#### **Autonomous and Mobile Robots**

## Kinodynamic motion planning for steerable WMRs

DEPARTMENT OF COMPUTER, CONTROL, AND MANAGEMENT ENGINEERING ANTONIO RUBERTI



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#### Introduction

- In recent years mobile robots with steering wheels are widely used in autonomous navigation, logistics, and service robotics applications.
- Path planning in complex and dynamic environments requires advanced algorithms that ensure safety and precision.
- KRRT\* (Kinodynamic Rapidly-exploring Random Tree Star) offers significant advantages over traditional methods in terms of computational efficiency and path quality

### Differences with other mobile platforms

#### **Car-like Robots:**

- Low production cost
- High load capacity
- Lack of maneuverability

#### **Omnidirectional Robots with unconventional wheels:**

- High production cost
- Low load capacity
- High maneuverability

#### **SWM Robots:**

- Low production cost
- High load capacity
- Higher maneuverability

#### **Contents**

- Kinematic Model for an off-centered SWMR
- Kinodynamic RRT\* motion planning
- Simulations and Results on different maps
- Analysis on efficiency and drawbacks

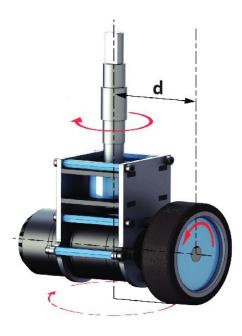
### **Assumptions**

- Localization Precision in Simulation
- Absence of Friction or External Forces
- Pure Rolling Constraints
- Rigid Body Assumption
- A Completely Known Environment

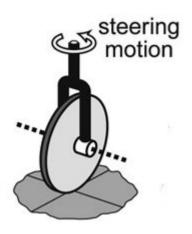
## **Neobotix MPO-700**

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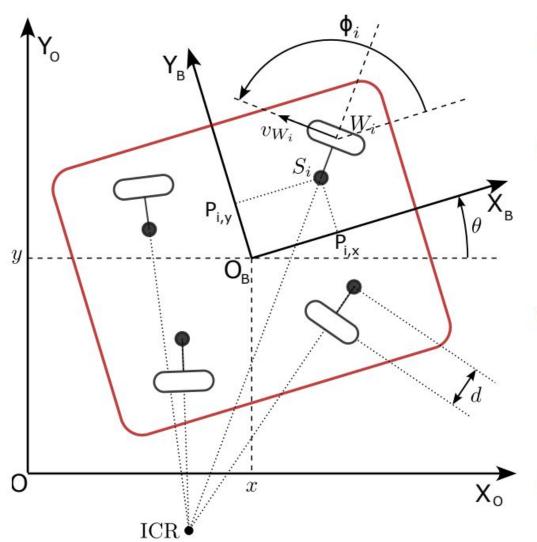
- 4 steerable independent actuated wheels
- Omnidirectionality







#### **Schematic model of MPO-700**



$$\boldsymbol{\xi} = \begin{bmatrix} x & y & \theta \end{bmatrix}^T \in SE(2)$$

$$oldsymbol{q} = egin{bmatrix} oldsymbol{\xi}^T & oldsymbol{\phi}^T \end{bmatrix}$$

## Position of $S_i$

$$\mathbf{o}_{S_i} = \begin{bmatrix} x \\ y \end{bmatrix} + \mathbf{R}(\theta) \begin{bmatrix} P_{i,x} \\ P_{i,y} \end{bmatrix}$$

### Position of $W_i$

$$\overrightarrow{\mathbf{X}}_{o}$$
  $\mathbf{o}_{W_{i}} = \mathbf{o}_{S_{i}} + \mathbf{R}(\theta + \phi_{i}) \begin{bmatrix} 0 \\ -d \end{bmatrix}$ 

## Model

#### **Pfaffian constraints**

Each wheels is subject to the pure rolling constraint

$$\begin{bmatrix} -\sin(\theta + \phi_i) \\ \cos(\theta + \phi_i) \end{bmatrix}^T \dot{\mathbf{o}}_{W_i} = 0$$

#### Implicit model

$$\begin{bmatrix} -\sin(\theta + \phi_1) & \cos(\theta + \phi_1) & \Delta_1 & 0 & \cdots & 0 \\ -\sin(\theta + \phi_2) & \cos(\theta + \phi_2) & \Delta_2 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ -\sin(\theta + \phi_{n_s}) & \cos(\theta + \phi_{n_s}) & \Delta_{n_s} & 0 & \cdots & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{\phi}_1 \\ \vdots \\ \dot{\phi}_{n_s} \end{bmatrix} = 0$$

#### where

$$\Delta_i = P_{i,x}\cos(\phi_i) + P_{i,y}\sin(\phi_i)$$

#### Geometric constraints

- All axles of the wheels must intersect at a single point (ICR) or the platform will not move.
- ICR can be seen as a geometric constraint
- ullet ICR must depend on the geometrical path  $oldsymbol{\xi}(t)$

Resolving i-th Pfaffian constraint for  $\phi_i$  we obtain this geometric constraint:

$$\phi_{i} = h_{i}(\boldsymbol{\xi}, \dot{\boldsymbol{\xi}}) = \arctan\left(\frac{-\sin\theta\dot{x} + \cos\theta\dot{y} + P_{i,x}\dot{\theta}}{\cos\theta\dot{x} + \sin\theta\dot{y} - P_{i,y}\dot{\theta}}\right)$$

## A general kinematic model

The implicit kinematic model can be reduced

$$\begin{bmatrix} -\sin(\theta + \phi_1) & \cos(\theta + \phi_1) & \Delta_1 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{\phi}_1 \end{bmatrix} = 0$$

$$\boldsymbol{q} = \begin{bmatrix} x & y & \theta & \phi_1 \end{bmatrix}^T$$

To be used with these geometric constraints:

$$\phi_i = h_i(\boldsymbol{\xi}, \dot{\boldsymbol{\xi}}), \quad i = 2, \dots, n_s$$

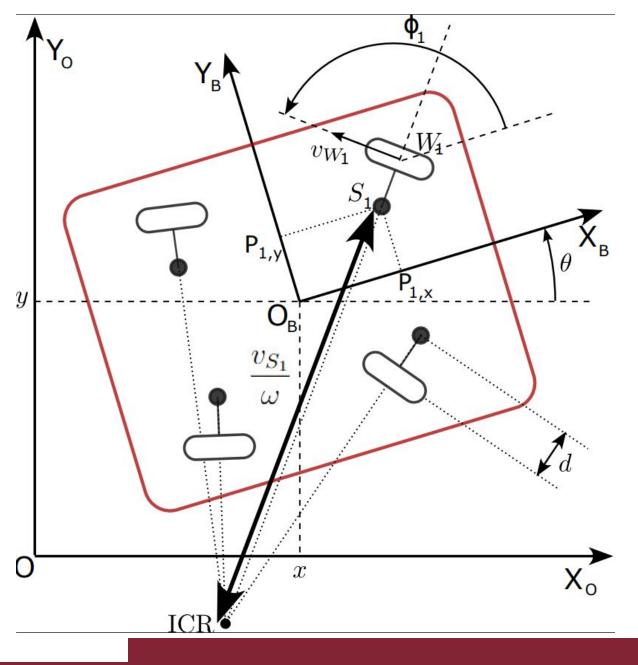
#### **Explicit general kinematic model**

$$\dot{q} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{\phi}_1 \end{bmatrix} = \begin{bmatrix} \cos(\theta + \phi_1) \\ \sin(\theta + \phi_1) \\ 0 \\ 0 \end{bmatrix} v_{S_1} + \begin{bmatrix} P_{1,x} \sin(\theta) + P_{1,y} \cos(\theta) \\ -P_{1,x} \cos(\theta) + P_{1,y} \sin(\theta) \\ 1 \\ 0 \end{bmatrix} \omega + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} v_{\phi_1}$$

- ullet  $v_{S_1}$  velocity of the point  $S_1$  in the wheel frame
- ullet  $\omega$  angular velocity of the platform
- ullet  $v_{\phi_1}$ steering velocity of the wheel  $W_1$

The driving velocity of  $W_1$  can be evaluated as:

$$v_{W_i} = v_{S_i} + d(\dot{\theta} + \dot{\phi}_i)$$



ICR on the  $W_{\rm 1}$  axes with distance  $v_{S_1}/\omega$  from the joint  $S_{\rm 1}$ 

#### **Coordinating functions (1)**

$$\dot{x} = v_{S_1} \cos(\theta + \phi_1) + \omega(P_{1,x} \sin \theta + P_{1,y} \cos \theta)$$

$$\dot{y} = v_{S_1} \sin(\theta + \phi_1) + \omega(-P_{1,x} \cos \theta + P_{1,y} \sin \theta)$$

$$\dot{\theta} = \omega$$

$$\dot{\phi}_1 = v_{\phi_1}$$

$$\phi_{i} = h_{i}(\boldsymbol{\xi}, \dot{\boldsymbol{\xi}}) = \arctan\left(\frac{-\sin\theta\dot{x} + \cos\theta\dot{y} + P_{i,x}\dot{\theta}}{\cos\theta\dot{x} + \sin\theta\dot{y} - P_{i,y}\dot{\theta}}\right)$$



$$\phi_i = h_i(v_{S_1}, \omega, \phi_1) = \arctan\left(\frac{v_{S_1}\sin\phi_1 + \omega(P_{i,x} - P_{1,x})}{v_{S_1}\cos\phi_1 + \omega(P_{1,y} - P_{i,y})}\right)$$

#### **Coordinating function (2)**

$$\phi_i = h_i(v_{S_1}, \omega, \phi_1) = \arctan\left(\frac{v_{S_1}\sin\phi_1 + \omega(P_{i,x} - P_{1,x})}{v_{S_1}\cos\phi_1 + \omega(P_{1,y} - P_{i,y})}\right)$$

- ullet This functions return two solutions. We need to pick that closer to the previous  $\phi_i$
- Structural singularities when ICR is located on i-th joint, and the  $\phi_i$  can have arbitrary orientation.

