluster flange, since that spot will be opened and closed the most often. Each copper
⁷ stranded cable inside was switched to a coaxial one and the mantle was connected
⁸ to the chamber wall, which was set to ground. A Faraday cup was installed below
⁹ the wobble stick, to accurately measure the beam current (further details in). The
¹⁰ aluminum foil was extended to cover all four sides of the screen.

ref ch:Beam characterization

¹¹ 5.2.2 Fastening

¹² When attaching flanges, it is important to start with a low torque and to fasten
¹³ opposite screws to prevent too much force on one side of the gasket. For M6 screws, the
¹⁴ torque was incrementally set to 6 N m, 10 N m, 15 N m and 20 N m and for M8 screws

5 Vacuum test chamber

8 N m, 16 N m and 25 N m. After finishing every opposite screw pair at a set torque,
the procedure was repeated twice before going to a higher torque. This was done in
order guarantee a tight and even seal.

1
2
3

¹ 6 Deflection Electronics

² 6.1 Demands on the setup

³ For the QuaK experiment it is paramount to be able to deflect the beam precisely
⁴ and with the right frequency. As previously mentioned, our deflection system simply
⁵ consists of two pairs of parallel plates between which a voltage is applied. Controlling
⁶ this voltage allows us to control the deflection of the beam. Various aspects are
⁷ important here (illustrated in fig. 6.1):

Optional: insert
Foto of CRT's
flection plates -
fig:DeflectionSe

⁸ **Offset:** Although the deflection of the beam is controlled by the voltage between the
⁹ plates, it is necessary to be able to set their mean potential as well. During
¹⁰ normal operation this offset voltage is at 96 V for the x-direction and at 78 V for
¹¹ the y-direction.

¹² **Amplitude:** The deflection coefficients in the x and y planes are 19 V cm^{-1} and
¹³ 11.5 V cm^{-1} respectively (see [D14363GY123-manual]). We therefore need
¹⁴ to be able to supply approximately 70 V.

¹⁵ **Frequency:** The final goal is to be able to deflect the beam at the hyperfine splitting
¹⁶ frequency of ^{39}K , which is 461.7 MHz. This is likely to prove impossible with this
¹⁷ CRT-model, observations at the highest frequency we have tried so far will be
¹⁸ discussed in section (Missing).

¹⁹ **Waveform:** Ultimately we want the cold atoms to experience a field that oscillates like
²⁰ a sine wave. As a first try it is therefore reasonable to apply a sinusoidal voltage.

Insert Reference
last section

²¹ **Lissajous curves:** Having the ability to control the deflection in both the x- and the
²² y- axis, allows us to have our beam draw out Lissajous Curves (fig. 6.2). By
²³ applying sine waves of equal frequency to both pairs of deflection plates and by
²⁴ being able to control the phase between them we can have the beam oscillate on
²⁵ a straight line or a circle. This allows us to generate either a linearly or circularly
²⁶ polarized field.

