

# Magnetohydrodynamics and Electromagnetics in the FUSE Integrated-Modeling Framework

by

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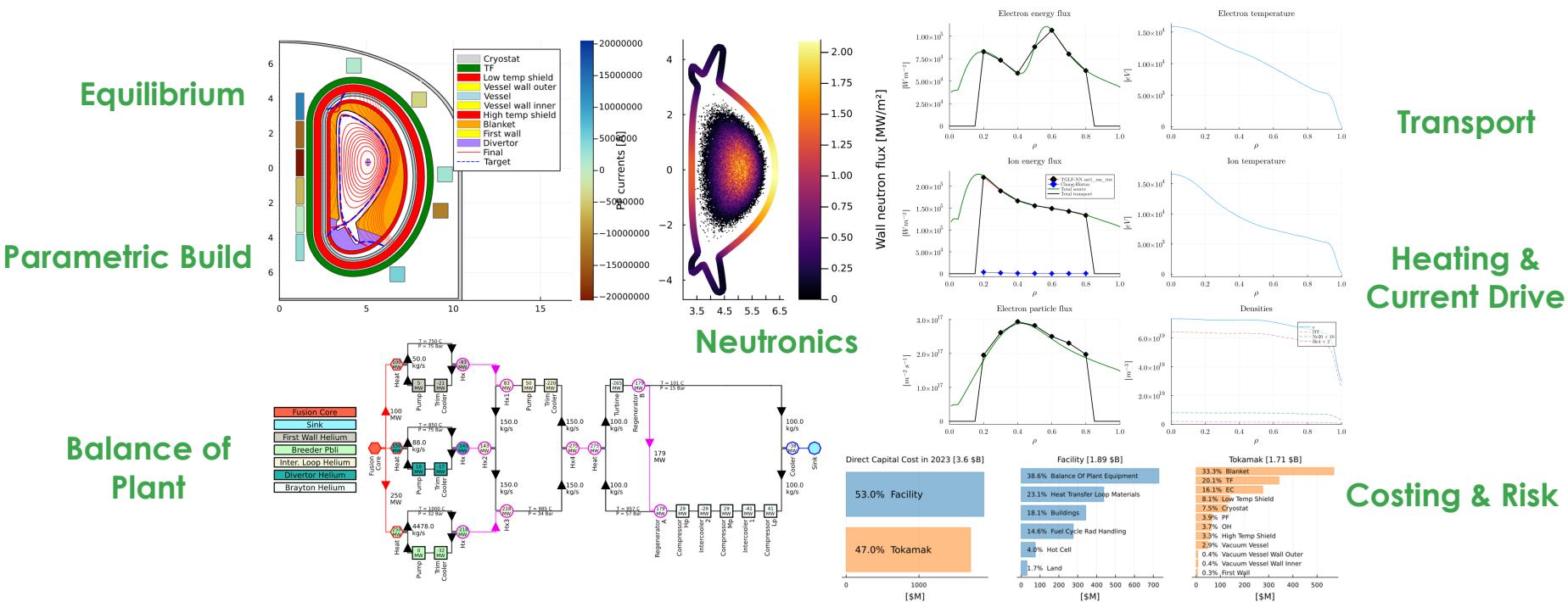
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# Fusion pilot plant design motivates development of radically new modeling framework

- **FUSE: a flexible, integrated framework for whole-facility FPP modeling**
    - Go from idea to concept design in minutes rather than months
    - Evaluate and optimize wildly different concepts on same footing
    - Provide physics/engineering teams high-quality, integrated design
    - Support modeling needs from design to operations
  - **Models span from plasma, through build, to site boundary**
  - **Developed from the ground-up based on GA modeling expertise**
    - Built around ITER IMAS ontology for modularity and maximum interoperability
    - All in one language: Julia (high-level like Python but as fast as C/Fortran)



# Grad-Shafranov Equilibria

$$\Delta^* \Psi = (2\pi)^2 \mu_0 R J_\varphi$$

# TEQUILA provides fixed-boundary equilibria using efficient spectral representation of flux surface geometry

- Initialized by what is known in future devices: desired boundary and pressure/current profiles
- Solves for  $\Psi$  in poloidal coordinates with cubic Hermite finite elements in  $\rho_{\text{pol}}$  and Fourier modes in  $\theta$
- Boundary and flux surfaces defined by Miller extended harmonic representation [1]

