

# New Time-Frequency Transform for Non-Stationary Signals

Prof L. Gelman

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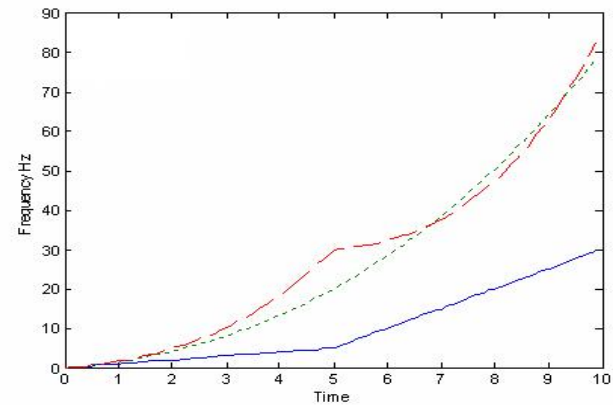
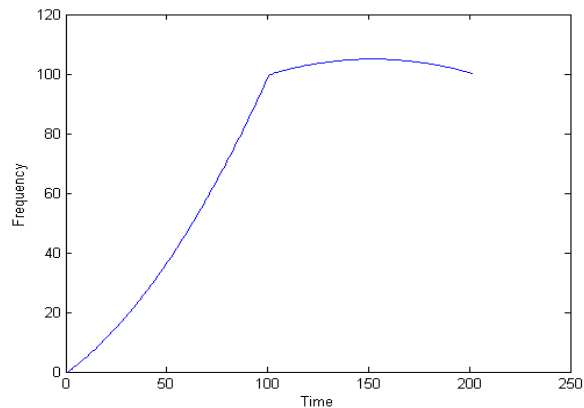
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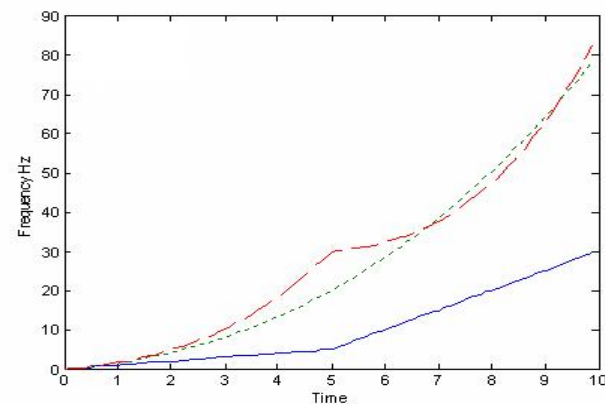
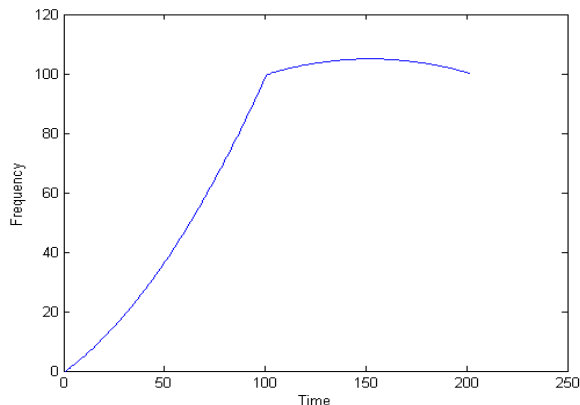
# Part 1

## Introduction



# Introduction

- For some important applications (e.g. radar, sonar and mechanical systems with transient shaft rotation, etc.) it is necessary to process transient signals with any (i.e. linear and *nonlinear*) polynomial variation of the instantaneous frequency.
- Examples of those signals are as follows: changes of the shaft frequency during aircraft engine operation, start up and shut down of engines, radar and sonar signals, electromagnetic interference, etc.

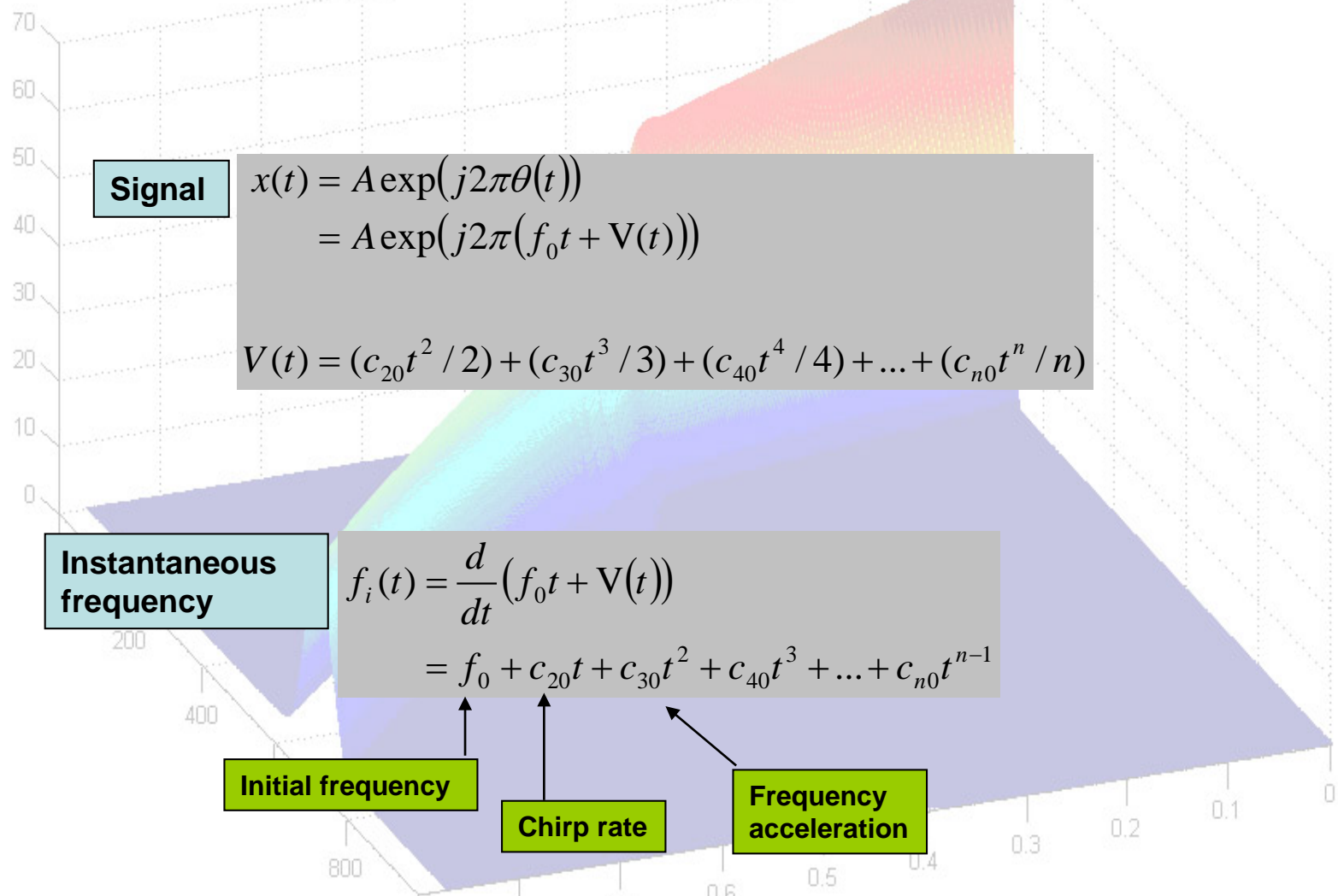


# Problem Statement

- Normally, for transient signals from complex mechanical systems (e.g. turbines, gearboxes, etc.) time variations of the instantaneous frequency are *known* from independent synchronous measurements (e.g. from tachometer signals, etc.).
- Sometimes, these frequency variations are even known *a priori*.
- Therefore, the main problem for these systems is *amplitude estimation* for transient signals (on the background of an interference) with *known* nonlinear time variation of the instantaneous frequency.



# Non-Stationary Higher Order Chirps I



The chirp rate (i.e. the frequency speed), the frequency acceleration and higher order parameters of the higher order chirps are **not varying** in time

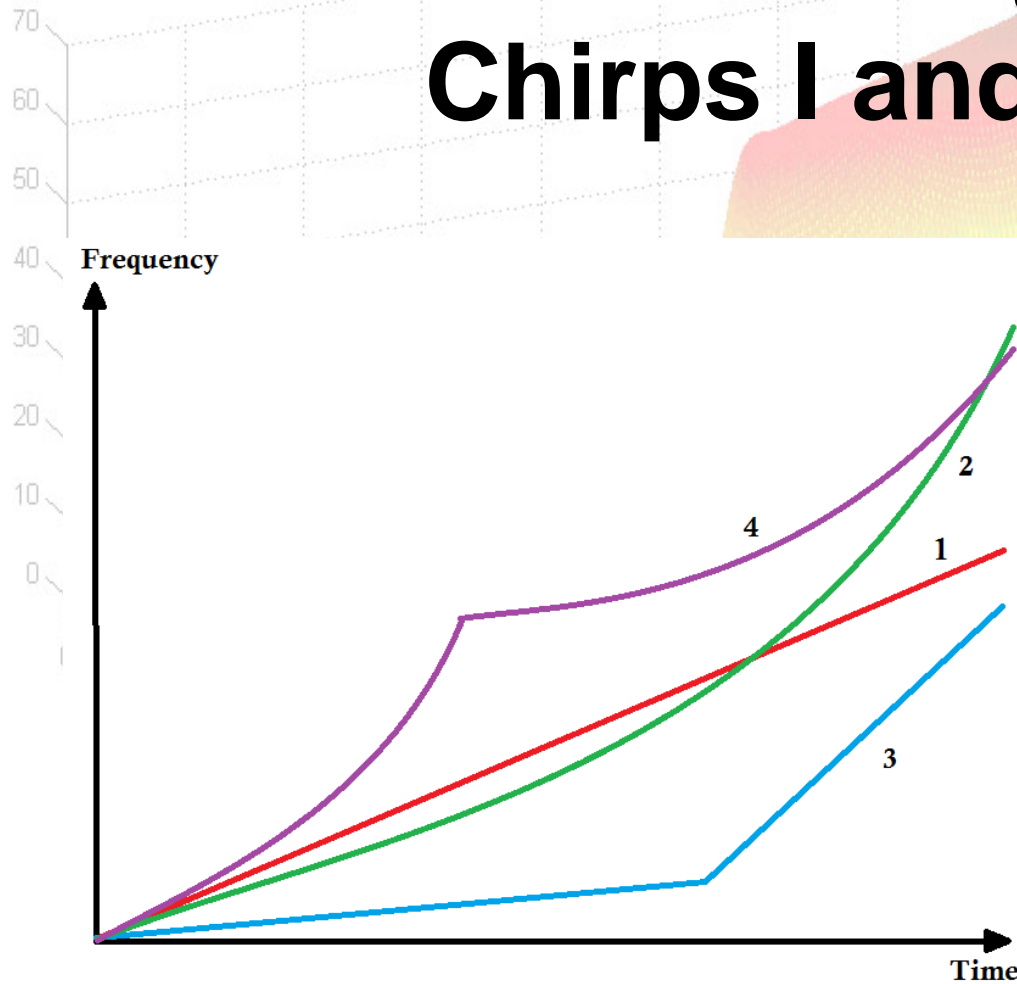
# Non-Stationary Higher Order Chirps

## II

$$V_0(t) = [c_{20}(t)t^2 / 2] + [c_{30}(t)t^3 / 3] + [c_{40}(t)t^4 / 4] + \dots + [c_{n0}(t)t^n / n]$$

The chirp rate (i.e. the frequency speed), the frequency acceleration and higher order parameters of the higher order chirps are **varying in time**