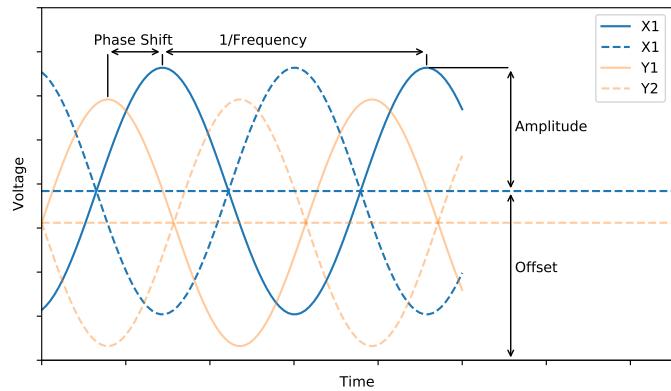


Figure 6.1

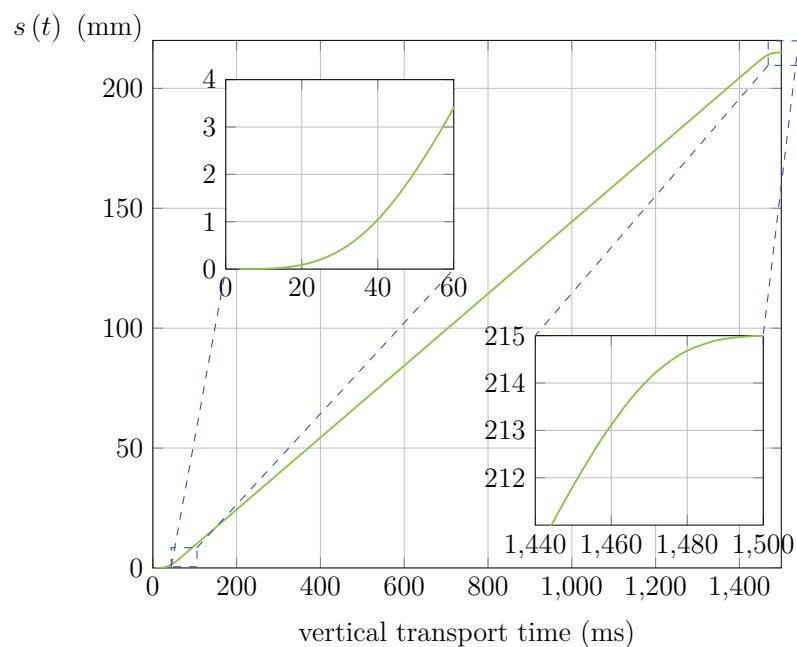


Figure 6.2: Lissajous Curves

¹ 6.2 Implementation

² A first setup with which we can try to obtain the desired voltages is depicted in
³ fig. 6.3. On the very left we have a signal generator that is capable of producing the
⁴ right frequency (461.7 MHz) this signal is then split up into an x-, and a y-branch.
⁵ One of the two branches is connected to a phase shifter, which is able to delay the
⁶ input signal by up to 200°, allowing us to set any desired phase shift between x-, and
⁷ y-deflection and to correct for inadvertent delays from the other electronics. Both the
⁸ x-, and y-signal are then amplified using (amplifier) . In the final step, a center tapped
⁹ transformer allows us to produce voltages for the plates X1 and X2 (or Y1 and Y2
¹⁰ respectively) with a phase shift of exactly 180° between them. By setting the center
¹¹ tap to the desired offset potential, we should get the voltage curves described above.
¹² To understand this setup in more detail, it is useful to examine its most important
¹³ parts more closely:

¹⁴ **Amplifier:** Up to now we have used the XXX and the YYY amplifier, they amplify
¹⁵ the signal by a fixed gain of (How much?) , inputs and outputs can simply be
¹⁶ connected via BNC cables, the amplifier is powered by a linear power supply
¹⁷ with a DC voltage of 24 V via two banana plugs in the front. Since we want to
¹⁸ control the Lissajous curves shapes (as the deflection coefficients for the x- and
¹⁹ y- plates differ), it is desirable to be able to adjust the amplifier gain in future
²⁰ versions of the setup.

²¹ **Center Tapped Transformer:** The center tapped transformer we use is the Mini-
²² Circuits TC8-1G2+ ([TC8-1G2]), a transformer for frequencies between 2 MHz
²³ to 500 MHz, with an impedance ratio of 8. Figure 6.6 shows how the center
²⁴ tapped transformer is implemented. The in- and outputs, as well as the bias
²⁵ voltage can be connected via BNC cables. As usual, the shields of all these cables
²⁶ are connected to ground, furthermore they are connected to each other and to
²⁷ the housing. As a safety feature, both outputs X1 and X2 are directly connected
²⁸ to the bias through an arrangement of diodes: Two connections, each with a
²⁹ normal diode and a Zener diode facing in opposite directions. The breakthrough
³⁰ voltage of the Zener diode is 200 V, during normal operation the voltage on it
³¹ stays below this value and none of the connections let any current through as
³² one of the two diodes is always blocking it. However if one of the plates in the
³³ CRT accidentally comes in contact with high voltage, the connection with the
³⁴ appropriately oriented Zener diode opens up, preventing a voltage spike on the
³⁵ center tapped transformer and thereby protecting the electronics connected to
³⁶ its primary circuit.

