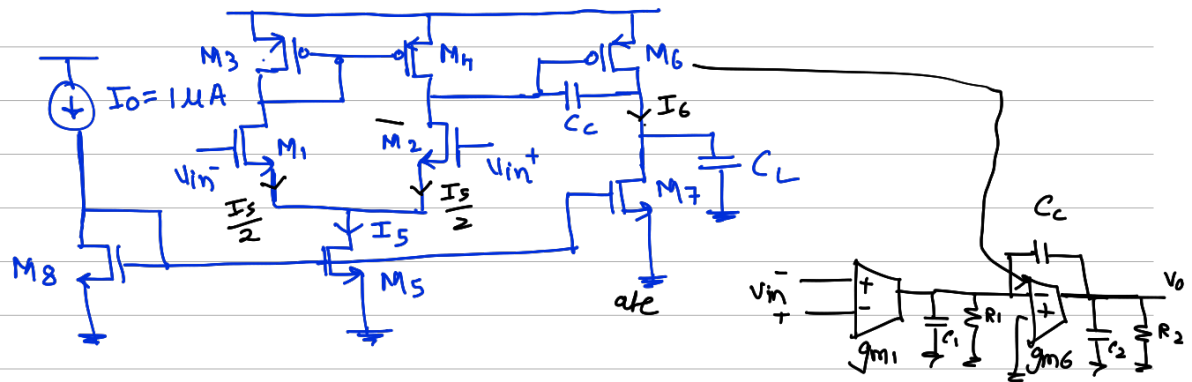


• Required specifications:

- 1)  $A_{dc} = 60 \text{ dB}$  ( $1000 \text{ V/V}$ )
- 2)  $GBW = 10 \text{ MHz}$
- 3)  $PM = 75^\circ$
- 4)  $CMRR = 50 \text{ dB}$
- 5)  $P_{diss} = 30 \mu\text{W}$
- 6)  $V_{dd} = 1.2 \text{ V}$
- 7)  $C_L = 100 \text{ fF}$



Design:

- ① Assume  $(\text{Gain})_{1st \text{ stage}} = 40$   $(\text{Gain})_{2nd \text{ stage}} = 25$

$$\textcircled{2} \quad P_{\text{dominant}} \approx \frac{(g_{ds2} + g_{ds4})}{\left[1 + \frac{g_{m6}}{(g_{ds6} + g_{ds7})}\right] C_L} ; \quad P_{\text{non-dominant}} \approx \frac{g_{m6}}{(C_L + C_C)}$$

$$\textcircled{3} \quad PM: -180 + 75^\circ = -105^\circ = -\tan^{-1} \left[ \frac{GBW}{P_{\text{dom}}} \right] - \tan^{-1} \left[ \frac{GBW}{P_{\text{non-dominant}}} \right] - \tan^{-1} \left[ \frac{GBW}{Z} \right]$$

assume  $Z \geq 10 GBW$ .

$$-105^\circ = -90^\circ - \tan^{-1} \left( \frac{GBW}{P_{nd}} \right)$$

$$\Rightarrow \boxed{P_{nd} = 3.73 \times GBW}$$

we employ zero cancelling resistor  $\therefore 0$

$$\Rightarrow P_{nd} = \frac{g_{m6}}{C_L + C_C} \approx \frac{g_{m6}}{C_L} \quad \left( \because C_C \text{ is smaller than } C_L. \text{ But if comparable, let } C_{C \text{ max}} = 2 \cdot C_L \right)$$

$\therefore$  whatever value comes from  $g_{m6}/C_L$ , we will take 3 times of calculated  $g_{m6}$

$$\Rightarrow \frac{g_{m6}}{C_L} = 373 \times 2\pi \times 10^7$$

$$\Rightarrow g_{m6} = 373 \times 2\pi \times 10^7 \times 100 \times 10^{-15}$$

$$g_{m6} = 23.43 \mu\text{S}$$

$$\Rightarrow \boxed{g_{m6} = (25 \times 3) = 75 \mu\text{S}}$$

$$\textcircled{4} \quad \text{First stage gain} = 40 ; \quad \frac{g_{m1}}{g_{ds2} + g_{ds4}} > 40$$

assuming  $g_{ds2} = g_{ds4}$

$$\Rightarrow \frac{g_{m1}}{g_{ds2}} > 80$$

From GBW,  $\frac{g_{m1}}{C_c} \geq 2\pi \times 10^7$

Here we considered  $C_{cmax} = 2C_L$

$\Rightarrow$  assume  $C_c = 100 \text{ fF}$  for now.

