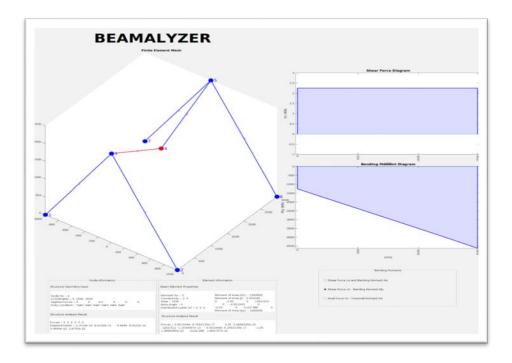
# **BEAMALYZER**



12/3/2015

# ECI 211 Final Project Report

Beamalyzer is a 3D finite element program to solve space frame problems of 1st Order. It's a GUI based program developed in Matlab with abilities of visualizing structure, deformed mesh and individual members deflection diagram and shear force & bending moment diagram

# **BEAMALYZER**

#### ECI 211 FINAL PROJECT REPORT

### INTRODUCTION

Beamalyzer is a 3-D finite element program for solving space frame problems. It's a GUI based program developed in Matlab. Some of the main features of this program are

- Very flexible input and output
- Visualization of geometry(mesh) and deformed structure
- Ability to take distributed loads and settlement at nodes
- Shear Force and Bending moment diagram
- Deflection Diagram of beams
- Ability to save files and reopen it later
- Easily extendable to accommodate temperature loads

#### INSIDE THE CODE

Beamalyzer is developed in Matlab using various subroutines. The basic flow of the program is as shown below

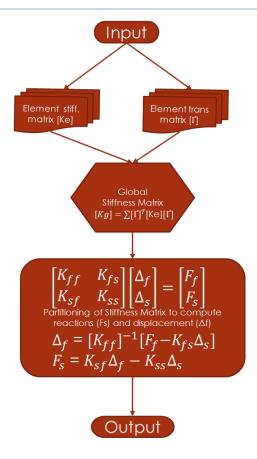


FIGURE 1 BASIC PROGRAM FLOW IN MATLAB

#### **INPUT**

The input basically comprises of three parts as shown below. Along with each part the matrix-variable name in Matlab are also given in brackets.

- Defining nodal geometry and forces
  - Number of nodes (nnodes)
  - Coordinates (coord)
  - Nodal Forces (concen)
  - Fixities (fixity)
- Defining element and its properties
  - O Number of Elements (nele)
  - Connectivity (ends)
  - Beta Angle (beta\_ang)
  - Distributed Load (w)
- Defining material and section properties
  - O Area of the crossection (A)
  - Moment of Area about z-axis (Izz)
  - Moment of Area about y-axis (lyy)
  - Moment of Area about x-axis (J)
  - O Young's Modulus (E)
  - Poisons ratio (v)

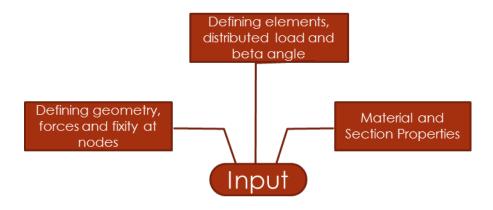


FIGURE 2 INPUT STRUCTURE FOR THE PROGRAM

#### ASSEMBLY OF GLOBAL STIFFNESS MATRIX AND FORCE VECTOR

Once the program has all the inputs with it, the next step is to create local stiffness matrix and transformation matrix for each individual elements and finally assemble it to generate the global stiffness matrix.

In order to take in account of the **distributed loads**, equivalent nodal loads are computed inside the program for each beam and are then added to the force vector.

And finally, the global stiffness matrix is portioned to calculate the reactions as supports and deflections at free joints.

Matlab subroutine *Finiteleyzer.m* takes all the input and performs the task. The code snippet with comments is shown below.

