

# Dynamic-Flow-at-Pressure: A Potentially Useful Concept for Pandemic Ventilators

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## Abstract

NOTE: I recently learned of the existence of pressure-regulators that regulate pressure without flow. This requires a change to some of this discussion below. Mechanical ventilation must do work on the airway in order to inflate the lungs. Considering the power done on the airway may have several uses:

- Computing the maximum required power on the airway in a clinical situation provides engineers a minimum power output requirement by an air drive mechanism.
- Dynamic Flow at Pressure (DFP) is independent of the means of air production, whether by fan, blower, pump, piston, self-inflating bag-squeezer, or bellows. It therefore may serve as a unifying means of controlling air production to meet a clinical goal independent of the means of production.
- Developing a predictive model of work enables detection of work done by the patient in either in support (synchronised) or (against) the ventilator. This may help enable avoidance of problematic patient-ventilator asynchrony and enable fine tuning of ventilation patterns that encourage the patient to work with the ventilator.

By specifying an *air drive* as a modular component in a ventilator system that produces medical gases by producing flow-at-pressure into the airway according to a standardized specification and protocol, it may be possible to separate the concern of pressurized medical gas production from other

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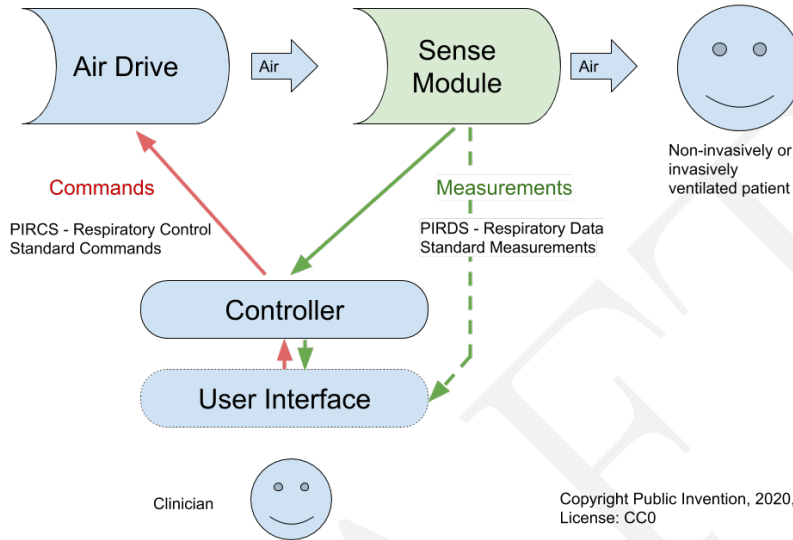


Figure 1: A Basic Modular Structure of a Ventilator

concerns of building ventilators to address the COVID-19 pandemic. This approach improves supply chain resilience by allowing air drives to be an interchangeable part with no need for extensive redesign, testing, and certification.

## 1 Introduction

*NOTE: I recently learned of the existence of pressure-regulators that regulate pressure without flow. This requires a change to some of this discussion below.*

Let us define the term *air drive* to mean the mechanism that produces air and air/oxygen/medical gas mixtures in a mechanical ventilation system. Because of the COVID-19 pandemic, many humanitarian engineering teams have experimented with squeezing inexpensive bag mask valves (BMVs), or *bag squeezers*. Other mechanisms include pistons, bellows, positive displacement pumps, which tend to produce a fixed volume against a variable pressure. Still other mechanisms such as velocity pumps, fans and blowers tend to produce a fixed pressure against a variable back-pressure leading to the injection of a variable volume. One goal in this paper is to unify these two very different mechanisms.

A second goal is to champion a modular approach to ventilator design and construction to better address the COVID-19 pandemic. As of June, 2020, many teams are independently building new ventilator designs. Cooperation and

division of labor might increase the number of lives saved. This paper proposes a means of separating the technical problem of precisely producing medical air on demand from other concerns of building a ventilator. By providing a standard interface to the “Air Drive” module of Figure 1, work on that module can proceed independent of other modules. Finally, creating air drives as a module provides supply-chain resilience.

MIT has presented a useful computation of the work that must be done on the airway for maximum patient need, from which they conclude a minimum power requirement for an air drive for mechanical ventilation[7]. Expanding on this work is a second goal of this paper.

