热统习题的部分答案 (野生版)

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1 第一章

1.1 习题 1.6

$$\begin{split} \alpha &= \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{p V} \quad \Rightarrow \quad \left(\frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{p} \\ &\Rightarrow \quad V = \frac{\nu R T}{p} + g(p) \quad \text{代入 } \kappa = \frac{1}{p} + \frac{a}{V} = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T \\ &\Rightarrow \quad \mathrm{d}(p g(p)) = -\frac{a}{2} \mathrm{d}(p^2) \\ &\Rightarrow \quad p g(p) = -\frac{a}{2} p^2 + \mathrm{const} \quad \text{代入第二行式子并整理} \\ &\Rightarrow \quad p V = \nu R T - \frac{a}{2} p^2 + \mathrm{const} \; . \end{split}$$

1.2 习题 1.8

1) 利用广延量假设,

$$S = Ns, V = Nv, U = Nu \Rightarrow s = A(vu)^{1/3}$$

$$\Rightarrow Tds = TA \frac{vdu + udv}{3(vu)^{2/3}} = du + pdv$$

$$du, dv 前的系数对应相等并恢复广延量 \Rightarrow \begin{cases} T = \frac{3u^{2/3}}{Av^{1/3}} = \frac{3U^{2/3}}{A(NV)^{1/3}} & 易得: U \sim T^{3/2} \\ p = \left(\frac{N}{V}\right)^{1/2} \left(\frac{AT}{3}\right)^{3/2} \end{cases}$$

$$C_V = \left(\frac{\partial U}{\partial T}\right)_V = \frac{1}{2}\sqrt{\frac{A^3NVT}{3}}$$
 利用了前面的温度表达式.

2) 对于每个热源而言, 我们有:

$$dQ = dU \sim T^{1/2} dT$$

由于高温热源放出热量 $(\Delta Q_h < 0)$ 必定大于等于低温热源吸热 $(\Delta Q_c > 0)$,不失一般性,我们假设 $T_1 > T_2$,

$$\Delta Q_h + \Delta Q_c \le 0 \quad \Rightarrow \quad \left(\int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) T^{1/2} dT \le 0$$

$$\Rightarrow \quad T_f \le \left(\frac{T_1^{3/2} + T_2^{3/2}}{2} \right)^{2/3} ;$$

另一方面, 由热力学第二定律: $\Delta S \geq 0$,

$$\begin{split} \Delta S &= \left(\int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{\mathrm{d}Q}{T} \sim \left(\int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{1}{T^{1/2}} \mathrm{d}T \geq 0 \\ \Rightarrow \quad T_f \geq \left(\frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^2 \,. \end{split}$$

由第一题的温度表达式, 我们得到:

$$U = \left(\frac{AT(NV)^{1/3}}{3}\right)^{3/2} = CT^{3/2}.$$

对于整个系统而言,

$$W = -\Delta U_{\rm B} = C \left(T_1^{3/2} + T_2^{3/2} - 2 T_f^{3/2} \right) \leq \sqrt{\frac{A^3 NV}{27}} \left[T_1^{3/2} + T_2^{3/2} - 2 \left(\frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^3 \right] \; .$$

1.3 习题 1.11

首先, 我们需要求出范氏气体的内能表达式,

由范氏气体的状态方程
$$\Rightarrow$$
 $\left(\frac{\partial p}{\partial T}\right)_V = \frac{R}{V - b}$ 代人书上式子 (1.9.16) \Rightarrow $\left(\frac{\partial U}{\partial V}\right)_T = -p + T\left(\frac{\partial p}{\partial T}\right)_V = \frac{a}{V^2}$ \Rightarrow $\mathrm{d}U = C_V \mathrm{d}T + \left(\frac{\partial U}{\partial V}\right)_T \mathrm{d}V = C_V \mathrm{d}T + \frac{a}{V^2} \mathrm{d}V$ \Rightarrow $U = C_V T - \frac{a}{V} + U_0$.