³⁷ At the point of writing there are still some problems with the behavior of the
³⁸ center tapped transformer, the capacitance of the diodes introduces an undesired

Find out which
amplifier

which model?

which model?

Check amplifier
specifications

Optional: Go to
lab and measure
their performance
with an Oszil.

I don't really know
whether a high
resistance bias or
low resistance bias
is better.

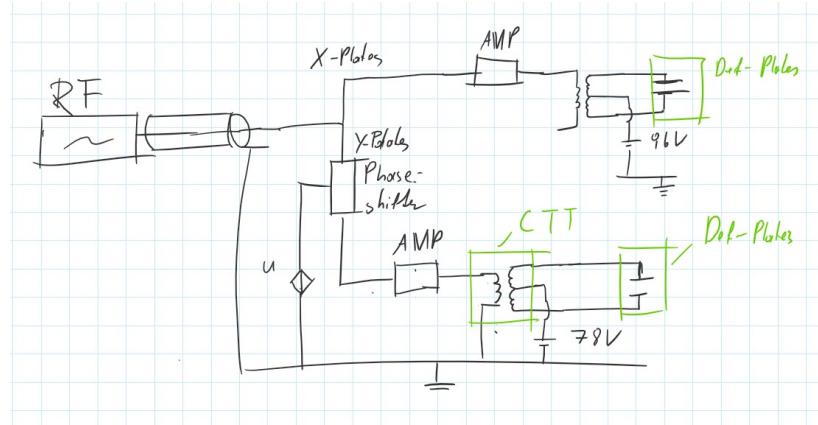


Figure 6.3: Deflection circuit

phase shift between the two signals. Figure 6.5a shows the circuit's behavior at 465 MHz without its diodes, here the signals are shifted by $120 \text{ ps} \hat{=} 20^\circ = 0.35 \text{ rad}$. Additionally, applying a bias voltage leads to differing amplitudes, as can be seen in fig. 6.5b.

Phase Shifter: To control the phase shift between the x- and y-deflection plates, we use a Mini-Circuits [JSPHS-661] phase shifter. This part was put in a housing ([Hammond1455D601RD]) on a separate PCB and can be connected via BNC cables. Figure 6.4a shows how the phase shifter is connected and fig. 6.4b shows the corresponding PCB layout. Note that again the shields of the BNC cables are connected among each other and to the housing. The JSPHS-661+ is designed for frequencies in the range 400 MHz to 600 MHz. By applying a DC voltage of 0 V to 12 V to the bias connector, it is possible to introduce a phase shift of up to 200° to the signal.

(figure) _____
 (Performance) _____

- 1
- 2
- 3
- 4
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- 12
- 13

14 Insert fotos of finished circuits in housings
 15

Optional: Go to the Lab, set the whole thing up, look at its performance on the scope

