

# 热统习题的部分答案 (野生版)

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# 1 第一章

## 1.1 习题 1.6

$$\begin{aligned}
 \alpha &= \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{pV} \Rightarrow \left( \frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{p} \\
 &\Rightarrow V = \frac{\nu RT}{p} + g(p) \quad \text{代入 } \kappa = \frac{1}{p} + \frac{a}{V} = -\frac{1}{V} \left( \frac{\partial V}{\partial p} \right)_T \\
 &\Rightarrow d(pg(p)) = -\frac{a}{2} dp^2 \\
 &\Rightarrow pg(p) = -\frac{a}{2} p^2 + \text{const} \quad \text{代入第二行式子并整理} \\
 &\Rightarrow pV = \nu RT - \frac{a}{2} p^2 + \text{const}.
 \end{aligned}$$

## 1.2 习题 1.8

1) 利用广延量假设,

$$\begin{aligned}
 S = Ns, V = Nv, U = Nu &\Rightarrow s = A(vu)^{1/3} \\
 &\Rightarrow Tds = TA \frac{vdu + u dv}{3(vu)^{2/3}} = du + p dv \\
 du, dv \text{ 前的系数对应相等并恢复广延量} &\Rightarrow \begin{cases} T = \frac{3u^{2/3}}{Av^{1/3}} = \frac{3U^{2/3}}{A(NV)^{1/3}} \quad \text{易得: } U \sim T^{3/2} \\ p = \left( \frac{N}{V} \right)^{1/2} \left( \frac{AT}{3} \right)^{3/2} \end{cases}
 \end{aligned}$$

$$C_V = \left( \frac{\partial U}{\partial T} \right)_V = \frac{1}{2} \sqrt{\frac{A^3 NV T}{3}} \quad \text{利用了前面的温度表达式.}$$

2) 对于每个热源而言, 我们有:

$$dQ = dU \sim T^{1/2} dT,$$

由于高温热源放出热量 ( $\Delta Q_h < 0$ ) 必定大于等于低温热源吸热 ( $\Delta Q_c > 0$ ), 不失一般性, 我们假设  $T_1 > T_2$ ,

$$\begin{aligned}
 \Delta Q_h + \Delta Q_c \leq 0 &\Rightarrow \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) T^{1/2} dT \leq 0 \\
 &\Rightarrow T_f \leq \left( \frac{T_1^{3/2} + T_2^{3/2}}{2} \right)^{2/3};
 \end{aligned}$$

另一方面, 由热力学第二定律:  $\Delta S \geq 0$ ,

$$\begin{aligned}
 \Delta S &= \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{dQ}{T} \sim \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{1}{T^{1/2}} dT \geq 0 \\
 &\Rightarrow T_f \geq \left( \frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^2.
 \end{aligned}$$

由第一题的温度表达式, 我们得到:

$$U = \left( \frac{AT(NV)^{1/3}}{3} \right)^{3/2} = CT^{3/2}.$$

对于整个系统而言,

$$W = -\Delta U_{\text{总}} = C \left( T_1^{3/2} + T_2^{3/2} - 2T_f^{3/2} \right) \leq \sqrt{\frac{A^3 NV}{27}} \left[ T_1^{3/2} + T_2^{3/2} - 2 \left( \frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^3 \right].$$

### 1.3 习题 1.11

首先, 我们需要求出范氏气体的内能表达式,

$$\begin{aligned}
 \text{由范氏气体的状态方程} &\Rightarrow \left(\frac{\partial p}{\partial T}\right)_V = \frac{R}{V-b} \\
 \text{代入书上式子 (1.9.16)} &\Rightarrow \left(\frac{\partial U}{\partial V}\right)_T = -p + T \left(\frac{\partial p}{\partial T}\right)_V = \frac{a}{V^2} \\
 &\Rightarrow dU = C_V dT + \left(\frac{\partial U}{\partial V}\right)_T dV = C_V dT + \frac{a}{V^2} dV \\
 &\Rightarrow U = C_V T - \frac{a}{V} + U_0.
 \end{aligned}$$