Imposing velocity of  $S_i$  in the wheel frame  $W_i$  different from zero during the path in order to prevent the joints to be ICR

$$v_{S_i} = \begin{bmatrix} \cos(\theta + \phi_i) \\ \sin(\theta + \phi_i) \end{bmatrix}^T \dot{\mathbf{o}}_{S_i} \neq 0$$

# Dynamic extension of general kinematic model

$$\dot{x} = v_{S1}\cos(\theta + \phi_1) + \omega(P_{1,x}\sin\theta + P_{1,y}\cos\theta), 
\dot{y} = v_{S1}\sin(\theta + \phi_1) + \omega(-P_{1,x}\cos\theta + P_{1,y}\sin\theta), 
\dot{\theta} = \omega, 
\dot{\phi}_1 = v_{\phi_1}, \qquad \mathbf{u} = \begin{bmatrix} v_{\phi_1}, a_{S_1}, a_{\omega} \end{bmatrix}^T 
\dot{v}_{S_1} = a_{S_1}, 
\dot{\omega} = a_{\omega} \qquad \mathbf{q} = \begin{bmatrix} x, y, \theta, \phi_1, v_{S_1}, \omega \end{bmatrix}^T$$

Previous model controlled directly velocity of  $S_1$  and angular velocity of the platform, with no free evolution of the state.

#### Why this extension

- It's easier to calculate the derivative of coordinating functions (necessary for driving velocity of each wheel) having in the model directly derivative of  $v_{S_1}$  and  $\omega$
- 2. As we will see later, the linearization of this dynamic model is controllable, that is a necessary condition for KRRT\*.

Driving velocity of wheel 
$$W_i$$
:  $v_{W_i} = v_{S_i} + d(\dot{\theta} + \dot{\phi}_i)$ 

$$v_{W_i} = v_{S_i} + d(\dot{\theta} + \dot{\phi}_i)$$

#### where

$$\phi_i = h_i(v_{S_1}, \omega, \phi_1) = \arctan\left(\frac{v_{S_1}\sin\phi_1 + \omega(P_{i,x} - P_{1,x})}{v_{S_1}\cos\phi_1 + \omega(P_{1,y} - P_{i,y})}\right)$$



#### **Motion Planning**

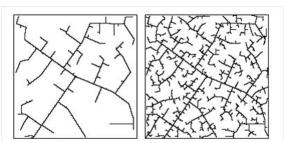
Find a collision-free motion that takes the robot from an initial to a final configuration

#### **KRRT\***

- Probabilistic method
- Robot with linear dynamics and with non-holonomic constraints
- Asymptotic optimality

#### RRT (Rapidly-exploring Random Tree)

- Probabilistic method
  - Utilize random sampling to construct a roadmap of the configuration space as a Tree T structure where the root is the initial configuration
- Probabilistically complete
- Single query
- Exploration biased towards larger Voronoi regions



- 1. Select the closest nodes  $\mathbf{Q}_{\text{neighbors}}$  to  $\mathbf{q}_{\text{new}}$  in the Tree  $\mathcal{T}$ , using a fixed radius r.
- 2. Choose the parent  $\mathbf{q}_{\text{parent}}$  of  $\mathbf{q}_{\text{new}}$  between  $\mathbf{Q}_{\text{neighbors}}$  as the node with lower cost=  $C^*(\mathbf{q}_{\text{parent}}) + c(\mathbf{q}_{\text{parent}}, \mathbf{q}_{\text{new}}) \text{ and such that the segment between } \mathbf{q}_{\text{parent}} \text{ and } \mathbf{q}_{\text{new}}$ is free of collisions.
- For each node q<sub>near</sub> in Q<sub>neighbors</sub> if its current cost is higher than the cost of reaching it passing from the newly added node (and the segment between the two is free of collision) update its parent and its cost.
- Add q<sub>new</sub> to T.

#### RRT\*

- RRT extension
- Use of a cost function
- Update the costs in the tree at each iteration
- Asymptotically optimal

#### KRRT\*

- RRT\* extension for more complex dynamics
- Builds a tree of trajectories in the free configuration space, rooted in the initial configuration
- Optimall connection of any pair of states, with a fixed-final-state free-final-time controller
- Probabilistic complete
- Asymptotically optimal

# Algorithm for optimally connecting two states

Applied to controllable linear system of this type:

$$\dot{\boldsymbol{q}}(t) = \boldsymbol{A}\boldsymbol{q}(t) + \boldsymbol{B}\boldsymbol{u}(t) + \boldsymbol{c}$$

#### Definition of trajectory of the system

$$\boldsymbol{\pi} = (\boldsymbol{q}(), \boldsymbol{u}(), \tau, c)$$

 $\tau$  is the total time of the trajectory

$$\boldsymbol{q}:[0,\tau]\to\boldsymbol{Q}$$

where

$$Q = \mathbb{R}^n$$

$$\boldsymbol{u}:[0,\tau]\to\boldsymbol{U}$$

where

$$U = \mathbb{R}^m$$

Cost of trajectory:

$$c(\boldsymbol{\pi}) = \int_0^{\tau} (1 + \boldsymbol{u}(t)^T \boldsymbol{R} \boldsymbol{u}(t)) dt$$
  $\boldsymbol{R} \in \mathbb{R}^{m \times m}$ 

#### **Objective:**

Given  $q_0$  and  $q_1$  and a controllable linear system, Finding the best trajectory connetting  $q_0$  and  $q_1$  that minimize the cost function c\* both in terms of control efforts and time  $\tau^*$  that are in a trade off relationship

For arbitrary  $\tau$  the best control policy is:

$$\boldsymbol{u}(t) = \boldsymbol{R}^{-1}\boldsymbol{B}^T \exp\left(\boldsymbol{A}^T(\tau-t)\right) \boldsymbol{d}(\tau)$$
 where

$$\boldsymbol{d}(\tau) = \boldsymbol{G}(\tau)^{-1} (\boldsymbol{q_1} - \boldsymbol{\bar{q}}(\tau))$$

#### **Differential equations**

G(t) (called weighted controllability matrix) is the solution to this Lyapunov equation:

$$\dot{G}(t) = AG(t) + G(t)A^{T} + BR^{-1}B^{T}, \quad G(0) = 0.$$

If the system is controllable, then G(t) is always positive-definite and then invertible

 $\bar{q}(t)$  (called free evolution of the state) is the solution to this differential equation:

$$\dot{\bar{q}}(t) = A\bar{q}(t) + c, \quad \bar{q}(0) = q_0.$$

## How to find $au^*$

$$\boldsymbol{u}(t) = \boldsymbol{R}^{-1} \boldsymbol{B}^T \exp \left( \boldsymbol{A}^T (\tau - t) \right) \boldsymbol{d}(\tau)$$



$$c(\boldsymbol{\pi}) = \int_0^{\tau} (1 + \boldsymbol{u}(t)^T \boldsymbol{R} \boldsymbol{u}(t)) dt$$

$$c(\tau) = \tau + (\boldsymbol{q_1} - \boldsymbol{\bar{q}}(\tau))^T \boldsymbol{d}(\tau)$$

$$\boldsymbol{d}(\tau) = \boldsymbol{G}(\tau)^{-1}(\boldsymbol{q_1} - \boldsymbol{\bar{q}}(\tau))$$

## Properties of c( au)

$$c(\tau) = \tau + (\boldsymbol{q_1} - \bar{\boldsymbol{q}}(\tau))^T \boldsymbol{d}(\tau)$$

$$\boldsymbol{d}(\tau) = \boldsymbol{G}(\tau)^{-1}(\boldsymbol{q_1} - \boldsymbol{\bar{q}}(\tau))$$

- ullet c( au)can have multiple local minima
- $c(\tau)$ >  $\tau$  for all  $\tau$ >0 being G(t) positive-definite

$$c(\tau)$$
=  $\tau$  + positive num.

We can study this function to find  $au^*$  that minimizes cost function

## Global minima of c( au)

To find the value of  $\mathcal{T}$  that globally minimizes the cost function, we can utilize the secondary properties of  $c(\tau)$  to monitor the value of  $\mathbf{c}^*$  during the forward integration loop of  $\dot{\mathbf{G}}(t)$  and  $\dot{\mathbf{q}}(t)$  using the 4th-order Runge-Kutta method. The value  $\mathbf{c}^*$  is guaranteed to be a global minimum when the iterative  $\mathcal{T}$  exceeds  $\mathbf{c}^*$  and then can no longer decrease.