1) 对于等温过程,

$$\Delta U = -\frac{a}{V_f} + \frac{a}{V_i}$$

$$W = \int_{V_i}^{V_f} p dV = \int_{V_i}^{V_f} \left(\frac{RT_i}{V - b} - \frac{a}{V^2} \right) dV = RT_i \ln \left(\frac{V_f - b}{V_i - b} \right) + \frac{a}{V_f} - \frac{a}{V_i}$$

$$\Delta S = \frac{\Delta U + W}{T_i} = R \ln \frac{V_f - b}{V_i - b};$$

2) 对于等压过程,

$$W = p_i(V_f - V_i) = \left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2}\right)(V_f - V_i)$$
利用状态方程 $\Rightarrow T_f = \left(p_i + \frac{a}{V_f^2}\right)(V_f - b)/R = \left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2} + \frac{a}{V_f^2}\right)(V_f - b)/R$

$$\Rightarrow \Delta U = C_V(T_f - T_i) - \frac{a}{V_f} + \frac{a}{V_i} = C_V\left[\left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2} + \frac{a}{V_f^2}\right)(V_f - b)/R - T_i\right] - \frac{a}{V_f} + \frac{a}{V_i}$$
由等压条件 $\Rightarrow TdS = dQ = C_pdT$

$$\Rightarrow dS = C_pd(\ln T)$$

$$\Rightarrow \Delta S = C_p \ln \frac{T_f}{T_i} = C_p \ln \left[\frac{V_f - b}{V_i - b} - a\left(\frac{1}{V_i^2} - \frac{1}{V_f^2}\right)\frac{V_f - b}{RT_i}\right];$$

3) 对于绝热过程,

$$dQ = dU + pdV = \left(\frac{\partial U}{\partial T}\right)_V dT + \left[\left(\frac{\partial U}{\partial V}\right)_T + p\right] dV = C_V dT + \left(\frac{a}{V^2} + p\right) dV = 0 \, ,$$
 结合状态方程 $\Rightarrow C_V dT + \frac{RT}{V - b} dV = 0 \,$ $\Rightarrow C_V \ln T + R \ln(V - b) = 0 \,$ $\Rightarrow T^{C_V} (V - b)^R = \text{const} \,$ $\Rightarrow T_f = T_i \left(\frac{V_i - b}{V_f - b}\right)^{R/C_V} \,$

因此, 我们容易得到:

$$\Delta U = C_V T_i \left[\left(\frac{V_i - b}{V_f - b} \right)^{R/C_V} - 1 \right] - \frac{a}{V_f} + \frac{a}{V_i}$$

$$W = -\Delta U$$

$$\Delta S = 0.$$

1.4 习题 1.13

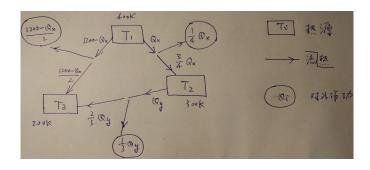
其中一个物体降温 (放热): $T_1 \to T_2$, 另一个物体升温 (吸热): $T_1 \to T_x$. 考虑整个体系, 由热力学第二定律,

$$\Delta S = \left(\int_{T_1}^{T_2} + \int_{T_1}^{T_x} \right) \frac{C_p dT}{T} \ge 0 \quad \Rightarrow \quad T_x \ge \frac{T_1^2}{T_2}.$$

因此,

$$W \ge \Delta U = C_p(T_x + T_2 - 2T_1) \ge C_p\left(\frac{T_1^2}{T_2} + T_2 - 2T_1\right) = C_p\frac{(T_1 - T_2)^2}{T_2}$$
.