## 2 Physical Preliminaries

Roughly speaking, volume times pressure is work. To inject an infinitesimal amount of air in to any air vessel or across any air threshold, the work is the product of the pressure in at the threshold and the volume injected. A threshold into a vessel of fixed size is easy to analyze. A vessel such as a balloon whose volume is dependent on internal pressure is slightly more complicated. A rubber balloon has a *compliance* which is defined to be the change in volume with a change in pressure.

A human lung system is even more complicated, because it has both static and dynamic compliance[10].

Nonetheless, if we use a simplified model, work done over time on an airway is the integral over time of injected volume multiplied by pressure, where both injected volume and pressure are a function of time.

If pressure in the airway is a constant  $p$  pascals, a machine which produces a flow of  $f$  cubic meters per second, the machine is performing  $p \cdot f$  watts on the airway.

## 3 Ventilation Modes

Mechanical ventilators offer a number of control modes, broadly divided into pressure-controlled and volume-controlled modes. Modern ventilators typically also provide modes that attempt to support, synchronise with, the patients’ own respiratory efforts. They patient may fight against the action of the ventilator, called dys-synchrony. However, if we disregard this clinically important problem, the modes are simple.

Pressure control mode create inspiration by providing air at an approximately fixed pressure for a fixed period of time. In response the flow rate reduces over the course of the inspiratory phase and lungs fill up and compliance reduces. Volume control mode pushes air at a constant flow rate for a predetermined length of time, thus delivering a specified volume with each breath. As a result the pressure within the system gradually increases to potentially

variable peak pressure unless a preset but limited to some maximum pressure is achieved.

Volume control mode is easy to achieve with a piston which is powerful enough: use the piston to push the desired volume of air out of a cylinder and into the airway. (A weak piston might not be able to do this.) In so doing we may control the speed of this push which will somewhat control the pressure. A positive-displacement pump with a small chamber may be pumped many times to achieve the desired volume; in this say a piston and positive-displacement pump are similar.

## 4 Human Breathing Requirements

The ranges of pressures, flows, and volumes and the precisions with which they must be controlled to ventilate a sick human being may surprise mechanical engineers, and help us contextualize the problem. Healthcare workers generally use cm  $H_2O$  as measure of physiological pressures.

For the designer of pandemic response ventilators, the maximum pressure, flow and respiration rate the machine should support is of critical importance. General medical consensus is:

- Maximum ventilation volume in one minute is 10 liters (typically 6 liters). (Note: A large healthy person exercising heavily may have a normal minute ventilation of 40 liters, but an ill person cannot need that much ventilation.)
- Maximum pressure needed to for ventilation is 45 cm  $H_2O$  [6, 1, 9]. (Note: 80 cm  $H_2O$  may be used test equipment, but not on a patient. The UK HRMA Rapidly Manufactured Ventilator standard mentions 35 cm  $H_2O$  maximum with a 70 cm  $H_2O$  in exceptional circumstances [8].)
- The Australian government recommends a maximum instantaneous flow rate of 100 liters per minutes [9].<sup>1</sup>
- A high-oxygen environment should be assumed. Engineers need to plan for anything in contact with medical air to be safe at 50% or 100% fractional oxygen ( $F_{iO_2}$ ).
- A maximum respiratory rate of 30 breaths per minute [8].
- Maximum ratio of Inspiration to Expiration (I:E) is 1:1, and generally its is 1:2 or 1:3, with a minimum of 1:5.

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<sup>1</sup>Much higher instantaneous flow rates have been observed in healthy individuals exercising heavily [3]. It also notes that respirators National Institute for Occupational Safety and Health's respirator test standards of 64, 85, and 100 L/min constant flow were often exceeded in these circumstances. Presumably instantaneous flows higher than 100 L/min are not needed in very sick people.

## 5 Power Calculation

The inspiring MIT E-Vent Power calculation[7] performs a pressure-based evaluation, because the Ambubag is guaranteed to have a volume greater than tidal volume (800ml) they apply.

However, by considering maximum needs, the problem is simplified. In mechanical ventilation, we can choose a maximum pressure of 50 cm H<sub>2</sub>O and maximum momentary flow rate of 100 liters per minute. (This may be a conservative overestimate of the maximum power ever needed in a medical emergency.) Converting to SI units, we convert the pressure of 45cmH<sub>2</sub>O to 4413 Pa and 100 lpm to 0.0017 cubic meters per second. The maximum momentary power on the airway required is the product, 7.355 watts. (To convert  $x$  cmH<sub>2</sub>O at a flow rate of  $y$  lpm, calculate  $x \cdot y \cdot 0.00163433333$  watts) Following the MIT team, we can conclude, for this choice of clinical conditions, any machine must provide at least 7.35 watts of power instanaously.

