# A Multi-dimensional Risk-based Optimization of a Fusion Pilot Plant

by

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with

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at the

64<sup>th</sup> APS-DPP Annual Meeting

Spokane, WA October 20, 2022



## System codes aim to quantify FPP design trade-offs

- High-level system studies can quickly approximate integrated solutions with relevant subsystem constraints
- Sensitivity scans show which parameters are most leveraging for an optimized FPP
- Past work has considered costoptimization sensitivity, but only with respect to a single baseline design point



 This study expands this effort with a 10-parameter sensitivity scan and a risk assessment analysis of over 4,000 optimized design points "Tornado" plot (from Wade & Leuer, FST 2021) shows cost sensitivity study around a single baseline design point

## GA Systems Code optimization workflow

- The GA Systems Code (GASC) generates 0D solutions for a netelectric, steady-state tokamak
- GASC constrained optimization workflow requires:
  - A set of constant input parameters
  - A set of free input parameters (with appropriate bounds)
  - A set of constrained output parameters
  - An optimization function to minimize: Direct Capital Cost

#### Free Inputs

- major radius
- toroidal field
- plasma current
- on-axis ion temp.
- normalized beta
- TF coil radial build
- CS coil radial build
- TF coil structural fraction
- CS coil structural fraction
- impurity fraction

Constant Inputs

- aspect ratio = 3.5
- triangularity = 0.7
- $T_e/T_i = 1.0$
- $T_{i0}/<T_i> = 2.3$
- $n_{e0}/<n_e> = 1.3$
- $n_{He}/n_e = 0.05$
- $Z_{impurity} = 36$
- $f_{NI} = 1.0$
- $\eta_{\text{thermal}} = 0.4$
- $\eta_{aux} = 0.4$
- $M_{\text{blanket}} = 1.2$
- and many more...

#### Constrained Outputs

- $\beta_N/\beta_{N,IW} < 0.8$
- $\kappa/\kappa_{\rm max} < 0.9$
- f<sub>BS</sub> < 0.8
- f<sub>GW,ped</sub> < 0.9
- q<sub>95</sub> > 3.0
- $P_{SOL}/P_{L-H} > 1.0$
- Z<sub>eff</sub> > 2.0
- $H_{DS03} < 1.0$
- N<sub>w</sub> < 3.0 MW/m<sup>2</sup>
- $q_{pol} < 2.5 \text{ GW/m}^2$
- $\omega_{ce0}^2 / \omega_{pe0}^2 < 1.0$
- P<sub>NET</sub> > 200 MWe



## Multi-dimensional scan over 10 constrained parameters

 Each constraint is scanned over 2 or 3 values, ranging from conservative (ITER baseline) to aggressive

Parameter	Definition	Constraint Values	ITER Q=10 Value
Bootstrap faction	$f_{BS} = C_{BS} \beta_P A^{-1/2}, C_{BS} = 2/3$	[0.4, 0.6, 0.8]	0.28
H <sub>DS03</sub>	Energy confinement scaling factor	[0.8, 1.0]	0.85
Neutron wall loading	Peak neutron power flux at first wall	[1.0, 3.0] MW/m <sup>2</sup>	0.75
BetaN limit fraction	$\beta_N / \beta_{N,IW}$ (MHD control)	[0.4, 0.6, 0.8]	0.37
Elongation fraction	$\kappa$ / $\kappa_{max}$ (VDE control)	[0.7, 0.9]	0.75
Poloidal heat flux	Poloidal heat flux at OMP	[1.5, 2.5] GW/m <sup>2</sup>	1.2
Peak coil stress	Peak Von Mises stress at IMP	[600,800] MPa	600
Coil current margin	J <sub>crit</sub> /J <sub>op</sub> margin in coil current	[3.0, 2.0]	3.0
Superconductor	Magnet conductor technology	[LTS, HTS]	LTS
Coil bucking	CS-TF contact with central plug	[No, Yes]	No