1.5 习题 1.22



由图, 我们有以下关系:

$$\frac{1200 - Q_x}{2} + \frac{Q_y}{3} + \frac{Q_x}{4} = 200 \quad \Rightarrow \quad \frac{3}{4}Q_x - Q_y = 1200$$

$$\Rightarrow \begin{cases} Q_2 = \frac{3}{4}Q_x - Q_y = 1200J \\ Q_3 = \frac{1200 - Q_x}{2} + \frac{2Q_y}{3} = -200J \end{cases}$$

$$\Rightarrow \begin{cases} \Delta S_1 = \frac{Q_1}{T_1} = \frac{-1200}{400} = -3J/K \\ \Delta S_2 = \frac{Q_2}{T_2} = \frac{1200}{300} = 4J/K \\ \Delta S_3 = \frac{1200}{200} = -1J/K \end{cases}$$

$$\Rightarrow \begin{cases} \Delta S_2 = \frac{Q_2}{T_2} = \frac{1200}{300} = -1J/K \\ \Delta S_3 = \frac{1200}{200} = -1J/K \end{cases}$$

1.6 习题 1.23

考虑等熵过程 $(S = S_0)$,

$$W_{S_0} = \int_{V_0}^{V} p(S_0, V') dV' = RS_0 \ln \frac{V}{V_0} \quad \Rightarrow \quad p(S_0, V) = \frac{dW_{S_0}}{dV} = \frac{RS_0}{V}$$
$$U(S_0, V) - U(S_0, V_0) = -W_{S_0} \quad \Rightarrow \quad U(S_0, V) = U_0 - RS_0 \ln \frac{V}{V_0}$$

现在考虑一个等体过程 $(V, S_0 \rightarrow V, S)$,

$$U(S,V) - U(S_0, V) = \int_{T(S_0, V)}^{T(S,V)} T(S', V) dS'$$
$$= \int_{S_0}^{S} \frac{RV_0}{V} \left(\frac{S'}{S_0}\right)^a dS'$$
$$= \frac{RV_0 S_0}{(a+1)V} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right]$$

因此,

$$U(S,V) = \frac{RV_0S_0}{(a+1)V} \left[\left(\frac{S}{S_0} \right)^{a+1} - 1 \right] - RS_0 \ln \frac{V}{V_0} + U_0$$

又由:

$$\left(\frac{\partial p}{\partial S}\right)_V = -\left(\frac{\partial T}{\partial V}\right)_S = \frac{RV_0}{V^2} \left(\frac{S}{S_0}\right)^a$$

$$\Rightarrow \quad p(S,V) = \frac{RV_0S_0}{(a+1)V^2} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right] + \frac{RS_0}{V}$$

$$W(S,V_0 \to V) = \int_{V_0}^V p(S,V') dV' = \frac{RV_0S_0}{a+1} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right] \left(\frac{1}{V_0} - \frac{1}{V}\right) + RS_0 \ln \frac{V}{V_0} \, .$$

2 第二章

2.1 习题 2.2

$$\begin{split} \overline{v^n} &= \frac{\int_0^{+\infty} v^{n+2} e^{-mv^2/2k_B T} \, \mathrm{d}v}{\int_0^{+\infty} v^2 e^{-mv^2/2k_B T} \, \mathrm{d}v} \\ &= \frac{\int_0^{+\infty} \left(\frac{2k_B T}{m}\right)^{\frac{n+3}{2}} s^{\frac{n+1}{2}} e^{-s} \, \mathrm{d}s}{\int_0^{+\infty} \left(\frac{2k_B T}{m}\right)^{\frac{3}{2}} s^{\frac{1}{2}} e^{-s} \, \mathrm{d}s} \quad \text{ 委量代换: } s = \frac{mv^2}{2k_B T} \\ &= \left(\frac{2k_B T}{m}\right)^{\frac{n}{2}} \frac{\Gamma(\frac{n+3}{2})}{\Gamma(\frac{3}{2})} \quad \text{ 利用 } \Gamma \text{ 函数的定义} \\ &= \frac{2}{\sqrt{\pi}} \left(\frac{2k_B T}{m}\right)^{\frac{n}{2}} \Gamma\left(\frac{n+3}{2}\right) \, . \end{split}$$

