

Optics, hw 4

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9.42:

Solution: Look at the source via each optical element. If the brightness is dimmed about a half, what you're holding is then a linear polarizer; if the brightness remains almost unchanged, then it is a quarter-wave plate.

9.43:

Solution: A \mathcal{L} -state has the light vector as

$$\vec{E}(z) = E_0 \cos(kz - \omega t) \vec{e}_x - E_0 \cos(kz - \omega t - \frac{\pi}{2}) \vec{e}_y. \quad (1)$$

After traversing, E_y is retarded for $\frac{\pi}{4}$ in phase. The light vector is then

$$\begin{aligned} \vec{E}(z) &= E_0 \cos(kz - \omega t) \vec{e}_x - E_0 \cos(kz - \omega t - \frac{\pi}{2} - \frac{\pi}{4}) \vec{e}_y \\ &= E_0 \cos(kz - \omega t) \vec{e}_x - \frac{\sqrt{2}}{2} E_0 [\cos(kz - \omega t) - \sin(kz - \omega t)] \vec{e}_y, \end{aligned} \quad (2)$$

which represents a left-handed \mathcal{E} -state showed in fig. 1.

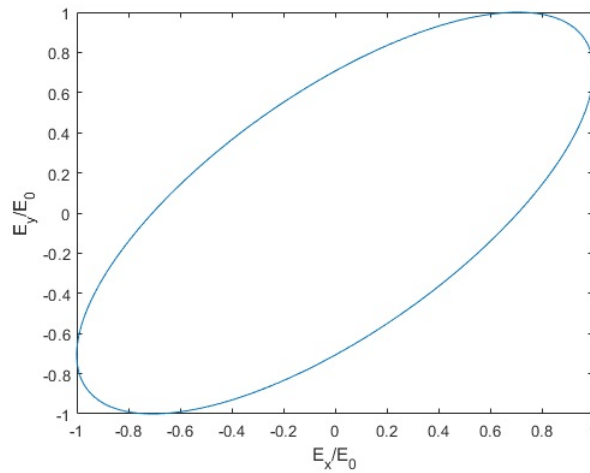


Figure 1: Polarization of the emerging light

9.48:

Solution: Rotatory for given solution is

$$\beta = \frac{66.45^\circ}{10 \text{ cm}} \times \frac{10 \text{ g/1000 cm}^3}{1 \text{ g/cm}^3} = 0.006645^\circ/\text{cm} \quad (3)$$

Orientation is then

$$\alpha = \beta l = 0.006645^\circ/\text{cm} \times 100 \text{ cm} = +0.6645^\circ \quad (4)$$

9.54:

- Solution: (a) $(1, 1, 0, 0)$ represents a horizontal \mathcal{P} -state (linear polarized in x direction). $(3, 0, 0, 3)$ represents a \mathcal{R} -state (right-circularly polarization).
 (b) Stokes vector of combined beam is $(1, 1, 0, 0) + (3, 0, 0, 3) = (4, 1, 0, 3)$, which represents an \mathcal{E} -state of flux density 4.
 (c) Degree of polatization is given by

$$V = \frac{\sqrt{S_1^2 + S_2^2 + S_3^2}}{S_0} = \frac{\sqrt{1^2 + 3^2}}{4} = 0.79 \quad (5)$$

- (d) A natural light with flux density 2. For any natural light can be decomposed into vertial and horizontal \mathcal{P} -state with equal amplitudes, combining two vertial and horizontal \mathcal{P} -state, reversely, results in a natural light.

9.69:

Solution: (a)

$$\begin{pmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{pmatrix} \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix} = \begin{pmatrix} \cos \theta \cos \alpha + \sin \theta \sin \alpha \\ \sin \theta \cos \alpha - \sin \alpha \cos \theta \end{pmatrix} = \begin{pmatrix} \cos(\theta - \alpha) \\ \sin(\theta - \alpha) \end{pmatrix} \quad (6)$$

(b)

$$\begin{pmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{pmatrix} \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} \cos \alpha + i \sin \alpha \\ -\sin \alpha + i \cos \alpha \end{pmatrix} = \frac{e^{i\alpha}}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix} \quad (7)$$

(c)

$$\begin{pmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{pmatrix} \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -i \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} \cos \alpha - i \sin \alpha \\ -\sin \alpha - i \cos \alpha \end{pmatrix} = \frac{e^{-i\alpha}}{\sqrt{2}} \begin{pmatrix} 1 \\ -i \end{pmatrix} \quad (8)$$

- (d) The filter is an optical rotator, constructed by, for example, sugar solution with specific rotation β and length $l = \alpha/\beta$.

9.71:

Solution: (a) Applying a horizontal \mathcal{P} -state yields

$$\begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} (1//0) = \begin{pmatrix} 1 \\ i \end{pmatrix}, \quad (9)$$

which stands for a \mathcal{R} -state.

Similarly, applying a vertical \mathcal{P} -state yields a \mathcal{L} -state.

$$\begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} (0//1) = \begin{pmatrix} i \\ 1 \end{pmatrix} \sim (1 \quad -i). \quad (10)$$

Therefore, the given matrix represents a quarter-wave plate with its fast axis on the line $y = -x$.

- (b) Using the same approach as (a), it can be easily identified that the given matrix represents a quarter-wave plate with its fast axis on the line $y = x$.

Ex.:

Solution: For a Jones vector $\begin{pmatrix} \hat{E}_x \\ \hat{E}_y \end{pmatrix}$, it can be decomposed to fast axis and slow axis as

$$\hat{E}_o = \hat{E}_x \cos \theta + \hat{E}_y \sin \theta; \quad (11)$$

$$\hat{E}_e = -\hat{E}_x \sin \theta + \hat{E}_y \cos \theta, \quad (12)$$

or

$$\begin{pmatrix} \hat{E}_o \\ \hat{E}_e \end{pmatrix} = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} \hat{E}_x \\ \hat{E}_y \end{pmatrix} \quad (13)$$

When emerging, the two components now become

$$\begin{pmatrix} \hat{E}'_o \\ \hat{E}'_e \end{pmatrix} = \begin{pmatrix} \hat{E}_o e^{-i\delta} \\ \hat{E}_e \end{pmatrix} = \begin{pmatrix} e^{-i\delta} & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \hat{E}_o \\ \hat{E}_e \end{pmatrix}. \quad (14)$$

Notice that the relationship between (\hat{E}_o, \hat{E}_e) and (\hat{E}_x, \hat{E}_y) is

$$\begin{pmatrix} \hat{E}'_x \\ \hat{E}'_y \end{pmatrix} = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} \hat{E}'_o \\ \hat{E}'_e \end{pmatrix}. \quad (15)$$

The overall relationship between \vec{E} and \vec{E}' is then

$$\begin{pmatrix} \hat{E}'_x \\ \hat{E}'_y \end{pmatrix} = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & e^{-i\delta} \end{pmatrix} \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} \hat{E}_x \\ \hat{E}_y \end{pmatrix}. \quad (16)$$

Corresponding Jones matrix is

$$\begin{aligned} J &= \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} e^{-i\delta} & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \\ &= \begin{pmatrix} \sin^2 \theta + \cos^2 \theta e^{-i\delta} & \frac{1}{2} \sin 2\theta (e^{-i\delta} - 1) \\ \frac{1}{2} \sin 2\theta (e^{-i\delta} - 1) & \cos^2 \theta + \sin^2 \theta e^{-i\delta} \end{pmatrix}. \end{aligned} \quad (17)$$