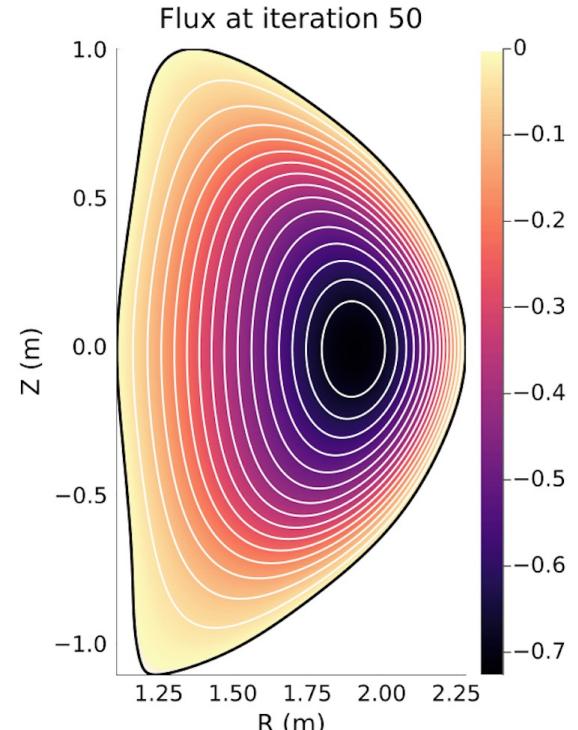
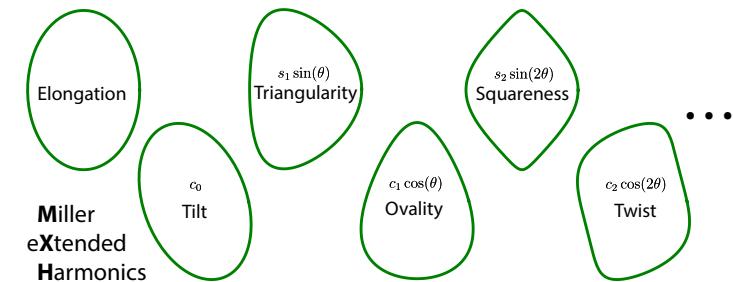
$$R(\rho, \theta) = R_0(\rho) + a(\rho) \cos [\Theta_R(\rho, \theta)]$$

$$Z(\rho, \theta) = Z_0(\rho) + \kappa(\rho)a(\rho) \sin(\theta)$$

$$\Theta_R(\rho, \theta) = \theta + c_0(\rho) + \sum_{m=1}^M [c_m(\rho) \cos(m\theta) + s_m(\rho) \sin(m\theta)]$$

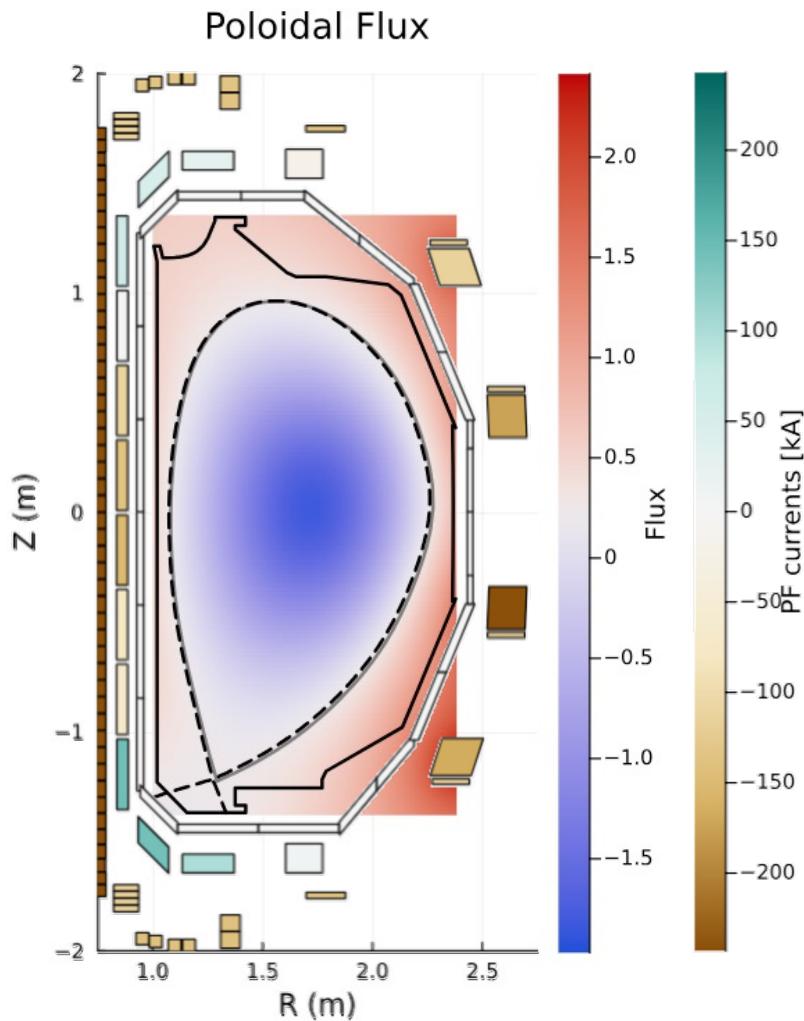
- G-S solve and poloidal flux coordinate fitting iterated until  $\theta$  dependence eliminated

[1] Arbon et al., PPCF 63, 012001 (2021)



