

$$y = \frac{4\lambda}{3\pi}$$

$$\overline{2} = \overline{y} = \frac{49}{3\pi}$$

$$\bar{z} = \frac{2 \int \sin x}{x}$$

$$\overline{z} = \frac{a+b}{3}$$

$$\overline{y} = \frac{h}{3}$$

$$I_x = I_y = \frac{\pi g^4}{4}$$

$$I_z = \frac{\pi g^4}{2}$$

$$T_{x} = I_{y} = \frac{\pi \lambda^{4}}{8}$$

$$T_{z} = \left(\frac{\pi}{8} - \frac{8}{4\pi}\right) \lambda^{4} = 0.113^{4}$$

$$I_{z} = \frac{\pi \lambda^{4}}{4}$$

$$I_{z} = I_{y} = \frac{\pi \lambda^{4}}{16}$$

$$I_{x} = I_{y} = \left(\frac{\pi}{16} - \frac{4}{4\pi}\right) \lambda^{4}$$

$$I_{z} = \frac{\pi \lambda^{4}}{8}$$

$$I_{2} = \frac{6h^{3}}{3} \qquad I_{y} = \frac{hb^{3}}{3}$$

$$I_{z_{0}} = \overline{I}_{x} = \frac{6h^{3}}{12} \qquad \overline{I}_{y} = \frac{hb^{3}}{12}$$

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$$I_{z_{0}} = \frac{1}{12} \qquad \overline{I}_{y} = \frac{1}{12}$$

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$$T_{2} = \frac{bh^{3}}{12}$$

$$T_{1} = \frac{bh^{3}}{12}$$

$$T_{2} = \frac{bh^{3}}{36}$$

$$T_{3} = \frac{bh^{3}}{36}$$

$$T_{4} = \frac{hb^{3}}{36}$$

$$T_{5} = \frac{hb^{3}}{4}$$

AREA MOI: The area MOI is the second moment of area shound a given

Afrea MOI around x-axis Ix = fy2dA

Radius of Gyration: The imaginary distance from centroid at which the area of cross section is imagined to be focused at a point in order to obtain the same MOI It is denoted by k. Measure of distribution of orea from the ref. axis considered.

Transfer of axis: The MOI of an area about a non centroidal axis can be easily expressed in terms of MOI about a parallel centroidal oxis

In= Iz + 12

Conditions for 1 axis theorem:

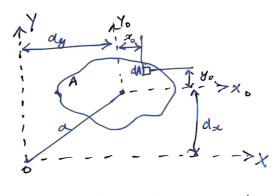
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1. Two axis should be there and must be 11 to each other 2. Between two axis, one axis has to pass through the centroidal axis.

Derivation of Parallel Dis Theorem By definition, the monsent of inertia of element dA about x-axis is

$$dI_{z} = (y_0 + d_z)^2 dA$$

$$I_{x=} \int y_0^2 dA + 2 dx \int y_0 dA + d_x^2 \int dA$$



fast integral is by definition of MOI Iz about centroidal xo-axis second integral = 0, since SyodA = Ayo & yo is automatically D with centroid on xo axis

$$I_{x} = \overline{I}_{x} + d_{x}^{2}(A)$$

$$I_{x} = \overline{I}_{x} + Ad_{x}^{2} + Ad_{x}^{2} = 0$$

$$I_{y}^{hy} = \overline{I}_{y} + Ad_{y}^{2} = 0$$

area of differential element dA = 211 An da,

$$I_{z} = \int 8^{2} dA$$

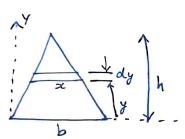
$$= \int 8^{2} 2\pi 8 dR_{0} = 2\pi \frac{94}{4} = \frac{\pi 9^{2}}{2} = \frac{A8^{2}}{2}$$