## Cost-optimization scan yields 4,608 FPP solutions

- Two net power targets considered: 100MWe and 200MWe
- Cost roughly correlates with facility size, with significant spread
- 30% of optimized design points are below \$10B



## Constraints ranked based on cost-reduction sensitivity

- Given a design point with a conservative constraint:
  - How much is cost lowered by changing the constraint to be more aggressive?
- Plasma-related constraints have a more leveraging impact on FPP cost
  - exception is poloidal heat flux





## Risk assessment is used to quantify design risk

- Risk management process can be expressed mathematically
- Total risk is defined as sum over individual risks, R<sub>i</sub>, which can be computed as the product of potential losses, L<sub>i</sub>, and their probabilities, p(L<sub>i</sub>):

$$- R_i = L_i p(L_i)$$
$$- R_{total} = \sum_i L_i p(L_i)$$

 Assume that risks are independent and linear (i.e. they are not correlated, and they do not compound)

#### Risk = loss x probability



Constraints are divided into three risk categories:

- Low: loss = 1
- Medium: loss = 3
- High: loss = 5

## Risk assessment categorization definitions

- Low-risk losses are more probable but less damaging
- High-risk losses have the potential to severely disrupt entire project

Parameter	Loss Method	Loss Severity	Risk
Bootstrap faction	Sub-par performance	Low (1)	0.1 – 0.5
H <sub>DS03</sub>	Sub-par performance		
Neutron wall loading	Shortened operational cycle		
BetaN limit fraction	MHD / transient heat flux	Medium (3)	0.1 – 0.75
Elongation fraction	VDE / disruption damage		
Poloidal heat flux	PFC erosion / melting		
Peak coil stress	Magnet damage	High (5)	0.1 – 1.0
Coil current margin	Magnet damage		
Superconductor type	TRL gateway fail		
Coil bucking	TRL gateway fail		

## Risk assessment differentiates designs with similar cost

- Lowest cost design points span a large range in risk
  - Design choices should prefer lower risk at comparable cost
- Higher net power is not inherently riskier, but is achieved via higher cost (15-20% more expensive to double output power)



## **Risk-cost metric allows comparison of parameters**

- It is desirable to quantify a combination of cost and risk into a single metric
  - Will allow for direct comparison of parameters
- Bottom-left boundary of dataset corresponds to a logical function:
  - $F = (cost) \times (risk)^{0.5}$
  - This metric weights cost twice as much as risk
- This is a subjective measure of risk vs. cost trade-off



## Risk-cost metric identifies plasma as highly leveraging

- Bootstrap, and betaN limit, and elongation fractions significantly reduce risk-cost, as does H<sub>DS03</sub> confinement factor
- Coil constraints (stress and current margin) increase risk-cost



# P<sub>NET</sub> = 100MWe design points



 $\begin{array}{l} {\sf R}_0 = 4.66m \\ {\sf B}_{\sf T} = 4.68T \\ {\sf I}_{\sf P} = 8.65MA \\ {\sf P}_{\sf aux} = 84MW \\ {\sf \beta}_{\sf N} = 4.27 \\ {\sf q}_{\sf pol} = 1.5GW/m^2 \\ {\sf Risk} = 3.3 \\ {\sf Cost} = \$5.6B \end{array}$ 

 $\begin{array}{l} {\sf R}_0 = 4.56m \\ {\sf B}_{\sf T} = 4.65T \\ {\sf I}_{\sf P} = 8.41MA \\ {\sf P}_{aux} = 77MW \\ {\sf \beta}_{\sf N} = 4.27 \\ {\sf q}_{pol} = 2.0GW/m^2 \\ {\sf Risk} = 4.5 \\ {\sf Cost} = \$4.7B \end{array}$ 