### Finitelyzer.m – main program which carries out the finite element analysis

```
function [DEFL, REACT, ELE_FOR, AFLAG]=Finiteleyzer( nnodes, nele, coord, concen, fixity, ends, A, Izz, Iyy, J, E, v, beta_ang, w)
        t = waitbar(0, 'Please wait...'); waitbar(0.1);
        DEFL=zeros(nnodes,6);
        REACT=zeros(nnodes,6);
        ELE_FOR=zeros(nele,12);
        % creating dof_id for each node
        node_id = 1:nnodes*6; node_id = reshape(node_id,6,nnodes)*; waitbar(0.15);
        % creating mem_id for each element
        mem_id = zeros(nele, 12); mem_id(:,1:6) = node_id(ends(:,1),:); mem_id(:,7:12) = node_id(ends(:,2),:);
        % creating free_dof and fixed_dof vectors
        D_{\text{vector}} = \text{fixity'}; D_{\text{vector}} = D_{\text{vector}}; free_dof = find(isnan(D_{\text{vector}})); fixed_dof = find(D_{\text{vector}} = 0); waitbar(D_{\text{vector}} = 0); waitbar(D_{
        % finding the length of element
        Length = sqrt(sum((coord(ends(:,1),:)'-coord(ends(:,2),:)').^2))'; waitbar(0.3);
        % finding x axis of the beam
        x_{axis} = (coord(ends(:,2),:)'-coord(ends(:,1),:)')'./([Length(:,1),Length(:,1),Length(:,1)]);
        % Building local stiffness stack
        k_{local\_stack} = zeros(nele, 12, 12); waitbar(0.35);
        for i=1:nele
```

```
 k\_local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),lyy(i,1),J(i,1),E(i,1),v(i,1),Length(i,1)); \\ \% \ reshape(k\_local\_stack(i,:,:),12,12); \\ (a) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),lyy(i,1),J(i,1),E(i,1),v(i,1),Length(i,1)); \\ \% \ reshape(k\_local\_stack(i,:,:),12,12); \\ (b) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),lyy(i,1),J(i,1),E(i,1),v(i,1),Length(i,1)); \\ \% \ reshape(k\_local\_stack(i,:,:),12,12); \\ (c) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),lyy(i,1),J(i,1),E(i,1),v(i,1),Length(i,1)); \\ \% \ reshape(k\_local\_stack(i,:,:),12,12); \\ (c) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),lyy(i,1),J(i,1),E(i,1),v(i,1),Length(i,1)); \\ \% \ reshape(k\_local\_stack(i,:,:),12,12); \\ (c) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),Length(i,1),Length(i,1)); \\ (c) \ local\_stack(i,:,:) = estiff(A(i,1),lzz(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),Length(i,1),
                           end
                           \% \ Building \ local\_global\_transformation\_stack
                           k_{trans_stack} = zeros(nele, 12, 12); waitbar(0.5);
                           for i=1:nele
                                      k_{trans_stack(i,:,:)} = etran(beta_ang(i,1),x_axis(i,:)'); %reshape(k_trans_stack(i,:,:),12,12)
                           % Building global_stiffness_stack
                           k_global_stack = zeros(nele, 12, 12); waitbar(0.6);
                           for i=1:nele
                                        k\_global\_stack(i,:,:) = (reshape(k\_trans\_stack(i,:,:), 12,12))!*(reshape(k\_local\_stack(i,:,:), 12,12))*(reshape(k\_trans\_stack(i,:,:), 12,12)); 
                           end
                           % Building total stiffness matrix
                           k_{total} = zeros(nnodes*6,nnodes*6); waitbar(0.7);
                           for i=1:nele
                                       k total(mem id(i,1:6), mem id(i,1:6)) = k total(mem id(i,1:6), mem id(i,1:6)) + reshape(k global stack(i,1:6,1:6),6,6);
                                       k_{total(mem_id(i,7:12),mem_id(i,1:6))} = k_{total(mem_id(i,7:12),mem_id(i,1:6))} + reshape(k_global_stack(i,7:12,1:6),6,6);
                                       k_{total(mem_id(i,1:6),mem_id(i,7:12))} = k_{total(mem_id(i,1:6),mem_id(i,7:12))} + reshape(k_global_stack(i,1:6,7:12),6,6);
                                       k_{total(mem_id(i,7:12),mem_id(i,7:12))} = k_{total(mem_id(i,7:12),mem_id(i,7:12))} + reshape(k_global_stack(i,7:12,7:12),6,6);
           \% Addding \ Distributed \ Loads , Temperature Loads .. etc to Nodes
                           concen_dl = zeros(nnodes, 6); waitbar(0.8);
                           for i=1:nele
                                      I = Length(i);
                                       F_{d} = [-w(i,1)*1/2;-w(i,2)*1/2;-w(i,3)*1/2;0;-w(i,3)*1^2/12;-w(i,2)*1^2/12;-w(i,1)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2
w(i,3)*1/2;0;w(i,3)*1^2/12;w(i,2)*1^2/12;
                                      F_d = (reshape(k_trans_stack(i,:,:),12,12))^**(-F_d);
                                      concen\_dl(ends(i, \frac{1}{2}),:) = concen\_dl(ends(i, \frac{1}{2}),:) + F\_d(\frac{1:6}{2})'; \\ concen\_dl(ends(i, \frac{2}{2}),:) = concen\_dl(ends(i, \frac{2}{2}),:) + F\_d(\frac{7:12}{2})'; \\ concen_dl(ends(i, \frac{2}),:) + F\_d(\frac{7:12}{2})'; \\ concen_dl(ends(i, \frac{2}{2}),:) + F\_d(
                           % Total Load vector
                           concen_tl = concen + concen_dl; waitbar(0.85);
                           % Partitioning the matrix
                           kff = k total(free dof, free dof);
                           kfs = k total(free dof, fixed dof);
                           ksf = k_total(fixed_dof,free_dof);
                           kss = k\_total(fixed\_dof,fixed\_dof);
                              if (det(kff)==0)
                                           errordlg('The structure is under-constrained','Error');
                                           return
                           % Building force vector
                           F_vector = concen_tl'; F_vector = F_vector(:);
                           D_{vector(free\_dof)} = kff \setminus (F_{vector(free\_dof)} - kfs*D_{vector(fixed\_dof)});
                           F_vector(fixed_dof) = ksf*D_vector(free_dof) + kss*D_vector(fixed_dof);
                           % Output matrix
                           DEFL = reshape(D_vector,6,nnodes)';
                           REACT = reshape(F_vector,6,nnodes)' - concen_tl;waitbar(0.95);
                           for i=1:nele
                                      ELE FOR(i,:) = (reshape(k local stack(i,:,:),12,12))*(reshape(k trans stack(i,:,:),12,12))*(D vector(mem_id(i,1:12)));
                                      I = Length(i); F_d = [-w(i,1)*1/2;-w(i,2)*1/2;-w(i,3)*1/2;0;-w(i,3)*1^2/12;-w(i,2)*1^2/2;-w(i,1)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2;-w(i,2)*1/2
                w(i,3)*1/2;0;w(i,3)*1^2/12;w(i,2)*1^2/12];
                                     ELE_FOR(i,:) = ELE_FOR(i,:) + F_d(:)';
                           ELE_FOR; AFLAG=1;
                end
```

**Finitelyzer.m** uses two additional sub-routines that help in generating element stiffness matrix (**estiff.m**) and element transformation matrix (**etran.m**). Both subroutines are shown below.