Polar Radius of gyration is
$$k = \sqrt{\frac{I}{A}}$$

By sumetry $I_x = I_y$

$$(I_z = I_z + I_y)$$
 \Rightarrow $I_x = \frac{1}{2}I_z = \frac{I_1\lambda^2}{4}$

q. Centroid of
$$\Delta$$



$$\frac{z}{b} = \frac{h-y}{h}$$

$$\frac{z}{b} = \frac{h-y}{h}$$

$$\overline{y} = \int_{A}^{y_c} dA$$

$$\int_{A}^{z} \int_{b}^{h} y \cdot b(h-y) dy$$

=
$$\frac{b}{hA} \int_{0}^{h} h - y^{2} dy = \frac{b}{h + 1} \int_{0}^{h} \frac{h^{2} - y^{3}}{h^{2}} \int_{0}^{h} \frac{b}{h^{2}} \int_{0}^{h} \frac{dh}{h^{2}} \int_{0}^{h}$$

$$= \frac{2}{h^2} \left[\frac{h^3 - h^3}{3} \right]$$

1= = bh

dA = x dy

aA = b(h-y)dy

area & differential element

$$=\frac{2}{h^2}\frac{h^3}{6}-\frac{h}{3/2}$$

$$Kz = \frac{8}{\sqrt{2}}$$

Q- MOI of
$$\Delta$$

$$A = x dy$$

$$A = b(h-y)dy$$

$$A = b(h-y)dy$$

$$= \int_{0}^{h} \int_{0}^{y^{2}} \frac{b(h-y)}{h} dy$$

$$= \frac{b}{h} \int_{0}^{h} y^{2}h - y^{3}$$

$$= \frac{b}{h} \left[\frac{y^3}{3} \left(h \right) - \frac{y^4}{4} \right]_0^h$$

$$\frac{1}{12h/3} = \frac{b}{h} \frac{h^4}{12} = \frac{b}{12} \frac{h^3}{12}$$

Ix=Ix-Ad2

$$I_{x} = I_{x} - Ad^{2}$$
 $= \frac{bh^{3}}{12} - \frac{bh}{18}$ $= \frac{bh^{3}}{12} - \frac{bh}{18}$ $= \frac{bh^{3}}{18}$

$$= \frac{2}{h^{2}} \frac{h^{3}}{6} - \frac{h}{3} / I_{x} = I_{x} + Ad^{2} \text{ of } \frac{bh^{3}}{36}$$

$$= \frac{bh^{3}}{12} + \frac{bh}{2} \frac{2h^{2}}{3} = \frac{bh^{3}}{4}$$

$$h = \frac{-h}{b-a}(x-b)$$

$$dA \qquad b$$

$$A = \frac{1}{2}b(h)$$

$$\bar{z} = \int x_c dA = \int \frac{x_c (hx) dx}{A} + \int \frac{x_c (-h)(x-b) dx}{a}$$

$$= \frac{h}{a} \left[\frac{x^3}{3} \right]_{\partial}^{a} + \frac{-h}{(b-a)} \int_{a}^{b} z^2 - bx \, dx$$

$$= \frac{h}{a} \left[\frac{x^3}{3} \right]_{\partial}^{a} + \frac{-h}{(b-a)} \int_{a}^{b} z^2 - bx \, dx$$

$$= \frac{ha^{2}}{3} - \frac{h}{(b-a)} \left[\frac{x^{3}}{3} - b \frac{x^{2}}{2} \right]_{a}^{b}$$

$$\frac{1}{2}bh$$

$$= \frac{h^{2}}{3} - \frac{h}{(b-a)} \left[\frac{(b^{3}-a^{3})}{3} - b \frac{(b^{2}-a^{2})}{2} \right]$$

$$= \frac{2a^{2}}{3b} - \frac{2}{b(b-a)} \left[\frac{(b^{3}-a^{3})}{3} - \frac{b(b^{2}-a^{2})}{2} \right]$$

$$2\alpha\beta(\bar{x}) = g^2 \left[\sin \bar{\sigma} \right]_{-\alpha}^{\alpha}$$