Note however, that that is a maximum instantaneous power of breathing. Because of the I:E ratio which corresponds to a duty cycle for the machine and because under normal conditions the breathing pressure will be much lower than 45 cm H<sub>2</sub>O, the power of breathing over a full minute maybe 200 times lower:

In a normal person, at rest the work of breathing is about 0.35 J/L, and the power of breathing is about 2.4 J/min (0.04 watts)[5].

## 6 Flow-at-Pressure is Power-on-the-Airway

Any real physical machine produces flow which is partially dependent on the pressure it is working against. Therefore a machine may be thought of as producing flow  $F$  as a function of pressure  $p$ ,  $F(p)$ . It is difficult to precisely and safely control ventilation without knowing the pressure  $p$  in the airway due to the extreme danger of barotrauma. Because flow times pressure is power, a machine producing  $F(p)$  on an airway at pressure  $p$  is doing  $F(p) \cdot p$  watts. In a real system during an inspiration of length  $l$ , both the flow and pressure will vary with time. Representing this as a subscript, the work of breathing  $W$  is the integral over time of this product:

$$W = \int_0^l F_t(p_t) \cdot p_t dt \quad (1)$$

This relationship between instantaneous flow and power is so tight we one can interchagably think in terms of Dynamic Flow at Pressure or Power-on-the-Airway. Power-on-the-airway has the advantage of being more relevant to mechanical engineers when operating on certain direct power devices. Flow-at-pressure makes more sense when considering pressure-release devices. It is important to note that clinicians should never need to know about this standard. We hope to insulate the doctor and patient from this decision, just as at some level they do not know or care what voltage is used internally by a device.

## 7 Practical Air Drive Components

Air flow may be produced by three basic mechanisms practical for addressing the pandemic.

- Pressure producing devices:
  - Fans and blowers
  - Centrifugal pumps
- Volume producing devices:
  - Positive displacement pumps
  - BMV squeezers
  - Pistons
  - Bellows
- Pressure releasing devices:
  - Electronically controlled valves,
  - Fluidically controlled devices.

### 7.1 Pressure Producing Devices

Pressure producing devices include fans, blowers, and centrifugal pumps, which all use a rotary motor to spin blades. They differ in blade configuration and housing.

In practice, the datasheets of fans show the flow of air they proceed against a given pressure. At some pressure, this flow drops to zero. In general, fans provide high flow but develop low pressure. They are generally unsuitable for respiration, which requires lower flow and higher pressure compared with most applications.

Note the following language from the RespiroWorks team addresses the problem directly [4]:

“Our design centers around a low inertia centrifugal blower, currently sourced from CPAP machines. These brushless fans with lifetime lubricated bearings can spin to high speeds very quickly, allowing a fine degree of time-resolved pressure control. At the same time, they can develop pressures well above 40 cmH<sub>2</sub>O; even accounting for flow losses, our test model exceeds 100 cmH<sub>2</sub>O.”

“One of our main assumptions is that access to CPAP blowers will be uninterrupted. We believe both that they are sourced in large quantities (the vendors we’ve contacted in China have more than 5,000 in stock), and that they do not present manufacturing difficulties (fundamentally, it is only three injection molded parts and a brushless DC motor).”

One firm, AirFan, [2], makes fans for ventilators using a low-inertial centrifugal pump.

## 7.2 Volume Producing Devices

The world is full of positive-displacement pumps and compressors. Diaphragm pumps are particularly suited because the airway is contained. Typical compressors fill tanks or tires to at least  $35 \text{ psi} = 2460.74 \text{ cm H}_2\text{O}$ , about 50 times more than the highest medical breathing pressures of  $50 \text{ cm H}_2\text{O}$ . A typical compressor to produce a 250 lpm flow (10 cubic feet per minute) costs more than \$200 and requires more than 1 horsepower (746 watts).

This typical pressure-too-high and flow-too-low situation may be why many teams have turned to using BMV squeezers, pumps and bellows, which can be considered positive-displacement pumps with an exceptionally large displacement that is pumped only once per breath. These devices have the apparent advantages of visible simplicity and supply-chain resilience.

A piston presents the problem of producing a reasonably tight seal without adding harmful lubricants into the high-oxygen airway. However, since breathing pressures are low, this may be a surmountable problem. A bellows with a flexible chamber, usually constrained to remain within a fixed volume, is another alternative. Both approaches tend to have simple geometries in which the change in volume can be easily calculated as a function of the change in the piston of fixed part of the bellows, making it straightforward to compute flow and therefore power-on-the-airway as a function of the position of the motive element.