#### **Algorithm 1** Forward Integration of $\dot{\boldsymbol{G}}(t)$ and $\dot{\boldsymbol{q}}(t)$

```
1: \tau, k = 0
 2: G[0] = 0
 3: \bar{q}[0] = q_0
 4: c^* = \infty
 5: \Delta t = 0.1
 6: h = \Delta t
 7: while \tau < c^* do
 8: \tau \leftarrow \tau + \Delta t
 9: k \leftarrow k + 1
10: \bar{\boldsymbol{q}}[k] \leftarrow \bar{\boldsymbol{q}}[k-1] + RK4(\dot{\bar{\boldsymbol{q}}}, \bar{\boldsymbol{q}}[k-1], h)
11: \boldsymbol{G}[k] \leftarrow \boldsymbol{G}[k-1] + RK4(\dot{\boldsymbol{G}}, \boldsymbol{G}[k-1], h)
12: c[\mathbf{k}] \leftarrow \tau + (\mathbf{q_1} - \bar{\mathbf{q}}[\mathbf{k}])^T \mathbf{G}[\mathbf{k}]^{-1} (\mathbf{q_1} - \bar{\mathbf{q}}[\mathbf{k}])
        if c[k] < c^* then
13:
          c^* \leftarrow c[\mathbf{k}]
14:
           \tau^* \leftarrow \tau
15:
             k^* \leftarrow k
16:
             end if
17:
18: end while
19: d(\tau^*) = G[k^*]^{-1}(q_1 - \bar{q}[k^*])
```

- Estimation of G(t)  $\bar{q}(t)$  and c(t) every  $k\Delta t$  seconds
- Monitoring step-by-step value of c(t) and c\*
- h is the interval of time used in 4-th order Runge kutta method
- Global minimal when \(\tau>c\*\) found until now

$$egin{aligned} oldsymbol{u}(t) &= oldsymbol{R}^{-1} oldsymbol{B}^T oldsymbol{\exp}\left(oldsymbol{A}^T ( au^* - t)
ight) oldsymbol{d}( au^*) \ \hline \mathbf{y}(\mathbf{t}) \end{aligned}$$

y(t) is the solution to this differential equation:

$$\dot{\boldsymbol{y}}(t) = -\boldsymbol{A}^T \boldsymbol{y}(t), \quad \boldsymbol{y}(\tau^*) = \boldsymbol{d}(\tau^*)$$

Substituting the optimal control policy in the linear system:

$$\dot{q}(t) = Aq(t) + BR^{-1}B^{T}y(t) + c, \quad q(\tau^{*}) = q_{1}$$

#### **Composite differential equation**

$$\begin{bmatrix} \dot{\boldsymbol{q}}(t) \\ \dot{\boldsymbol{y}}(t) \end{bmatrix} = \begin{bmatrix} \boldsymbol{A} & \boldsymbol{B}\boldsymbol{R}^{-1}\boldsymbol{B}^T \\ \boldsymbol{0} & -\boldsymbol{A}^T \end{bmatrix} \begin{bmatrix} \boldsymbol{q}(t) \\ \boldsymbol{y}(t) \end{bmatrix} + \begin{bmatrix} \boldsymbol{c} \\ \boldsymbol{0} \end{bmatrix} \begin{bmatrix} \boldsymbol{q}(\tau^*) \\ \boldsymbol{y}(\tau^*) \end{bmatrix} = \begin{bmatrix} \boldsymbol{q}_1 \\ \boldsymbol{d}(\tau^*) \end{bmatrix}$$

Integration backward in time through 4-th order Runge kutta method to obtain q(t) and y(t) estimated every  $k\Delta t$  seconds

$$\boldsymbol{u}(t) = \boldsymbol{R}^{-1} \boldsymbol{B}^T \boldsymbol{y}(t)$$

## Wrap up of the algorithm

#### **Input:**

- Linear Controllable system
- $q_0$  and  $q_1$

#### **Output:**

Optimal trajectory in terms of time and control effort

$$\pi^* = (q(t), u(t), \tau^*, c^*)$$

where

$$q(0) = q_0 \text{ and } q(\tau^*) = q_1.$$

```
Algorithm 2 Kinodynamic RRT*
  1: \mathcal{T} \leftarrow \{\mathbf{q}_{\mathrm{start}}\}
  2: \mathbf{q}_{\text{start}} \in \mathbf{Q}_{\text{free}}, \mathbf{q}_{\text{goal}} \in \mathbf{Q}_{\text{free}}
  3: for i = 1, \infty do
                Randomly sample \mathbf{q_i} \in \mathbf{Q}_{\text{free}}
  4:
               \mathbf{q} \leftarrow \arg\min_{\{\mathbf{q} \in \mathcal{T} | c^*[\mathbf{q}, \mathbf{q_i}] < r \land \text{COLLISIONFREE}[\pi^*[\mathbf{q}, \mathbf{q_i}]]\}} (\cos[\mathbf{q}] + c^*[\mathbf{q}, \mathbf{q_i}])
  5:
                parent[q_i] \leftarrow q
  6:
               cost[\mathbf{q_i}] \leftarrow cost[\mathbf{q}] + c^*[\mathbf{q}, \mathbf{q_i}]
  7:
               for all \{\mathbf{q} \in \mathcal{T} \cup \{\mathbf{q}_{goal}\}\}|c^*[\mathbf{q_i}, \mathbf{q}] < r \wedge \cos[\mathbf{q_i}] + c^*[\mathbf{q_i}, \mathbf{q}] < \cos[\mathbf{q}] \wedge
        COLLISIONFREE[\pi^*[\mathbf{q_i}, \mathbf{q}]] do
                       cost[\mathbf{q}] \leftarrow cost[\mathbf{q_i}] + c^*[\mathbf{q_i}, \mathbf{q}]
  9:
                       parent[\mathbf{q}] \leftarrow \mathbf{q}_i
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                end for
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                \mathcal{T} \leftarrow \mathcal{T} \cup \{q_i\}
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                                                                                     RANDOM SAMPLING
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                                                                                                                                 PARENT SELECTION
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  7:
                \mathbf{for} \ \mathbf{all} \ \{\mathbf{q} \in \ \mathcal{T} \cup \{\mathbf{q}_{\mathrm{goal}}\}\} | c^*[\mathbf{q_i}, \mathbf{q}] \ < \ r \ \land \ \mathrm{cost}[\mathbf{q_i}] \ + \ c^*[\mathbf{q_i}, \mathbf{q}] \ < \ \mathrm{cost}[\mathbf{q}] \ \land
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  5:
                parent[q_i] \leftarrow q
  6:
                                                                                                                                                                             REWIRING
                cost[\mathbf{q_i}] \leftarrow cost[\mathbf{q}] + c^*[\mathbf{q}, \mathbf{q_i}]
  7:
                \textbf{for all } \{\mathbf{q} \ \in \ \mathcal{T} \ \cup \ \{\mathbf{q}_{goal}\}\} | c^*[\mathbf{q_i}, \mathbf{q}] \ < \ r \ \land \ \mathrm{cost}[\mathbf{q_i}] \ + \ c^*[\mathbf{q_i}, \mathbf{q}] \ < \ \mathrm{cost}[\mathbf{q}] \ \land
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                 end for
11:
                 \mathcal{T} \leftarrow \mathcal{T} \cup \{\mathbf{q}_i\}
12:
13: end for
```

## **KRRT\*** implementation

- Nearest neighbours: full tree
- Exactly arrives at the final configuration
- Collision check:
  - Footprint of the robot not collides with any obstacle
  - Inputs in the admissible ranges
  - The constraints on v<sub>si</sub> are not violated

# Linearization

## **KRRT\*** for non-linear systems

Linearization of the original system with first order taylor expansion:

$$m{A} = rac{\partial m{f}}{\partial m{q}}(m{\hat{q}}, m{0}), \quad m{B} = rac{\partial m{f}}{\partial m{u}}(m{\hat{q}}, m{0}), \quad m{c} = m{f}(m{\hat{q}}, m{0}) - m{A}m{\hat{q}}.$$

#### where

$$\dot{x} = v_{S1}\cos(\theta + \phi_1) + \omega(P_{1,x}\sin\theta + P_{1,y}\cos\theta), 
\dot{y} = v_{S1}\sin(\theta + \phi_1) + \omega(-P_{1,x}\cos\theta + P_{1,y}\sin\theta), 
\dot{\theta} = \omega, 
\dot{\phi}_1 = v_{\phi_1}, \qquad \boldsymbol{u} = \begin{bmatrix} v_{\phi_1}, a_{S_1}, a_{\omega} \end{bmatrix}^T 
\dot{v}_{S_1} = a_{S_1}, 
\dot{\omega} = a_{\omega} \qquad \boldsymbol{q} = \begin{bmatrix} x, y, \theta, \phi_1, v_{S_1}, \omega \end{bmatrix}^T$$

At the beginning of each iteration re-linearization of the system in  $\hat{q}$ = $\mathbf{q_i}$  that is the randomly sampled configuration