= $g^2 \left[\sin \alpha - \sin(-\alpha) \right]$

$$dA = bdy$$

$$I_{x} = \int_{-h/2}^{h/2} y^2 b dy$$

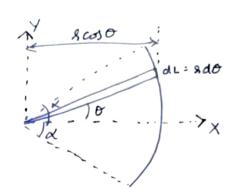
$$= b \left[\frac{y^3}{3} \right]_{-h/2}^{h/2} = \frac{b}{3} \left[\frac{h^3}{8} - \left(\frac{-h^3}{8} \right) \right]$$

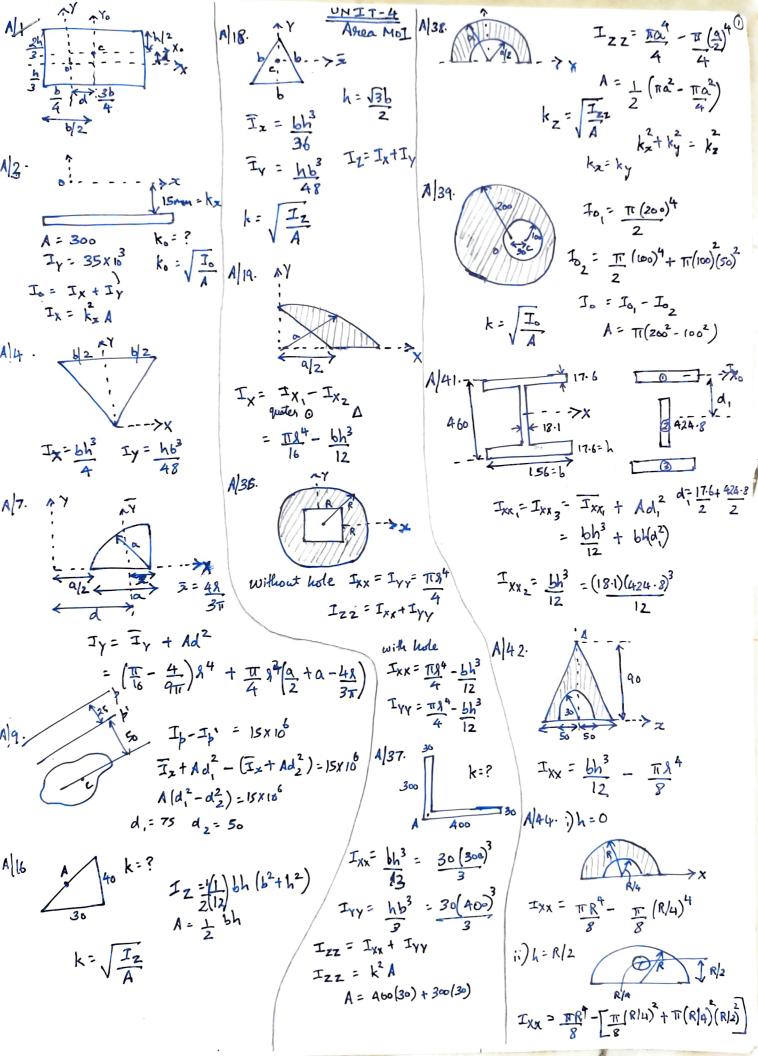
$$I_{z} = \frac{b}{3} \frac{b^{3}}{4} = \frac{1}{12} b b^{3}$$