On the other hand, a bag-squeezer produces difficult to model dynamic geometry changes which may be highly dependent on potentially changing elasticity and deformability of the bag material. It may not be possible to compute change in volume easily. The MIT paper suggest that power applied to the bag produces power on the airway in rough proportion, but the constant of proportionality may change during the squeezing action. However, it is easy enough to simply measure the volume as a function of the position of the squeezing apparatus, and thus to use an MCU to produce accurate power-on-the-airway when demanded. It is difficult to see how a bag-squeezer could provide precise control of any kind without either careful calibration or adaptive control based on rapid pressure measurements [Giseburt].

## 7.3 Pressure Releasing Devices

- Pressure releasing devices:
  - Electronically controlled valves,
  - Fluidically controlled devices.

A relatively common approach to ventilation is to assume a source of high-pressure air and control the release of this air into the airway with a solenoid

valve. This has even been done with pure fluidic control which has no moving parts by directing a flowing airstream into or away from the patient.

In such cases the power-on-the-airway is unrelated to power consumed by operation of the valve, and depends on the pressure and flow from the pressurized source. However, this is irrelevant to the control system.

## 7.4 Summary

To be supply-chain resilient, we would prefer to use commonly available parts. In general, fans produce too much flow and not enough pressure, and pumps produce too much pressure and not enough flow. This may be one of the reasons for preponderance of “bag squeezer” designs in pandemic ventilator projects. Some blowers designed specifically for CPAP machines have performance better matched to the breathing task. These may present supply-chain resilience problems.

## 8 Building an Air Drive

If a blower or centrifugal pump is used as the mechanism of an air drive and the speed of the blower or pump can be controlled by voltage, and air drive could consist of the blower, a means of digitally controlling voltage or pulse-width-modulation (PWM), an MCU to receive and interpret commands, and a map of the voltage or PWM required to produce a given flow/power at all allowable pressures. Such an air drive does not need a sensor. It simply a command in terms of watts, calls a subroutine to look up the voltage in a table or compute it via interpolation or some formula, and outputs the voltage control.

A positive displacement pump would be different. Generally any such pump produces a stable, known volume displacement with each stroke or rotation. The air drive would take its command in watts, divide the pressure sent by the controller to obtain the desired flow and then operate itself at a rate necessary to produce the desired flow.

A pressure gating valve would require that the pressure in the tank be known and the behavior of a valve be completely understood, but in principle it would also compute a desired flow and operate the valve to achieve that flow. It might, instead, have its own flow sensor and quickly adjust flow rate to the desired value by its own devices.

The whole point of the air drive is that the effect of all these machines will be unimportant or even unobservable to doctor and patient. It will not matter to them how the work is done.

## 9 Specification of a Power-on-the-airway Air Drive

Conceptually an air drive is a gas-pushing device which can be controlled moment-to-moment in a closed control loop by specifying two values:



- Desired flow into the airway, and
- The pressure in the airway.

In practice, these two values must be transmitted electronically to the air drive. Typically this would be done with an MCU controller that supports I2C, SPI, or a serial interface. The information could be encoded at the byte-level or in a human-readable format like JSON. Likewise, a physical standard, such as the ISO 22mm airway connector, would make it easier in practice for air drives to be truly interchangeable, but the definition of such protocols to embody this approach is beyond the scope of this paper.

We assume that when an air drive receives a command, it is required to do whatever is necessary to produce the specified watts on the airway if the airway is at the specified pressure. It is to continue doing this until it receives the next command.

An air drive may or may not have its own ability to sense the pressure in the airway for its own purposes. It is acceptable for an air drive to be a rather unintelligent machine that was simply calibrated at manufacture time to produce the required flow against the specified pressure to produce the required watts.

## 10 How to Test a Power-on-the-airway Air Drive

The performance of an air drive can be measured with the following values:

- power producible against maximum pressure,
- duty cycle,
- power accuracy is a percentage,
- command response time: maximum time to accept a new command in ms,
- power response time: maximum change in watts/ms per ms,
- mean time to failures in thousands of hours,

For example, a good air drive for mechanical ventilation would be able to produce 7.35 watts on the airway at any pressure up to 45 cm H<sub>2</sub>O within  $\pm 0.8$  watts, operate at a 50% duty cycle, and have a response time 0.2 watt/ms, reconfigurable every 10ms. Such a response time would allow the air drive, operating against a suitable mechanical system such as a test lung, to generate 45 cm H<sub>2</sub>O pressure at 100 lpm in 37 ms, and to release that pressure to zero when so ordered in 37 ms. It could reliably perform this work for thousands of hours at a duty cycle of 50%.