## Linearization for a generic point

$$\boldsymbol{B} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \boldsymbol{c} = \begin{bmatrix} \hat{v}_{S_1}(\hat{\theta} + \hat{\phi}_1)s(\hat{\theta} + \hat{\phi}_1) - \hat{\omega}\hat{\theta}(P_{1,x}c\hat{\theta} - P_{1,y}s\hat{\theta}) \\ -\hat{v}_{S_1}(\hat{\theta} + \hat{\phi}_1)c(\hat{\theta} + \hat{\phi}_1) - \hat{\omega}\hat{\theta}(P_{1,y}c\hat{\theta} + P_{1,x}s\hat{\theta}) \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

## Controllability of the resulting linearized system

The controllability matrix is:

$$\mathcal{C} = \begin{bmatrix} B & AB & A^2B & \cdots & A^5B \end{bmatrix}$$

the rank of submatrix  $\begin{bmatrix} \boldsymbol{B} & \boldsymbol{A}\boldsymbol{B} \end{bmatrix}$  is always 6 if  $v_{S_1} \neq 0$ 

This condition is always satisfied because we already discard the trajectories that do not meet it in COLLISIONFREE function

Therefore, the linear system is controllable as  $\mathcal C$  consistently maintains full rank

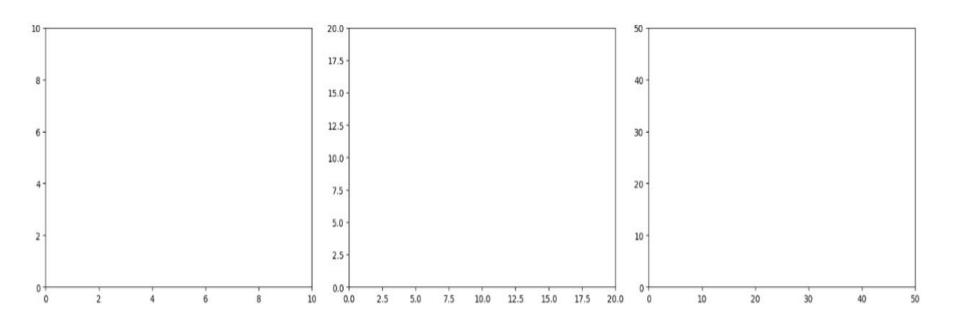
# **SIMULATIONS**

# **Maps Parameters**

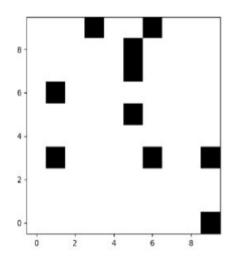
Map	Dimension	Resolution	Obstacle-probability
Small-empty	10 x 10 (m)	1 (m)	0.0
Small-few	$10 \times 10 \text{ (m)}$	1 (m)	0.12
Small-many	13 x 13 (m)	1 (m)	custom
Medium-empty	$20 \times 20 \text{ (m)}$	1 (m)	0.0
Medium-few	$20 \times 20 \text{ (m)}$	1 (m)	0.01
Medium-many	$20 \times 20 \text{ (m)}$	1 (m)	0.04
Big-empty	$50 \times 50 \text{ (m)}$	1 (m)	0.0
Big-few	$50 \times 50 \text{ (m)}$	1 (m)	0.005
Big-many	$50 \times 50 \text{ (m)}$	1 (m)	0.008

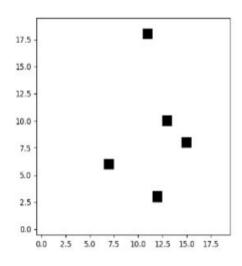
# Maps

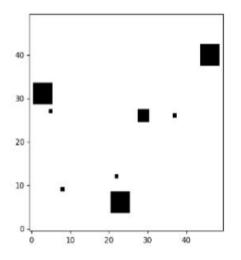
# **Empty maps**

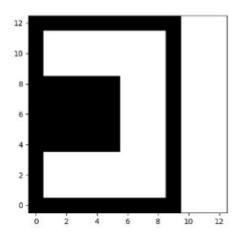


#### **Few Obstacles**

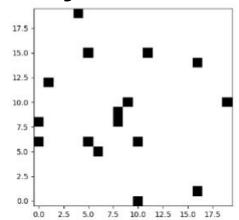


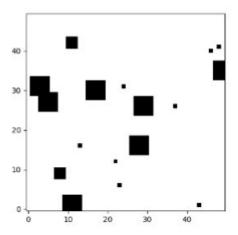






# **Many Obstacles**





# **Hyperparameters**

• We have tuned the matrix R in the following way:

$$\mathbf{R} = \begin{bmatrix} w_1 & 0 & 0 \\ 0 & w_2 & 0 \\ 0 & 0 & w_3 \end{bmatrix}$$

where  $w_1 = w_2 = 1$  and  $w_3 = 10$ 

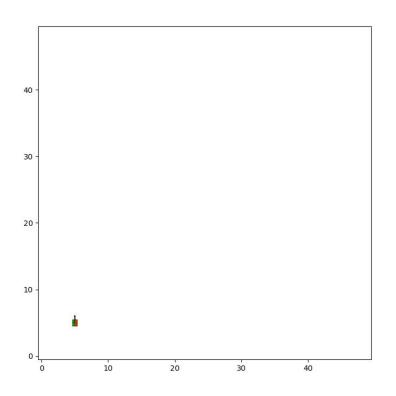
• We have constrained  $v_{s_1}$  to be always positive:

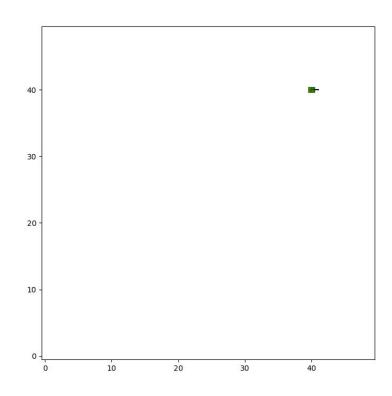
$$v_{s_1} > 0 \frac{m}{s}$$

# Simple - Hard trajectories

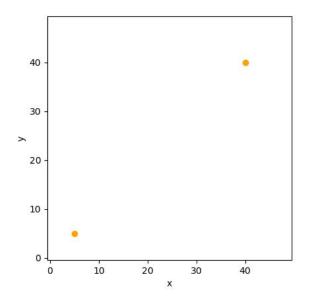
**Empty maps** 

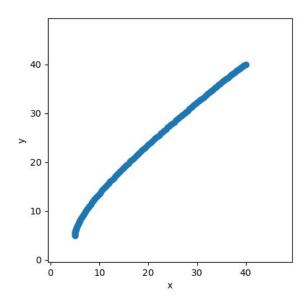
Start state =  $[5, 5, \frac{\pi}{2}, 0, 1, 0]$  Goal state = [40, 40, 0, 0, 1, 0]