# FRESCO provides free-boundary equilibria

- **G-S solve by two iterative loops**
- **Inner loop**
  - Invert G-S operator 2D finite differences with Fourier transform in Z coordinate
  - Update plasma boundary and  $J_\phi(R, Z)$
  - Relaxed Picard iterations
- **Outer loop**
  - Update Dirichlet boundary condition on  $\Psi$  using von Hagenow [1] boundary integral method
  - Forward solve: Update fictitious control coils for radial/vertical axis feedback
  - Inverse solve: Update physical coil currents to produce desired plasma shape



**Forward solve reproduces EFIT equilibrium**

[1] Lackner. Comput. Phys. Commun. 12, 33-44 (1976)

# Poloidal Vacuum Fields

# Flux from poloidal field coils and vacuum vessel computed from Green's functions

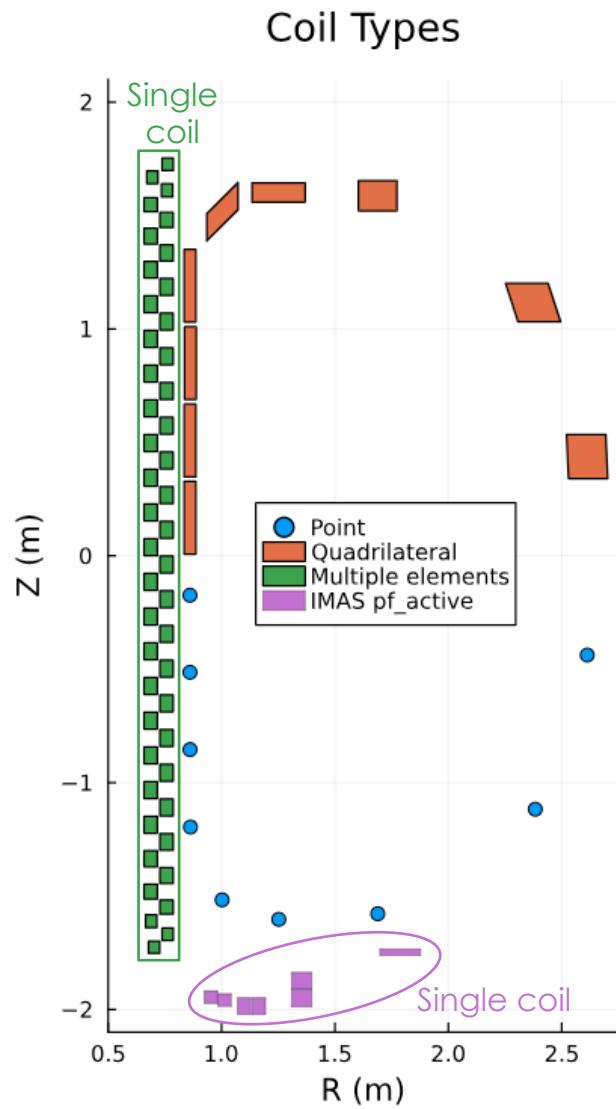
- Various coil types have been implemented, or can work directly from IMAS coils
- Use toroidal Green's function (including integration over coil area) to compute poloidal flux at any point

$$\Psi_c = 2\pi\mu_0 G(R, Z; R_c, Z_c) I_c$$

$$G(R, Z; R', Z') = \frac{\sqrt{RR'}}{2\pi k} [2E(k) - (2 - k^2)K(k)] \quad k^2 = \frac{4RR'}{(R + R')^2 + (Z - Z')^2}$$