#### Estiff.m - Program to generate element stiffness matrix

```
function[elk] = estiff(A,lz,ly,J,E,v,L)
  % Genearal Stiffness Matrix of Beam.
  % A = Crossectional-Area of The Beam.
  % Iz = Moment of Area of Beam about Izz-Axis.
  % ly = Moment of Area of Beam about lyy-Axis.
  % J = Torsoinal Moment of Area.
  % E = Young's Modulus of Material
  % v = Poison's ratio
  % L = Length of the Beam
  elk=E* [A/L
                 ,0
              ,12*lz/L^3 ,0
                                                         ,6*lz/L<mark>^2</mark>
        0
                                   ,0
                                               ,0
              ,0
                       ,12*ly/L^3 ,0
                                                ,-6*ly/L^2 ,0
        0
                                                                                                               ,-6*ly/L^2 ,0
              ,0
                       ,0
                                J/(2*(1
                                          v)*L) ,0
                                                                                             _{,-J/(2*(1+v)*L),0}
              ,0
                       ,-6*ly/L^2 ,0
                                               <mark>,4</mark>*ly/L
                                                                  ,0
                                                                           ,0
        0
                                                         ,0
                                                                                                            ,2*ly/L
                                                                                                                      ,0
                                              ,0
                                                        <mark>,4</mark>*lz/L
                                                                                                           ,0
                                                                  ,0
                                                                           ,-6*lz/L^2 ,0
        0
              ,6*lz/L^2 ,0
                                                                                                                     ,2*lz/L
              ,0
        -A/L
                                                                                  ,0
                                                                             ,12*lz/L^3 ,0
              ,-12*lz/L^3,0
                                                        ,-6*lz/L^2 ,0
                                                                                                              ,0
                                                                                                                        ,-6*lz/L^2 ;
                                               ,0
        0
              ,0
                       ,-12*ly/L^3 ,0
                                                                                     ,12*ly/L^3 ,0
                                               ,6*ly/L^2 ,0
        0
                                                                             ,0
                                                        ,0
                                                                                            ,J/(2*(1+v)*L) ,0
                                                                                                                      ,0
                                ,-J/(2*(1+v)*L),0
        0
              ,0
                                                                  ,0
                                               <mark>,2</mark>*ly/L
                                                                                    ,6*ly/L^2 ,0
        0
                       ,-6*ly/L^2 ,0
                                                                  ,0
              ,6*lz/L^2 ,0
                                                                           ,-6*lz/L^2 ,0
                                               ,0
                                                        ,2*Iz/L
                                                                                                ,0
                                                                                                                     ,4*Iz/L
```

#### Etran.m -Program to generate element transformation matrix

```
% Transformation Matrix for 3D frame member.
% beta_angle = Crossectional-Area of The Beam.
% xaxis
            = Moment of Area of Beam about Izz-Axis.
R_{zero} = zeros(3,3); e_y = [0;1;0];
alpha_x = xaxis./sqrt(sum(xaxis.^2));
if(alpha_x(1))=0 & (alpha_x(2))=1 | alpha_x(2)=-1) & alpha_x(3)==0;
  e_y = [-1;0;0];
end
alpha_z = cross(alpha_x,e_y)./sqrt(sum(cross(alpha_x,e_y).^2));
alpha_y = cross(alpha_z, alpha_x)./sqrt(sum(cross(alpha_z, alpha_x).^2));
R_axis = [ alpha_x'; alpha_y'; alpha_z'];
R_beta = [1,0]
       0 ,cos(beta_angle) ,sin(beta_angle)
          ,=sin(beta_angle) ,cos(beta_angle)
R = R_beta * R_axis;
gamma = [R]
                    ,R_zero
                              ,R_zero ,R_zero ;
                         ,R_zero
                 ,R
                                   ,R_zero ;
       R zero
       R zero
                 ,R zero
                           ,R
                                   ,R_zero
       R zero
                 ,R_zero
                           ,R_zero
```

end

end

function[gamma] = etran(beta\_angle,xaxis)

The **Finitelyzer.m** subroutine then spits out the output mainly deflection (**DEFL**), reactions (**REACT**) and element forces (**ELE\_FOR**). Also it checks for the stability of structure and sends error message if the structure is not stable.

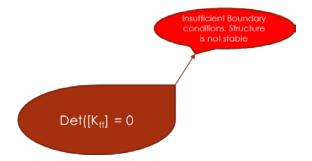


FIGURE 3 CHECKING THE STABILITY OF STRUCTURE

#### **OUTPUT - Reaction at supports, Deflection and element forces**

After the partitioning of matrix, the equations are solved to get the reaction at supports, deflection and element forces as commented in the code below.

```
% Partitioning the matrix
         kff = k_total(free_dof,free_dof);
         kfs = k_{total}(free_{dof}, fixed_{dof});
         ksf = k\_total(fixed\_dof,free\_dof);
         kss = k\_total(fixed\_dof,fixed\_dof);
         % Building force vector
         F_vector = concen_tl'; F_vector = F_vector(:);
         D vector(free dof) = kff\(F \ vector(free \ dof)-kfs*D \ vector(fixed \ dof));
         F_vector(fixed_dof) = ksf*D_vector(free_dof) + kss*D_vector(fixed_dof);
         % Output matrix
         DEFL = reshape(D_vector,6,nnodes)';
         REACT = reshape(F_vector, 6, nnodes)' - concen_tl;
         for i=1:nele
                  ELE_FOR(i,:) = (reshape(k\_local\_stack(i,:,:),12,12))*(reshape(k\_trans\_stack(i,:,:),12,12))*(D\_vector(mem\_id(i,1:12)));
                  I = Length(i); F_d = [-w(i,1)*1/2; -w(i,2)*1/2; -w(i,3)*1/2; 0; -w(i,3)*1^2/12; -w(i,2)*1^2/12; -w(i,1)*1/2; -w(i,2)*1/2; -w(i,2)*1/2
w(i,3)*1/2;0;w(i,3)*1^2/12;w(i,2)*1^2/12;
                  ELE_FOR(i,:) = ELE_FOR(i,:) + F_d(:)';
         end
```

From the outputs obtained the user can then draw the bending moment and shear force diagram for the beams, Also the deflection diagram for each beam can be drawn solving the differential equation of beam. The program Beamalyzer does all that for the user and presents a graphical results as would be illustrated later in the report.