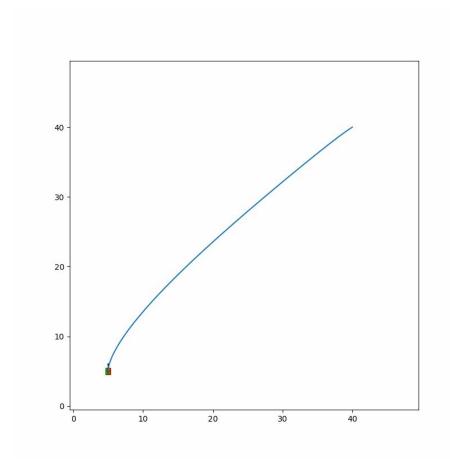


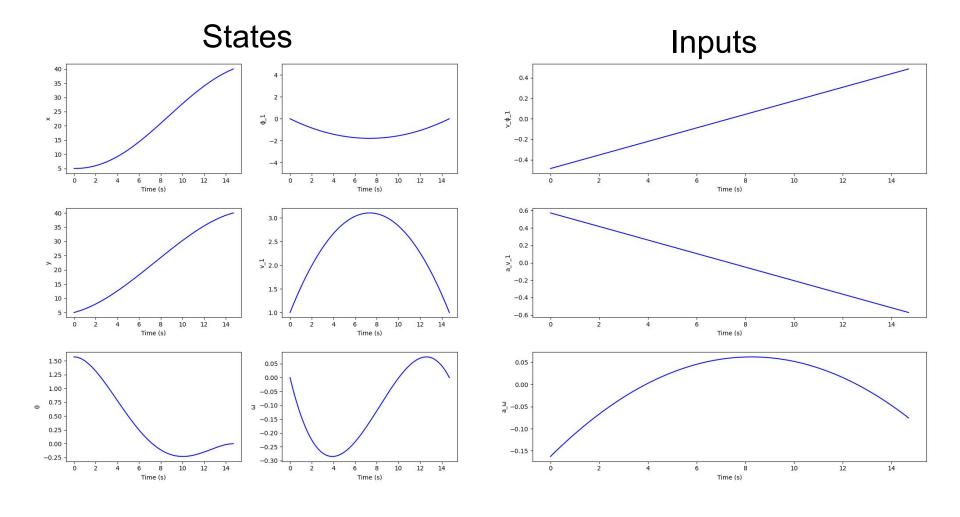


$$N = 1$$

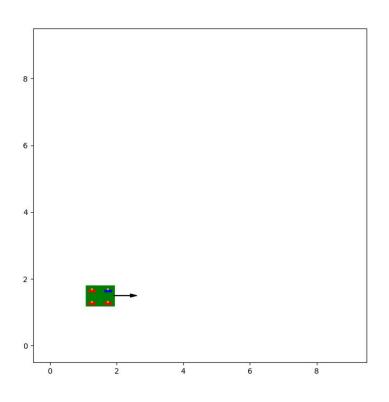


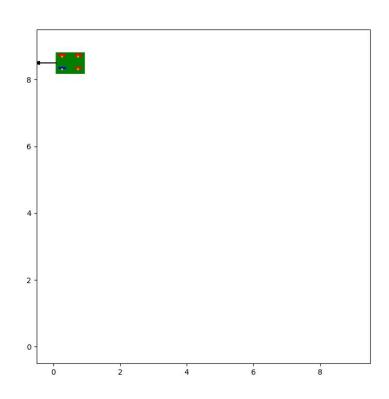




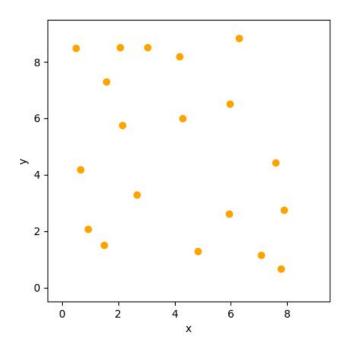


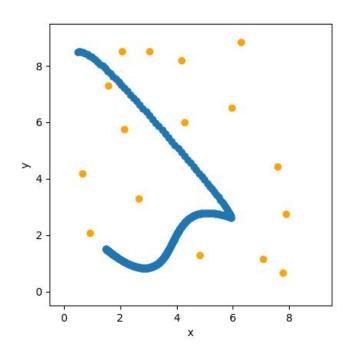
Start state = [1.5, 1.5, 0, 0, 0.01, 0] Goal state =  $[0.5, 8.5, \pi, 0, 0.01, 0]$ 

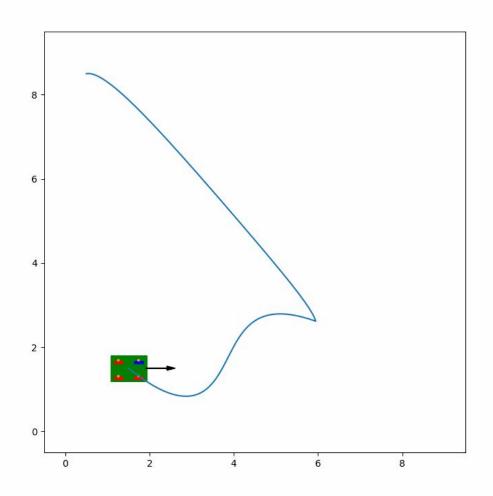




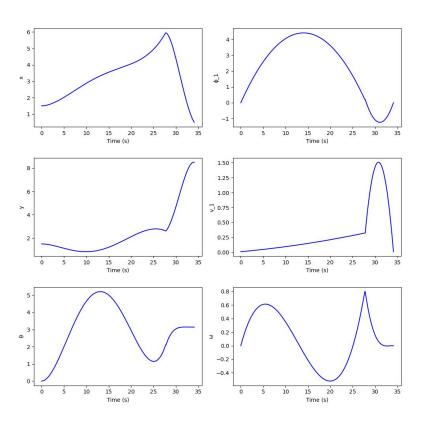
$$N = 100$$

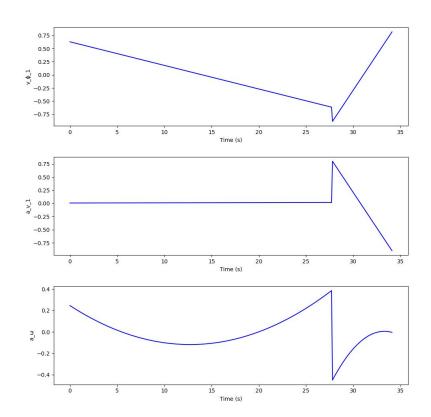






States Inputs

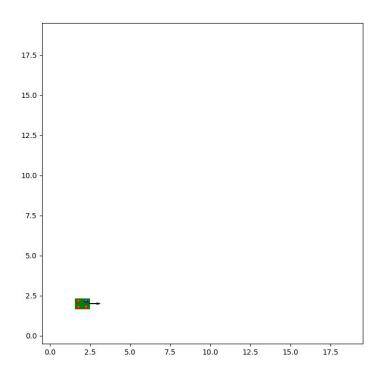


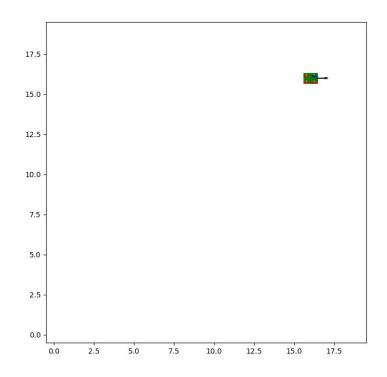


# **Different R Matrices**

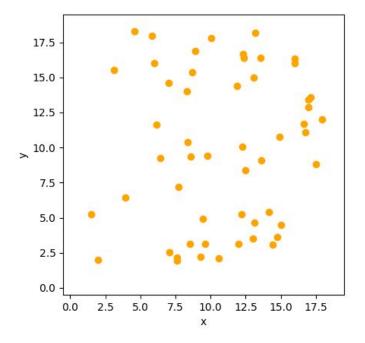
#### **Medium-empty Map**

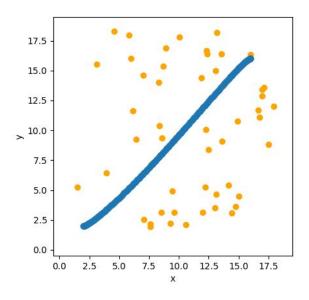
Start state = [2, 2, 0, 0, 0.1, 0] Goal state = [16, 16, 0, 0, 0.1, 0]



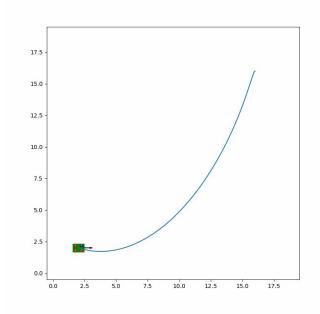


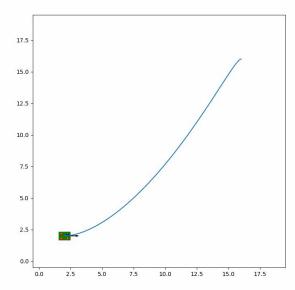
# **Medium-empty Map N** = 100

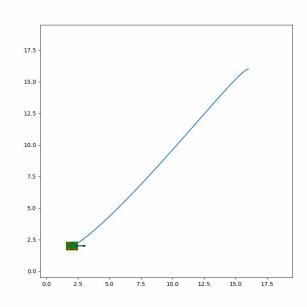




#### **Medium-empty Map**







$$w_1, w_2, w_3 = 1$$

$$w_1, w_2 = 1 \text{ and } w_3 = 10$$

$$w_1, w_2 = 1 \text{ and } w_3 = 10$$
  $w_1, w_2 = 1 \text{ and } w_3 = 100$ 

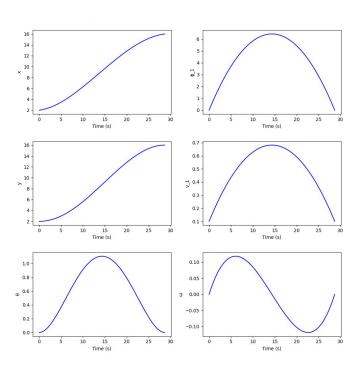
$$cost = 24$$

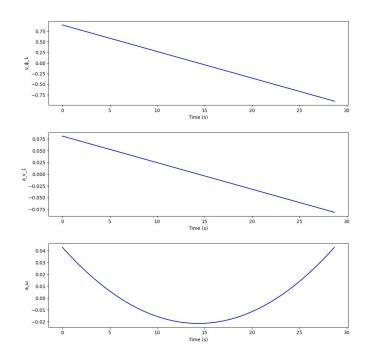
$$cost = 32$$

$$cost = 37$$

# **Medium-empty Map**

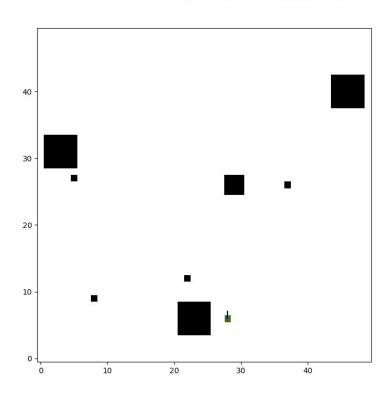
States Inputs

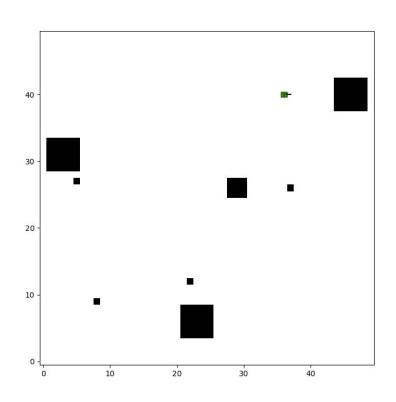




# **Forcing Nodes**

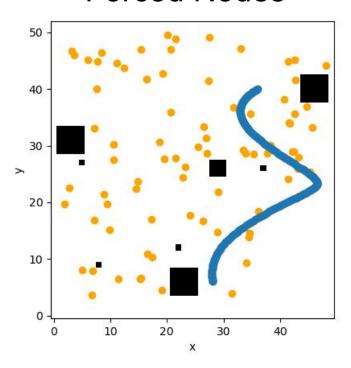
Start state =  $[28, 6, \frac{\pi}{2}, 0, 1, 0]$  Goal state = [36, 40, 0, 0, 1, 0]