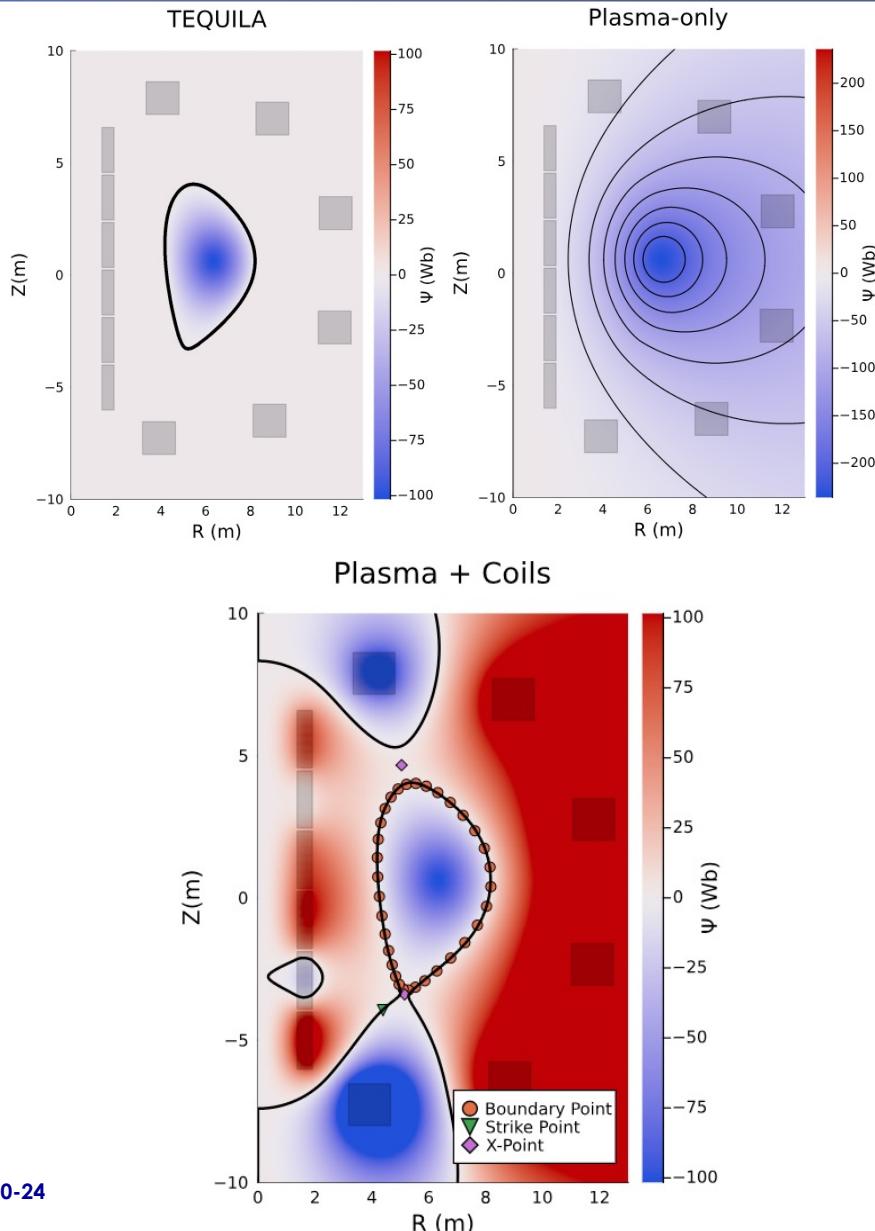
- Self/mutual inductance computed by double integral over coils

$$M_{12} = -\frac{2\pi\mu_0 N_1 N_2}{A_1 A_2} \int dA_1 \int dA_2 G(R_1, Z_1; R_2, Z_2)$$



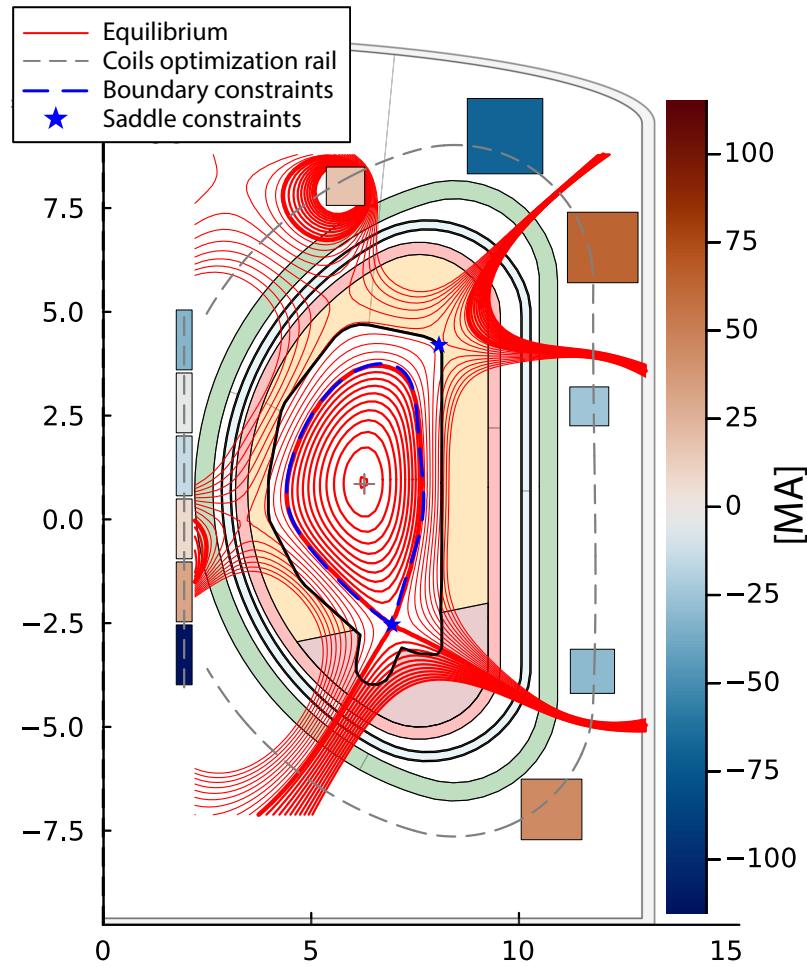
# Coil currents can be set to match plasma boundary with X-points and strike points