 $\begin{array}{l} {\sf R}_0 = 3.89 m \\ {\sf B}_{\sf T} = 5.36 {\sf T} \\ {\sf I}_{\sf P} = 8.23 {\sf M} {\sf A} \\ {\sf P}_{\sf aux} = 83 {\sf M} {\sf W} \\ {\sf \beta}_{\sf N} = 4.25 \\ {\sf q}_{\sf pol} = 2.5 {\sf G} {\sf W} / {\sf m}^2 \\ {\sf Risk} = 5.9 \\ {\sf Cost} = \$4.2 {\sf B} \end{array}$ 



- Three 'best' design points are shown for the 100MWe case
- All have similar  $\beta_N$  and  $P_{aux}$
- Increasing risk allows inclusion of bucking, and then HTS magnets
- Poloidal heat flux also increases

# P<sub>NET</sub> = 200MWe design points



 $\begin{array}{l} {\sf R}_0 = 5.10m \\ {\sf B}_{\sf T} = 4.83T \\ {\sf I}_{\sf P} = 9.77MA \\ {\sf P}_{\sf aux} = 88MW \\ {\sf \beta}_{\sf N} = 4.27 \\ {\sf q}_{\sf pol} = 1.5GW/m^2 \\ {\sf Risk} = 3.4 \\ {\sf Cost} = \$6.4B \end{array}$ 

 $\begin{array}{l} R_{0} = 5.07m \\ B_{T} = 4.85T \\ I_{P} = 9.74MA \\ P_{aux} = 88MW \\ \beta_{N} = 4.27 \\ q_{pol} = 1.5GW/m^{2} \\ Risk = 4.3 \\ Cost = $5.4B \end{array}$ 

 $\begin{array}{l} {\sf R}_0 = 4.45m \\ {\sf B}_{\sf T} = 5.28T \\ {\sf I}_{\sf P} = 9.28MA \\ {\sf P}_{\rm aux} = 82MW \\ {\sf \beta}_{\sf N} = 4.26 \\ {\sf q}_{\rm pol} = 2.5GW/m^2 \\ {\sf Risk} = 5.9 \\ {\sf Cost} = \$4.7B \end{array}$ 



- 200MWe case shows similar trends
- Size and cost is higher than lowpower case, but β<sub>N</sub> is the same
  - HTS magnets can be costcompetitive due to reduced SC volume

## **Summary and Future Work**

- GA Systems Code generates a cost-based optimization scan over 10 constrained parameters and identifies a large steady-state FPP design space
- Aggressive plasma-related constraints achieve target FPP power output at a lower cost than coil-related constraints
- Inclusion of a risk assessment study allows for differentiation between comparably costed solutions
- Subjective risk-cost metric further isolates bootstrap, elongation, and betaN limit fractions as highly leveraging

- Future work will address the inductive (pulsed) operation strategy, using physics-based constraints for ramp-up duration, flattop length, and dwell time
- Addition of thermal energy storage may provide a path to reduced cost, but only if tokamak cost savings from lower P<sub>NET</sub> outweigh extra cost of storage system

## **Backup Slides**



## Net power



#### full dataset

cost < \$10B



### **BetaN limit fraction**



#### full dataset

cost < \$10B



### **Bootstrap fraction**



#### full dataset

cost < \$10B



### **Elongation fraction**



#### full dataset



count

cost < \$10B

H<sub>DS03</sub>



cost < \$10B

1e2



### Peak neutron wall loading



cost < \$10B



## Poloidal heat flux



#### full dataset

cost < \$10B



### Superconductor type



#### full dataset





### Freestanding vs. bucked coils





#### cost < \$10B



## Peak coil stress (Von Mises)

#### full dataset



#### cost < \$10B



## Coil current margin





cost < \$10B



## Alternate risk assessment definition



## Alternate risk assessment definition

- What if all parameters are assigned to the same risk category: Medium (3)?
- Similar results, although less pronounced spread in risk at lower costs



## Alternate risk assessment definition

- No change in ordering of parameter effect on risk-cost metric
- Coil-related parameters become slightly more risk-cost effective