The response time is clinically important in order to allow efficient ventilation at high respiration rates. We do not yet have a mathematical model to understand the impact of low response time, but clearly if the air drive takes

a long time to start doing work on the airway and a long time to release it, gas exchange and possibly even maximum tidal volume will be impaired. [See Schulz and Read, Anesthesia.]

To test an air drive, attach the air drive to a pneumatic cylinder. Install a flow and pressure sensor between the two. Weight or activate the pneumatic cylinder to produce a range of pressures from 0 to the specified maximum. Command the air drive to produce a range of powers up to the maximum specified power. Perform this from a “standing start” or zero power and returning to zero power. The response time can be computed from the pressure and flow curve. At any point in time, power-on-the-airway is pressure times flows. Measure that the power-on-the-airway is within the specified accuracy.

If you don’t have a pneumatic cylinder, a test lung can accomplish approximately the same test because it’s small volume will quickly be pressurized. This will require a bit more study of power-on-the-airway to produce pressure, which will be a function of the restriction on the test lung, compliance, and total volume. Nonetheless it should be possible by ramping up power to measure all parameters at all pressures.

## 10.1 The Importance of Zero Power

It is important that zero power is a specifiable value which must be met by any air drive claiming to meet a spec. This situation may be illustrated by a plastic bag of 1-liter capacity stuffed inside a 500ml glass bottle. Such a model of a lung would be extreme, but must not be discounted. Such a lung model begins an inspiration with extraordinarily high compliance, which means that a tiny positive pressure makes the first 500ml flow quickly into the lung model. The compliance then drops to almost zero: not amount of additional pressure will increase the air in the lung (treating air as incompressible and assuming the bottle does not burst.)

However, we take as a principle that within the specifications a doctor should be able to prescribe any breathing that they see fit for the patient. So, upon reaching 500 ml, not more positive flow is possible, and therefore no positive work is possible. However, the air drive must not allow work to be done on it. That is, it must prevent the back flow of air into the air drive itself, which would be negative power on the airway. If a doctor says 500ml are to be held statically in the lungs for 1s, the air drive must be able to accomplish that be so verified, even if it is against zero flow. This has implications for some mechanical devices which must be considered.

## 11 Example Calculations

## 12 Implementing Ventilation Modes With Power-on-the-airway

In order to accomplish interchangeability of air drives within a ventilator without changing the observable behavior of the ventilator, we imagine a controller which is sending commands to the air drive. This controller implements one or more ventilation modes. The controller represents an algorithm for implementing a ventilation mode in terms of power-on-the-airway. In almost all cases, the algorithm will use pressure and possibly flow sensors on the airway that the controller can read. The air drive may not be able to sense these things itself.

There are a number of ways such an algorithm could be implemented, but one of the most familiar would be as a PID controller. In the terminology of such systems, the power-on-the-airway in watts is the *control variable*, but the *error value* depends on the ventilation mode.

### 12.1 Pressure Control Mode

Pressure Controlled Ventilation (PCV) is perhaps the most basic. In this mode the error value of the PID controller would be the difference between the desired PIP and the airway pressure during the inspiration phase, which is a fixed time, and the difference between the desired PEEP and the airway pressure during the fixed expiration period. A controller with a single airway pressure sensor can implement this mode.

### 12.2 Volume Control Mode

Volume Controlled Ventilation (VCV) may assign a fixed flow rate to be performed on the airway until a tidal volume is achieved. (Generally there remains a maximum pressure, either implemented mechanically with a pop-off valve, or electronically.) Since flow rate and tidal volume are fixed, the time of inspiration is calculated by tidal volume divided by flow rate. Such a mode can be implemented in two ways. If the controller has a flow sensor, the flow in the airway subtracted from the prescribed flow can be the error value. However, interestingly, if we have an air drive, the controller could implement volume control mode with a single pressure sensor, by multiplying the desired flow rate times the current pressure to produce the watts to command the air drive to produce. If the air drive does its job, the flow will be accurate to within the specified accuracy.

Note that in either case the simple and well-established PID controller approach can be used.

### 12.3 Power-on-the-airway as a clinical measure

The integration of power over time is work. Although a patient's lung restriction and compliance may change over time, any inspiration provided by a power-on-the-airway drive automatically provides the power of breathing if you simply sum up the watts commanded and divided by time in each time interval between commands. A controller using a power-on-the-airway drive thus almost automatically computes the inspiratory work of breathing.