The outputs are stored in the matrix variable **DEFL**, **REACT** and **ELE-FOR** in the program. The **AFLAG** variable return 1 if the structure is stable else its returns 0.

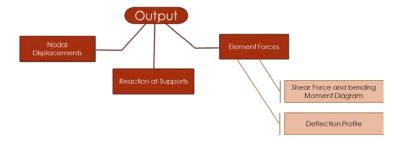


FIGURE 4 OUTPUT GENERATED BY THE PROGRAM

The subroutine **SFBMD.m** creates bending moment and shear force diagram for individual beams along all the axis of the beam. The Matlab subroutine is shown below.

#### SFBMD.m - Program to generate shear force & bending moment diagram about any axis

```
function SFBMD(option, forces, distloads, len)
  Xmin = -0.01*len;
  Xmax = 1.01*len;
  if(option==1)
     sf1 = forces(2); sf2 = forces(8);
     bm1 = forces(6); bm2 = forces(12);
     m = 1; w = distloads(2);
     sf\_label='Vy (KN)'; bm\_label='Mz (KN)';
  end
  if(option==2)
     sf1 = forces(3); sf2 = forces(9);
     bm1 = forces(5); bm2 = forces(11);
     m = 1; w = distloads(3);
     sf_label='Vz (KN)'; bm_label='My (KN)';
  end
  if(option==3)
     sf1 = forces(1); sf2 = forces(7);
     bm1 = forces(4); bm2 = forces(10);
     m = 0; w = distloads(1);
     sf\_label='\forall x \ (KN)'; \ bm\_label='Mx \ (KN)'; \\
  end
  if(option \sim = 0)
     h = waitbar(0, 'Please wait...');
     waitbar(0.2);
     syms sf_(x) bm_(x);
     % sf(x)=dsolve(diff(sf_1)==w_sf_0)==sf1,sf_0(en)==-sf2);
     %bm(x) = dsolve(diff(bm_1) = 1*m*sf(x),bm_(0) = -bm1,bm_(len) = -bm2);
     sf(x)=dsolve(diff(sf_,1)==w,sf_(0)==sf1); waitbar(0.5);
     bm(x)=dsolve(diff(bm_1))==1*m*sf(x),bm_0)==-bm1);waitbar(0.7);
     diff(bm_{-}, 1) == 1*m*sf(x);
     bm_{(0)} = -bm1;
     bm_(len)==bm2;
     x = linspace(0, len);
     %% Shear Force Diagram
     Structural_Diagrams_1 = findobj('Tag','Structural_Diagrams_1');
     cla(Structural_Diagrams_1); axes(Structural_Diagrams_1);
     X = [0,x,len]; Y = [0,sf(x),0];
     fill(X,Y,'b','facealpha',0.15,'edgecolor','none'); hold on;
     plot([0,x,len],[0,sf(x),0],b',Linewidth',2);hold off;
```

```
refline(0,0); xlabel('x(m)'); ylabel(sf_label);
     title('Shear Force Diagram', FontSize', 12);

Ymin = int64(min(Y)-1); Ymax = int64(max(Y)+1);
     Structural_Diagrams_1.XLim = [Xmin Xmax];
     Structural_Diagrams_1.YLim =[Ymin Ymax];
     rotateXLabels( Structural_Diagrams_1, 90 );
     set(Structural_Diagrams_1, 'FontSize', 10);
     Structural_Diagrams_1.Tag = 'Structural_Diagrams_1';
     %% Bending Moment Diagram
     Structural_Diagrams_2 = findobj('Tag','Structural_Diagrams_2');
     cla(Structural_Diagrams_2); axes(Structural_Diagrams_2);
     X = [0,x,len]; Y = [0,-bm(x),0];
     fill(X,Y,'b','facealpha',0.15,'edgecolor','none'); hold on;
     plot([0,x,len],[0,-bm(x),0],b','Linewidth',2);hold off;
     refline(0,0); xlabel('x(m)'); ylabel(bm_label);
     title('Bending Moment Diagram', 'FontSize', 12);
     Ymin = int64(min(Y)-1); \quad Ymax = int64(max(Y)+1);
     Structural\_Diagrams\_2.XLim = [Xmin Xmax];
     Structural_Diagrams_2.YLim = [Ymin Ymax];
     rotateXLabels(Structural_Diagrams_2, 90);
     set(Structural_Diagrams_2, FontSize', 10);
     Structural Diagrams 2.Tag = 'Structural Diagrams 2';
     waitbar(1);
     close(h)
  end
end
% Example Cantelever load with concentrated force at the end; SFBMD(1,[0,1,0,0,0,1,0,0,-1,0,0,0,0],[0,0,0],10)
% Example Cantilever example with distributed load; SFBMD(1,[0,10,0,0,0,50,0,0,0,0,0,0],[0,-1,0],10)
```

Similarly, to draw deflection diagram Matlab subroutine **DD.m** is used. The code for deflection diagram is shown below.