- **Plasma flux in vacuum computed efficiently from virtual-casing method**
  - Fixed-boundary simulations assume  $\Psi=0$  on boundary, which requires image current on boundary
  - Compute flux from image current
$$\Psi_{im}(R, Z) = \oint_{\Omega_p} \frac{d\ell'}{R'} G(R, Z; R', Z') \frac{\partial \Psi}{\partial n}$$
  - Then on & outside boundary, plasma flux is opposite image flux
- **Coil currents found from least-squares linear optimization to match control points when summed with plasma flux**
- **Various control points implemented**
  - Flux value
  - Isoflux ( $\Psi_1 = \Psi_2 = \Psi_3 \dots$ )
  - X-point ( $d\Psi/dR = d\Psi/dZ = 0$ )

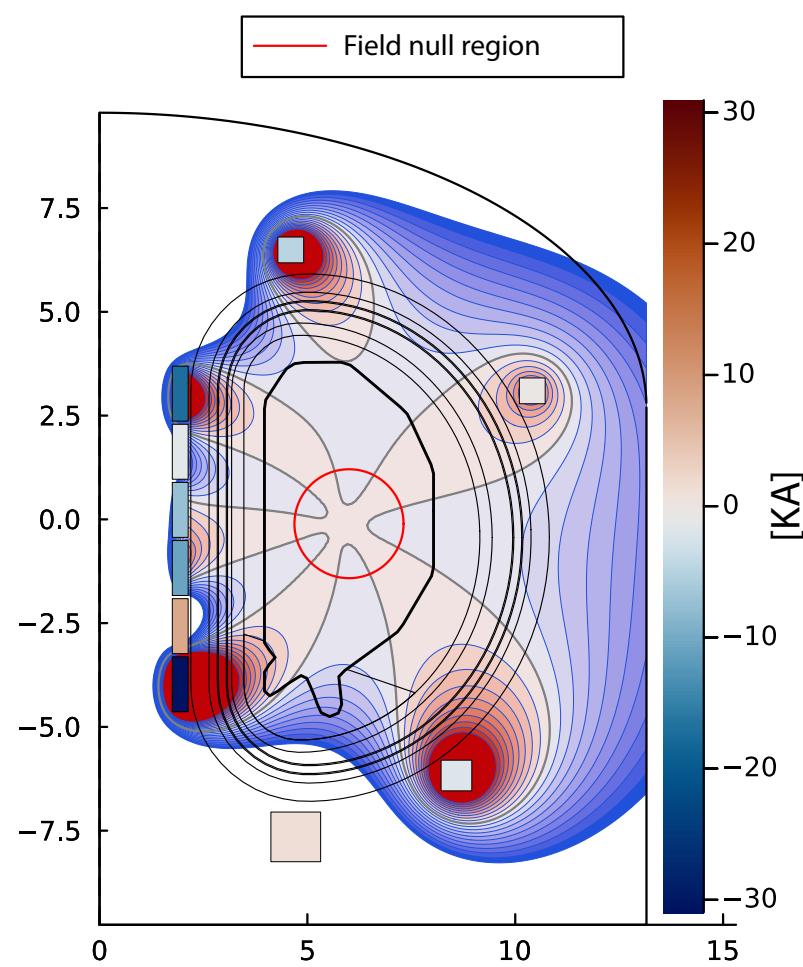


# Coil locations can be optimized to produce desired plasma boundary and/or initial field null

## Plasma Boundary

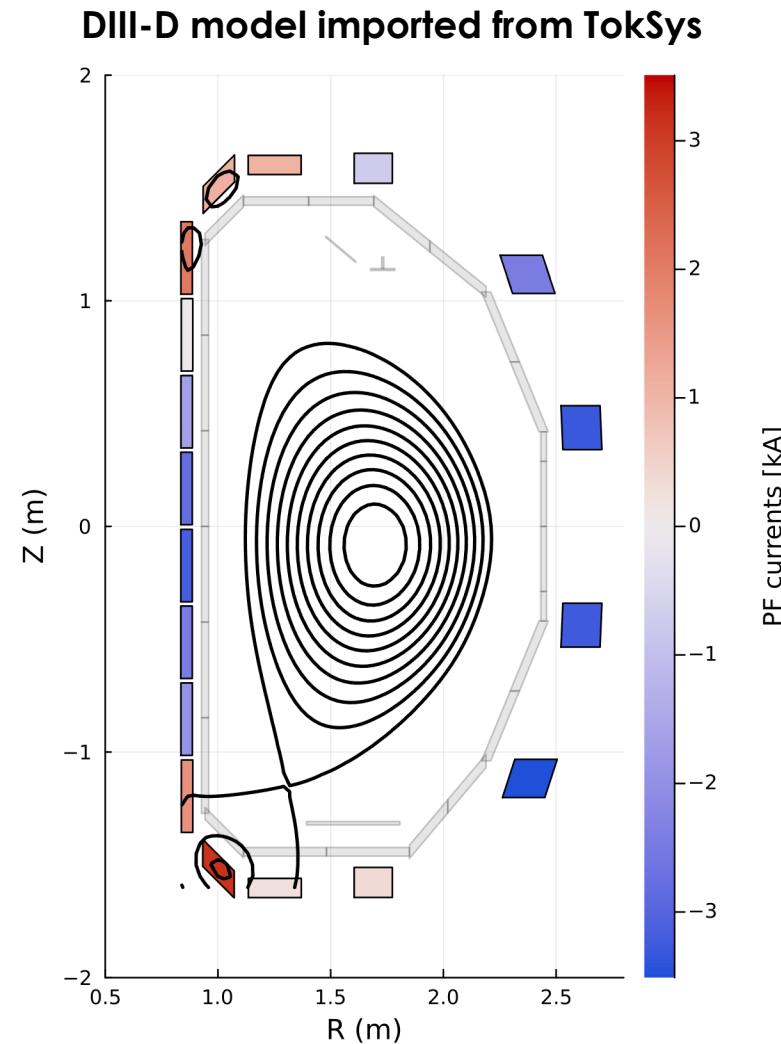


