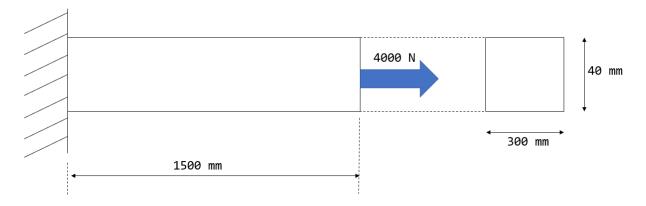
## 1D Bar Finite Element Method (FEM) Analysis

- This project contains Python code for performing Finite Element Method (FEM) analysis on 1D bar elements with Non-Linear Constitutive Behaviour.
- The code includes implementations for Static Non-Linear for problems with Linear and Non-Linear Constitutive Behaviour.
- When Non-Linear FEM code is used to solve Linear Problem, the solution is obtained in 2 iterations only.
- For a regular Non-Linear Problem, the solution is obtained in multiple steps.
- The Non-Linearity effect can be observed only if, the  $E_0$  is small or F is large.

## 1D Bar Static Analysis Problem



The Non-Linearity considered,

$$\sigma(\varepsilon) = E_0 \; \varepsilon + E_1 \; \varepsilon^3$$

The strong form equation of 1D bar can be written as,

$$A\frac{d}{dx}(\hat{\sigma}(\varepsilon)) + b = 0, [0, l_e]$$

Were,

$$\varepsilon = \frac{du}{dx}$$

If no body forces are considered, b = 0

$$A\frac{d}{dx}(\hat{\sigma}(\varepsilon)) = 0, [0, l_e]$$

The boundary conditions are as described below:

$$u = 0,$$
  $x = 0$   
 $A\hat{\sigma}\left(\frac{du}{dx}\right) = F,$   $x = l_e$ 

The equation can be converted into weak form by multiplying with a weight function and integrating over the entire domain as,

$$A\int_0^l \frac{d}{dx}(\hat{\sigma}(\varepsilon))wdx = 0$$

Integrating by parts,

$$A \int_0^l \frac{d}{dx} (\hat{\sigma}(\varepsilon)) \frac{dw}{dx} dx = Pw(l)$$

Now, given  $\hat{\sigma}(\varepsilon)$  is a non-linear function in  $\varepsilon$ , it should be linearized to obtain the solution. To linearize, Newton Raphson method is used where  $u^{k+1}=u^k+\Delta u^k$  is considered and using Taylor series expansion

$$\widehat{\sigma}\left(\frac{du^{k+1}}{dx}\right) = \widehat{\sigma}\left(\frac{d(u^k + \Delta u^k)}{dx}\right) = \widehat{\sigma}\left(\frac{d(u^k)}{dx}\right) + \widehat{\sigma}'\left(\frac{d(u^k)}{dx}\right) \frac{d\Delta u^k}{dx}$$

Now,

$$A \int_0^l \left( \hat{\sigma} \left( \frac{d(u^k)}{dx} \right) + \hat{\sigma}' \left( \frac{d(u^k)}{dx} \right) \frac{d\Delta u^k}{dx} \right) \frac{dw}{dx} dx = Pw(l)$$

$$A \int_0^l \hat{\sigma}' \left( \frac{d(u^k)}{dx} \right) \frac{d\Delta u^k}{dx} \frac{dw}{dx} dx = Pw(l) - A \int_0^l \hat{\sigma} \left( \frac{d(u^k)}{dx} \right) \frac{dw}{dx} dx$$

The above equation is used to obtain  $\Delta u^k$  which is the in kth step and is added to  $u^k$  to get the displacement for the  $(k+1)^{th}$  iteration. This equation is solved till the residue which is the RHS of equation becomes less than a tolerance value. The value of  $\hat{\sigma}'$  and  $\hat{\sigma}$  are obtained based on the assumed Constitutive mode (in this case  $\sigma(\varepsilon) = E_0 \ \varepsilon + E_1 \ \varepsilon^3$ ) for each iteration.