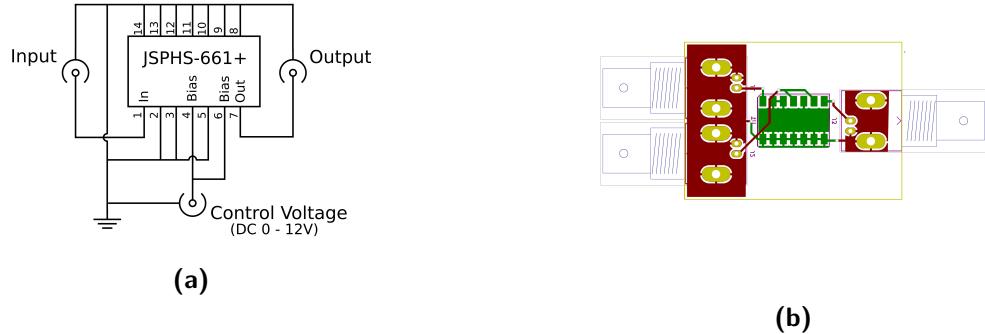
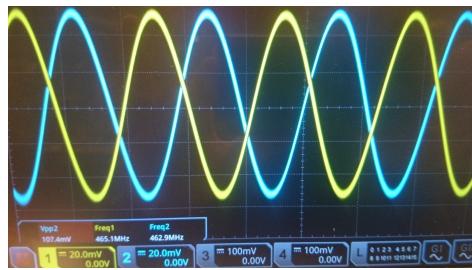


Figure 6.4



(a) Signal of center tapped transformer without diodes, unbiased at 465 MHz



(b) Signal of center tapped transformer without diodes, biased at 465 MHz

Figure 6.5

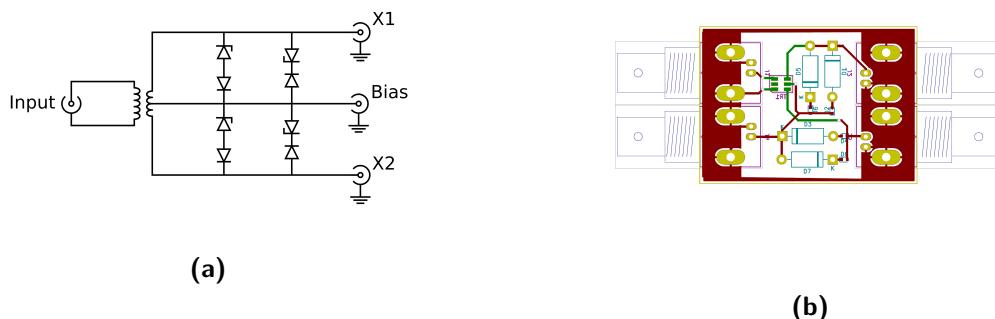


Figure 6.6

Todo list

1

■ können die Maße stimmen?	3	2
Figure: Image of CRT	5	3
■ namechange?	10	4
■ http://www.tobiastiecke.nl/archive/PotassiumProperties.pdf	12	5
■ model number	12	6
■ 1:100 or 100:1	12	7
■ current?	12	8
■ how to cite figure	13	9
■ how to cite figure	13	10
■ current empty or '-' symbol	14	11
■ how to cite source	14	12
■ find name of big yellow probe	15	13
■ somewhere 2.5-4, find exact value	15	14
Figure: Figure of SHV & BNC connector cable.	15	15
■ 100:1 or 1:100	15	16
■ check if really 14Ω or if it event exists	18	17
Figure: Image of glove box.	19	18
Figure: Image of Stage.	20	19
■ where ?	20	20
■ pure nitrogen name?	23	21
■ length	23	22
■ how many pins and model name?	23	23
■ ref ch:Beam characterization, include picture there	23	24

¹	rod length?	24
²	Figure: Image of CRT mounting mechanism.	25
³	ref ch:Beam characterization	25
⁴	Optional: insert Foto of CRT's deflection plates - fig:DeflectionSetup	27
⁵	Insert Reference to last section	27
⁶	Find out which amplifier	29
⁷	which model?	29
⁸	which model?	29
⁹	Check amplifier specifications	29
¹⁰	Optional: Go to the lab and measure their performance with an Oszi.	29
¹¹	I don't really know whether a high resistance bias or a low resistance bias is better.	29
¹³	Optional: Go back to the Lab and fix the problem with the diodes?	30
¹⁴	Insert fotos of finished circuits in housings	30
¹⁵	Optional: Go back to the Lab, set up the whole thing and look at its performance on the oszi	30
¹⁶		