# Instantaneous Frequency-Time Variations for the Higher Order Chirps I and II



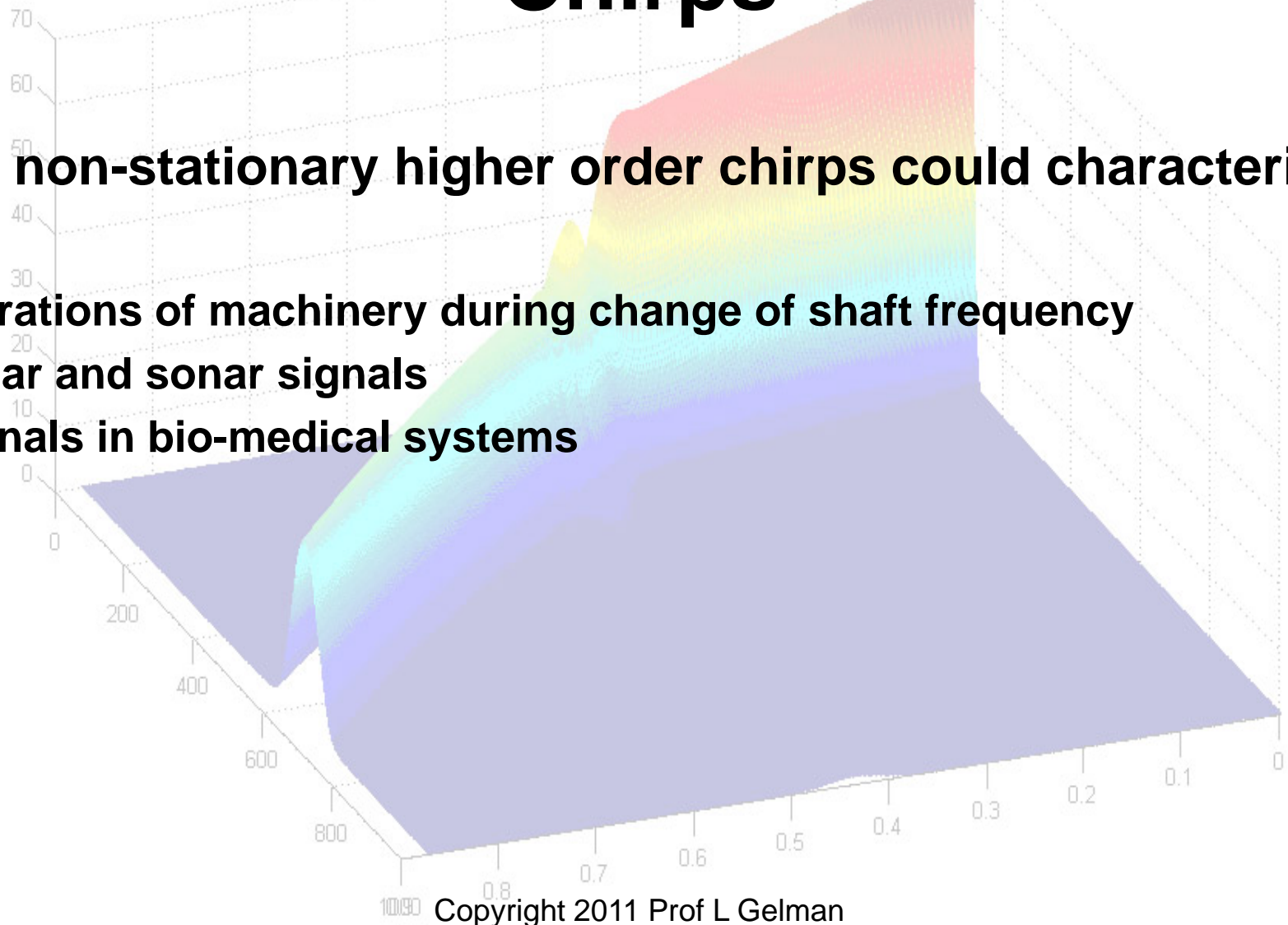
1. The Linear Chirp
2. The Higher Order Chirp
3. The Piece-Wise Chirp
4. The Piece-Wise Higher Order Chirp



# The Non-Stationary Higher Order Chirps

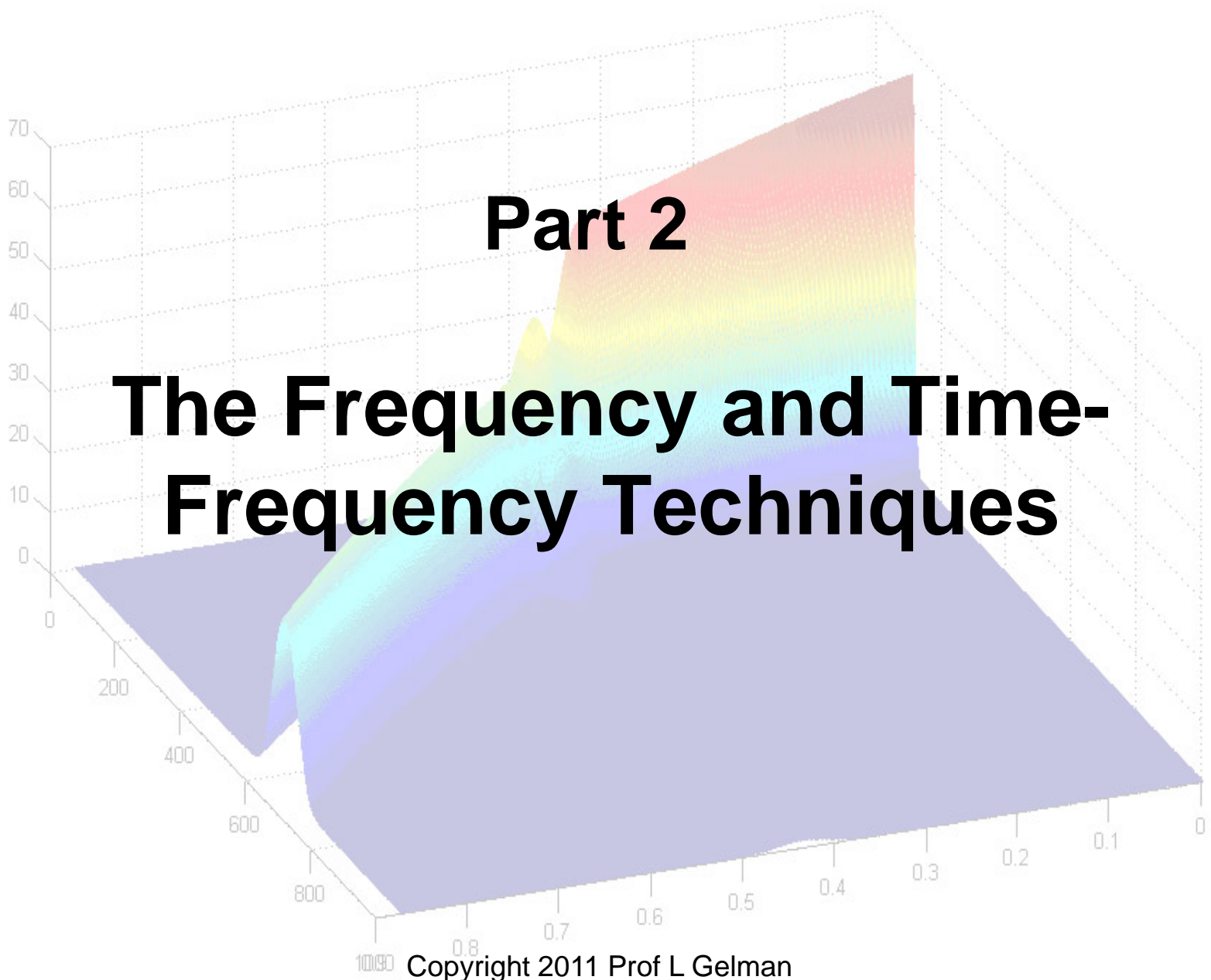
**The non-stationary higher order chirps could characterize:**

- **vibrations of machinery during change of shaft frequency**
- **radar and sonar signals**
- **signals in bio-medical systems**