2.2 习题 2.12

直接利用书上例 1 的结果,

$$F = -Nk_BT \ln Z = -Nk_BT \left(\ln V_1 + \frac{3}{2} \ln(2\pi m k_BT) \right),$$

$$S_{混前总} = Nk_B [\ln V_1 V_2 + 3 \ln(2\pi m k_BT) + 3] + 2S_0$$

$$= 2Nk_B [\ln \sqrt{V_1 V_2} + \frac{3}{2} \ln(2\pi m k_BT) + \frac{3}{2}] + 2S_0,$$

$$S_{混后总} = 2Nk_B [\ln(V_1 + V_2) + \frac{3}{2} \ln(2\pi m k_BT) + \frac{3}{2}] + 2S_0,$$

$$\Delta S = S_{混后总} - S_{混前总}$$

$$= 2Nk_B \ln \left(\frac{V_1 + V_2}{\sqrt{V_1 V_2}} \right)$$

$$= 2Nk_B \ln \left(\frac{p_1 + p_2}{\sqrt{p_1 p_2}} \right) \quad \text{利用理想气体的状态方程.}$$

2.3 习题 2.15

利用书上式子 2.5.16 及 2.5.22:

$$\begin{cases} \left(\frac{\partial p}{\partial T}\right)_v = \left(\frac{\partial s}{\partial v}\right)_T = \frac{R}{v - b} \\ T\left(\frac{\partial p}{\partial T}\right)_v - p = \left(\frac{\partial u}{\partial v}\right)_T = \frac{a}{v^2} \end{cases} \Rightarrow \left(p + \frac{a}{v^2}\right)\left(v - b\right) = RT.$$

2.4 习题 2.16

a,b)

$$\begin{split} \mathrm{d} U &= T \mathrm{d} S - p \mathrm{d} V = T \bigg(\frac{\partial S}{\partial p} \bigg)_V \mathrm{d} p + \bigg[T \bigg(\frac{\partial S}{\partial V} \bigg)_p - p \bigg] \, \mathrm{d} V \\ \Rightarrow & \begin{cases} \left(\frac{\partial U}{\partial p} \right)_V = T \bigg(\frac{\partial S}{\partial p} \right)_V = -T \bigg(\frac{\partial V}{\partial T} \bigg)_S; \\ \left(\frac{\partial U}{\partial V} \right)_p = T \bigg(\frac{\partial S}{\partial V} \bigg)_p - p = T \bigg(\frac{\partial p}{\partial T} \bigg)_S - p. \end{cases} \end{split}$$

c)

$$\begin{split} \mathrm{d}U &= T \mathrm{d}S - p \mathrm{d}V = T \left(\frac{\partial S}{\partial T}\right)_V \mathrm{d}T + \left[T \left(\frac{\partial S}{\partial V}\right)_T - p\right] \mathrm{d}V \\ &\Rightarrow T \left(\frac{\partial S}{\partial V}\right)_T - p = \left(\frac{\partial U}{\partial V}\right)_T = \frac{-1}{\left(\frac{\partial V}{\partial T}\right)_U \left(\frac{\partial T}{\partial U}\right)_V} \quad \mathrm{and} \quad \left(\frac{\partial U}{\partial T}\right)_V = T \left(\frac{\partial S}{\partial T}\right)_V \\ &\Rightarrow \left(\frac{\partial T}{\partial V}\right)_U = p \left(\frac{\partial T}{\partial U}\right)_V - T \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial T}{\partial U}\right)_V \\ &= p \left(\frac{\partial T}{\partial U}\right)_V - T \left(\frac{\partial S}{\partial V}\right)_T \frac{1}{T} \left(\frac{\partial T}{\partial S}\right)_V \\ &= p \left(\frac{\partial T}{\partial U}\right)_V + \left(\frac{\partial T}{\partial V}\right)_S \\ &= p \left(\frac{\partial T}{\partial U}\right)_V - T \left(\frac{\partial p}{\partial U}\right)_V \quad \text{All } a) \text{ $4$$$$$$}\&. \end{split}$$

d)

e)

