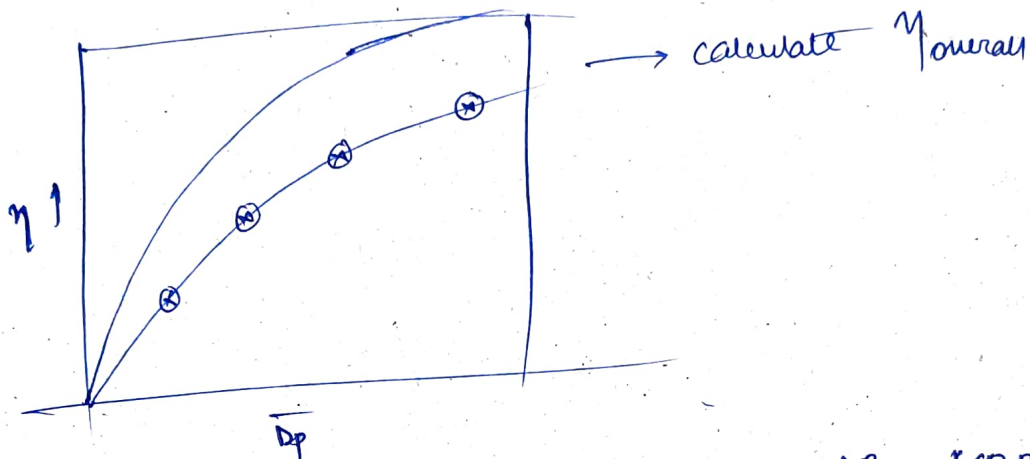
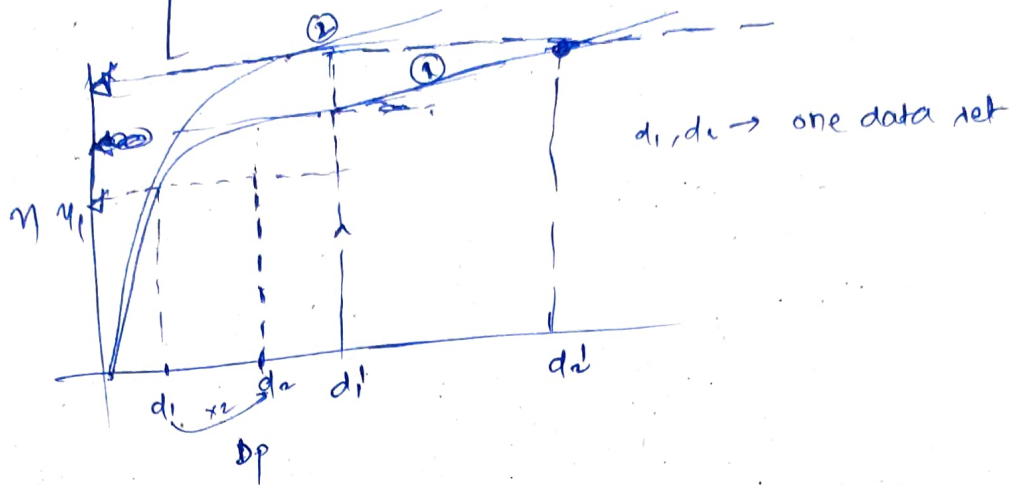


Q $\frac{d_2}{d_1} = 2.0 \Rightarrow [d_2 = 0.2 \cdot d_1]$



$\Rightarrow d_1 = 5 \text{ mm}, d_2 = 10 \text{ mm}$

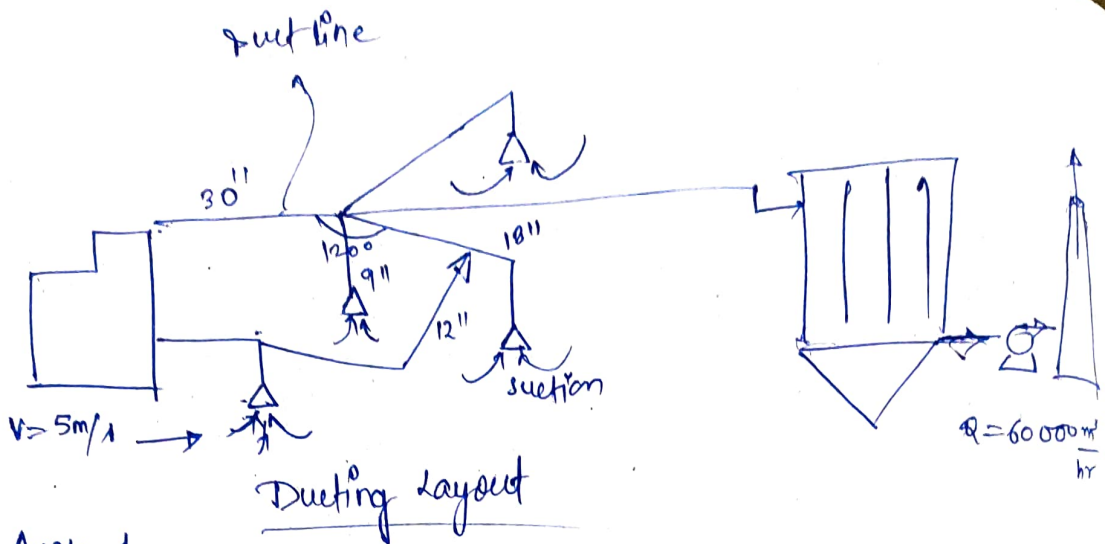
$\Rightarrow d_1 = 15 \text{ mm}, d_2 = 30 \text{ mm}$