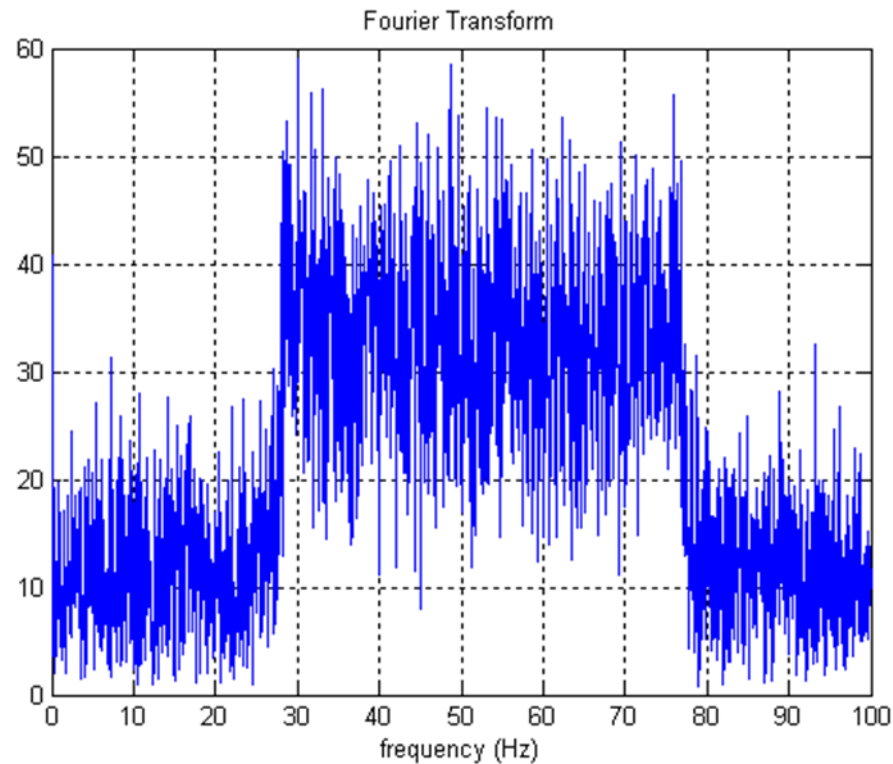
## Part 2

# The Frequency and Time-Frequency Techniques

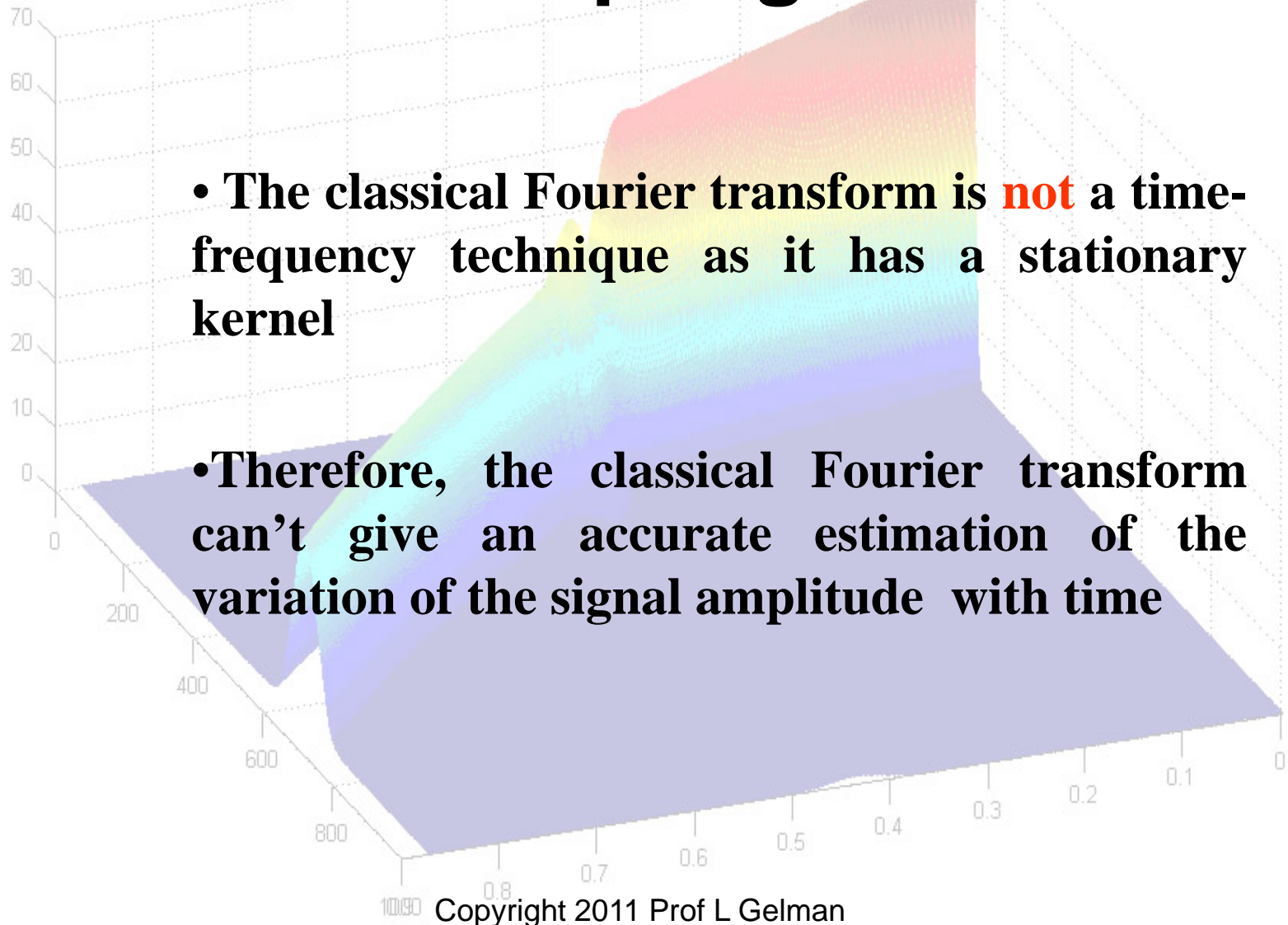


# The Classical Fourier Transform of the Chirp Signal

$$X(f) = \int x(t) \cdot e^{-2\pi \cdot i \cdot f \cdot t} dt$$

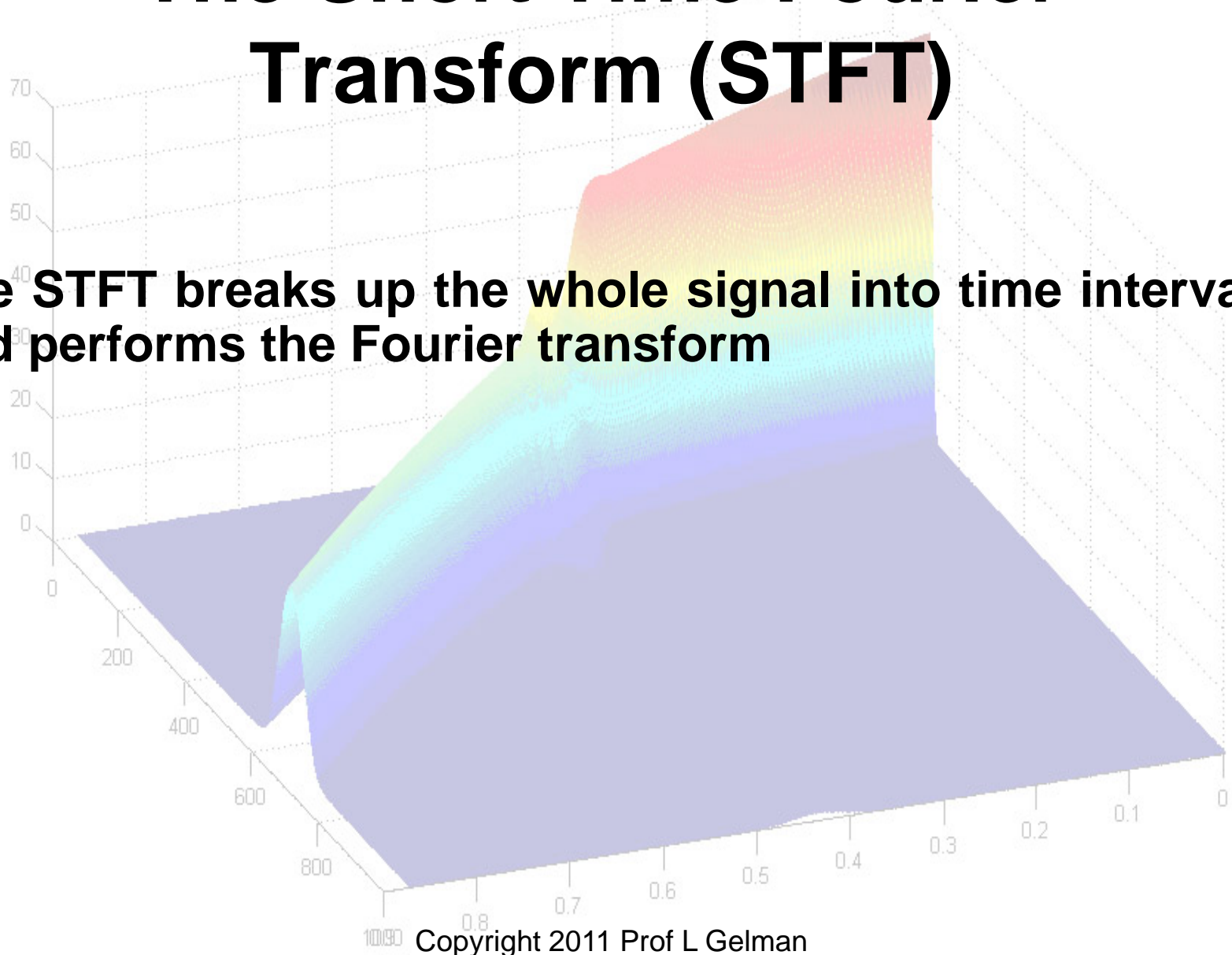


# The Classical Fourier Transform of Chirp Signals



# The Short Time Fourier Transform (STFT)

**The STFT breaks up the whole signal into time intervals and performs the Fourier transform**



# The Short Time Fourier Transform

**As intervals go smaller:**

- better time resolution
- worse frequency resolution

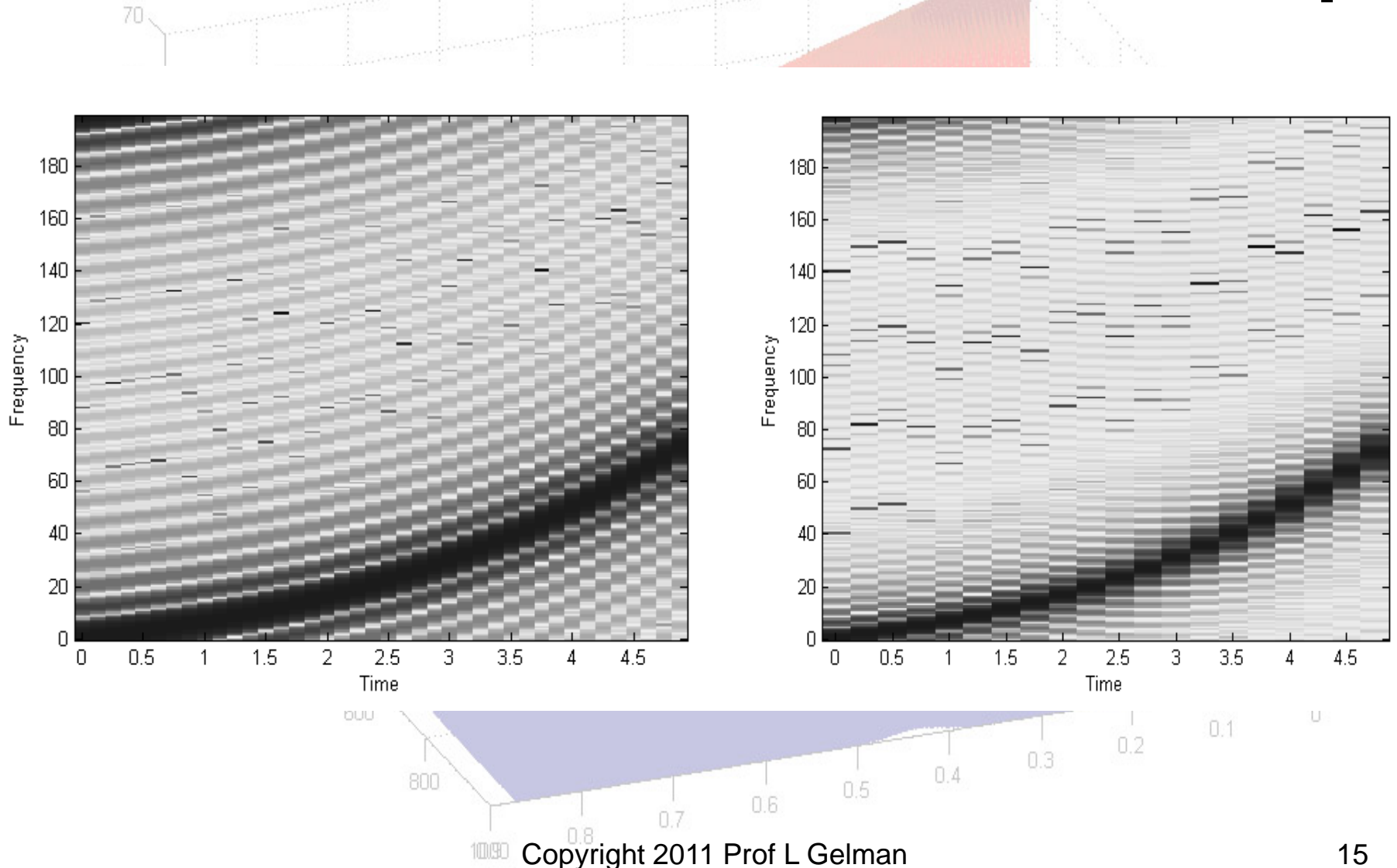
**As intervals go bigger:**

- better frequency resolution
- worse time resolution

- The STFT has a problem with time and frequency resolutions for chirp processing

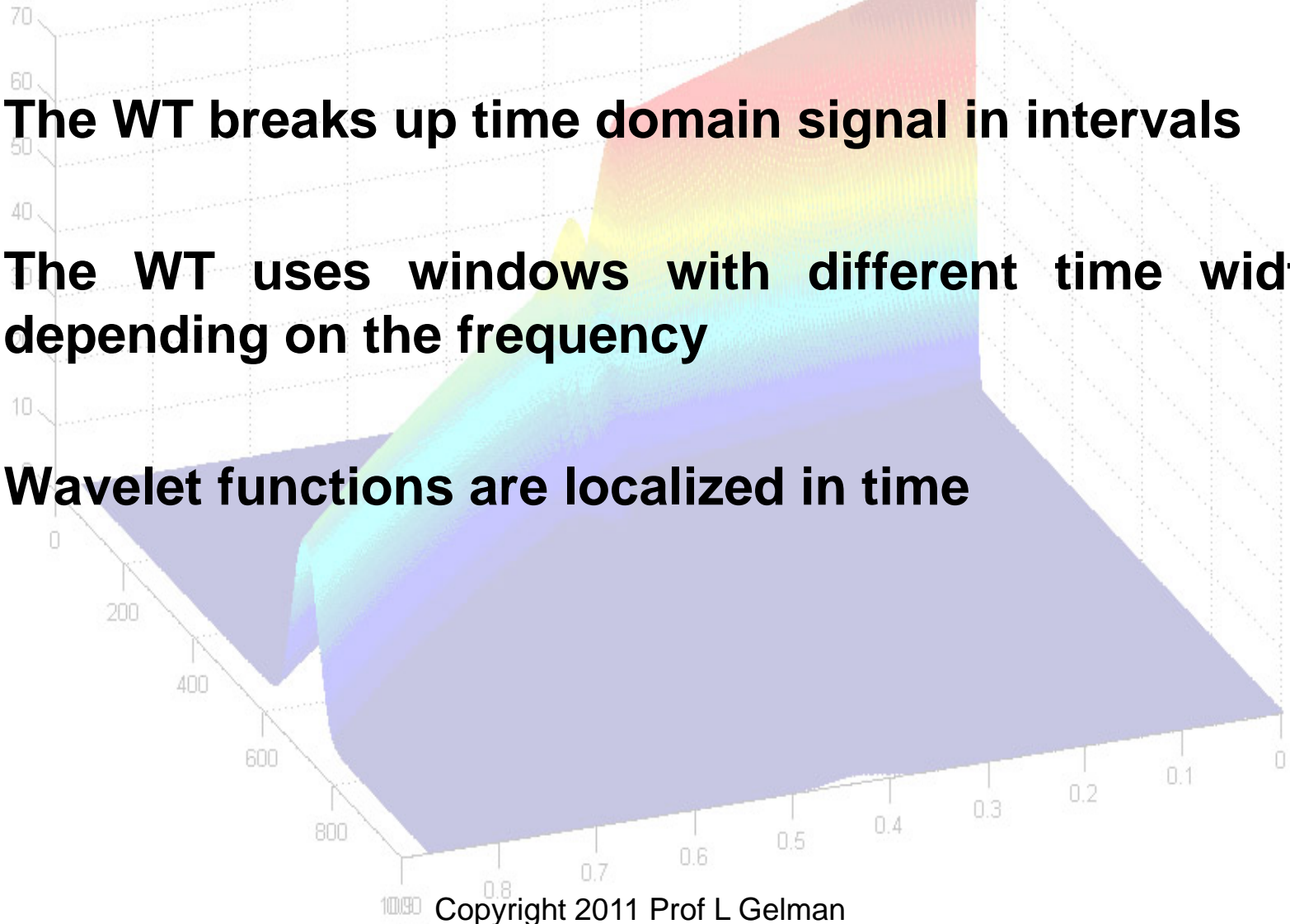


# Case Study: the Short Time Fourier Transform of the Quadratic Chirp



# The Wavelet Transform (WT)

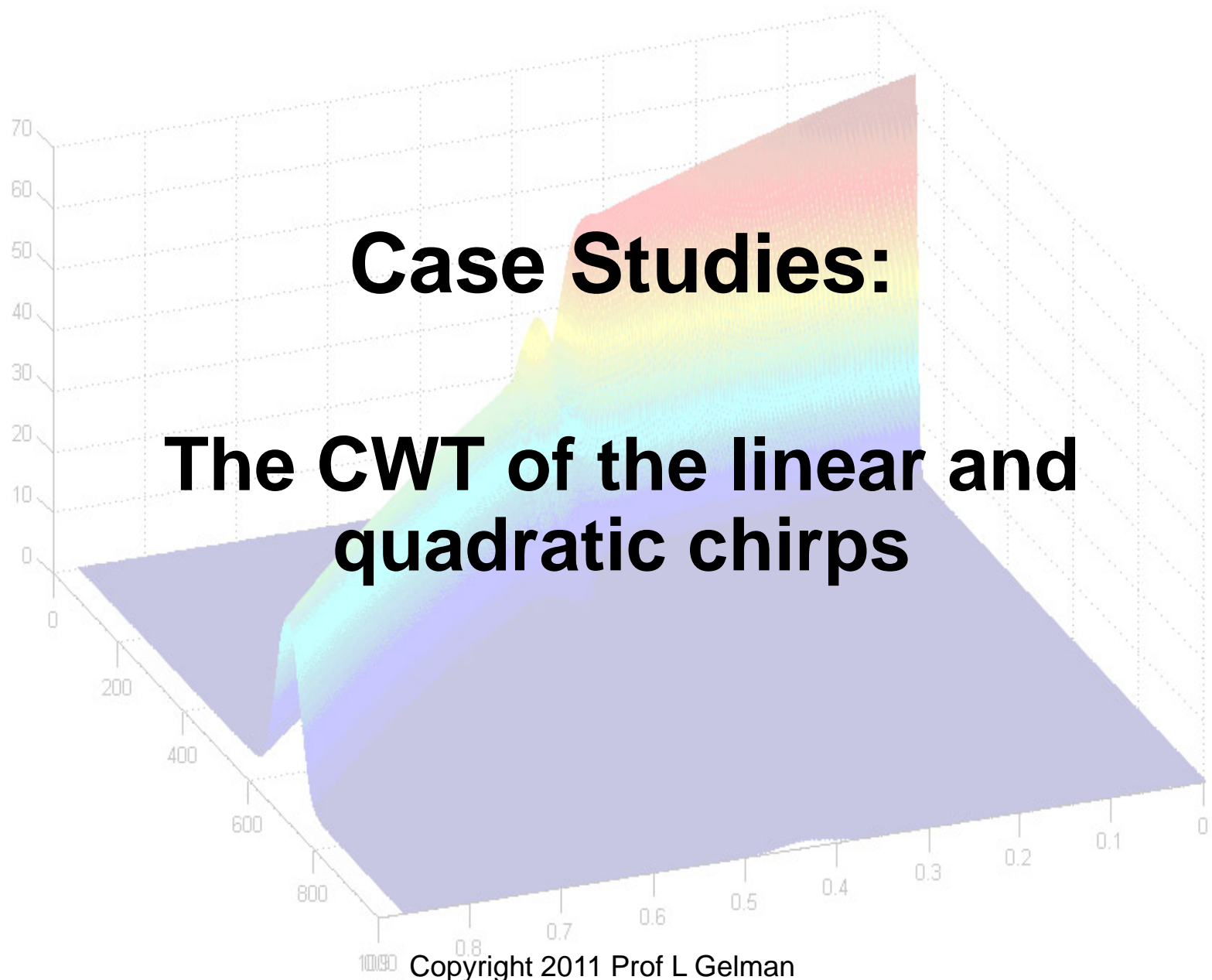
- The WT breaks up time domain signal in intervals
- The WT uses windows with different time width depending on the frequency
- Wavelet functions are localized in time