$$\begin{split} \mathrm{d}H &= T\mathrm{d}S + V\mathrm{d}p = V\left(\frac{\partial p}{\partial T}\right)_S \mathrm{d}T + \left[V\left(\frac{\partial p}{\partial S}\right)_T + T\right] \mathrm{d}S \\ &\Rightarrow V\left(\frac{\partial p}{\partial S}\right)_T + T = \left(\frac{\partial H}{\partial S}\right)_T \quad \text{and} \quad \left(\frac{\partial H}{\partial T}\right)_S = V\left(\frac{\partial p}{\partial T}\right)_S \\ &\Rightarrow \left(\frac{\partial T}{\partial S}\right)_H = -\frac{\left(\frac{\partial H}{\partial S}\right)_T}{\left(\frac{\partial H}{\partial T}\right)_S} \\ &= -\frac{T}{V}\left(\frac{\partial T}{\partial p}\right)_S - \frac{\left(\frac{\partial p}{\partial S}\right)_T}{\left(\frac{\partial p}{\partial T}\right)_S} \\ &= -\frac{T}{V}\left(\frac{\partial T}{\partial p}\right)_S + \frac{T}{T\left(\frac{\partial S}{\partial T}\right)_p} \\ &= -\frac{T^2}{V}\left(\frac{\partial V}{\partial H}\right)_p + \frac{T}{C_p} \quad \text{利用了} \ d) \ \text{第 5 } \text{行}. \end{split}$$

2.5 习题 2.17

a)

$$dU = TdS - pdV = T\left(\frac{\partial S}{\partial T}\right)_{V} dT + \left[T\left(\frac{\partial S}{\partial V}\right)_{T} - p\right] dV$$

$$= C_{V}dT + \left[T\left(\frac{\partial p}{\partial T}\right)_{V} - p\right] dV;$$

$$dH = TdS + Vdp = T\left(\frac{\partial S}{\partial T}\right)_{p} dT + \left[T\left(\frac{\partial S}{\partial p}\right)_{T} + V\right] dp$$

$$= C_{p}dT + \left[-T\left(\frac{\partial V}{\partial T}\right)_{p} + V\right] dp.$$

由全微分条件

$$\left(\frac{\partial C_V}{\partial V} \right)_T = \left(\frac{\partial \left[T \left(\frac{\partial p}{\partial T} \right)_V - p \right]}{\partial T} \right)_V = T \left(\frac{\partial^2 p}{\partial T^2} \right)_V;$$

$$\left(\frac{\partial C_p}{\partial p} \right)_T = \left(\frac{\partial \left[-T \left(\frac{\partial V}{\partial T} \right)_p + V \right]}{\partial T} \right)_p = -T \left(\frac{\partial^2 V}{\partial T^2} \right)_p.$$

对于理想气体而言:

$$\left(\frac{\partial C_V}{\partial V}\right)_T = 0 \quad \text{and} \quad \left(\frac{\partial C_p}{\partial p}\right)_T = 0,$$

因此, 其 C_V, C_p 均仅为温度的函数. 对于范氏气体而言:

$$\left(\frac{\partial C_V}{\partial V}\right)_T = 0,$$

因此, 其 C_V 仅为温度的函数.

b) 由前半小题, 我们有

$$\begin{split} & \left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial p}{\partial T}\right)_V = \int \frac{1}{T} \left(\frac{\partial C_V}{\partial V}\right)_T \mathrm{d}T \,; \\ & \left(\frac{\partial S}{\partial p}\right)_T = - \left(\frac{\partial V}{\partial T}\right)_p = \int \frac{1}{T} \left(\frac{\partial C_p}{\partial p}\right)_T \mathrm{d}T \,. \end{split}$$

易得,

$$S = \int_{V} dV \int_{T} \frac{1}{T} \left(\frac{\partial C_{V}}{\partial V} \right)_{T} dT = \int_{T} \frac{1}{T} dT \int_{V} dV \left(\frac{\partial C_{V}}{\partial V} \right)_{T} = \int_{T} \frac{C_{V_{0}}}{T} dT;$$

$$S = \int_{p} dp \int_{T} \frac{1}{T} \left(\frac{\partial C_{p}}{\partial p} \right)_{T} dT = \int_{T} \frac{1}{T} dT \int_{p} dp \left(\frac{\partial C_{p}}{\partial p} \right)_{T} = \int_{T} \frac{C_{p_{0}}}{T} dT$$

