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Assignment - 2 (PDC)

Back I

$$\frac{dC_b}{dt} = (H - F_d) C_b = f, (C_b, C_e, F_d)$$

at steady state -

$$F_{de}(C_{ef} - C_{ee}) - \frac{M_e C_{he}}{P} = 0 \xrightarrow{\mathcal{D}} \frac{M_e = F_{de}}{C_{ef} - C_{ee}} = \frac{G_{he}}{P} = 0$$

where
$$M_s = \frac{M_m C_{ss}}{K_m + C_{ss} + K_1 C_{ss}^2} + C_{cs}$$
, C_{bs} of $F_{ds} = S$ tendy state value.

Linear state space model for the given system to control Co by manipulating Fa.

Linear shale space model -

$$\dot{x} = Ax + Bu$$

where,
$$X = \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} C_b - C_{bs} \\ C_s - C_{ss} \end{bmatrix}$$

$$B = \begin{bmatrix} \frac{\partial f_i}{\partial u} \\ \frac{\partial f_i}{\partial u} \end{bmatrix} = \begin{bmatrix} \frac{\partial f_i}{\partial f_i} \\ \frac{\partial f_i}{\partial f_i} \end{bmatrix} = \begin{bmatrix} -C_{bs} \\ C_{sf} - C_{ss} \end{bmatrix} \qquad U = F_d - F_{ds}$$

$$\frac{df_1}{dC_b} = H_s - F_{ds} = 0 \left[eq^n 3 \right] \left| \frac{df_1}{dC_s} = H'C_{bs} \right| \quad \text{where} \quad H' = \frac{dH}{dC_s} \Big|_{C_{ss}}$$

$$\frac{df_2}{dC_s} = -\frac{\mu_s}{P} = \frac{f_b}{P}$$

$$\frac{df_2}{dC_s} = -F_{ds} - \frac{\mu'C_{bs}}{P}$$

$$A = \begin{bmatrix} 0 & \mu' C_{bs} \\ -\frac{F_{ds}}{P} & -F_{ds} - \frac{\mu' C_{bs}}{P} \end{bmatrix}$$

Contra

$$\begin{bmatrix} \dot{n}_{i} \\ \dot{n}_{i} \end{bmatrix} = \begin{bmatrix} 0 & H'C_{bs} \\ -\frac{F_{Ls}}{P} & -\left(F_{ds} + \frac{H'C_{bs}}{P}\right) \end{bmatrix} \begin{bmatrix} \eta_{i} \\ \eta_{l} \end{bmatrix} + \begin{bmatrix} -C_{bs} \\ \frac{C_{bs}}{P} \end{bmatrix} U$$

Controllability Matrix
$$(C_B) = [B]$$

$$C_B = \begin{bmatrix} -C_{bs} & \underline{\mu'c_{bs}^2} \\ \underline{C_{bs}} & \underline{F_{ds}c_{bs}} - \underline{F_{ds}c_{bs}} - \underline{\mu c_{bs}^2} \\ \underline{P} & \underline{P} & \underline{P} \end{bmatrix}$$

$$C_B = \begin{bmatrix} C_{bs} & \underline{\mu'c_{bs}^2} \\ \underline{P} & \underline{P} & \underline{P} \end{bmatrix}$$

$$C_{\mathcal{B}} = \begin{bmatrix} -C_{bs} & \frac{\mathcal{H}'C_{bs}}{P} \\ \frac{C_{bs}}{P} & -\frac{\mathcal{H}'C_{bs}}{P^2} \end{bmatrix}$$

$$del(C_B) = \frac{\mu'c_{hs}^2}{p^2} - \frac{\mu'c_{hs}^2}{p^2} = 0$$

The given system is not fully state - controllable because Rank(6) 12 Irrespective of pameter and steady-state values

Prob2:

$$\frac{dC_{A}}{dt} = \frac{F}{V} (C_{AF} - C_{A}) - k_{1} C_{A} - k_{3} C_{A}^{2}$$

$$\frac{dC_{B}}{dt} = -\frac{F}{V} C_{B} + k_{1} C_{A} - k_{2} C_{B}$$

$$\frac{dC_{B}}{dt} = -\frac{F}{V} C_{B} + k_{1} C_{A} - k_{2} C_{B}$$

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Sole:

for steady value of CA & CB at Fs = 60

at steady state --

$$0 = \frac{F_s}{V} \left(f_{Af} - C_{As} \right) - k_1 C_{As} - k_3 C_{As}^2 - - - 0$$

$$\frac{60}{I} \left(10 - C_{Rs} \right) - 50 C_{As} - 10 C_{Rs}^2 = 0$$

$$C_{Rs}^2 + 11 C_{Rs} - 60 = 0$$

$$\left(C_{As} + 15 \right) \left(C_{As} - 4 \right) = 0$$

(CPs # -15, concentration of species cannot be negative)

$$0 = -\frac{F_s}{V}C_{Bs} + K_1C_{ns} - K_2C_{Bs}$$

$$0 = -6\beta C_{Bs} + 6\beta C_{As} - 10\beta C_{Bs}$$

$$C_{Bs} = \frac{5}{16}C_{As} = 1.25$$

. Bleady state value, CAs = 4 & CAS = 1.25 at Fs = 60.