$\Delta P = 100 \text{ psi}$
in a
cyclic
std value

\Rightarrow if η is not achieved with one cycle then add 4 or 2 more to it

\rightarrow i. Assume some data if given in exam but assumption should be based on some std source.

\rightarrow If suction is very low then we need to do friction calc in suction pipe to overcome such losses



Angle of

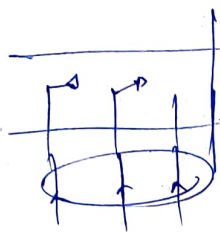
bend that are forbidden $\rightarrow 90^\circ, 60^\circ, 45^\circ, 30^\circ$

\rightarrow now using dia, length and angle of bend we can find out our total pressure loss

let we get $Q_{new} = 80,000 \text{ m}^3/\text{hr}$ from our calculation



\rightarrow using ducting layout we find the hood that is asked we add up all suction line ~~friction~~ up to that



by calculating all pressure losses due to friction and bends.

Prob 1: A conventional cyclone of dia of 500mm is used to treat the flue gas containing cement dust particulate of 3.5 gm/m^3 at 165°C and 1.0 atm pressure. The inlet gas velocity is 17 m/s and no. of turn the gas completes in the cyclone is 5. $\rho_p = 2700 \text{ kg/m}^3$, $\rho_g = 1.04 \text{ kg/m}^3$. Viscosity of gas = 0.019 cP

Particle size (μm)	>50	50-40	40-30	30-20	20-15	15-10	10-5	<5
% of dust	19.5	10.0	7.5	15.0	21.0	15.0	9.5	2.5

Calculate:

Or

- 1) cut size particle diameter
- 2) overall collection efficiency of the cyclone
- 3) settler concⁿ of dust from cyclone.

Given:

$$D = 500 \text{ mm}$$

$$\rho = 3.5 \text{ gm/m}^3$$

$$T = 165^\circ \text{C}$$

$$P = 1.0 \text{ atm}$$

$$\textcircled{1} D_{pmin} = \left[\frac{q \mu_f b}{\pi N V (\rho_p - \rho_F)} \right]^{1/2}$$

$b = 0.2D$
 $h = 0.5D$

$$= \left[\frac{9 \times 0.019 \times 10^{-3} \times 0.2 \times 0.5}{\pi \times 5 \times 17 (2700 - 1.04)} \right]^{1/2}$$

$$D_{pmin} = 4.87 \times 10^{-6} \text{ m}$$

$$\left[D_{pmin} = \underline{4.87 \text{ } \mu\text{m}} \right]$$

②

$$\eta = \frac{1}{1 + (D_p / D_{pmin})^2}$$

d_p → max mean dia = 27.0 μm

$$\eta = \frac{1}{1 + (D_p / D_{pmin})^2}$$

$$\eta_1 = 0.99$$

$$\eta_2 = 0.988$$

$$\eta_3 = 0.981$$

$$\eta_4 = 0.963$$

$$\eta_5 = 0.928$$

$$\eta_6 = 0.868$$

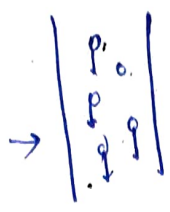
$$\eta_7 = 0.606$$

$$\eta_8 = 0.513$$

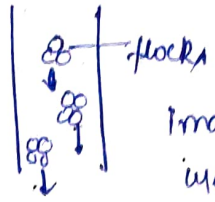
$$\frac{0.99}{100 \times 10} \rightarrow$$

② Flocculation %

Discrete settling

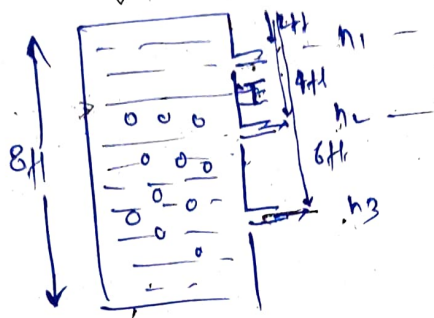


Flocculation



Imagining technique to find flock size

(not for material flocculating mix)



