HWR

(Vm) plactical = Vm - V/r Ideal Practical

Bridge FWR (Vm) partial = Vm-2Vk I Practical Ideal

Corter Tay FWR Vm-Vk Practical Ideal

Vm Vdc  $\frac{V_{vn}-V_{k}}{V_{k}}$ Vams Vm Z  $\frac{V_m - V_k}{2}$  2 (Vm - 2Vk)

2(Vm - Vk)

Ide Im T Igms Im 2 7

Vm-2VK

Vm - Vk 2 Im In VZ Im V2

1.21 1.21 40.6% 40.6%

0.48 0.48 81.2% 81-27.

0.48 0.48 81.2% 81.2%

PIV >Vm > Vm fleg. 60= fi fo=f:

٦

>Vm

 $> V_m - V_k$ 

>2 Vm

 $>2V_m-V_k$ 

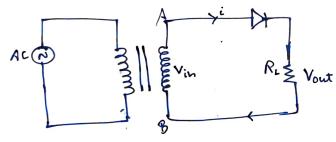
f.=2f:

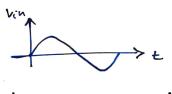
fo= 2fi

€0= 2fi

f = 2 f:

-> Half Wave Rectifies





\* VDC & Varg = 1 2T V dust

\* Vams = \[ \frac{1}{2\pi} \int \left( \n \text{sin wet} \right)^2 dwet \] 1/2

V = Vm sinust => Yde = I [ JVm Sin (wt) dwt]

= [Vm, ] (singt) + ] D] 1/2 = \[ \frac{\frac{1}{\sqrt{m}}}{2\pi} \int \frac{\left(1-\left{Est}2\left)}{2} \dust \] \[ \frac{1/2}{2} \]

= 1 [ Tym sin(wt) dust + [o dust]; = Vm (-cosut)

 $= \left[ \frac{v_m^2}{2\pi} \left( \frac{us^{\frac{1}{2}} - \underline{sin}^2 us^{\frac{1}{2}}}{2(2)} \right)_{x}^{T} \right]^{\frac{1}{2}}$ 

 $= \frac{V_m}{2\pi} \left[ -(-1) - (-1) \right] = \frac{V_m}{4\pi}$ 

$$= \left[\frac{V_{m}^{2}}{2\pi} \left(\frac{\pi}{2}\right)\right]^{1/2} = \frac{V_{m}}{2}$$

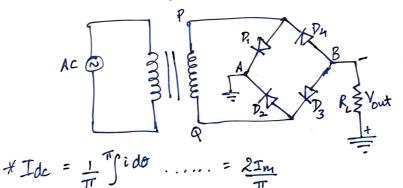
$$\frac{1}{4} = \frac{V_{\text{m}} \sin \theta}{4f + R_{\text{L}}} \qquad \frac{1}{4\pi} \int_{0}^{\infty} \sin \theta \, d\theta = \frac{V_{\text{m}} \left[\cos \theta\right]_{0}^{T}}{2\pi \left(4f + R_{\text{L}}\right)} = \frac{2 V_{\text{m}}}{2\pi \left(4f + R_{\text{L}}\right)} = \frac{1}{4\pi} \int_{0}^{\infty} \sin \theta \, d\theta$$

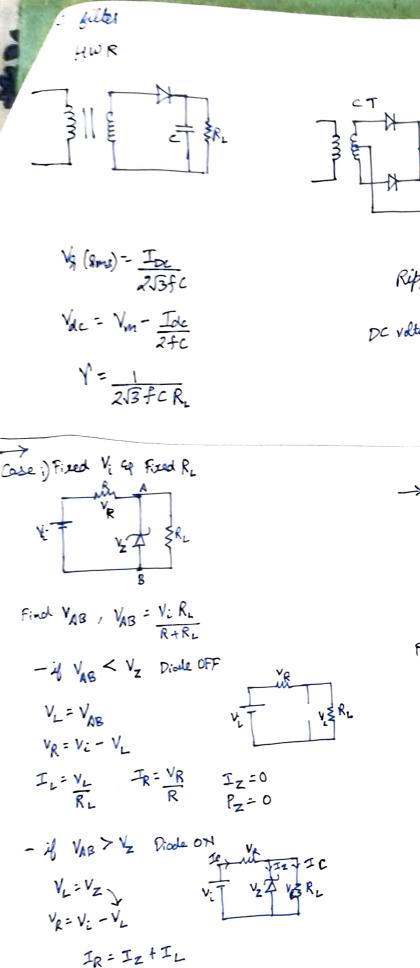
Idc= Im

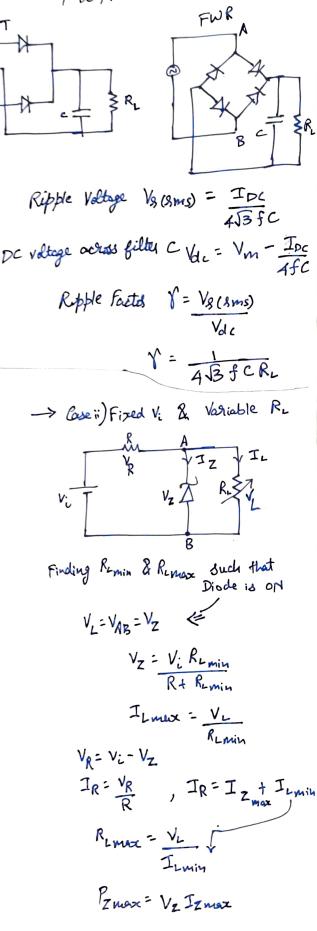
! Igms = Im

Power Sating = 0.7 Im

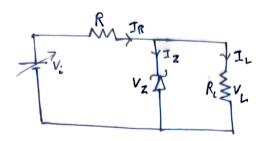
$$*$$
  $\gamma = \sqrt{\frac{Igms}{Tds}^2 - 1}$ 







-> Case iii) Variable Vi & Foxed RL



$$V_{AB} = V_{L} = V_{Z}$$

$$V_{Z} = \frac{V_{imin}R_{L}}{R + R_{L}}$$

$$I_{L} = \frac{V_{L}}{R_{L}} = \frac{V_{Z}}{R_{L}}$$

$$I_{R_{max}} = I_{Z_{max}} + I_{L}$$

$$V_{R} = V_{i} - V_{Z}$$

$$V_{i} = V_{R} + V_{Z}$$