## Initial Field Null



# Coupled plasma-coil system provides metrics for vertical stability

- Vacuum vessel and other conducting structures treated as coils
- Two metrics for vertical stability
  - Inductive stability margin  $m_s$ 
    - Ideal instability for  $m_s < 0$
    - $m_s > 0.15$  for practical requirement
    - Depends on
      - Coil/vessel currents and mutuals
      - Plasma current
      - First & second vertical derivative of plasma-coil/vessel mutuals
  - Normalized, massless growth rate  $\gamma\tau$ 
    - Requires coil/vessel resistances as well
    - $\gamma\tau < 10$  for controllability
- Benchmarked to TokSys
- Future work: constrained optimization of passive plate locations to maximize vertical stability



# Plasma and Coil Current Evolution

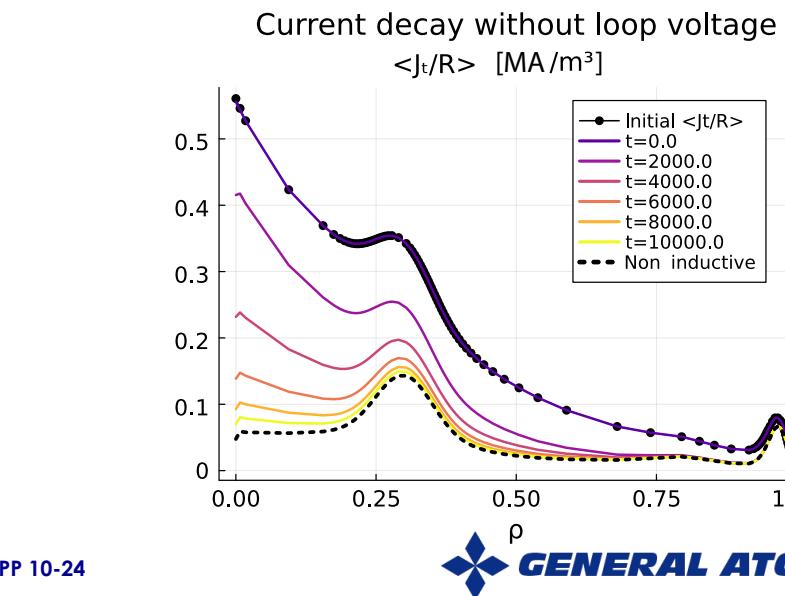
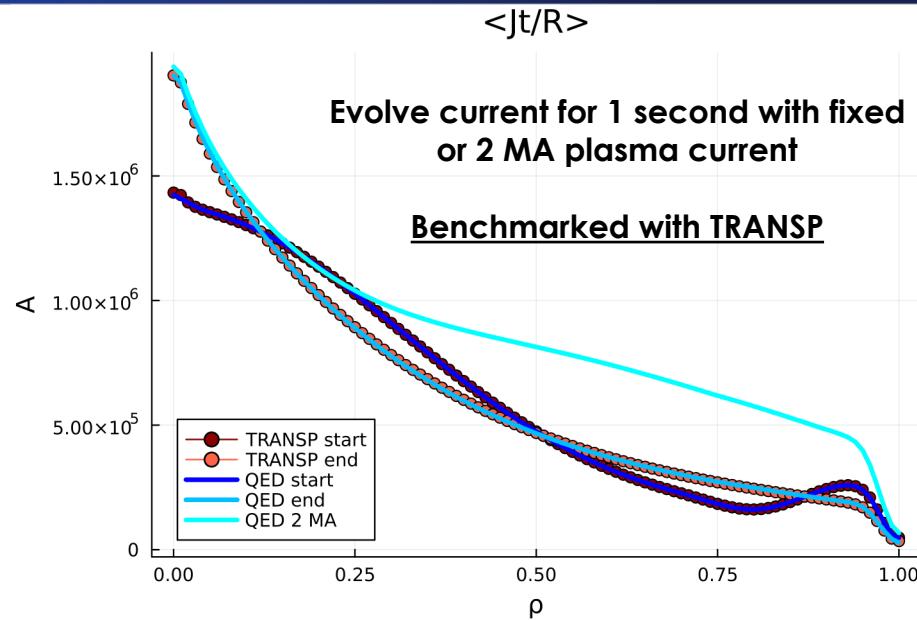
# QED solves diffusion equation for rotational transform