We speculate that it might be clinically valuable to define a ventilation mode which controls the power-on-the-airway done in a given inspiration.

## 13 Future Work

MatLab/Simulink can be used to simulate a human lung and breathing circuit driven by a source of flow[`mitsumlinklungmodel`]. We have modified this model to support driving by a source of pressure. A complete model of a air drive, including a model of random deviations in performance, would allow a ventilator mode programmed in MatLab to be verified in simulation. This would be strong evidence that we can build a ventilator that is independent of the particular air drive used.

If this were combined with a demonstration of being able to build highly performance air drives, we would have strong evidence that we can build a ventilator that allows air drives to be swapped out at low risk, though addressing a world-wide supply chain problem and moving closer to ensuring ventilators are always available. We have begun experimenting with building an initial air-drive out of multiple small positive-displacement aquarium pumps. To be maximally compelling, we need a demo of an air drive in each of the hardware classes we have identified.

## 14 References and Notes

This article: [3] discusses maximum momentary flow rates for healthy individuals under heavy exercise, and obtained much higher rates.

Get numbers from here [https://docs.google.com/document/d/1GqadQ2PMJ5qcTDh9ssFBqXj\\_ttbMyajY\\_QyK9WKKuSQQ/edit#](https://docs.google.com/document/d/1GqadQ2PMJ5qcTDh9ssFBqXj_ttbMyajY_QyK9WKKuSQQ/edit#)

What the regulators said in their specifications (todo) - UK Coronavirus (COVID-19): RMVS ventilator specification (talks extensively about limiting fresh gas flow from wall supply but silent on expected flow to be delivered to patient), Australian TGA specification (requires peak flow rates of 100lpm desirably 150lpm), USA FDA Authorisation, and Association for the Advancement of Medical Instrumentation AAMI Emergency Use Ventilator Design Guidance

## References

## References

- [1] Thomas Bein et al. “The standard of care of patients with ARDS: ventilatory settings and rescue therapies for refractory hypoxemia”. In: *Intensive care medicine* 42.5 (2016), pp. 699–711.
- [2] *Centrifugal Blower for Hospital and Home Care Respiratory Treatment*. [Online; accessed 05-June-2020]. 2020. URL: <http://www.airfan.fr/mfa0300.html> (visited on 06/05/2020).
- [3] Karen Coyne et al. “Inspiratory flow rates during hard work when breathing through different respirator inhalation and exhalation resistances”. In: *Journal of occupational and environmental hygiene* 3.9 (2006), pp. 490–500.
- [4] *Helpful Engineering Proposal Submission template for Pandemic Ventilator Project (Respiraworks)*. [Online; accessed 05-June-2020]. 2020. URL: <https://docs.google.com/document/d/1CE33EcGAd1NdnJA9XW9oGD9veOWSuuBIR2MPmKtkjYQ/edit#> (visited on 06/05/2020).
- [5] J Mancebo et al. “Comparative effects of pressure support ventilation and intermittent positive pressure breathing (IPPB) in non-intubated healthy subjects”. In: *European Respiratory Journal* 8.11 (1995), pp. 1901–1909.
- [6] Gustavo FJ de Matos et al. “How large is the lung recruitability in early acute respiratory distress syndrome: a prospective case series of patients monitored by computed tomography”. In: *Critical care* 16.1 (2012), R4.
- [7] *MIT Emergency Ventilator: Power Calculation*. [Online; accessed 05-June-2020]. 2020. URL: <https://e-vent.mit.edu/mechanical/power-calculation/> (visited on 06/05/2020).
- [8] *UK HRMA Rapidly Manufactured Ventilator System v4.0*. [Online; accessed 20-June-2020]. 2020. URL: [https://assets.publishing.service.gov.uk/government/uploads/system/uploads/attachment\\_data/file/879382/RMVS001\\_v4.pdf](https://assets.publishing.service.gov.uk/government/uploads/system/uploads/attachment_data/file/879382/RMVS001_v4.pdf) (visited on 06/20/2020).
- [9] *Ventilator for COVID-19 use in Australia*. [Online; accessed 20-June-2020]. 2020. URL: <https://www.tga.gov.au/ventilator-covid-19-use-australia> (visited on 06/20/2020).
- [10] John Burnard West. *Respiratory physiology: the essentials*. Lippincott Williams & Wilkins, 2012.