# The Morlet Wavelet

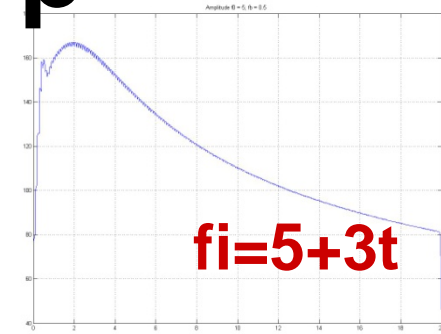
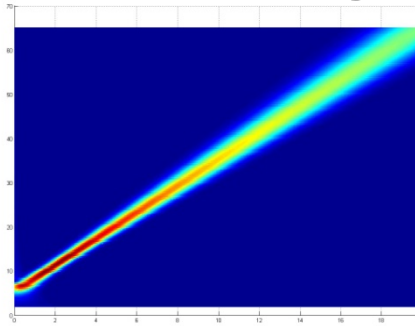
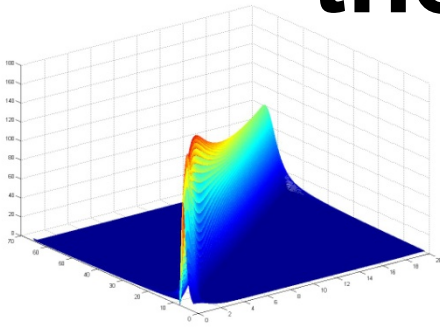
$$\psi(t) = \left( \frac{2}{f_b \pi} \right)^{1/4} \left( \exp(j2\pi f_0 t) - \exp(-(2\pi f_0)^2 / 2) \right) \exp\left(-\frac{t^2}{f_b}\right)$$

- The bandwidth parameter  $f_b$  defines a width of the Gaussian window that modulates the complex exponential signal
- Gaussian window is wider with bigger values of  $f_b$
- The optimum  $f_b$  provides
  - thinnest distribution in the frequency-time plane
  - smallest amplitude errors

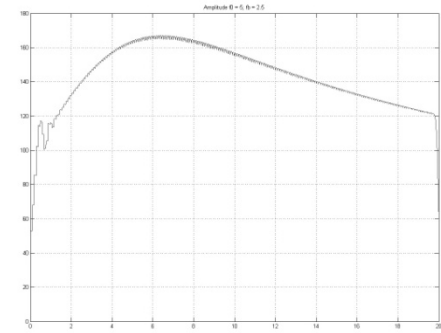
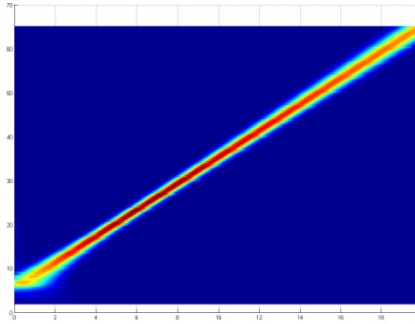
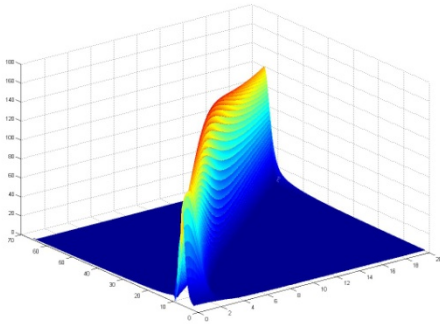


# The Morlet Wavelet Transform for the Linear Chirp

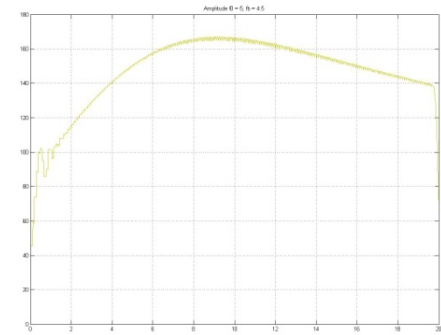
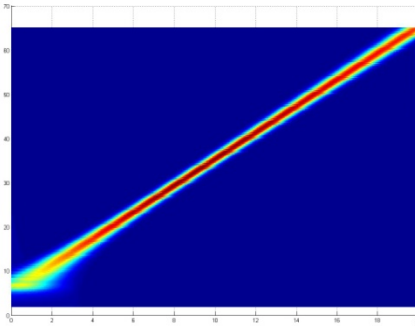
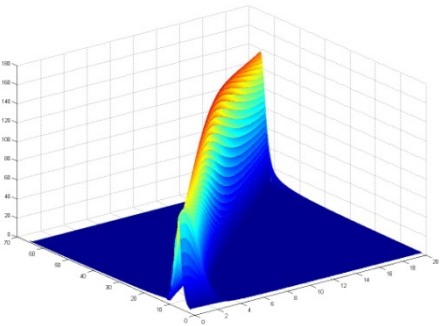
$$f_b = 0.5$$



$$f_b = 2.5$$



$$f_b = 4.5$$



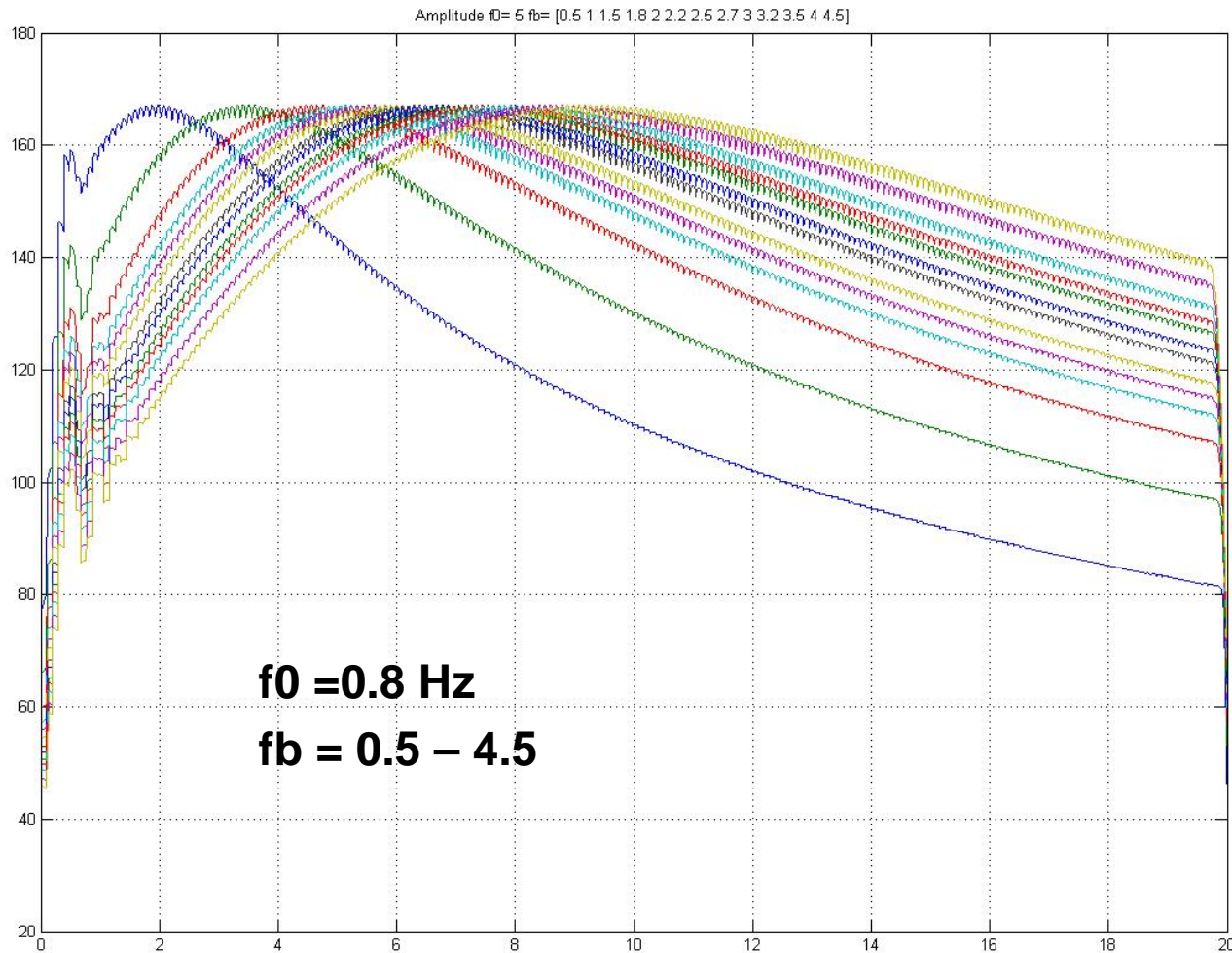
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The wavelet follows the instantaneous frequency variation with amplitude errors



# The Morlet Wavelet Transform for the Linear Chirp

## Amplitude Profile



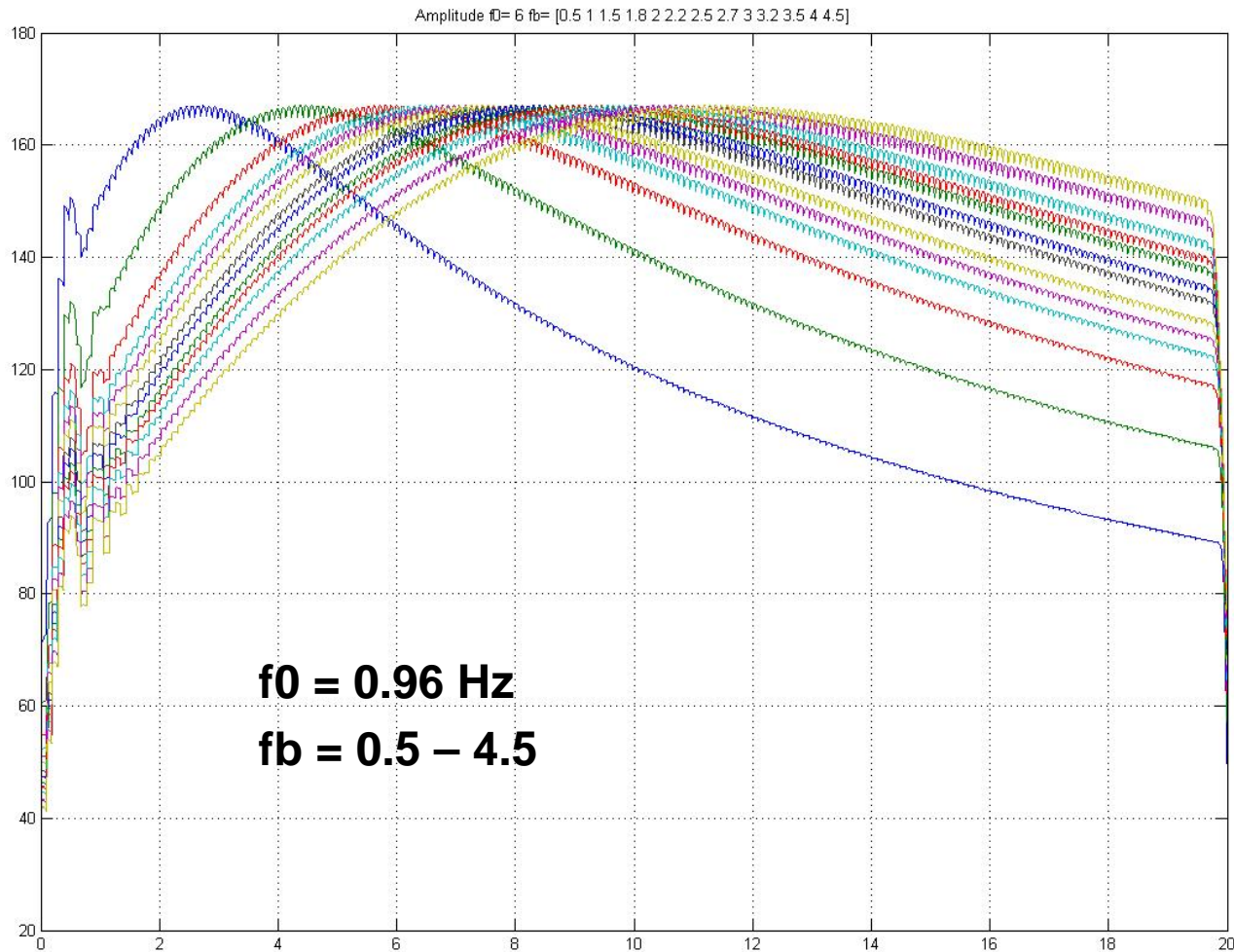
$$f_i = 5 + 3t$$

Low values of the bandwidth parameter give a maximum of the transform at low frequencies