#### DD.m- Deflection Diagram for beams

```
function DD(forces,dsp,distloads,len,E,lzz,lyy,J,A)

Xmin = -0.01*len;

Xmax = 1.01*len;

Structural_Diagrams_2 = findobj('Tag','Structural_Diagrams_2');
cla(Structural_Diagrams_2);

Structural_Diagrams_1 = findobj('Tag','Structural_Diagrams_1');
cla(Structural_Diagrams_1); axes (Structural_Diagrams_1);

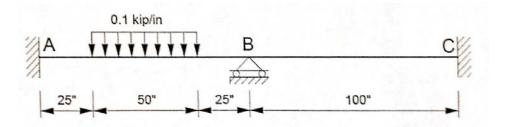
t = waitbar(0,'Please wait...');
waitbar(0.2);

%%%%% Vy Mz --> gives y coordinates
sf1 = forces(2); sf2 = forces(8);
bm1 = forces(6); bm2 = forces(12);
m = 1; w = distloads(2);
```

```
syms sf_y(x) bm_z(x) y_(x); Dy_ = diff(y_, x);
     sfy(x)=dsolve(diff(sf_y,1)==w,sf_y(0)==sf1);waitbar(0.3);
     bmz(x)=dsolve(diff(bm_z,1)==1*m*sfy(x),bm_z(0)==-bm1); waitbar(0.4);
     Y(x) = dsolve(diff(y_,2) == bmz(x)/lzz/E, y_(0) == dsp(2), y_(len) == dsp(8)); waitbar(0.5);
  % x = linspace(0,len);
  % plot(x,Y(x)); hold on;
  \%\%\%\%\% Vz My --> gives z coordinates
     sf1 = forces(3); sf2 = forces(9);
     bm1 = forces(5); bm2 = forces(11);
     m = 1; w = distloads(3);
     syms sf_z(x) bm_y(x) z_x(x); Dz_z = diff(z_x, x);
     sfz(x)=dsolve(diff(sf_z,1)==w,sf_z(0)==sf1);waitbar(0.6);
     bmy(x) = dsolve(diff(bm_y, 1)) = 1*m*sfz(x), bm_y(0) = -bm1); waitbar(0.7);
     Z(x) = dsolve(diff(z_,2) == bmy(x)/E/lyy, z_(0) == dsp(3), z_(len) == dsp(9)); waitbar(0.8);
  x = linspace(0, len);
  plot3(Structural_Diagrams_1,x,Y(x),Z(x),b',Linewidth',2); waitbar(0.95);
  xlabel(Structural\_Diagrams\_1, 'x(m)');
  ylabel(Structural_Diagrams_1,'Disp_y(m)');
  zlabel(Structural_Diagrams_1,'Disp_z(m)');
  title(Structural_Diagrams_1,'Deflection Diagram','FontSize',12)
  Ymin = int64(min(Y(x))-1); Ymax = int64(max(Y(x))+1);
  % Structural_Diagrams_1.CameraPosition=[0,0,1];
  view(Structural_Diagrams_1,[0,0,1]);
  waitbar(1);
  close(t);
end
% Example Cantelever load with concentrated force at the end; DD([0,1,0,0,0,10,0,-1,0,0,0,0],[0,0,0,0,0,0,0,0,-333.33,0,0,0,-
50],[0,0,0],10,1,1,1,1,1)
% Example Cantilever example with distributed load; DD([0,10,0,0,0,50,0,0,0,0,0],[0,0,0,0,0,0,0,0,0,0,0,-1250,0,0,0,-166.66],[0,-1,0],10,1,1,1,1,1)
```

#### DEMONSTRATION OF BEAMALYZER

In this section we are going to see how Beamalyzer works i.e. how to give inputs, plot mesh and generate outputs and visualize the structure and draw bending moment, shear force and deflection diagrams. We would be using the following structure as shown below to see show how Beamalyzer works. To run the program just type Beamalyzer in Matlab.



#### 1. Input

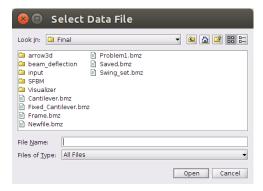
In Beamalyzer, Input can be given through a number of ways as described below

Through file – Beamalyzer has an option to load input or analysis file directly into the program. A
typical file for this problem would look like as shown below

```
- Nodal geometry force and boundary conditions
   nnodes
 coord
0.000000 0.000000 0.000000
25.000000 0.000000 0.000000
175.000000 0.000000 0.000000
100.0000000 0.000000 0.000000
200.000000 0.000000 0.000000

        concen
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
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        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        .000000
        <th
- Element connectivity and distributed loads
   --- Material properties of beams
lzz
21.333330
21.333330
21.333330
21.333330
lyy
21.333330
21.333330
21.333330
21.333330
```

The file is given to the program using the file menu option on the top.



A message is prompted about the success of import as shown below.



Manual Input – Beamalyzer has also a flexible way of defining input variable (Nodal geometry,
Element Properties and Material & Section properties) directly in the program through its GUI interface.
Different tabs corresponding to three different inputs has been made to directly edit the input for the structure. The user can navigate to individual tabs

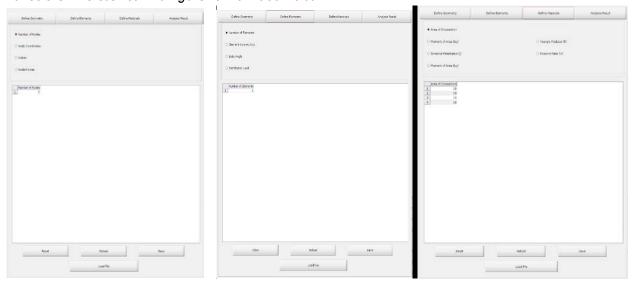


FIGURE 5 MANUAL EDITING OF INPUT THROUGH GUI INTERFACE

The clear, reload, save and load file command provides more flexibility in editing the input.

#### 2. Visualizing the Geometric Mesh

Through Beamalyzer one can visualize the mesh and the nodal forces on the structure. To do this, the user has to just press the 'Check Geometry Mesh' option.