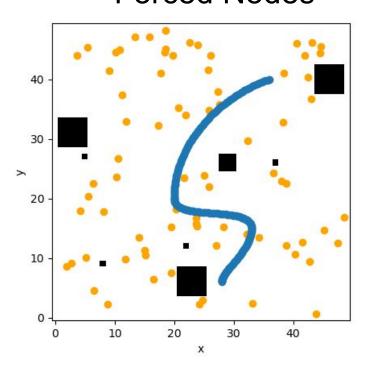


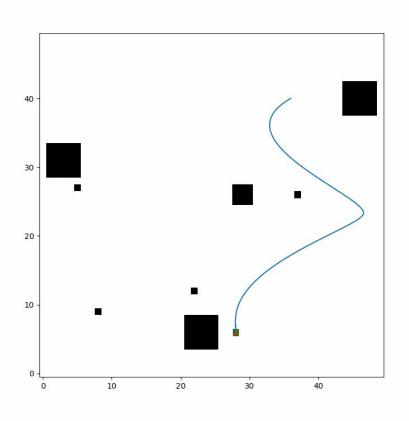
N = 100

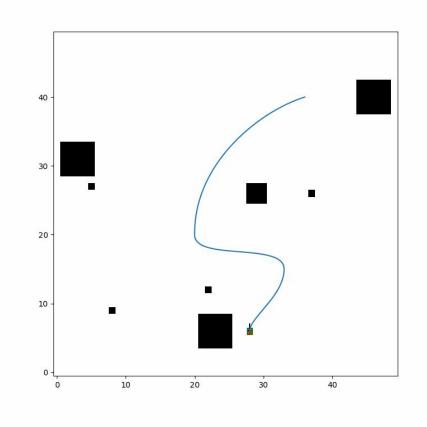
Without Forced Nodes



With Forced Nodes



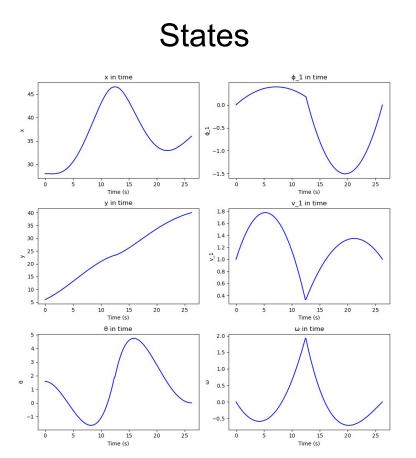




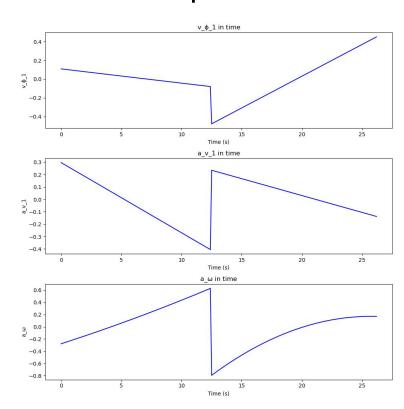
$$cost = 77$$

$$cost = 61$$

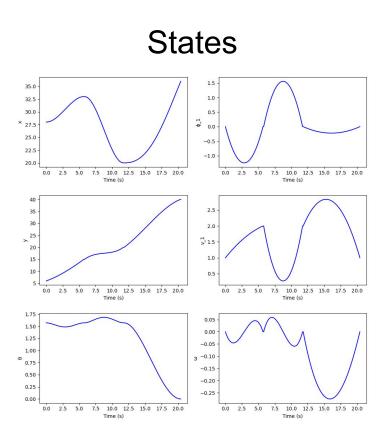
#### Without Forced Nodes

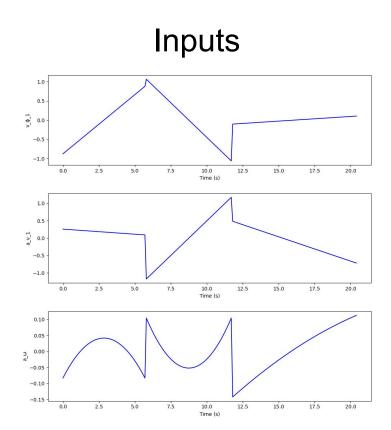


# Inputs

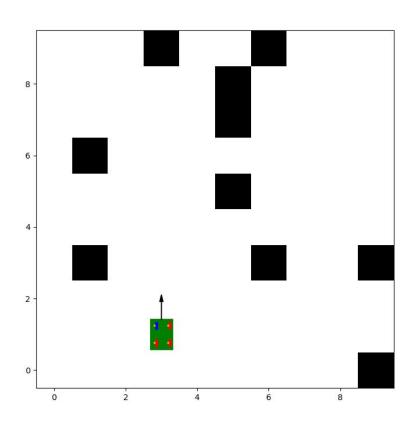


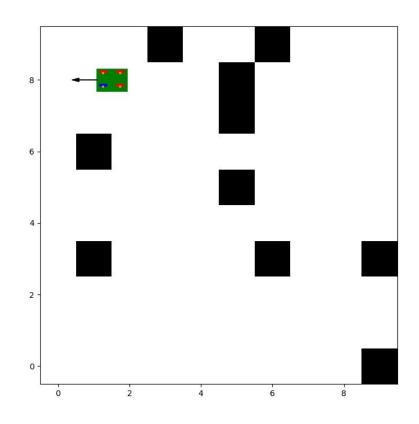
#### With Forced Nodes



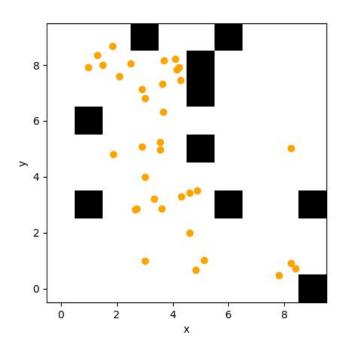


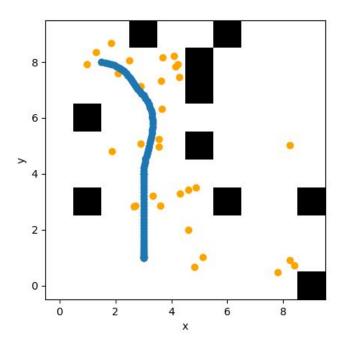
Start state =  $[3, 1, \frac{\pi}{2}, 0, 0.01, 0]$  Goal state =  $[1.5, 8, \pi, 0, 1, 0]$ 

