

# Supporting Information for "Local hydraulic conductivity in heterogeneous porous media"

Quirine Krol<sup>1</sup>, Itzhak Fouxon<sup>1,2</sup>, Pascal Corso<sup>1</sup>, Markus Holzner<sup>1,2,3,4</sup>

<sup>1</sup>ETH Zurich, Stefano Franscini-Platz 5, 8093 Zurich, Switzerland

<sup>2</sup>Department of Computational Science and Engineering, Yonsei University, Seoul 120-749, South Korea

<sup>3</sup>Swiss Federal Institute for Water Science and Technology EAWAG

<sup>4</sup>Swiss Federal Institute for Forest, Snow and Landscape Research WSL

## Contents of this file

1. Direct numerical simulation of Stokes flow in porous media.
2. Pseudo code: Measuring local hydraulic conductivity.
3. Measuring the Transversal and Longitudinal Energy Dissipation tensor.

## Additional Supporting Information (Files uploaded separately)

1. Isopressure surfaces video
2. Pore identification video

## Introduction

Below we describe the necessary steps and specific settings of the analysis presented in methodology. The first part consists of the description of the direct numerical simulations performed that are used as a numerical experiment. In the second part we describe the

---

details of the extraction of iso pressure surfaces and fluxes from which the hydraulic conductivity is calculated and integrated along consecutive pores. In the last part we take three samples from the three porous media to test the hypothesis that is made in Eq.() of the main article.

**Direct Numerical Simulations** To generate heterogeneous porous media we have used Gaussian Random Fields to generate 3 porous media. A threshold is used to define the porous media-fluid interface  $\Gamma$  and its porosity. eq 0.6, .5 and .25 redto be evaluated!. These porous media are used as input for direct numerical simulations (OpenFOAM v. 4.1) ? (?) that solves the Navier-Stokes equations in the pore space. The boundary conditions are defined at the inlet  $p_1$  and outlet  $p_2$  and a no-slip for the porous media-fluid interface. A visualization of the three porous media an the result of the DNS is visualized in Fig. ??

- Three geometries generated by gaussian random fields, with porosity, specific surface area, Euler characteristic of
- DNS employed with boundary conditions at the inlet and outlet defined by  $\delta p$ . A no slip boundary condition is enforced on the domain walls as well as the porous media interface.

- Result of the DNS gives estimated Re numbers by

$$Re = u/s\eta \quad (1)$$

- Residuals were standard, check  $10^{-6}$  took about 8 hours using 32 cores using the Euler cluster.

**Extraction of pores based on isopressure surfaces** Then a chain of VTK-based image analysis techniques ? (? , ?) are employed to extract iso-pressure surfaces  $\mathcal{S}(p)$  and enumerate the disconnected areas identifying as an iso-pressure slice  $\mathcal{S}_i(p)$ , part of a pore and measure its surface area  $A_i(p)$ , sphericity  $\gamma_i(p)$ , average location  $\mathbf{x}_i(p)$  and average flux  $Q_i(p)$ . For each  $\mathcal{S}_i(p)$  its closest neighbor  $\mathcal{S}_j(p + \delta p)$  is identified by its smallest distance  $d_{i,j} = |\mathbf{x}_i(p) - \mathbf{x}_j(p + \delta p)|$ . By forward integration of the first iso-pressure patches  $\mathcal{S}_i(p_0)$  we identify all patches belonging to the same pore  $\mathcal{P}_l(\Delta p) = \{\mathcal{S}_k(p_i)\}$ . By conditioning the distances of consecutive iso pressure patches to a maximum, the ends of a pore is defined. When a splitting/merging of pores is at hand, the average position is rather sensitive, and the distance between two consecutive iso-pressure pore patches will exceed the maximum distance. Fig. ?? shows a visualization of the positions of the identified pores. For each  $\delta p$  we can now evaluate Eq. ?? and for each pore, we can evaluate Eq. ?. A visualization of an iso-pressure surface  $\mathcal{S}(p)$  and its deviation of patches is shown in Fig.??.

**Measuring the relative Longitudinal and Transversal energy dissipation on an isopressure surface** In the theoretical section of the paper we have derived expressions for the longitudinal and transversal energy dissipation tensors, by

$$|\nabla_i u_j|^2 \approx |\nabla_r u_p|^2 + |\nabla_p u_p|^2. \quad (2)$$

where we have assumed that the terms  $|\nabla_n u_n|^2$  and  $|\nabla_p u_n|^2$