1) 对于等温过程,

$$\begin{aligned}
 \Delta U &= -\frac{a}{V_f} + \frac{a}{V_i} \\
 W &= \int_{V_i}^{V_f} p dV = \int_{V_i}^{V_f} \left( \frac{RT_i}{V-b} - \frac{a}{V^2} \right) dV = RT_i \ln \left( \frac{V_f-b}{V_i-b} \right) + \frac{a}{V_f} - \frac{a}{V_i} \\
 \Delta S &= \frac{\Delta U + W}{T_i} = R \ln \frac{V_f-b}{V_i-b};
 \end{aligned}$$

2) 对于等压过程,

$$\begin{aligned}
 W &= p_i(V_f - V_i) = \left( \frac{RT_i}{V_i-b} - \frac{a}{V_i^2} \right) (V_f - V_i) \\
 \text{利用状态方程} &\Rightarrow T_f = \left( p_i + \frac{a}{V_f^2} \right) (V_f - b)/R = \left( \frac{RT_i}{V_i-b} - \frac{a}{V_i^2} + \frac{a}{V_f^2} \right) (V_f - b)/R \\
 &\Rightarrow \Delta U = C_V(T_f - T_i) - \frac{a}{V_f} + \frac{a}{V_i} = C_V \left[ \left( \frac{RT_i}{V_i-b} - \frac{a}{V_i^2} + \frac{a}{V_f^2} \right) (V_f - b)/R - T_i \right] - \frac{a}{V_f} + \frac{a}{V_i} \\
 \text{由等压条件} &\Rightarrow T dS = dQ = C_p dT \\
 &\Rightarrow dS = C_p d(\ln T) \\
 &\Rightarrow \Delta S = C_p \ln \frac{T_f}{T_i} = C_p \ln \left[ \frac{V_f-b}{V_i-b} - a \left( \frac{1}{V_i^2} - \frac{1}{V_f^2} \right) \frac{V_f-b}{RT_i} \right];
 \end{aligned}$$

3) 对于绝热过程,

$$\begin{aligned}
 dQ = dU + p dV &= \left( \frac{\partial U}{\partial T} \right)_V dT + \left[ \left( \frac{\partial U}{\partial V} \right)_T + p \right] dV = C_V dT + \left( \frac{a}{V^2} + p \right) dV = 0, \\
 \text{结合状态方程} &\Rightarrow C_V dT + \frac{RT}{V-b} dV = 0 \\
 &\Rightarrow C_V \ln T + R \ln(V-b) = 0 \\
 &\Rightarrow T^{C_V} (V-b)^R = \text{const} \\
 &\Rightarrow T_f = T_i \left( \frac{V_i-b}{V_f-b} \right)^{R/C_V}
 \end{aligned}$$

因此, 我们容易得到:

$$\begin{aligned}
 \Delta U &= C_V T_i \left[ \left( \frac{V_i-b}{V_f-b} \right)^{R/C_V} - 1 \right] - \frac{a}{V_f} + \frac{a}{V_i} \\
 W &= -\Delta U \\
 \Delta S &= 0.
 \end{aligned}$$

## 1.4 习题 1.13

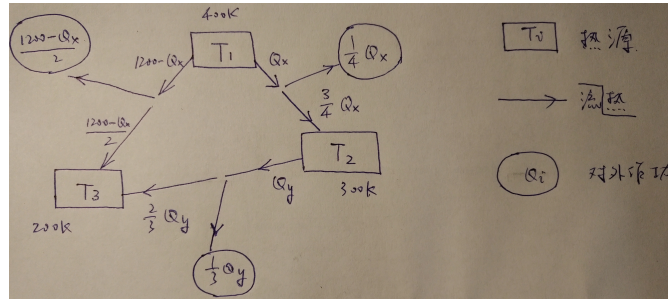
其中一个物体降温 (放热):  $T_1 \rightarrow T_2$ , 另一个物体升温 (吸热):  $T_1 \rightarrow T_x$ . 考虑整个体系, 由热力学第二定律,

$$\Delta S = \left( \int_{T_1}^{T_2} + \int_{T_1}^{T_x} \right) \frac{C_p dT}{T} \geq 0 \Rightarrow T_x \geq \frac{T_1^2}{T_2}.$$