According to FEA approximation, the values of displacements can be considered as sum of displacements at nodes multiplied by weight functions as shown below,

$$u^{k}(x) = \sum_{i=1}^{N} u_{i}^{k} \varphi_{i}(x) = \sum_{i} u_{i}^{k} \varphi_{i}(x)$$

$$w^{k}(x) = \sum_{j=1}^{N} \varphi_{j}(x) = \sum_{j} \varphi_{j}(x)$$

$$\Delta u^{k}(x) = \sum_{m=1}^{N} \Delta u_{m}^{k} \varphi_{m}(x) = \sum_{m} \Delta u_{m}^{k} \varphi_{m}(x)$$

Now the equation becomes,

$$A \int_0^l \widehat{\sigma}' \left( \frac{d(\sum_i u_i^k \varphi_i(x))}{dx} \right) \frac{d(\sum_m \Delta u_m^k \varphi_m(x))}{dx} \frac{d(\sum_j \varphi_j(x))}{dx} dx = P - A \int_0^l \widehat{\sigma} \left( \frac{d(\sum_i u_i^k \varphi_i(x))}{dx} \right) \frac{d(\sum_j \varphi_j(x))}{dx} dx$$

$$\left[ \sum_{m} \sum_{j} A \int_{0}^{l} \hat{\sigma}' \left( \sum_{i} \frac{d\varphi_{i}}{dx} u_{i}^{k} \right) \frac{d\varphi_{m}}{dx} \frac{d\varphi_{j}}{dx} dx \right] \left\{ \Delta u_{m}^{k} \right\} = \left\{ P \right\} - \left\{ \sum_{j} A \int_{0}^{l} \hat{\sigma} \left( \sum_{i} \frac{d\varphi_{i}}{dx} u_{i}^{k} \right) \frac{d\varphi_{j}}{dx} dx \right\}$$

Substituting the values of shape functions for each node, the equation simplifies to,

If i<N:

$$\begin{split} &A\left(\int_{X_{i-1}}^{X_{i}} \sigma'\left(\frac{u_{i}-u_{i-1}}{X_{i}-X_{i-1}}\right) \varphi'_{i} \varphi'_{i-1} dx\right) \Delta u_{i-1} + A\left(\int_{X_{i}}^{X_{i+1}} \sigma'\left(\frac{u_{i+1}-u_{i}}{X_{i+1}-X_{i}}\right) \varphi'_{i} \varphi'_{i+1} dx\right) \Delta u_{i+1} \\ &+ \left(A\int_{X_{i-1}}^{X_{i}} \sigma'\left(\frac{u_{i}-u_{i-1}}{X_{i}-X_{i-1}}\right) \varphi'_{i}^{2} dx + A\int_{X_{i}}^{X_{i+1}} \sigma'\left(\frac{u_{i+1}-u_{i}}{X_{i+1}-X_{i}}\right) \varphi'_{i}^{2} dx\right) \Delta u_{i} \\ &= -A\int_{X_{i-1}}^{X_{i}} \sigma\left(\frac{u_{i}-u_{i-1}}{X_{i}-X_{i-1}}\right) \varphi'_{i} dx - A\int_{X_{i}}^{X_{i}} \sigma\left(\frac{u_{i+1}-u_{i}}{X_{i+1}-X_{i}}\right) \varphi'_{i} dx + Fv_{i} \end{split}$$

If i=1 or i=N, i.e at the end points of the bar

These equations can be analytically solved, as  $\phi$  is a linear function of X. Solving it accordingly the equation simplifies to, where  $h_i = X_{i+1} - X_i$ 

$$\begin{split} &A\ \sigma'\left(\frac{u_{i}-u_{i-1}}{h_{i-1}}\right)\left(\frac{-1}{h_{i-1}}\right)\Delta u_{i-1} + A\ \sigma'\left(\frac{u_{i+1}-u_{i}}{h_{i}}\right)\left(\frac{-1}{h_{i}}\right)\Delta u_{i+1} \\ &+ A\ \sigma'\left(\frac{u_{i}-u_{i-1}}{h_{i-1}}\right)\left(\frac{1}{h_{i-1}}\right)\Delta u_{i} + A\ \sigma'\left(\frac{u_{i+1}-u_{i}}{h_{i}}\right)\left(\frac{1}{h_{i}}\right)\Delta u_{i} \\ &= A\ \sigma\left(\frac{u_{i}-u_{i-1}}{h_{i-1}}\right) + A\ \sigma\left(\frac{u_{i+1}-u_{i}}{h_{i}}\right) + Fv_{i} \end{split}$$