- Lightweight, computationally efficient, stand-alone current-diffusion solver
- $\theta$ -implicit time advance of diffusion equation on rotational transform with non-inductive source

$$\frac{\partial \iota}{\partial t} = \frac{1}{\Phi'} \frac{\partial V_L}{\partial \rho}$$

$$V_L = \frac{\eta F}{\mu_0 V' \langle R^{-2} \rangle} \frac{\partial}{\partial \rho} \left[ \frac{\Phi' V'}{2\pi F} \left\langle \frac{|\nabla \rho|^2}{R^2} \right\rangle \iota \right] - \frac{\eta}{F \langle R^{-2} \rangle} \langle \mathbf{B} \cdot \mathbf{J}_{NI} \rangle$$

- Rotational transform and all geometric quantities represented by cubic Hermite finite elements
- Boundary conditions
  - Constant  $I_p$  – Dirichlet on  $\iota$
  - Constant edge  $V_L$  – Robin on  $\iota$



# Coupling QED to time-dependent coil equations models inductive current drive and vessel response

- All coils obey coupled circuit equations**

$$L_i \frac{dI_i}{dt} + \sum_{j \neq i} M_{ij} \frac{dI_j}{dt} + M_{pi} \frac{dI_p}{dt} + \frac{dM_{pi}}{dt} I_p + R_i I_i = V_i$$

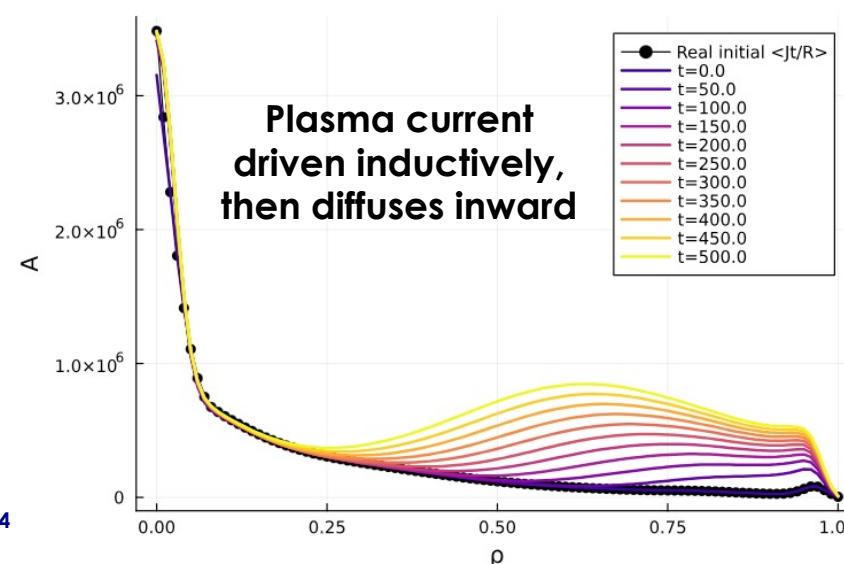
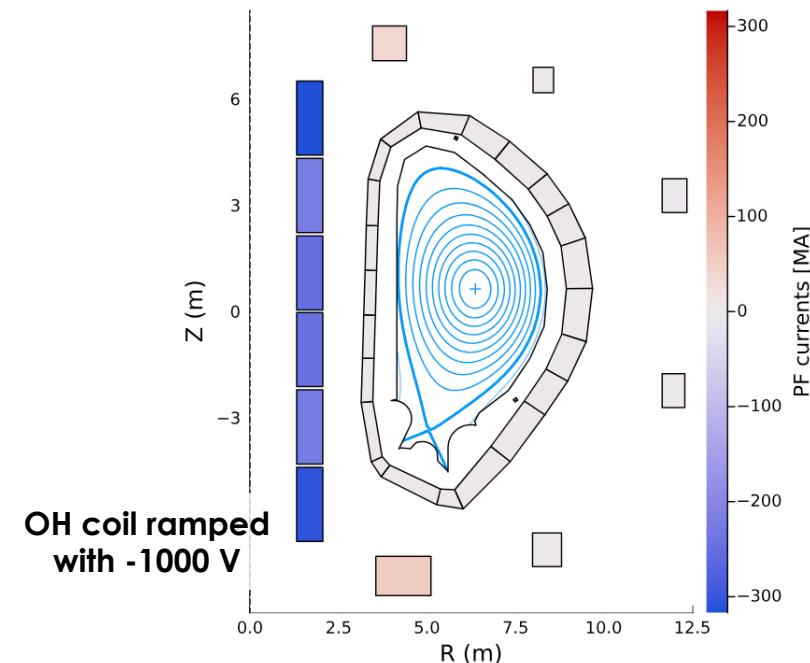
- Coupled to plasma through additional circuit equation with scalar resistance, inductance, and non-inductive voltage**

$$L_p \frac{dI_p}{dt} + \sum_j M_{pj} \frac{dI_j}{dt} + R_p I_p = V_{NI}$$

- Couples to internal plasma current diffusion equation through boundary condition**

$$I_p = \frac{1}{(2\pi)^2 \mu_0} \frac{d\Phi}{d\rho} \frac{dV}{d\rho} \left\langle \frac{|\nabla \rho|^2}{R^2} \right\rangle \iota \Big|_{\rho=1}$$