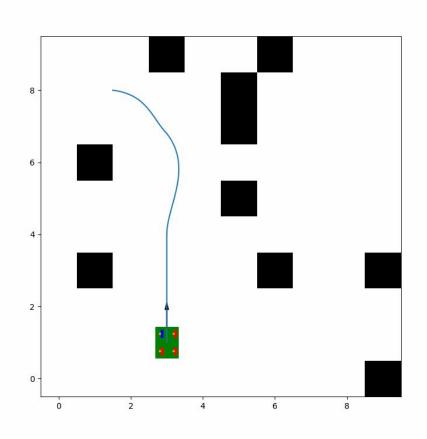


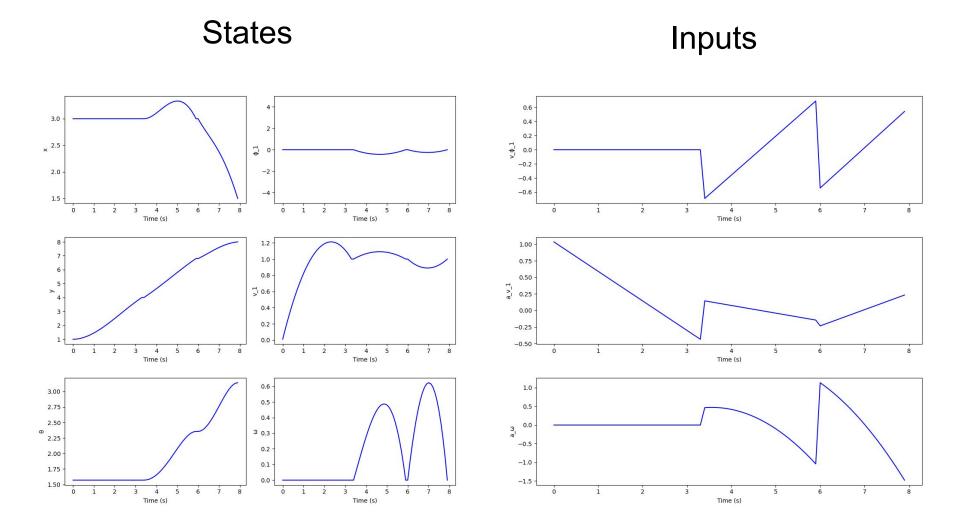


$$N = 200$$



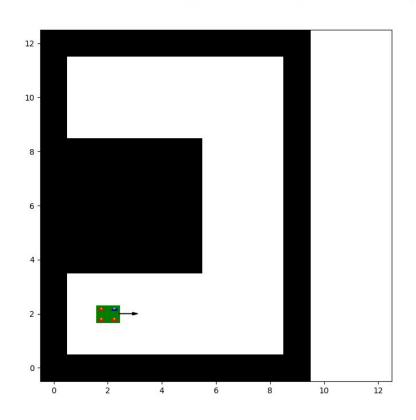


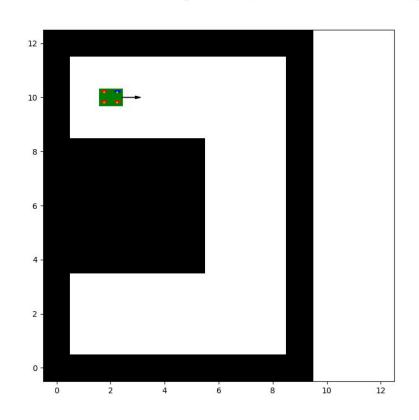




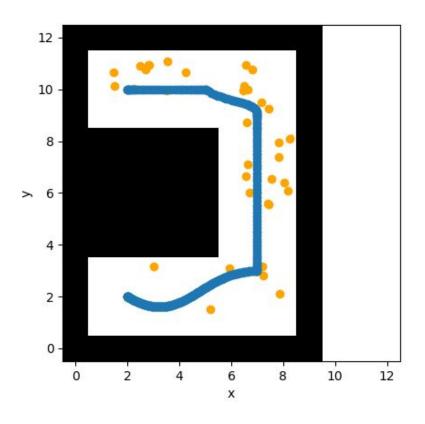
# **Custom Map**

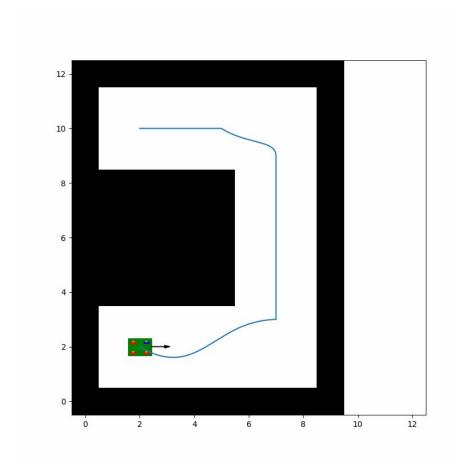
Start state = [2, 2, 0, 0, 0.01, 0] Goal state = [2, 10, 0, 0, 0.01, 0]



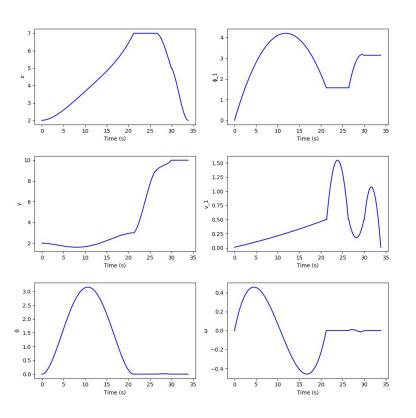


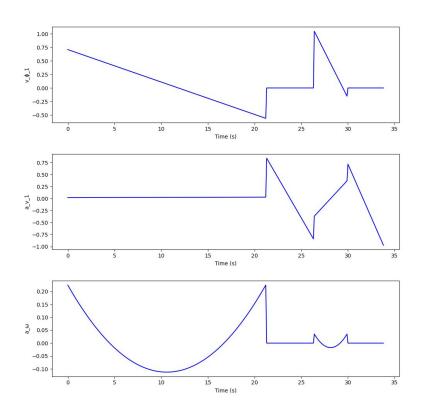
$$N = 500$$





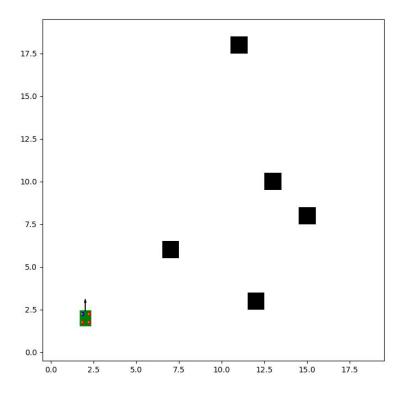
States Inputs



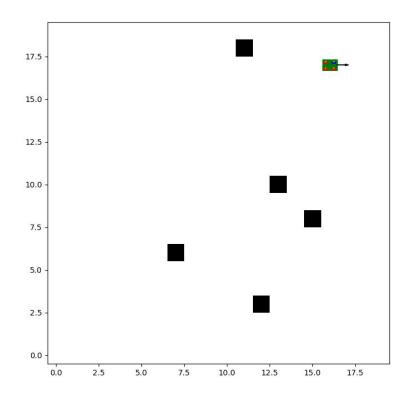


## **Other Simulations**

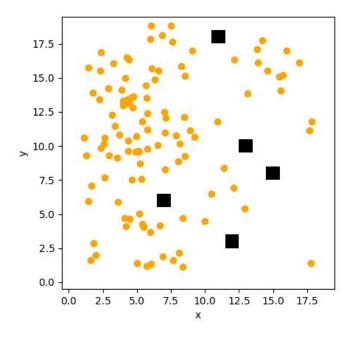
Start state =  $[2, 2, \frac{\pi}{2}, 0, 1, 0]$ 

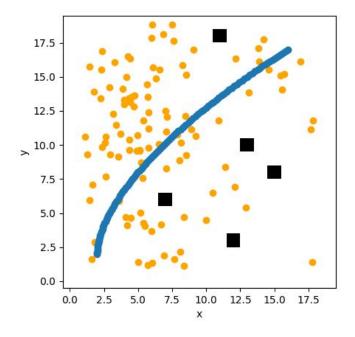


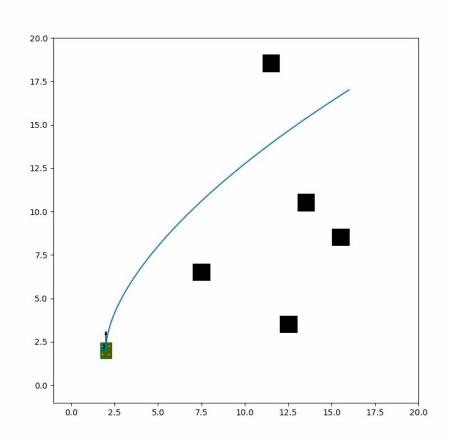
Goal state = [16, 17, 0, 0, 1, 0]