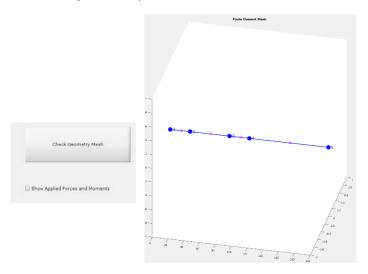


FIGURE 6 VISULIZING THE GEOMETRIC MESH OF THE STRUCTURE

#### 3. ANALYSIS of the structure

To analyze the structure the user has to just press the analyze button located on the bottom-left of beamalyzer application window. The program takes some time to solve the equations and thus shows a wait bar to tell the user the percentage of work completed and remaining so that the user made aware about the time taken by the program.

If there are any errors i.e. the structure is unstable an error message indicating an unstable structure is thrown. The results of the analysis can be seen the last 'Analysis Result' tab as shown below.

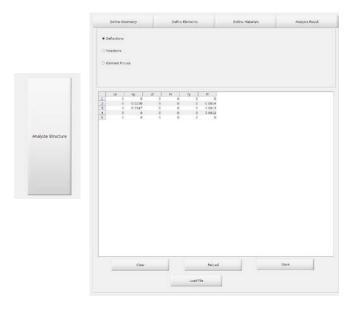


FIGURE 7 PICTURE SHOWING THE ANALYSIS BUTTON AND RESULT PRESENTED IN 'ANALYSIS' TAB

#### 4. Visualization of Deformed Structure

Beamalyzer has an option to visualize the deformed structure by pressing the '**Deformed Structure**' button. There is also an option to control the magnification of deformation if in case the deformations are too small to reflect in the deformed structure. The deformed structure for the sample structure is shown below.

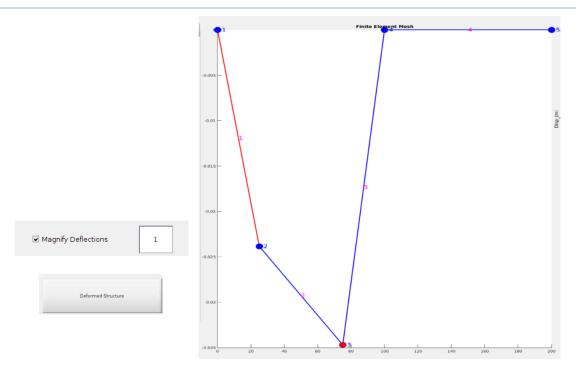


FIGURE 8 VISUALIZING DEFORMED STRUCTURE

### 5. Shear Force, Deflection and Bending Moment Diagram

Beamalyzer has an option to draw the shear force and bending moment and deflection diagram for any beam in 3-D space along local coordinates of that beam. The user can select any beam and node and can see the information of that beam or node. The information panel shows the information about the selected nodes and elements. An example for the node and element selected in figure 8 has been shown below.



FIGURE 9 INFORMATION PANEL FOR SELECTED NODES AND ELEMENTS

The user can then draw the shear force and bending moment diagram for the selected beam. An example of bending moment diagram for the selected beam for the given sample problem is shown below.

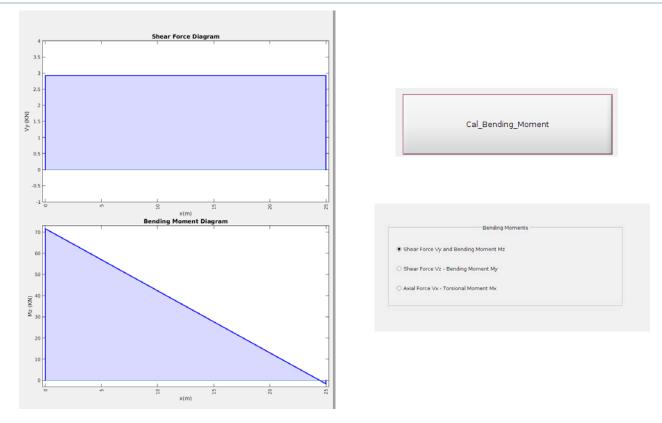


FIGURE 10 DRAWING SHEAR FORCE AND BENDING MOMENT DIAGRAM FOR THE SELECTED BEAM

Also, the user has the option to draw deflection diagrams for the selected beam as shown below by just pressing the 'Deflection Diagram' button.

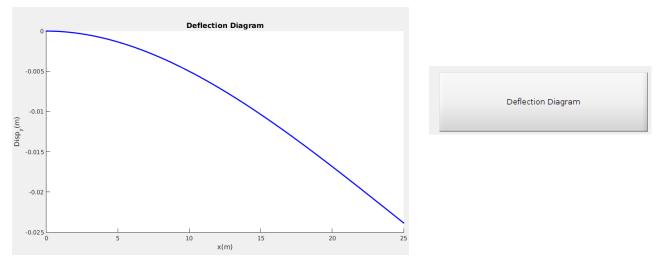


FIGURE 11 DEFLECTION DIAGRAM OF THE SELECTED BEAM

## 6. Save the Analysis/Result File

Beamalyzer has option to save the analysis result along with all the inputs for the structure to any folder. The analysis results just gets appended to the input file at the end. The analysis results appended to the file would look like as shown below.