因此,

$$\begin{split} F &= -\int p \mathrm{d}V - \int S \mathrm{d}T = -\int p \mathrm{d}V - \int \mathrm{d}T \int \frac{C_{V_0}}{T} \mathrm{d}T \,; \\ G &= \int V \mathrm{d}p - \int S \mathrm{d}T = \int V \mathrm{d}p - \int \mathrm{d}T \int \frac{C_{p_0}}{T} \mathrm{d}T \,. \end{split}$$

2.6 习题 2.19

能量由两部分组成,分别是平动动能 ϵ^t 与转动动能 ϵ^r . 注意到我们的目标是求状态方程,因此我们只需要关心配分函数对 V 的依赖,

$$Z = Z^t \cdot Z^r = \int e^{-\beta \frac{p^2}{2m}} \mathrm{d}x \mathrm{d}y \mathrm{d}z \mathrm{d}p_x \mathrm{d}p_y \mathrm{d}p_z \times \int e^{-\frac{\beta}{2T} \left(p_\theta^2 + \frac{p_\varphi^2}{\sin^2 \theta}\right)} \mathrm{d}\theta \mathrm{d}\varphi \mathrm{d}p_\theta \mathrm{d}p_\varphi = V \times g(\text{\texttt{π}} \text{\texttt{$\#$}} \text{\texttt{V}}).$$

因此, 状态方程为:

$$p = \frac{N}{\beta} \frac{\partial \ln Z}{\partial V} = \frac{N}{\beta V},$$

即为理想气体的状态方程.

3 第三章

3.1 习题 3.1

先计算体系的配分函数

$$P = Z^N = V^N \left[\frac{2\pi m}{\beta} \right]^{\frac{3N}{2}},$$

a) 由此可得体系的平均能量

$$\bar{E} = -\frac{\partial \ln P}{\partial \beta} = \frac{3}{2} N k_B T;$$

b) 求最概然能量 E_p 需写出能量的概率分布

$$f(E)dE = e^{-\Psi - \beta E}d\Omega(E) = e^{-\Psi - \beta E}\Omega'(E)dE \propto e^{-\beta E}E^{\frac{3N}{2} - 1}dE \quad \Rightarrow \quad f(E) \propto e^{-\beta E}E^{\frac{3N}{2} - 1},$$

因此

$$\frac{\partial f(E)}{\partial E}\Big|_{E=E_p} = 0 \quad \Rightarrow \quad E_p = \left(\frac{3}{2}N - 1\right)k_BT.$$

3.2 习题 3.3

考虑到每个自旋有两种状态,记为: +1,-1,且分别对应了两个能量的取值: $-\mu H$, $+\mu H$.体系的所有自旋的状态的选取确定了体系的一个构型 (configuration),例: $\{s_i\} = \{+1,-1,-1,-1,+1,\cdots\}$,表示体系第 1 个自旋处于 +1 的状态,第 2 个自旋处于 -1 的状态,等等.为了求体系的配分函数,我们需要对体系的所有构型求和

$$P = \sum_{\{s_i\}} e^{-\beta \sum_{i=1}^{N} (-1)^{(s_i+1)/2} \mu H} = \sum_{\{s_i\}} \prod_{i=1}^{N} e^{-\beta (-1)^{(s_i+1)/2} \mu H}$$
$$= \prod_{i=1}^{N} \sum_{s_i = \pm 1} e^{-\beta (-1)^{(s_i+1)/2} \mu H} = \prod_{i=1}^{N} \left(e^{-\beta \mu H} + e^{\beta \mu H} \right)$$
$$= \left(2 \cosh(\beta \mu H) \right)^{N},$$