因此,

$$W \geq \Delta Q = C_p(T_x + T_2 - 2T_1) \geq C_p \left( \frac{T_1^2}{T_2} + T_2 - 2T_1 \right) = C_p \frac{(T_1 - T_2)^2}{T_2}.$$

## 1.5 习题 1.22



由图, 我们有以下关系:

$$\begin{aligned} \frac{1200 - Q_x}{2} + \frac{Q_y}{3} + \frac{Q_x}{4} &= 200 \Rightarrow \frac{3}{4}Q_x - Q_y = 1200 \\ &\Rightarrow \begin{cases} Q_2 = \frac{3}{4}Q_x - Q_y = 1200\text{J} \\ Q_3 = \frac{1200 - Q_x}{2} + \frac{2Q_y}{3} = -200\text{J} \end{cases} \\ &\Rightarrow \begin{cases} \Delta S_1 = \frac{Q_1}{T_1} = \frac{-1200}{400} = -3\text{J/K} \\ \Delta S_2 = \frac{Q_2}{T_2} = \frac{1200}{300} = 4\text{J/K} \\ \Delta S_3 = \frac{Q_3}{T_3} = \frac{-200}{200} = -1\text{J/K} \\ \Delta S_{\text{总}} = \sum_{i=1}^3 \Delta S_i = 0\text{J/K}. \end{cases} \end{aligned}$$

## 1.6 习题 1.23

考虑等熵过程 ( $S = S_0$ ),

$$\begin{aligned} W_{S_0} &= \int_{V_0}^V p(S_0, V') dV' = RS_0 \ln \frac{V}{V_0} \Rightarrow p(S_0, V) = \frac{dW_{S_0}}{dV} = \frac{RS_0}{V} \\ U(S_0, V) - U(S_0, V_0) &= -W_{S_0} \Rightarrow U(S_0, V) = U_0 - RS_0 \ln \frac{V}{V_0}. \end{aligned}$$

现在考虑一个等体过程 ( $V, S_0 \rightarrow V, S$ ),

$$\begin{aligned} U(S, V) - U(S_0, V) &= \int_{T(S_0, V)}^{T(S, V)} T(S', V) dS' \\ &= \int_{S_0}^S \frac{RV_0}{V} \left( \frac{S'}{S_0} \right)^a dS' \\ &= \frac{RV_0 S_0}{(a+1)V} \left[ \left( \frac{S}{S_0} \right)^{a+1} - 1 \right] \end{aligned}$$

因此,

$$U(S, V) = \frac{RV_0 S_0}{(a+1)V} \left[ \left( \frac{S}{S_0} \right)^{a+1} - 1 \right] - RS_0 \ln \frac{V}{V_0} + U_0$$

又由:

$$\begin{aligned} \left( \frac{\partial p}{\partial S} \right)_V &= - \left( \frac{\partial T}{\partial V} \right)_S = \frac{RV_0}{V^2} \left( \frac{S}{S_0} \right)^a \\ \Rightarrow \quad p(S, V) &= \frac{RV_0 S_0}{(a+1)V^2} \left[ \left( \frac{S}{S_0} \right)^{a+1} - 1 \right] + \frac{RS_0}{V} \\ W(S, V_0 \rightarrow V) &= \int_{V_0}^V p(S, V') dV' = \frac{RV_0 S_0}{a+1} \left[ \left( \frac{S}{S_0} \right)^{a+1} - 1 \right] \left( \frac{1}{V_0} - \frac{1}{V} \right) + RS_0 \ln \frac{V}{V_0}. \end{aligned}$$