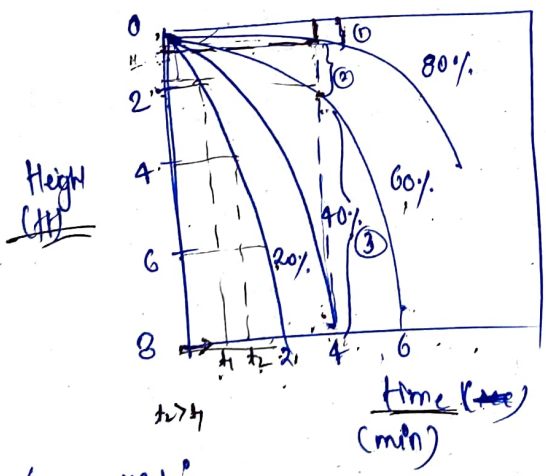
time	% solid removed		
	h_1	h_2	h_3
0	—	—	—
t_1	—	—	—
t_2	—	—	—
t_3	—	—	—

volume of water (Co)

by checking outlet at diff ht

Height	time required for a specific % separation		
	(20%)		
h_1	t_1	t_1'	t_1''
h_2	t_2	t_2'	t_2''
h_3	t_3	t_3'	t_3''
	↓	↓	↓
	for 20%	40%	60%

when conc is at outlet of a certain h i.e. h_1, h_2, h_3



If residence time = 4 min

- ① $\approx 0.5H$
- ② $\approx 0.2H$
- ③ $\approx 6.8H$

% removed:

$$Q \left(40 + \frac{60 \times 6.8}{8} + \frac{80 \times 0.2}{8} + \frac{100 \times 0.5}{8} \right)$$

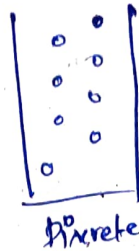
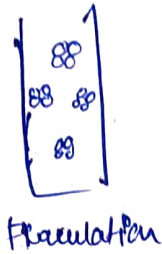
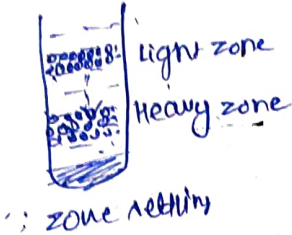
% removal of solids achieved.

→ we can take any residence time % to how much separation we need

Flock $\begin{cases} \text{easily breakable} \\ \text{unbreakable (ex: suspended + polyacrylamide)} \end{cases}$

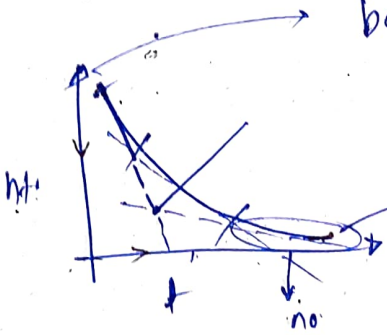
③ zone settling

when no



In z.s we see different zone of particle light zone, heavy zone settle.

→ happen when cone is very high.



based on residence time (t) we can find height of solids in cylinder
 $\rightarrow h \times A \rightarrow$ volume of solid collected \rightarrow we find how much solid removed

not due to settling but to compression occurs ~~during~~ to due to p-top settling particles.

$\tau \uparrow$ (res. time) \uparrow vol tank \uparrow

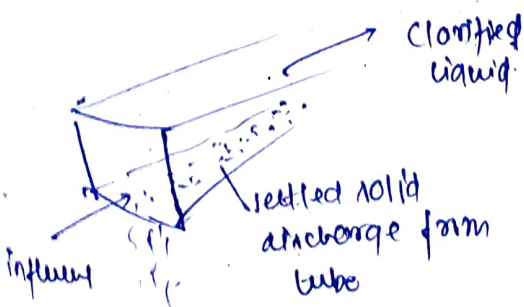
$$A (\text{area of settling tank}) = \frac{Q \times t_u}{h_0} \quad \begin{matrix} \text{flow rate} \\ \text{time} \\ \text{initial ht.} \end{matrix}$$

$$\tau = \frac{V}{Q}$$

$$V = Q \times t_u$$

volume of settling tank.

Inclined plate or tube settling



Q at $t=0$ $Q=Q_0$ $z \rightarrow Q_1$
 Q at $t=t$ $Q=Q$ (due to layer dept) $\rightarrow Q_2$
 \downarrow gradually decrease with time

$Q = \frac{Q_1 + Q_2}{2} \rightarrow$ for designing bag filter

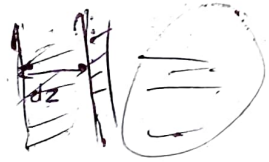
constant pressure filtration.

\rightarrow for industrial unit (bag filter) constant ~~pressure~~ pressure filtration is used.