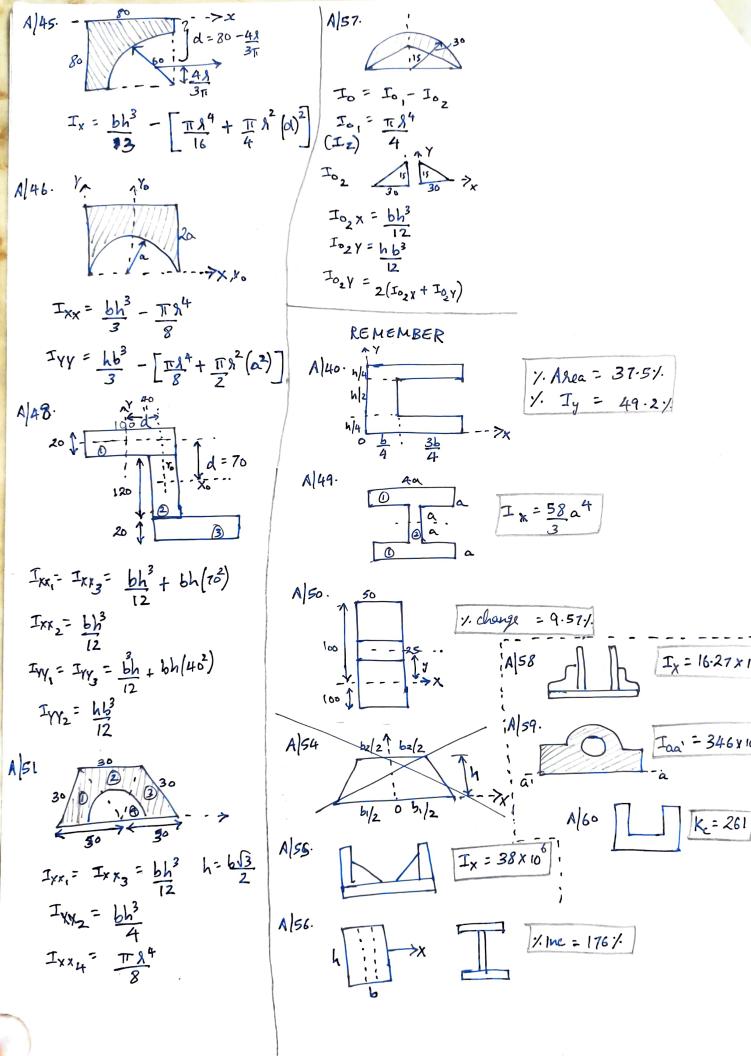
$$I_{X_0} = I_X + Ad^2$$
 (llosis theden)
= $\frac{1}{12}bh^3 + bh(\frac{h}{2})^2 = \frac{4}{12}bh^3 = \frac{bh^3}{3}$

$$||_{Z_{0}}^{hy} I_{Y_{0}} = \frac{h_{0}^{13}}{3}$$

$$I_{Z_{0}} = I_{X_{0}} + I_{Y_{0}}$$







$$3 \frac{3}{3} \frac{$$

5/47
$$\stackrel{?}{\downarrow}$$
 40 $\stackrel{?}{\downarrow}$ $\stackrel{?}{\downarrow$

5/49.

$$\frac{15}{15} = \frac{15}{120} = \frac{15}{120} = \frac{200(15)(15)}{200(15)} + \frac{2(15)(120)(15 + 120)}{200(15)} = \frac{5/57}{200(15)} = \frac{15}{200(15)} = \frac{15}$$

$$0 \quad A = 15(120) \quad \bar{z} = -50/2 \quad \bar{y} = \frac{120}{2}$$

(2)
$$A = 150 (120)$$
 $\bar{x} = 150/2$ $\bar{y} = 120/2$

(3)
$$A = \frac{1}{2}(100)(120)$$
 $\bar{x} = \frac{150}{3}$ $y = \frac{120}{3}$

②
$$\hat{y}_2 = 35 + \frac{273}{2} \quad A = 273(22)$$

$$A = \frac{1}{2} \left(\frac{100}{140} \right)$$

$$\tilde{z} = \frac{100}{2} \quad \tilde{y} = \frac{40}{2}$$

$$\widehat{y} = \frac{\mathbb{I} \left(74\right)^{2} \left(\frac{4(74)}{3\pi}\right) - 64(32)(32/2)}{\frac{\mathbb{I} \left(74\right)^{2} - 64(32)}{2}}$$