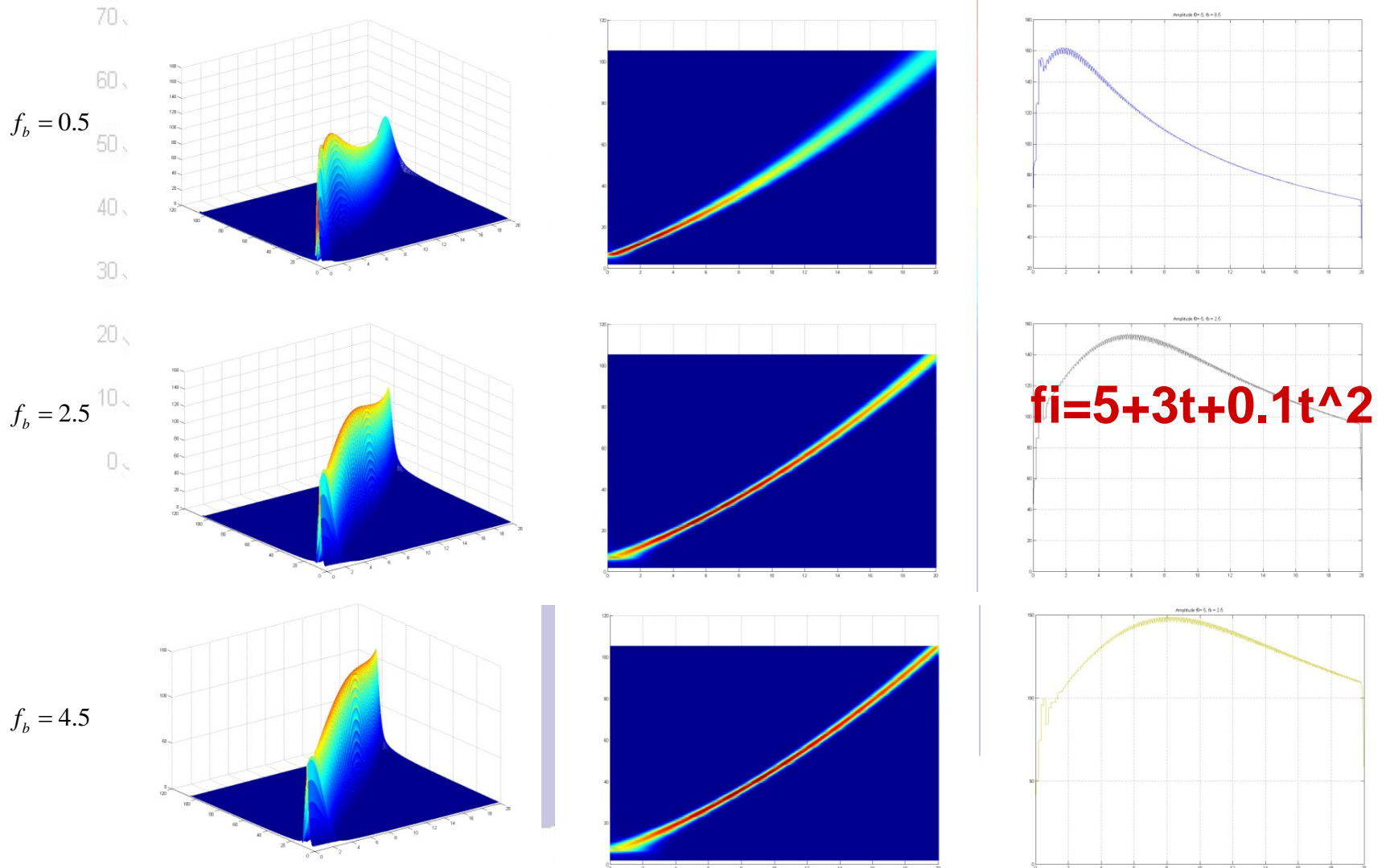
# The Morlet Wavelet Transform for the Linear Chirp

## Amplitude Profile



Low values of the bandwidth parameter give a maximum of the transform at low frequencies

# The Morlet Wavelet Transform for the Quadratic Chirp

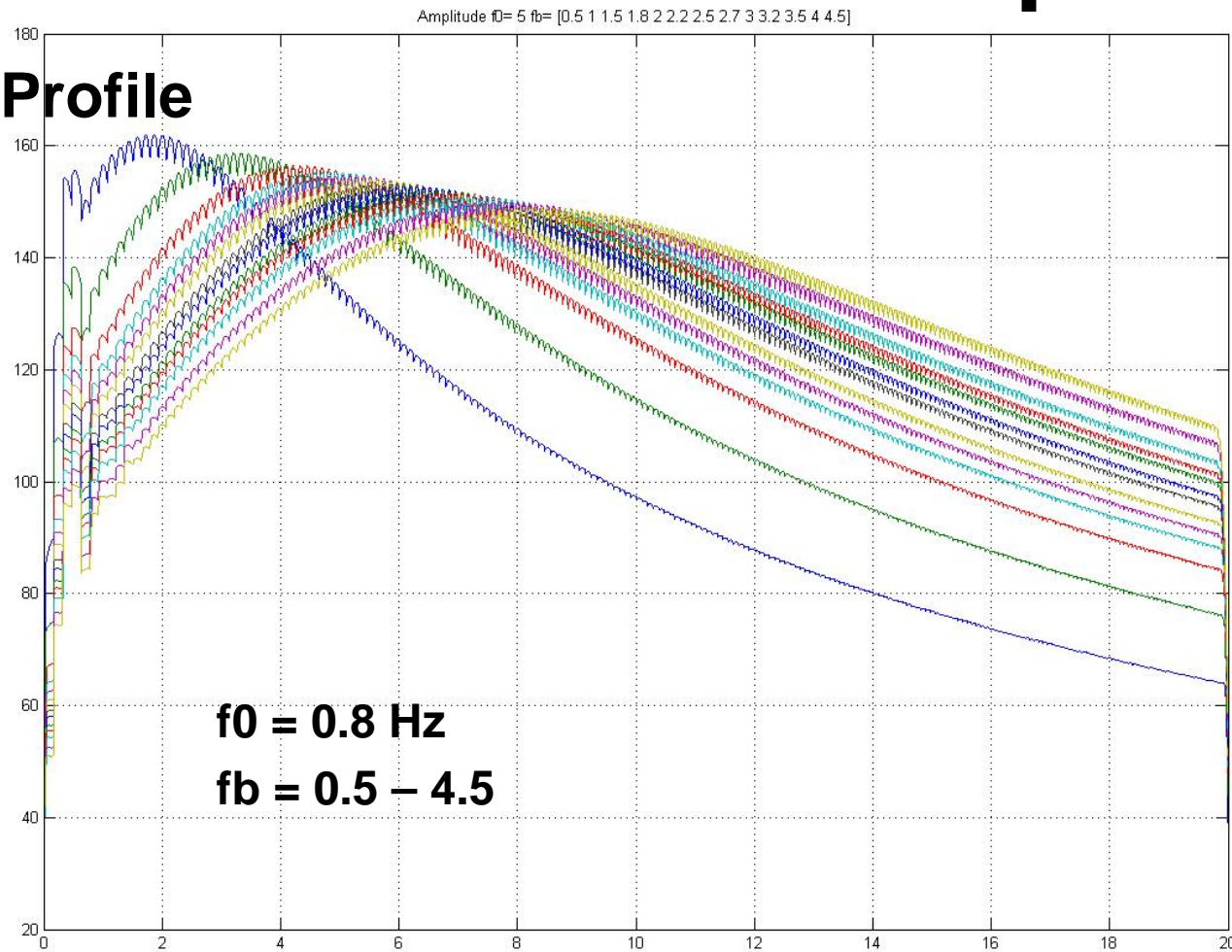


The wavelet follows the instantaneous frequency with amplitude errors

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# The Morlet Wavelet Transform for the Quadratic Chirp

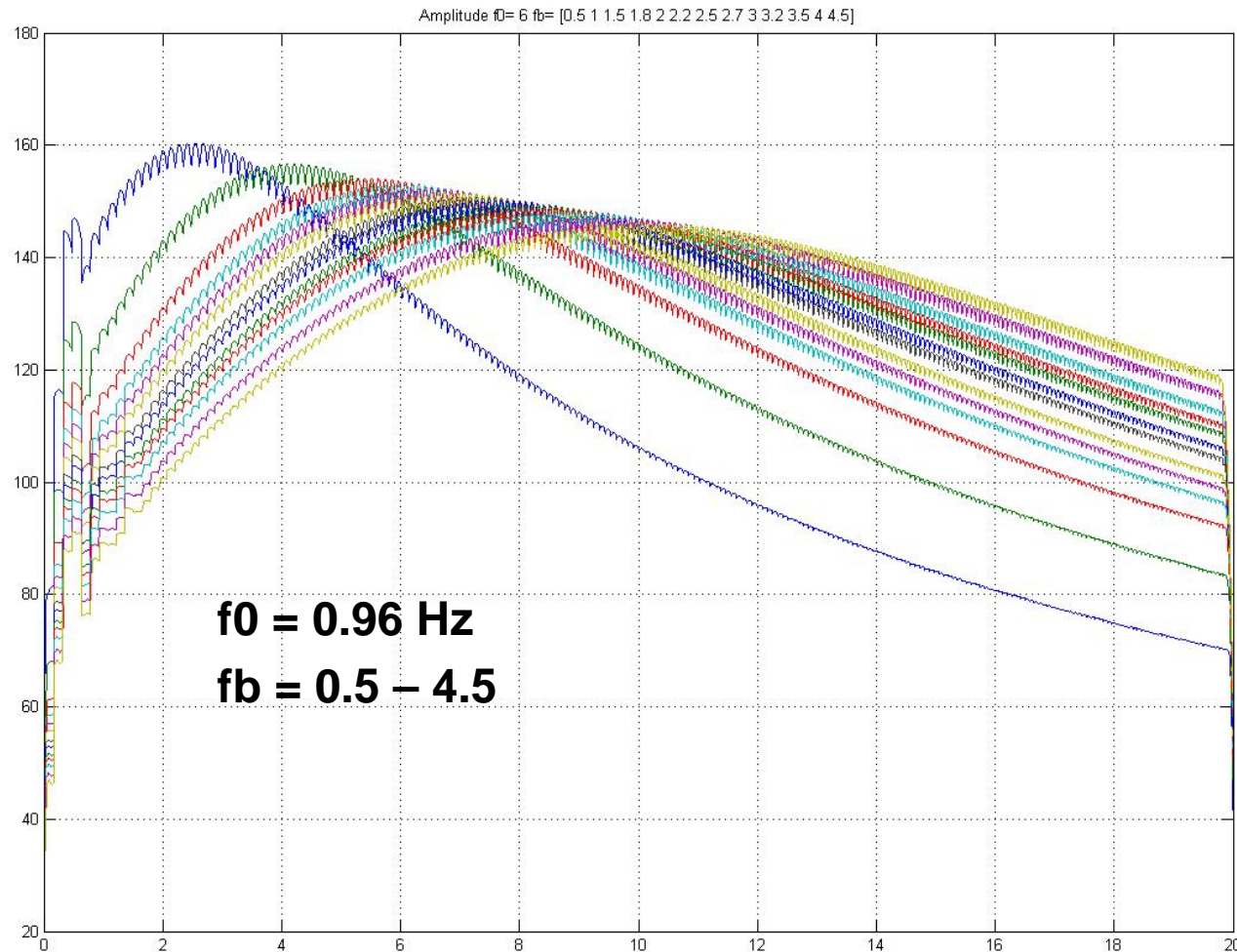
## Amplitude Profile



Low values of the bandwidth parameter give a maximum of the transform at low frequencies