Filter velocity = $\frac{Q_G}{A}$ \rightarrow gas flow rate
 $A \rightarrow$ surface area.

$t = t_f + t_c$ $\left\{ \begin{array}{l} t_f \rightarrow \text{time for filtration} \\ t_c \rightarrow \text{time required to clean the filter} \end{array} \right.$

if not given, we $t_c = t_f$
 truly Q_{max} when $t_c \approx 0$



① Constant Pressure filtration —

$$t_f = \left(\frac{B}{2\Delta P} \right) V_a^2 + \left(\frac{C}{\Delta P} \right) V_G$$

V_a — vol. of gas filtered for deposited dust of (dz) thickness.

$B, C \rightarrow$ will have to be provided.

\rightarrow If resistance of filter is negligible then —

$$t_f = \left(\frac{B}{2\Delta P} \right) V_a^2 \quad \text{where, } \beta = \left(\frac{M_a \cdot C}{\beta_B K} \right) \frac{1}{A^2} = \frac{K}{A^2}$$

$C =$ cunnigham collection factor

$\beta_B =$ bulk density of filter cake

$A =$ collection area through which gas is allowed to pass

$$t_f = K^* \cdot \frac{V_a^2}{A^2}, \quad K^* = \frac{K}{2\Delta P}$$

now

$$\underline{Q} = \frac{V_a}{t_f + t_c}$$

② Constant Rate filtration: ($Q = \text{const.}$) \rightarrow rarely used

$$\Delta P = BQ^2 + cQ \quad \text{--- (v)}$$

$$\mathcal{C} \neq 0 \quad \Delta P = CQ$$

$$\Delta p = \dots \quad (1)$$

$$A_p = (BV_a + D) \cdot Q$$

$$\left[\omega = \frac{\omega_a}{1 + j\omega} \right] \text{--- operation range}$$

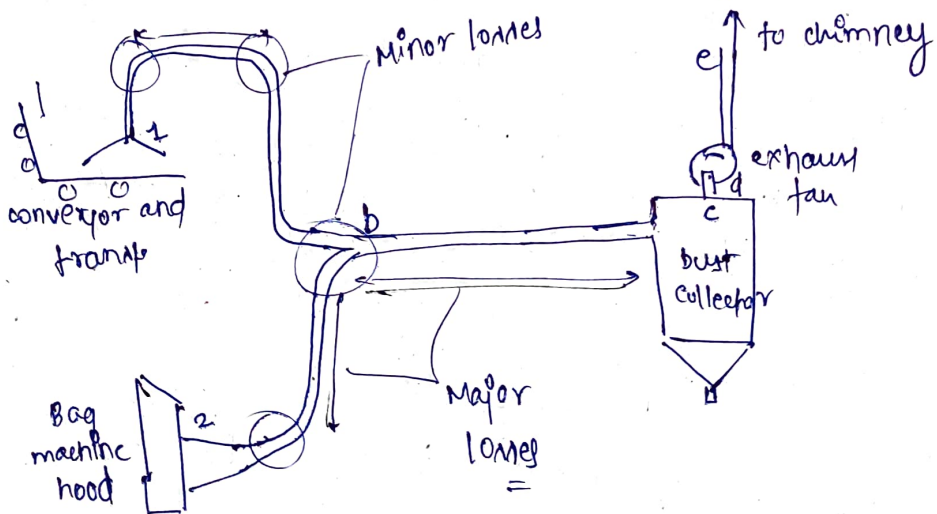
for Q_{max} find A/C ratio. $\cdot \frac{1}{2}$ ~~q~~ two time grader

Increase the area - $A_c = ?$

find no. of bags needed $\Rightarrow (N \times A_{CF} = A_C)$

→ In stead of one large bag, if we use multiple small bags (20-30 cm dia, 8-10 ft long) the surface area will increase using A/c ratio.

→ To optimise A/c, plated bag filters are used.



$1b = \text{distan}$ $1 \rightarrow b$
 "
 $2b$ $2 \rightarrow b$

we use table given for different sections ~~for~~ length and bend angle to calculate pressure drop

pressure as at present. The time req. to change both unit is 4 min. And max % inc in overall capacity that could be attained by adopting this suggestion.

Radioactive Waste Management:

① Introduction slide -

② Content -

1. ~~What~~ What is radioactive waste

(a) Composition

(b) Type R.A waste with little brief

2. Difference b/w other industrial waste & radioactive waste.

→ why it is more difficult to handle

~~4. Adverse effects~~
~~(a) On humans and animals~~
~~(b) on environment~~

~~3. where and when is waste produced?~~

4. Adverse effects

(a) on living beings Human, Animals

(b) on Environment.

5. Storage and Disposal

a) storage techniques

b) Disposal techniques

(with India go discuss next E)

15. Treatment and Conditioning