$\Rightarrow g_{m1} \geq 2\pi \times 100 \times 10^7$

$\Rightarrow g_{m1} \geq 6.28 \mu\text{S}$

$\Rightarrow g_{m1,2} = 7 \mu\text{S}$

Now we assume  $\left(\frac{g_m}{I_d}\right)_{1,2} = 20$  ( $\because$  we require high-gain from these)

$\therefore (I_d)_{1,2} = \frac{7 \mu}{20} = \underline{0.35 \mu\text{A}}$

We look into  $\frac{g_m}{g_{ds}}$  Vs  $\frac{g_m}{I_d}$  for nMOS at  $\frac{g_m}{I_d} = 20$

$\Rightarrow$  for  $L = 1.1 \mu\text{m}$  we satisfy the cond<sup>n</sup> of  $\frac{g_m}{g_{ds}} \geq 80$ .

$\therefore$  Choose  $L_{1,2} = 1.1 \mu\text{m}$

From  $\frac{I_d}{W}$  Vs  $\frac{g_m}{I_d}$  of nMOS at  $L = 1.1 \mu$  &  $\frac{g_m}{I_d} = 20$

we get  $W_{1,2} = 526 \text{ nM}$

⑤ For  $M_3, M_4$ , assume  $\frac{g_m}{I_d} = 10$ . We calculated  $(I_d)_{3,4} = 0.35 \mu$ .

$\Rightarrow (g_m)_{3,4} = 3.5 \mu\text{S}$

We had assumpt<sup>n</sup>  $\frac{g_{m1}}{g_{ds2}} > 80 \Rightarrow \frac{7 \mu}{80} > g_{ds2}$

$\Rightarrow g_{ds2} < 87.5 \text{ n}$

$\therefore g_{ds4} < 87.5 \text{ n}$

$\therefore \frac{(g_m)_{3,4}}{(g_{ds})_{3,4}} = \frac{3.5 \mu}{87.5 \text{ n}} > 40$

Repeating the step of ⑤ for calculation of  $M_3, M_4$  of PMOS we get  $L_{3,4} = 700 \text{ nM}$

$W_{3,4} = 133 \text{ n}$

⑥ For calculation of  $M_6$ :

Assume  $\left(\frac{g_m}{I_d}\right)_6 = 15$  [since it is a driver for 2<sup>nd</sup> stage]

From point ③, we assumed  $g_{m6} = 7.5 \mu\text{S}$

$\therefore I_{d6} = \underline{5 \mu\text{A}}$

We assumed 2<sup>nd</sup> stage gain  $> 25$  :  $\frac{g_{m6}}{g_{ds6} + g_{ds7}} > 25$

assuming  $g_{ds6} = g_{ds7}$  :  $\frac{g_{m6}}{g_{ds6}} > 50$

$$\therefore (g_{ds6}) < \frac{75 \mu}{50} = 1.5 \text{ n}$$

Again repeating steps from (5) to get 'L' where  $\frac{g_m}{g_{ds}} > 50$

we get  $L_6 = 600 \text{ n}$   
 $W_6 = 3.93 \mu$

(7) Design of  $M_5$  &  $M_7$ : done using current Mirror.

$\Rightarrow$  Assume current mirror's  $\frac{g_m}{I_d} = 15$ .

$\Rightarrow$  From  $V_{th}$  vs  $\frac{g_m}{I_d}$  plots, we found range of  $V_{th} = 330$  to  $350 \text{ mV}$ .

$\Rightarrow$  We will try to select  $V_{gs}$  such that  $V_{gs} > 350 \text{ mV}$ .

$\Rightarrow$  Then by looking at  $V_{gs}$  vs  $g_m/I_d$  plots for  $\frac{g_m}{I_d} = 15$ , we observe that  $L = 500 \text{ nM}$  satisfies above cond<sup>n</sup>.

$\Rightarrow$  Now from  $\frac{I_d}{W}$  vs  $g_m/I_d$  plot at  $\frac{g_m}{I_d} = 15$  &  $L = 500 \text{ nM}$ .

we get  $W_8 = 246 \text{ nM}$  (it carries  $1 \mu\text{A}$  current)

$$\therefore W_5 \text{ gets by scaling: } W_5 = \frac{I_5}{I_6} \times W_6 = \frac{0.7 \mu}{1 \mu} \times 246$$

$$\Rightarrow W_5 = 172.2 \text{ nM}$$

$$\text{Similarly for } W_7: \frac{I_7}{I_6} \times W_6 = \frac{5}{1} \times 246 \Rightarrow W_7 = 1.23 \mu\text{M}$$

But on simulation, we got less current  $\therefore$  we tuned it to increase  $W_7 = 1.07 \mu$

Here we keep  $L_{7,6} = 500 \text{ nM}$ .

(8) we employed zero canceling resistor  $= \frac{1}{g_{m6}} = 13.33 \text{ k}$