5/55. AY

$$0 \quad \overline{y} = \frac{2}{3} \quad \alpha \quad \frac{\sin \pi}{4}$$

$$A = \frac{1}{4} \pi \alpha^{2}$$

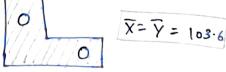
$$\frac{1}{2} \frac{1}{4} \frac{1}{5} \frac{2}{3} \frac{1}{4}$$

$$\frac{2}{3} \frac{1}{4} \frac{2}{5} \frac{2}{3} \frac{1}{4} \frac{1}{5} \frac{2}{5} \frac{1}{5} \frac$$

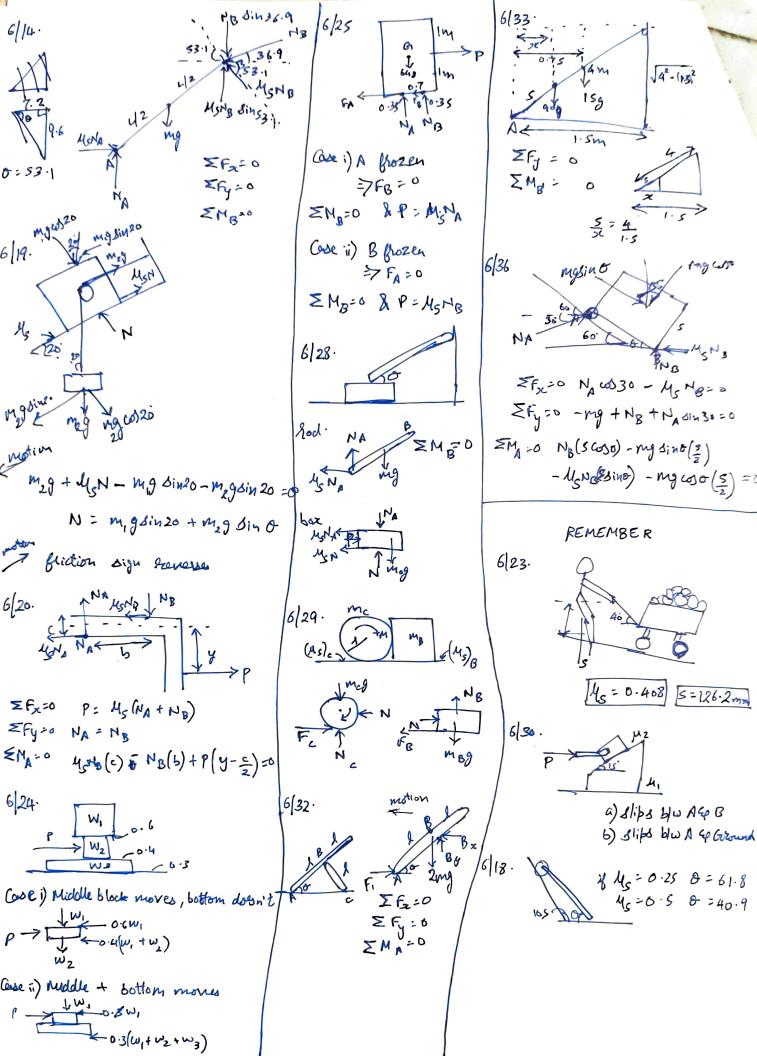
$$\overline{x} = \frac{1}{3}\pi 3^{2} = \frac{1}{3}\pi 3^{2}$$