# The Morlet Wavelet Transform for the Quadratic Chirp

Amplitude Profile

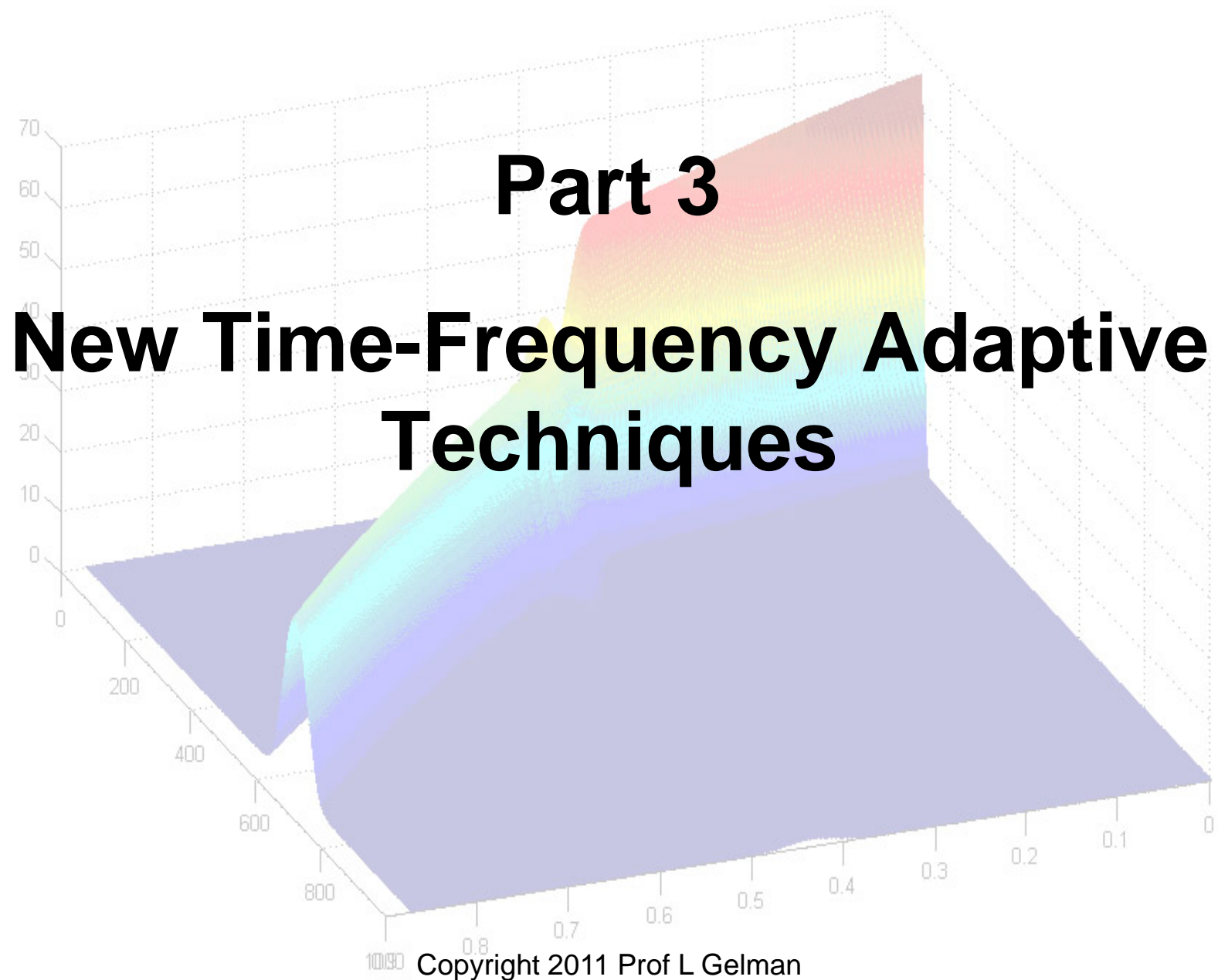


Low values of the bandwidth parameter give a maximum of the transform at low frequencies



# The Morlet Wavelet Transform for the Linear and Quadratic Chirps

- Bigger values of bandwidth parameter  $b_b$  make the frequency-time distribution thinner
- The instantaneous frequency-time variation is properly recognized by the transform
- Amplitude errors make the wavelet analysis not suitable for the linear and quadratic chirps





# The Short Time Chirp-Fourier Transform

- Let's consider a signal with the linear and piece-wise dependencies of the instantaneous frequency in time
- For these signals a new technique, the short-time chirp-Fourier transform, is proposed and defined as follows:

$$S(f, T, c_2) = \frac{1}{T} \int_{-T/2}^{T/2} h_i(t - T/2) x_1(t) e^{-j2\pi(f t + \frac{c_2}{2} t^2)} dt$$

# The Short Time Chirp-Fourier Transform

$$S(f, T, c_2) = \frac{1}{T_i} \int_{-\infty}^{\infty} h_i(t - T) x_1(t) e^{-j2\pi\left(ft + \frac{c_2(t)}{2}t^2\right)} dt$$

where  $h(t)$  is a time window,  $T_i$  is the window duration;  $i = 1, 2, \dots, N$

$f$  is frequency;  $c_2(t)$  is the variable frequency speed of the transform;  
 $T$  is window centre.

The frequency speed of the transform is constant during duration of a constant frequency speed of a signal

# The Short Time Chirp-Fourier Transform

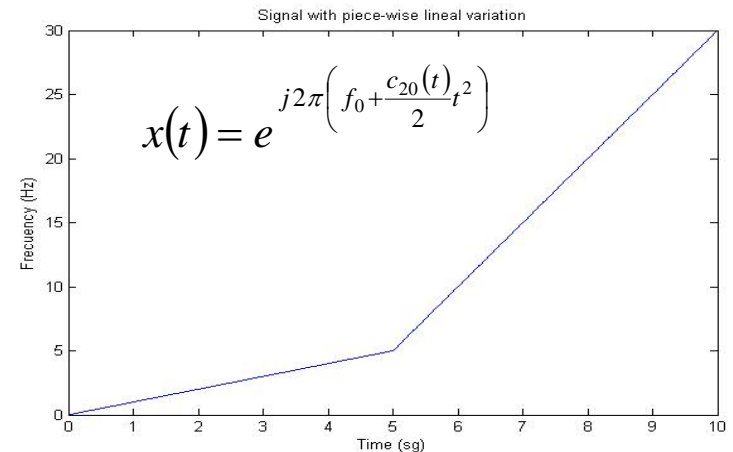
- The proposed transform is a generalization of the short-time Fourier transform for the case of the chirps
- **Adaptation conditions for the transform is**  $c_2/c_1=1$
- The simulation results for the proposed transform with rectangular window for curve 3 are shown in the next slides
- The simulated piece-wise chirp has one chirp rate for the signal period  $t_1 = 0 - 5s$  and another chirp rate for the signal period  $t_2 = 5 - 10s$

# THE PIECE-WISE CHIRP: A SIGNAL AND A KERNEL

## SIGNAL CHARACTERISTICS:

The piece-wise chirp with piece-wise variation of the instantaneous frequency

Each part of the signal has different chirp rate



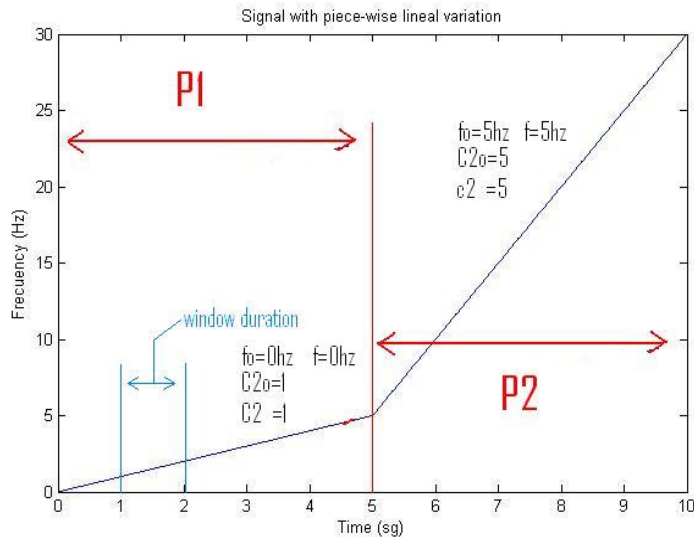
## KERNEL CHARACTERISTICS:

Kernel is characterized by the chirp rate of the transform

## KERNEL

$$e^{-j2\pi\left(f + \frac{c_2(t)}{2}t^2\right)}$$

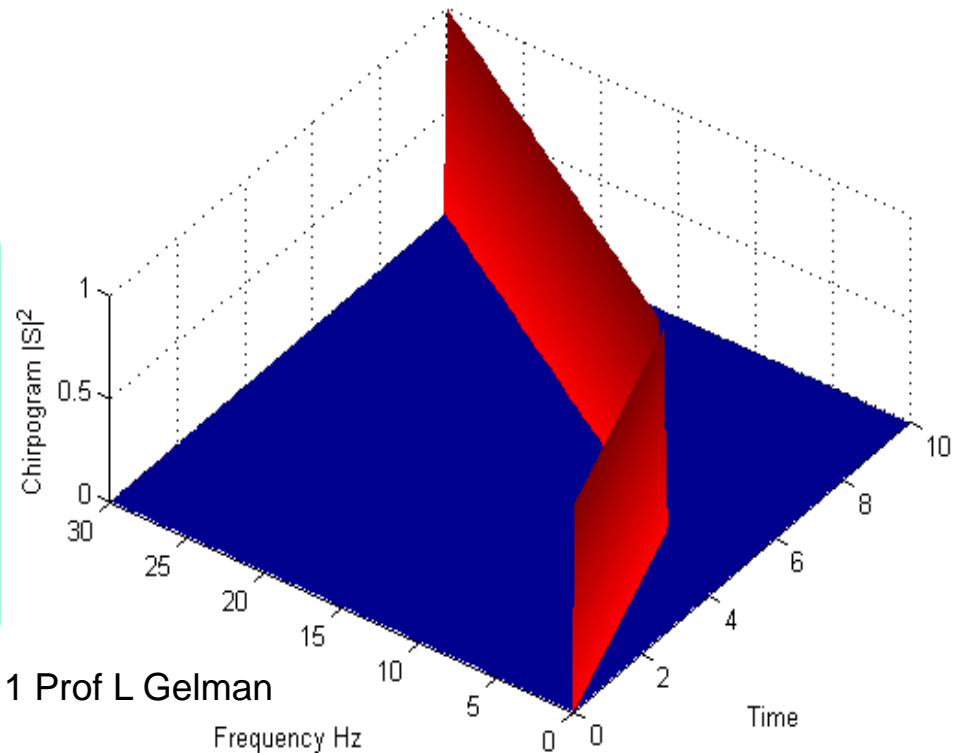
# THE PIECE-WISE CHIRP: THE KERNEL IS MATCHED



PARAMETERS OF THE SIGNAL AND KERNEL  
ARE MATCHED

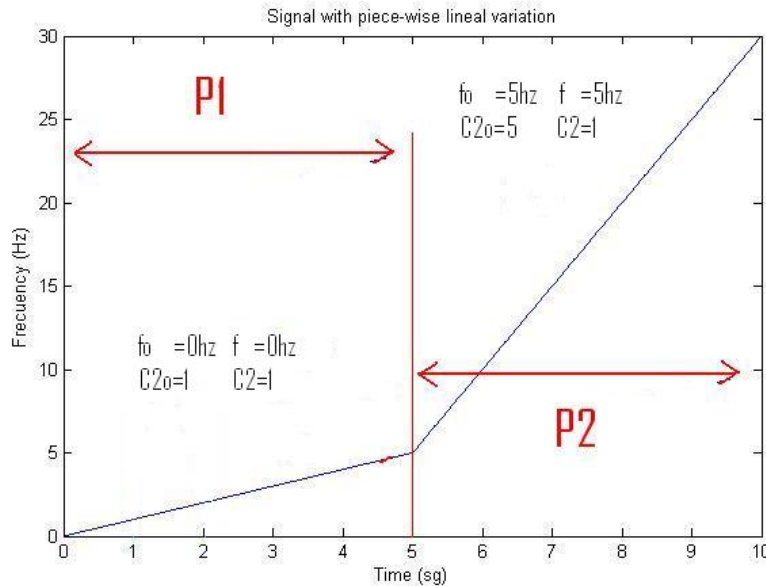
- Sampling frequency is 200 Hz
- P1=0-5s
- P2=5-10s

ONE CAN EVALUATE THE PIECE-WISE  
FREQUENCY-TIME DEPENDENCY OF THE  
SIGNAL AND CHIRP RATE FOR EACH PART  
OF THIS DEPENDENCY AND EMPLOY THE  
CHIRP FOURIER TRANSFORM WITH  
APPROPRIATE CHIRP RATES ON EACH  
SIGNAL PART.