$$\frac{dC_{A}}{dt} = \frac{F}{V} (C_{AF} - C_{A}) - k_{1}C_{A} - k_{2}C_{A}^{2} = f_{1}(C_{A}, F)$$

$$\frac{dC_{B}}{dt} = -\frac{F}{V} (C_{B} + k_{1}C_{A} - k_{2}C_{B} = f_{2}(C_{A}, C_{B}, F)$$

Linear state space model -

where,
$$X = \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} C_n - C_{n_s} \\ C_B - C_{B_s} \end{bmatrix}$$
 is $u = F - F_s$

$$A = \begin{bmatrix} \frac{\partial f_1}{\partial n_1} & \frac{\partial f_2}{\partial n_2} \\ \frac{\partial f_2}{\partial n_2} & \frac{\partial f_2}{\partial n_2} \end{bmatrix} = \begin{bmatrix} \frac{\partial f_1}{\partial c_n} & \frac{\partial f_2}{\partial c_n} \\ \frac{\partial f_2}{\partial c_n} & \frac{\partial f_2}{\partial c_n} \end{bmatrix} + B = \begin{bmatrix} \frac{\partial f_1}{\partial c_n} & \frac{\partial f_2}{\partial c_n} \\ \frac{\partial f_2}{\partial c_n} & \frac{\partial f_2}{\partial c_n} \end{bmatrix}$$

$$\frac{df_{1}}{dc_{B}} = -\frac{F_{s}}{V} - k_{1} - 2k_{3}c_{Bs} = -190 \left| \frac{df_{1}}{dc_{B}} = 0 \right|$$

$$\frac{d\hat{f}_2}{dC_{\rm pl}} = k_1 = 50 \quad \left| \frac{d\hat{f}_2}{dC_{\rm pl}} = -\frac{\hat{f}_2}{V} - k_2 = -160 \right|$$

$$\frac{df_1}{dF} = \frac{1}{V} \left(C_{AF} - C_{AS} \right) = \frac{1}{1} (10 - 4) = 6 \left| \frac{df_2}{dF} = -\frac{C_{BS}}{V} = -1.25$$

$$\begin{vmatrix}
\dot{n}_1 \\
\dot{n}_2
\end{vmatrix} = \begin{vmatrix}
-190 & 9 \\
50 & -160
\end{vmatrix} \begin{vmatrix}
\eta_1 \\
\eta_2
\end{vmatrix} + \begin{vmatrix}
6 \\
-1.25
\end{vmatrix} u$$

$$y = [0 \ i] \begin{bmatrix} y_i \\ y_j \end{bmatrix} + [0] u$$

$$\eta_1 = C_B - C_{Bs} = C_B$$

@ Blow, for dusing designing a state feedback controller using Bass-Gurn method -

Eigenvalue of
$$A \rightarrow |\lambda I - A| = \begin{vmatrix} \lambda + 190 & 0 \\ -50 & \lambda + 100 \end{vmatrix} \Rightarrow (\lambda + 190)(\lambda + 160) = 0$$

$$\lambda_{1/2} = -190, -160$$

Let the desired location of closed loop poler, M1,2 = -180, -180
Bass-Gura Medhod

$$We \ k_{70W}, \qquad C_B \ W = \begin{bmatrix} 6 & -1140 \\ -1.25 & 500 \end{bmatrix} \begin{bmatrix} 250 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} 960 & 6 \\ 62.5 & -1.25 \end{bmatrix}$$

$$T^{-1} = \frac{1}{-1575} \begin{bmatrix} -1.25 & -6 \\ -62.5 & 960 \end{bmatrix} = \frac{1}{155} \begin{bmatrix} 1.25 & 6 \\ 62.5 & -960 \end{bmatrix}$$

$$K = \left[\alpha_{2} - \alpha_{1} \quad \alpha_{1} - \alpha_{1}\right] T^{-1} = \left[32400 - 30400 \quad 340 - 350\right] \frac{1}{1515} \left[\frac{1.25}{62.5} + \frac{1}{162}\right]$$

$$= \frac{1}{1575} \left[2000 \quad 10\right] \left[\frac{1.25}{62.5} - \frac{6}{960}\right]$$

State feedback controller for the xactor —
$$\begin{bmatrix}
\dot{n}_1 \\
\dot{n}_2
\end{bmatrix} = \begin{bmatrix}
-190 & 0 \\
50 & -160
\end{bmatrix} \begin{bmatrix}
\dot{n}_1 \\
\dot{n}_2
\end{bmatrix} + \begin{bmatrix}
6 \\
-1.25
\end{bmatrix} u$$

$$U = -\left[1.984 \right] \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix}$$