$$\tilde{y} = \frac{400}{2} = 200$$

area of sector



6th February, 2023 * always assume egm. 6/11. * prove it right/whong FRICTION 6/1. FB = HONA =0.3 NA FA= Maria >Fx:0 fe . 4, No ZFy = 0 ZM61 = 0 ZFy=0 0.3 NA (0.2) +0.3 NB (0.2) - M = 0 to max = 45N if F < fsmax > cgm EFx = 0 0.3 Ng 6530 + Ng 6060 - NA = 6 F > fsmx => motion <fy > 0 Ng din 60 - 0.3 NB din 30 - 30g + 0.3 NA = 0 F= 4N 509 8in 25 6/2. P. Psino 6/12. N = 509 Cos 25 i) motion down Pcs>75 5 Pado 509 sin 25 45 - F ii) motion up ≥ fy = 0 Pcos 75 - mg cos 15 + N = 0 Psin75 + F-mg sin15 = 0 0.3HE ZMG = 0 sug Binzs - P(8/2) + F(1) = 0 Psin20 - 50g cus15 7 Pcs 20 - 509 din 15 mgsin20 6/8 6/13 mg 6030 a) P=0 12(9) assume agm b) P=250N F=4KNB 4 = ? 50g (75 sino) - (2g (200 - 75 sino) = 0 if F> Formax 4kNB = mg sin 30 Mrin = tano NA + NB = mg cosso 5M2=0 c) P= ? fd mdion NB(b) - mg sin30(b). 16/9.434 - mg cos 30(b)=0 Jug sin sliding 6/4 · mg upo 4-NA 6037 + NA 60553 -P + 45NB = 0 F- MKT NA + NA COO37 - 1009 - MONASIN 37 = 0 EMB=0 MK(N) = mg sin & POZZSN N = mg coso



solids are in contact under a condition of sliding / tendency to slide.

* A flictional folice tangent to surface of contact occurs both during the interval and leading upto impending slippage and when slippage takes place.

* The direction of this friction always opposes the direction of motion.

* Also called Coulomb Friction

Fluid Friction: * Fluid friction occurs when adjacent layers in a fluid (1iz | gas) are moving at diffe velocities.

* This motion causes frictional forces by fluid elements, and these forces depend on relative velocity by layers.

* No grelative velocity => No fluid friction

* Fluid friction depends on _ velocity gladients within the fluid _ viscosity of liquid.

3. Internal Friction: * Internal friction occurs in all solid materials which are subjected to endical loading.

*For highly elastic materials the recovery from deformation occurs with very little loss of energy due to internal friction

#Static Friction

* Static friction force is determined by the equations of egm. This frictional force may have any value from 0 upto including the max value. For a given value of meeting surfaces the experiment shows that the max value of static friction is propositional to the normal parce N.

Fraz = MsN

Ms is the proportionality constant, called coefficient of static friction

#Kinetic Friction

* After slippage occurs, the frictional folce which accompanies the ensuing motion is called kinetic friction. Kinetic Friction is usually < max static fliction folce. o

Ex= MkH coefficient of kinetic friction # Angle of Friction

* Angle made by the resultant of namal reaction and limiting friction with the normal occaption is called angle of friction.

Coefficient of static friction is equal to the tangent of angle of frution.

Angle of Rapose

* It is the minimum angle that an inclined plane makes with the horizontal when a body placed on it just begins to slide down.

lets day an inclined plane with a angle with hatizontal apa body of mass m

my sind - 4N

N= mg 000

tano = pe

0 = tan'(M)

angle of repose

Come of Friction

* If the resultant reaction is rotated about the normal reaction folce, it will form a cone known as come of friction. It is a right circular come with vertex at the point of contact of the two bedies (& suffices), axis in disection of normal reaction and vertical angle - angle of friction.

Factors affecting friction

* generation of high local temp and adhesion at contact points * relative hardness of meting surfaces

* presence of this surface files of oxide, oil, dirt of other substances

* molecular attraction

* loughness/smoothness of the sliding object

* houghness/smoothness of the sliding surface

* shape/design of objects

* Normal Folce

* Type of friction involved (rolling / sliding)