# THE PIECE-WISE CHIRP: THE KERNEL IS UNMATCHED

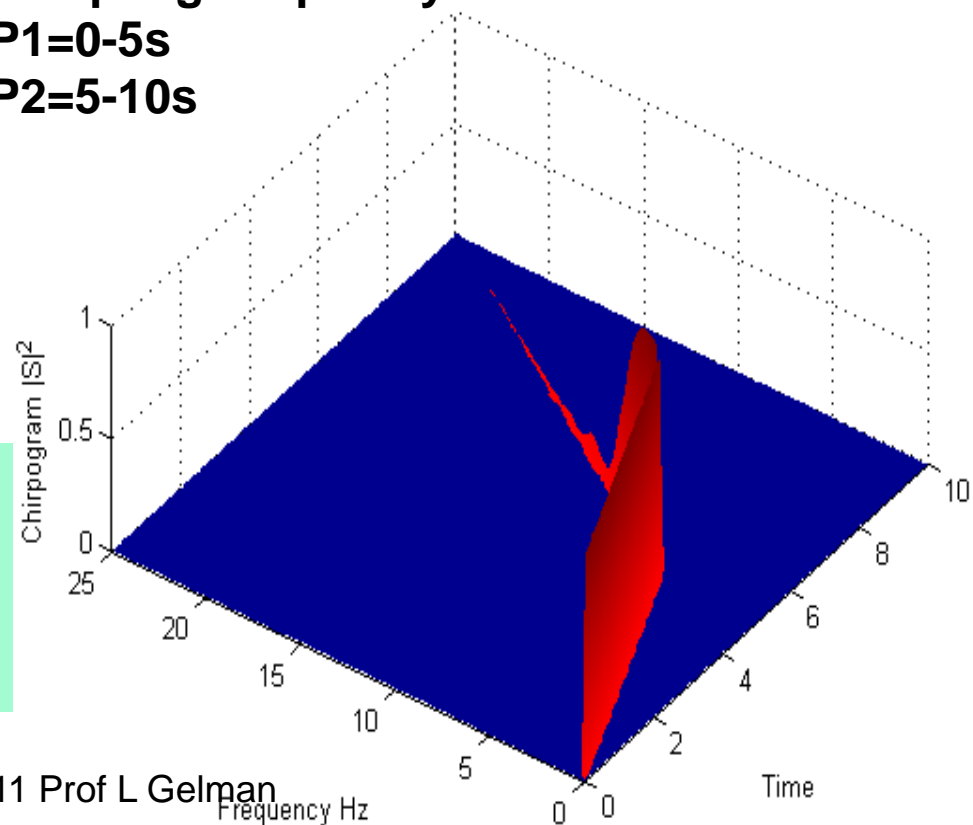


PARAMETERS OF SIGNAL AND KERNEL ARE UNMATCHED FOR **PERIOD 2**

- Sampling frequency is 200 Hz
- P1=0-5s
- P2=5-10s

• THE TRANSFORM DOES NOT WORK PROPERLY WHEN KERNEL AND SIGNAL ARE UNMATCHED

• THE SIGNAL AMPLITUDE OF THE FIRST PERIOD IS ESTIMATED WITH HIGH ACCURACY





# The Short Time Chirp-Fourier Transform: Adaptation

- Results in the previous slides show the essential advantage of the proposed transform: it could be used for selective detection of the linear chirps and piece-wise chirps
- It could be done by the following two step adaptation procedure:
  - to evaluate the frequency-time dependency of the chirps and chirp rates
  - to employ the short time chirp-Fourier transform with the adapted chirp rates following **adaptation conditions for the transform**  
 **$c_2/c_{20}=1$**

# The Linear Chirp

**Signal**

$$x(t) = e^{2\pi j \cdot t \left( f_o + \frac{c_{20}}{2} t \right)}$$

**The Short Time Chirp-Fourier Transform**

$$S(f, T, c_2) = \frac{1}{T_i} \int_{-\infty}^{\infty} h_i(t - T) x_1(t) e^{-j2\pi \left( ft + \frac{c_2}{2} t^2 \right)} dt$$

**Simulation:**

**Matched Kernel**

**Unmatched Kernel**

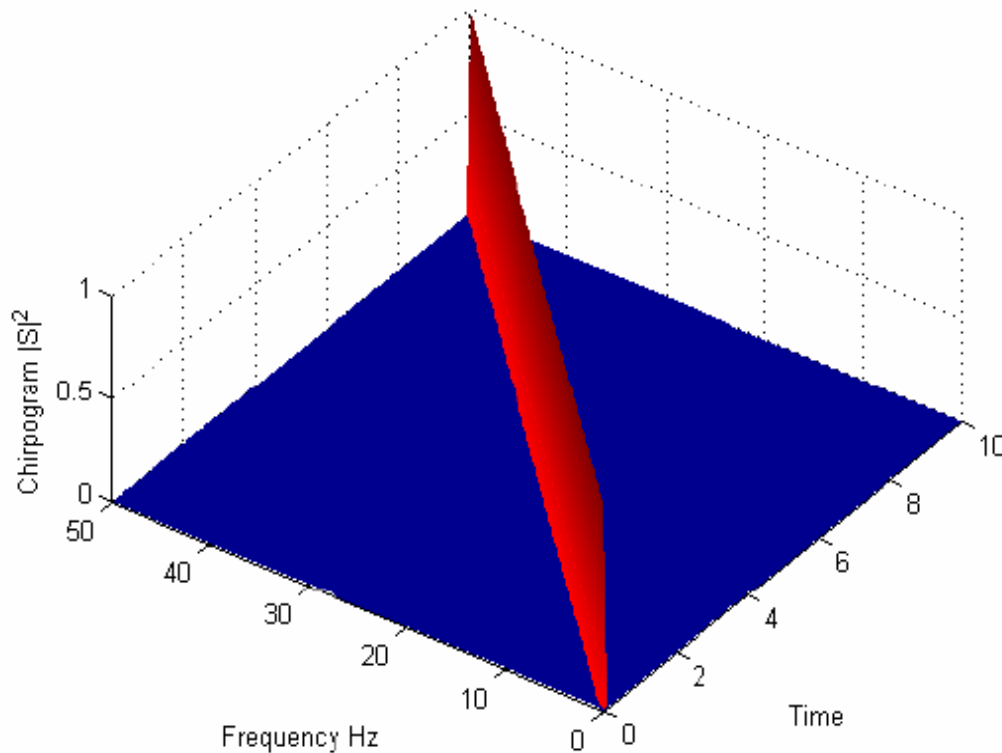
$$c_2/c_{20}=1$$

$$c_2/c_{20}<1$$

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# The Linear Chirp: the Kernel is Matched

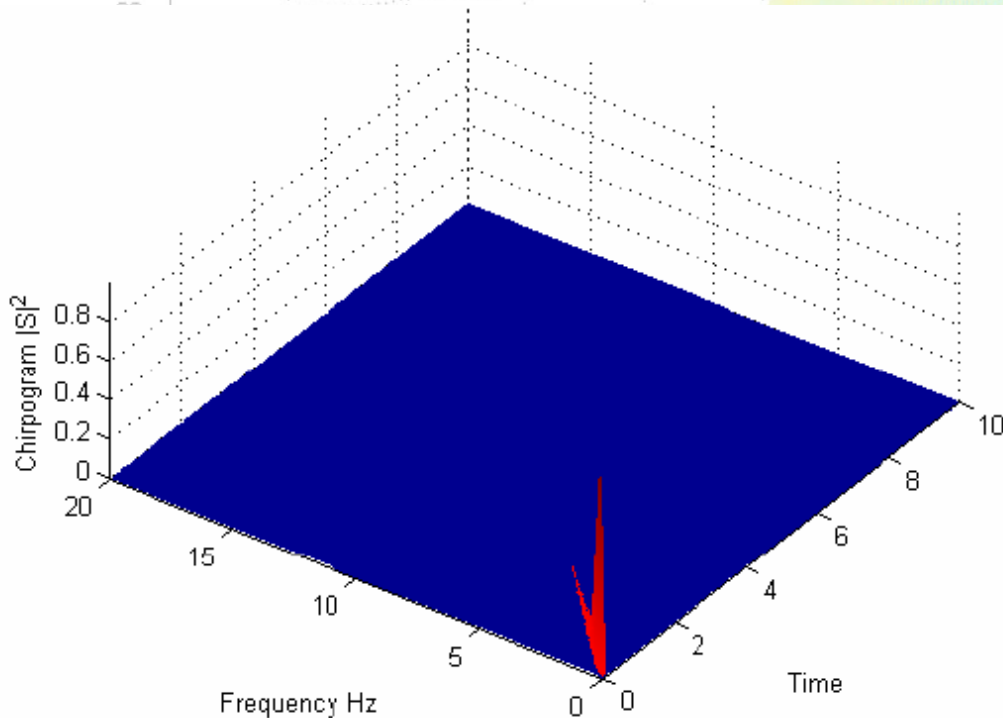
- Chirp rate ratio  $c_{20}/c_2=1$
- $c_{20}=5\text{Hz/s}$
- Constant signal amplitude



The chirpogram (i.e. the squared magnitude of the chirp-Fourier transform) ideally follows the instantaneous frequency without amplitude errors

# The Linear Chirp: the Kernel is Unmatched

- Chirp rate ratio  $c_2/c_{20}=0.8$
- $c_{20}=5\text{Hz/s}$   $c_2=4\text{Hz/s}$
- Constant signal amplitude



**The chirpogram does not follow the instantaneous frequency; there are essential amplitude errors**

# The Short Time Higher Order Chirp-Fourier Transform: Kernel Selection

$$T(\dots) = \int x(t) \psi(\dots) dt$$

The Fourier Transform  $e^{-2\pi \cdot i \cdot f \cdot \tau}$

The Wavelet Transform  $\psi(\text{scale}, \text{shift}, t)$

The Higher Order  
Chirp-Fourier  
Transform

Kernel proposed

$$e^{-2\pi \cdot j \cdot t \cdot \left( f + \frac{c_2}{2} t + \frac{c_3}{3} t^2 + \dots + \frac{c_n}{n} t^{n-1} \right)}$$



# The Short Time Higher Order Chirp-Fourier Transform

**Signal**

$$x(t) = e^{2\pi j \cdot t \left( f_o + \frac{c_{20}}{2}t + \frac{c_{30}}{3}t^2 + \dots + \frac{c_{n0}}{n}t^n \right)}$$

**The Short Time Higher Order Chirp-Fourier Transform**

$$S(f, T_0, c_2, c_3, \dots, c_n) = \frac{1}{T_k} \int_{-\infty}^{\infty} h_k(t - T_0) x(t) e^{-j2\pi \left( ft + \frac{c_2(t)}{2}t^2 + \frac{c_3(t)}{3}t^3 + \frac{c_4(t)}{4}t^4 + \dots + \frac{c_n(t)}{n}t^n \right)} dt$$

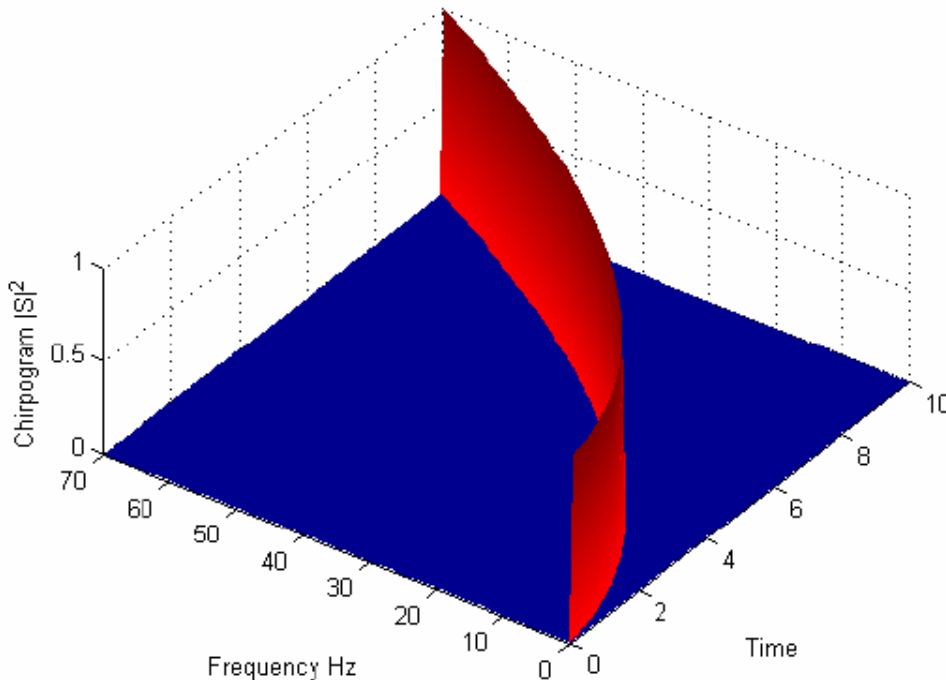
**Simulation:**

**Matched Kernel**

**Unmatched Kernel**

# The Matched Kernel

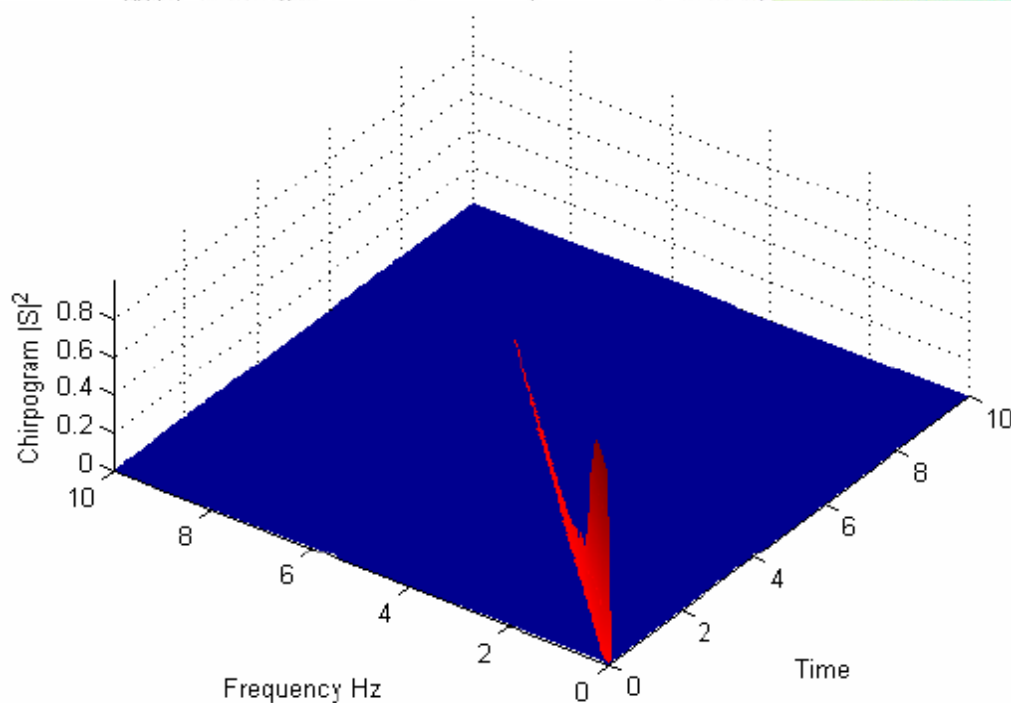
- **Signal  $f_0=0$ ;  $c_{20}=1$  Hz/s;  $c_{30}=0.5$  Hz/s<sup>2</sup>;  $c_{40}=0.01$  Hz/s<sup>3</sup>**
- **Kernel  $f=0$ ;  $c_2=1$  Hz/s;  $c_3=0.5$  Hz/s<sup>2</sup>;  $c_4=0.01$  Hz/s<sup>3</sup>**