\_\_\_\_\_\_ Analysis Result \_\_\_\_\_\_

#### , ind., / 510 N

#### DEFL

 $\begin{array}{c} 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.001414\ 0.000000\ -0.034694\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.001269\ 0.000000$ 

#### REACT

 $\begin{array}{c} 0.000000\ 2.929687\ 0.000000\ 0.000000\ 0.000000\ 71.614583\\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\\ 0.000000\ 2.500000\ 0.000000\ 0.000000\ 0.000000\ 0.000000\\ 0.000000\ -0.429688\ 0.000000\ 0.000000\ 0.000000\ 0.14322917 \end{array}$ 

#### ELE FOR

 $\begin{array}{c} 0.0\overline{0}00000 \ 2.929687 \ 0.000000 \ 0.000000 \ 0.000000 \ 0.000000 \ 71.614583 \ 0.000000 \ -2.929687 \ 0.000000 \ 0.000000 \ 0.000000 \ 1.627604 \ 0.000000 \ 2.929688 \ 0.000000 \ 0.000000 \ 0.000000 \ 0.000000 \ -1.627604 \ 0.000000 \ 2.070313 \ 0.000000 \ 0.000000 \ 0.000000 \ 23.111979 \ 0.000000 \ 2.070313 \ 0.000000 \ 0.000000 \ 0.000000 \ -28.645833 \ 0.000000 \ 0.429688 \ 0.000000 \ 0.000000 \ 0.000000 \ 2.845833 \ 0.000000 \ -0.429688 \ 0.000000 \ 0.000000 \ 14.322917 \end{array}$ 

The user can load or edit this file and can be used again in beamalyzer application. This feature makes the reusability of input files again and again with minimum changes.

# **SWING SET VERIFICATION PROBLEM**

The 3-D swing set problem was verified using Beamalyzer program. The input file for this verification problem is saved in folder **Examples** with name **Swing\_set.bmz**. The input file for Beamalyzer for this structure is shown below.

Input File to Beamalyzer	
Nodal geometry force and boundary conditions	
nnodes	
7	
coord	
-1000.000000 0.000000 0.000000 1000.000000 0.000000 0.000000	
1000.000000 0.000000 0.000000 0.000000 0.000000 2500.000000	
0.000000 1500.000000 2500.000000	
0.000000 3000.000000 2500.000000	
1000.00000 3000.000000 0.000000	
-1000.000000 3000.000000 0.000000	
concen	
0.000000 0.000000 0.000000 0.000000 0.000000	
0.000000 0.000000 0.000000 0.000000 0.000000	
0.000000 0.000000 0.000000 0.000000 0.000000	
0.000000 0.000000	
0.000000 0.000000 0.000000 0.000000 0.000000	
0.000000 0.000000 0.000000 0.000000 0.000000	
frage.	
fixity 0.000000 0.000000 NaN NaN NaN	
0.000000 0.000000 NaN NaN NaN	
NaN NaN NaN NaN NaN NaN	
NaN NaN NaN NaN NaN	
NaN NaN NaN NaN NaN	
0.000000 0.000000 NaN NaN NaN	
0.000000 0.000000 NaN NaN NaN	
Element connectivity and distributed loads	
nele	
6	
ends	
13	
23	
3 4	
4.5	
5 6 5 7	
beta_ang	
0.000000 0.000000	
0.000000	

```
0.000000
0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000\ 0.000000\ 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
--- Material properties of beams
1430.000000
1430.000000
1430.000000
1430.000000
1430.000000
1430.000000
200.000000
200.000000
200.000000
200.000000
200.000000
200.000000
0.300000
0.300000
0.300000
0.300000
0.300000
0.300000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
1260000.000000
2520000.000000
2520000.000000
2520000.000000
2520000.000000
2520000.000000
2520000.000000
```

Visualization of Structural Mesh in Beamalyzer

The mesh for the given swing set problem was visualized in Beamalyzer to see that the program takes all the correct values and the structure looks the same that's intended to be. The mesh is shown in the figure below. The mesh shows the node numbering, element numbering and the nodal forces applied.

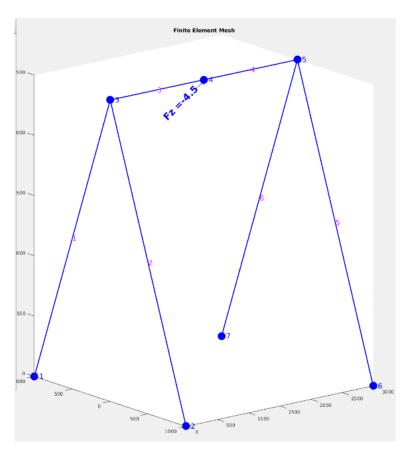


FIGURE 12 VISUALIZATION OF THE STRUCTURE MESH OF VERIFICATION PROBLEM

#### **Results from the Analysis**

The structure was then analyzed to get the final reactions at support, displacements at free ends and individual beam-element forces.

	Rx	Ry	Rz	Mx	My	Mz
1	0.4498	0.2505	1.1250	0	0	0
2	-0.4498	0.2505	1.1250	0	0	0
3	0	0	0	0	0	0
4	0	0	0	0	0	0
5	0	0	0	0	0	0
6	-0.4498	-0.2505	1.1250	0	0	0
7	0	0	0	0	0	0

	ux	uy	uz	rx	ry	rz
1	0	0	0	7.5737e-04	2.5418e-06	-0.0013
2	0	0	0	7.5737e-04	-2.5418e-06	0.0013
3	6.5238e-19	0.0026	-0.0123	-0.0026	4.4301e-22	-8.2405e-20
4	8.1897e-17	-3.7113e-12	-4.4649	-3.6245e-16	1.3905e-21	9.0591e-21
5	-4.7729e-18	-0.0026	-0.0123	0.0026	-1.6843e-21	5.7019e-20
6	0	0	0	-7.5737e-04	-2.5418e-06	-0.0013
7	0	0	0	-7.5737e-04	2.5418e-06	0.0013