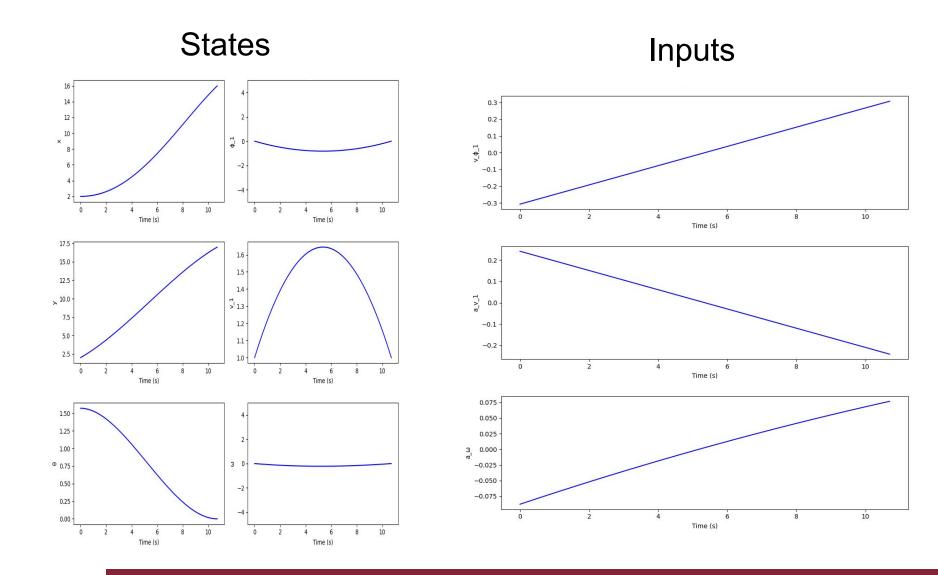


$$N = 500$$

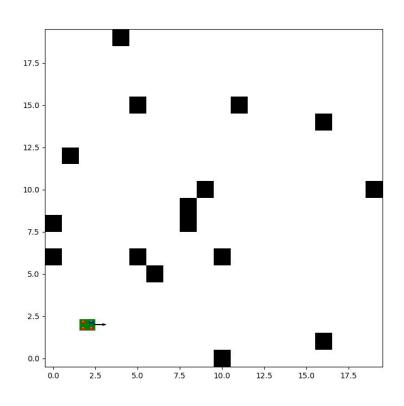


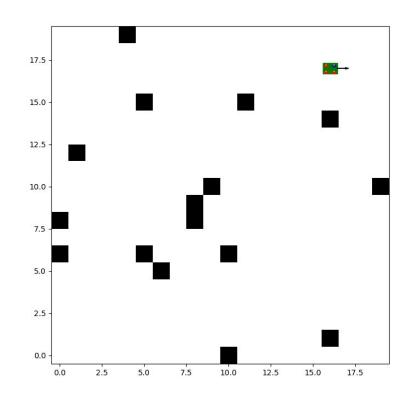




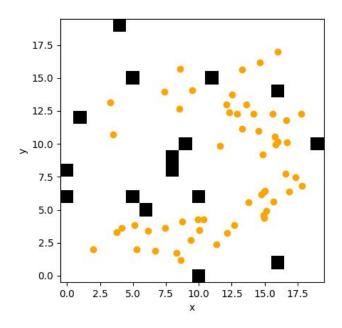


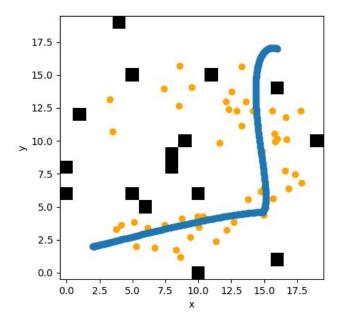
Start state = [2, 2, 0, 0, 0.1, 0] Goal state = [16, 17, 0, 0, 0.1, 0]

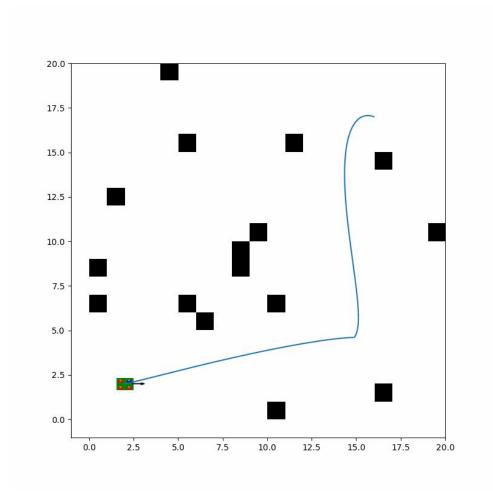




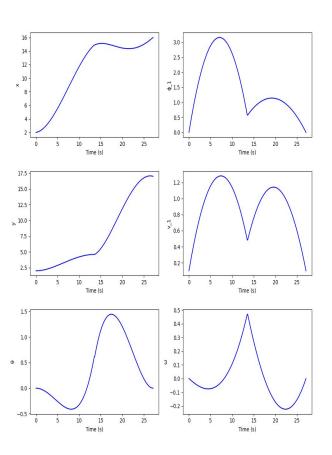
$$N = 500$$

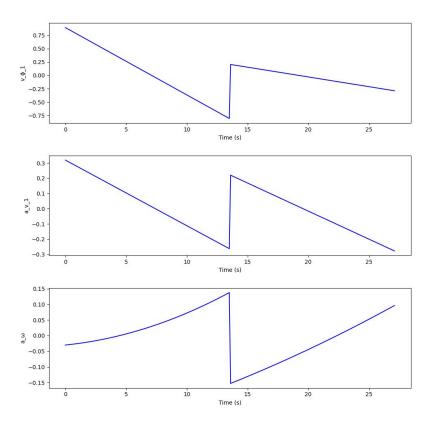




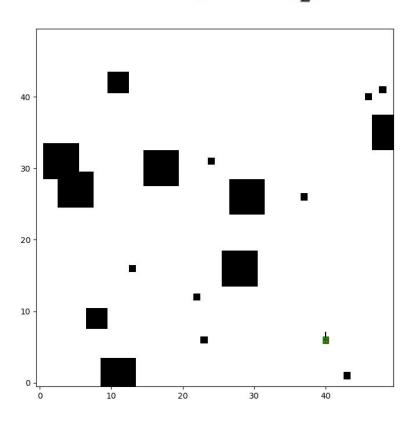


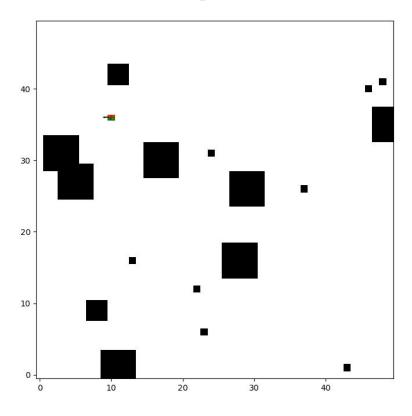
States Inputs



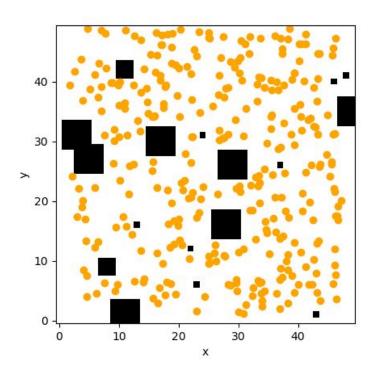


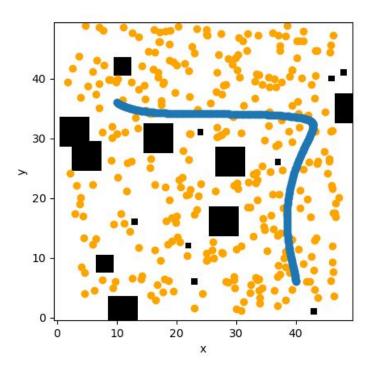
Start state =  $[40, 6, \frac{\pi}{2}, 0, 1, 0]$  Goal state =  $[10, 36, \pi, 0, 1, 0]$ 

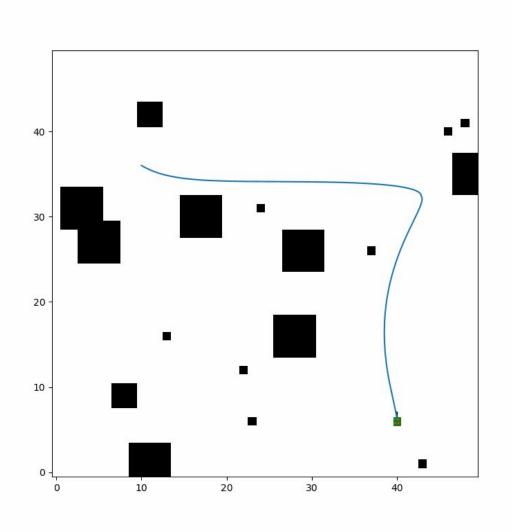




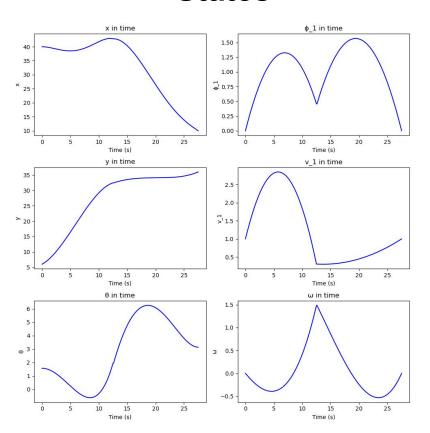
N = 500



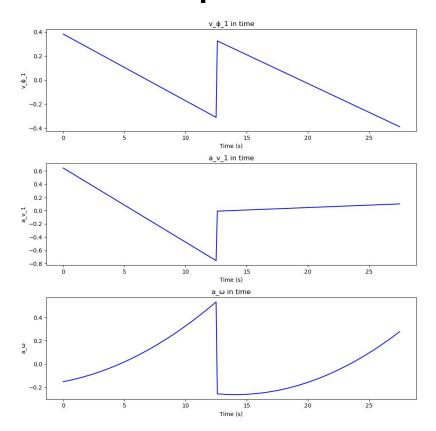




#### **States**



#### **Inputs**



### **Results**

Map	Cost	Iterations	KRRT* Time	Traj. Time	Nodes
Small-empty	84.59	100	42 (s)	33 (s)	19
Small-few	26.8	200	301 (s)	8 (s)	37
Small-many	249.69	500	1362 (s)	34 (s)	55
Medium-empty	37.51	100	367 (s)	28 (s)	53
Medium-few	13.66	500	2659 (s)	12 (s)	109
Medium-many	66.79	500	1491 (s)	28 (s)	56
Big-empty	18	1	0.12 (s)	15 (s)	2
Big-few	61.82	100	426 (s)	21 (s)	84
Big-many	64.691	500	9349 (s)	27 (s)	324

#### **Conclusions**

- Kinematic Model for SWMR
- KRRT\*
- Different R matrices
- Number of iterations
- Obstacle avoidance

#### **Future works**

- K-d tree for efficient Neighbors search
- Controller for trajectory tracking

# THANK YOU FOR YOUR ATTENTION