The chirpogram ideally follows the instantaneous frequency without amplitude errors

# The Unmatched Kernel

- Signal  $f_0=0$ ;  $c_{20}=1$  Hz/s;  $c_{30}=0$  Hz/s<sup>2</sup>;  $c_{40}=0$  Hz/s<sup>3</sup>
- Kernel  $f=0$ ;  $c_2=1$  Hz/s;  $c_3=0.5$  Hz/s<sup>2</sup>;  $c_4=0.01$  Hz/s<sup>3</sup>



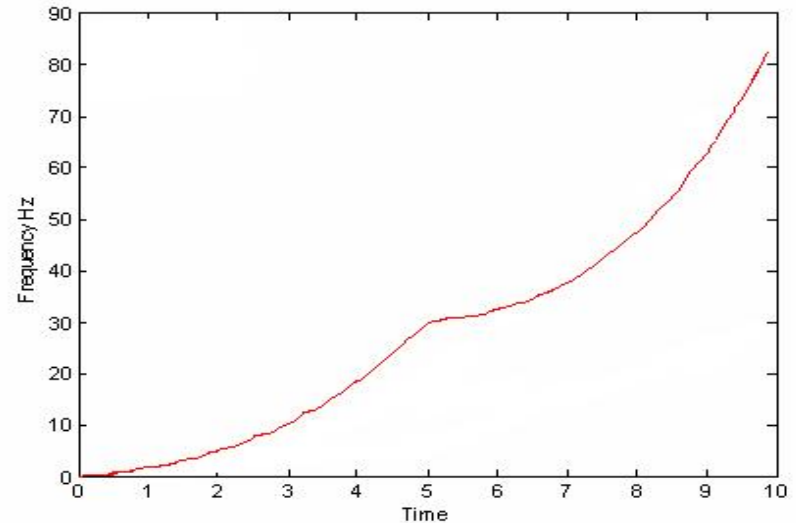
The chirpogram does not follow the instantaneous frequency; there are essential amplitude errors

# THE HIGHER ORDER PIECE-WISE CHIRP: A SIGNAL AND TRANSFORM KERNEL

## SIGNAL CHARACTERISTICS:

The piece-wise higher order chirp is characterized by:

- **C20:** the chirp rate
- **C30:** the frequency acceleration
- **C40, C50, ...:** the higher order parameters



## THE KERNEL CHARACTERISTICS:

The kernel is characterized by

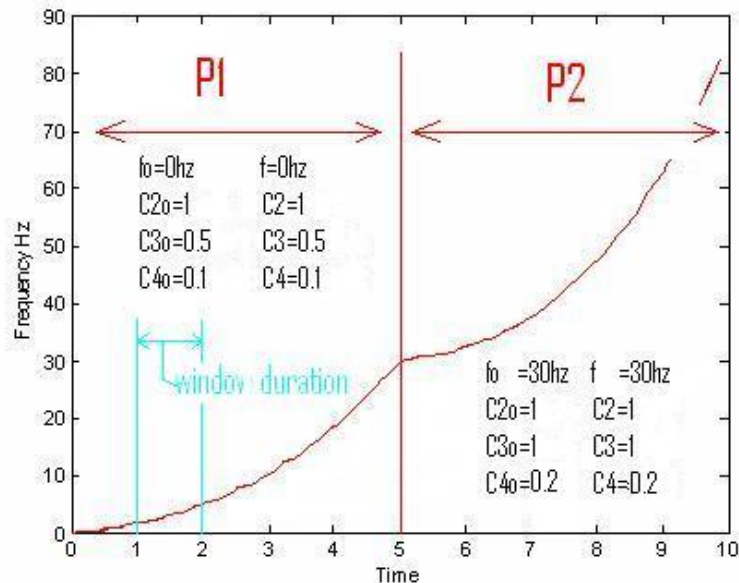
- **C2:** the chirp rate of the transform
- **C3:** the frequency acceleration of the transform
- **C4, C5, ...:** the higher order parameters of the transform

$$x(t) = e^{2\pi j \cdot t \left( f_0 + \frac{C_{20}}{2}t + \frac{C_{30}}{3}t^2 + \dots + \frac{C_{n0}}{n}t^n \right)}$$

**Kernel proposed**

$$e^{-2\pi j \cdot t \cdot \left( f + \frac{C_2}{2}t + \frac{C_3}{3}t^2 + \dots + \frac{C_n}{n}t^{n-1} \right)}$$

# THE HIGHER ORDER PIECE-WISE CHIRP: KERNEL IS MATCHED

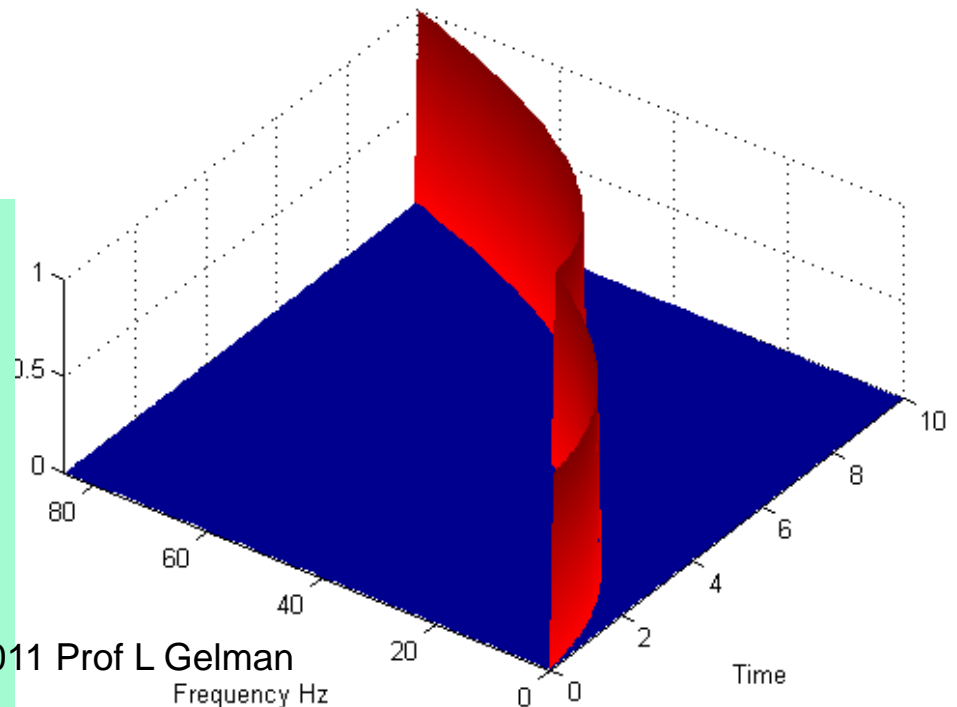


PARAMETERS OF THE SIGNAL AND KERNEL ARE MATCHED

- Sampling frequency is 200 Hz
- P1=0-5s
- P2=5-10s

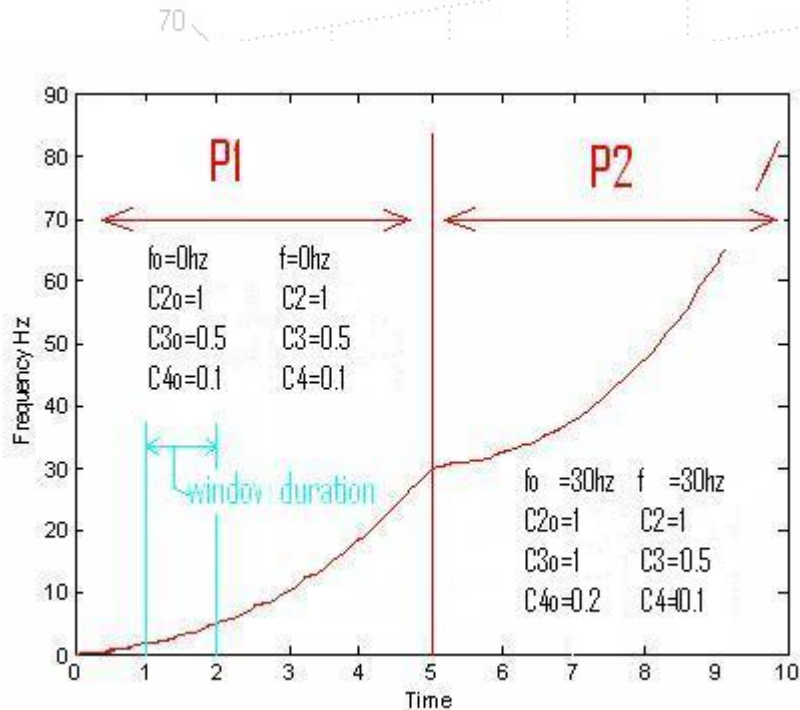
ONE CAN EVALUATE THE PIECE-WISE FREQUENCY-TIME DEPENDENCY OF THE SIGNAL AND PARAMETERS FOR EACH PART OF THIS DEPENDENCY AND

EMPLOY THE HIGHER ORDER CHIRP FOURIER TRANSFORM WITH THE ADAPTED PARAMETERS ON EACH SIGNAL PART.





# THE HIGHER ORDER PIECE-WISE CHIRP: KERNEL IS UNMATCHED

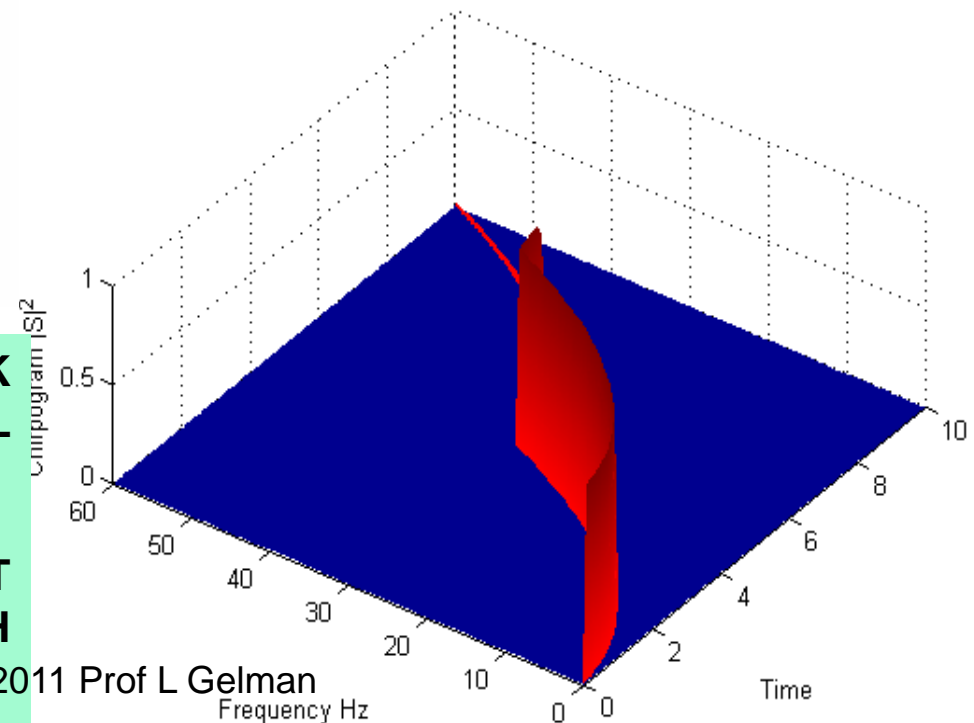


PARAMETERS OF THE SIGNAL AND KERNEL  
ARE UNMATCHED FOR **PERIOD 2**

Sampling frequency is 200 Hz  
P1=0-5s  
P2=5-10s

• THE TRANSFORM DOES NOT WORK PROPERLY WHEN KERNEL AND SIGNAL ARE UNMATCHED

• THE SIGNAL AMPLITUDE ON THE FIRST PERIOD IS ESTIMATED WITH HIGH ACCURACY



# The Adaptive Short Time Higher Order Chirp-Fourier Transforms

- Results in the previous slides show the essential advantage of the proposed transforms: they could be used for selective detection of the higher order chirps
- It could be done by the following on-line two step adaptation procedure:
- to evaluate the frequency-time dependency of the higher order chirp and parameters of this dependency
- to employ the short time higher order chirp-Fourier transforms with the adapted transform parameters:  $c_2/c_{20}=1$ ,  $c_3/c_{30}=1$ ,  $c_4/c_{40}=1 \dots c_n/c_{n0}=1$