FIGURE 13 REACTION AT NODES

FIGURE 14 DEFLECTION AT NODES

	Rx_1	Ry_1	Rz_1	Mx_1	My_1	Mz_1	Rx_2	Ry_2	Rz_2	Mx_2	My_2	Mz_2
1	1.2116	0.2505	1.7670e-04	-2.2913e-14	-2.8100e-17	5.1115e-14	-1.2116	-0.2505	-1.7670e-04	2.2913e-14	-0.4758	674.5522
2	1.2116	0.2505	-1.7670e-04	1.9719e-14	8.2922e-17	6.2572e-14	-1.2116	-0.2505	1.7670e-04	-1.9719e-14	0.4758	674.5522
3	0.5010	2.3507e-17	2.2500	-1.2244e-16	-1.2526e+03	2.2644e-15	-0.5010	-2.3507e-17	-2.2500	1.2244e-16	-2.1224e+03	3.2996e-14
4	0.5010	-3.3252e-17	-2.2500	3.9735e-16	2.1224e+03	-3.2996e-14	-0.5010	3.3252e-17	2.2500	-3.9735e-16	1.2526e+03	-1.6882e-14
5	1.2116	0.2505	-1.7670e-04	0	0.4758	674.5522	-1.2116	-0.2505	1.7670e-04	0	1.1102e-16	0
6	1.2116	0.2505	1.7670e-04	0	-0.4758	674.5522	-1.2116	-0.2505	-1.7670e-04	0	1.1102e-16	0

FIGURE 15 BEAM ELEMENT FORCES

#### **Visualization of Deformed Structure**

The deformed mesh is shown in the figure below

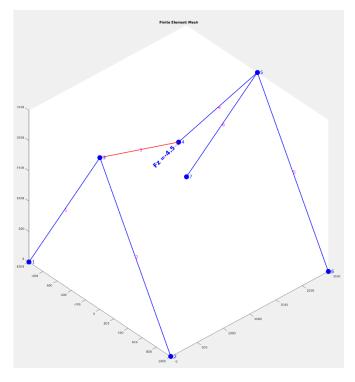


FIGURE 16 DEFORMED STRUCTURE AFTER LOAD APPLICATION

Visualizing Bending Moment, Shear force diagrams and deflection diagrams

An example of bending moment, shear force and deflection diagram of the selected beam in Figure 16 is shown below.

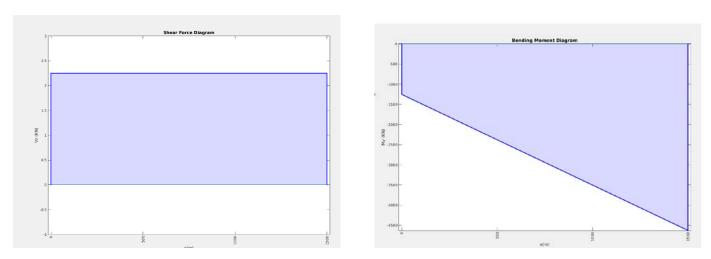


FIGURE 17 SHEAR FORCE ( $V_z$ ) AND BENDING MOMENT ( $M_X$ ) DIAGRAM OF BEAM 3

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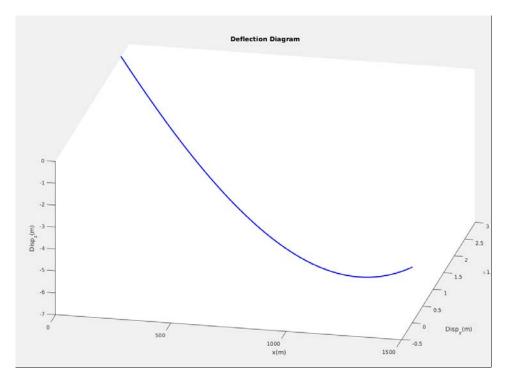


FIGURE 18 3-D DEFLECTION DIAGRAM FOR BEAM 3

#### Reporting Desired Results asked the Verification problem

In the model analyzed in Beamalyzer

- Node a corresponds to node no. 1
- Node b corresponds to node no. 2
- Node c corresponds to node no. 3
- Node d corresponds to node no. 4
- Element a-c corresponds to element no. 1
- Element c-b corresponds to element no. 2 [from node b (2) to node c (3)]
- Element c-d corresponds to element no. 3

#### Thus,

#### 1. Deflection at **node c** and **d** are

Deflection at nodes c and d							
Node No	u v w Ox Oy					Θz	
С	0	0.002628	-0.01229	-0.00259	0	0	
d	0	0	-4.46491	0	0	0	

#### 2. Reactions at node a and b are

Reactions at nodes a and b								
Node No	Fx (kN)	Fx (kN) Fy (kN) Fz (kN) Mx (kN-mm) My (kN-mm						
а	0.44981	0.250522	1.125	0	0	0		
b	-0.44981	0.250522	1.125	0	0	0		

### 3. Element Forces

	Element Forces in Local reactions for element a-c, c-b and c-d											
Element	Fx1 (kN)	Fy1 (kN)	Fz1 (kN)	Mx1 (kN-mm)	My1 (kN-mm)	Mz1 (kN-mm)	Fx2 (kN)	Fy2 (kN)	Fz2 (kN)	Mx2 (kN-mm)	My2 (kN-mm)	Mz2 (kN-mm)
а-с	1.211591	0.250522	0.000177	0	0	0	-1.211591	-0.25052	-0.00018	0	-0.475776	674.5522
c-b	1.211591	0.250522	-0.00018	0	0	0	-1.211591	-0.25052	0.000177	0	0.475776	674.5522
c-d	0.501045	0	2.25	0	-1252.61199	0	-0.501045	0	-2.25	0	-2122.38801	0

### 4. Axial Forces of beams a-c, c-b and c-d

Axial Force						
Element	Axial Force (kN)					
а-с	1.211591					
c-p	1.211591					
c-d	0.501045					