- Whole linear system can be advanced implicitly (e.g., Crank-Nicholson)**
- Accuracy can be improved through iterative solving of G-S equilibrium and/or predictor-corrector on scalar plasma quantities**



# Towards a Time-Dependent, Whole-Device Model

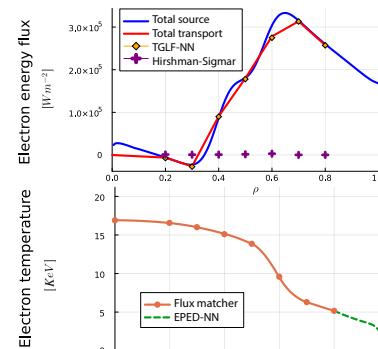
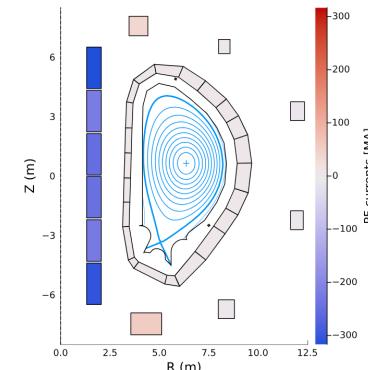
# Plasma-build evolution coupled to implicit flux matching will create Grad-Hogan-like solver

- Profiles found from turbulent & neoclassical flux matching (cf. TGYRO), with implicit time-derivative “sources”

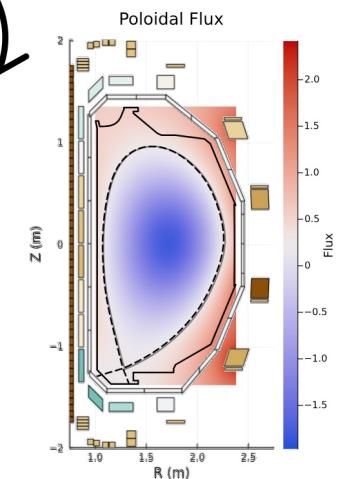
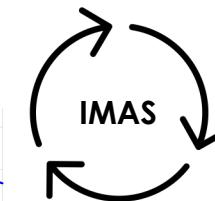
$$\langle \nabla \cdot \Gamma \rangle = S - \frac{\partial f}{\partial t}$$

- Long time stepping, limited only by
  - Current-diffusion time
  - Timescale of interest, e.g.,
    - Rapid shape change
    - LH transition
    - Burn initiation
- Multi-objective optimization can be used for actuator trajectory optimization

QED: Advance coil & plasma currents w/ control



FluxMatcher: update kinetic profiles



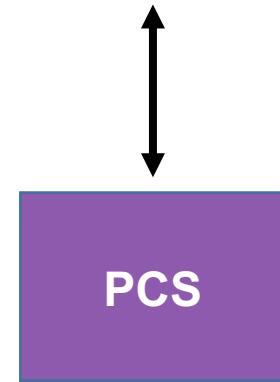
FRESCO: update equilibrium

# Coupling FUSE and TokSys will create high-fidelity plasma, build, & control model for scenario development

- Integrated simulations essential for testing control and safety, from commissioning through operation
- Co-simulation between TokSys/FUSE
  - FUSE provides high-fidelity plasma model and parametric builds
  - TokSys provides realistic control algorithms via plasma control system (PCS)
- Allows evaluation of all phases of tokamak operations
  - Pulse schedule development/validation
  - Control problem diagnosis
  - Control system development

**TokSys**  
**(Fast control oriented plant simulator)**

Useful for algorithm  
development and diagnosis



Useful for scenario  
modeling, pulse design  
development & validation

**FUSE**  
**(High fidelity plant simulator)**

# Conclusions

- **FUSE has an extensive suite of MHD and EM capabilities**
  - Fixed and free-boundary plasma equilibria
  - PF coil current and position optimization
  - Vertical stability assessment
  - Coupled plasma current profile and coil current evolution
- **Ongoing work**
  - Couple all of the above plus transport solver to make Grad-Hogan solver
  - Couple to TokSys for realistic control simulations (“flight simulator”)
- **Long-term goals**
  - Time-dependent scenario development of existing & prospective devices
  - Digital twins of experiments and reactors
- **FUSE and all packages are available as open-source Julia packages**
  - Contact [lyonsbc@fusion.gat.com](mailto:lyonsbc@fusion.gat.com) or [meneghini@fusion.gat.com](mailto:meneghini@fusion.gat.com)
  - For more information, visit the [fuse.help](https://fusehelp.jl) website:



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