因此可得体系的内能, 熵, 热容和总磁矩分别为

$$\begin{cases} U = -\frac{\partial}{\partial \beta} \ln P = -N\mu H \tanh(\beta \mu H); \\ S = S_0 + k_B \left(\ln P - \beta \frac{\partial}{\partial \beta} \ln P \right) = S_0 + Nk_B \left(\ln(2\cosh\beta \mu H) - \beta \mu H \tanh\beta \mu H \right); \\ C_H = \left(\frac{\partial U}{\partial T} \right)_H = -k_B \beta^2 \left(\frac{\partial U}{\partial \beta} \right)_H = Nk_B \frac{(\beta \mu H)^2}{\cosh^2(\beta \mu H)}; \\ M = \frac{1}{\beta} \frac{\partial \ln P}{\partial H} = N\mu \tanh(\beta \mu H). \end{cases}$$

3.3 习题 3.7

先求体系的配分函数

$$P = V^N \left[4\pi \int_0^{+\infty} e^{-\beta cp} p^2 dp \right]^N = \left[\frac{8\pi V}{(c\beta)^3} \right]^N,$$

由此可得体系的状态方程与内能

$$\begin{cases} p = \frac{1}{\beta} \frac{\partial \ln P}{\partial V} = \frac{N}{\beta V} \quad \Rightarrow \quad pV = Nk_B T; \\ U = -\frac{\partial \ln P}{\partial \beta} = 3Nk_B T. \end{cases}$$

3.4 习题 3.11

由能均分定理

$$\overline{\frac{1}{2}mv_i^2} = \frac{1}{2}k_BT \quad \Rightarrow \quad \overline{v_i^2} = \frac{k_BT}{m},$$

a)

$$\overline{v_x^3} \propto \int_{-\infty}^{+\infty} e^{-\beta m v_x^2/2} v_x^3 \mathrm{d}v_x = 0;$$

b)

$$\overline{v_x^3 v_y} \propto \int_{-\infty}^{+\infty} e^{-\beta m v_x^2/2} v_x^3 dv_x \times \int_{-\infty}^{+\infty} e^{-\beta m v_y^2/2} v_y dv_y = 0;$$

c)

$$\overline{v_x^2 v_y^2} = \overline{v_x^2} \times \overline{v_y^2} = \left(\frac{k_B T}{m}\right)^2;$$

d)

$$\overline{(v_x + av_y)^2} = \overline{v_x^2 + 2av_xv_y + a^2v_y^2} = \overline{v_x^2} + 0 + a^2\overline{v_y^2} = (a^2 + 1)\frac{k_BT}{m};$$

e)

$$\overline{v^2v_x} = \overline{v_x^3} + \overline{v_y^2v_x} + \overline{v_z^2v_x} = 0.$$

3.5 习题 3.12

a)

由能均分定理
$$\Rightarrow$$
 $\bar{\epsilon} = \frac{5}{2}k_BT$;

b)

$$\frac{1}{2}m(v_y - v_0)^2 = \frac{1}{2}mv_y^2 + \frac{1}{2}mv_0^2 - mv_yv_0 = \frac{1}{2}mv_y^2 - \frac{1}{2}mv_0^2 = \frac{1}{2}k_BT,$$

因此, 我们有

$$\overline{\frac{1}{2}mv_y^2} = \frac{1}{2}k_BT + \frac{1}{2}mv_0^2 \,.$$

3.6 习题 3.15

a)

$$\begin{split} \left\langle \frac{\Omega(E)}{\Omega'(E)} \right\rangle_{\text{c.e.}} &= \int_{\Omega} e^{-\Psi - \beta E} \frac{\Omega(E)}{\Omega'(E)} \mathrm{d}\Omega(E) \\ &= \int_{0}^{+\infty} e^{-\Psi - \beta E} \Omega(E) \mathrm{d}E \\ &= -\frac{1}{\beta} \int e^{-\Psi} \Omega(E) \mathrm{d}e^{-\beta E} \\ &= -\frac{1}{\beta} e^{-\Psi - \beta E} \Omega(E) \bigg|_{E=0}^{E=+\infty} + \frac{1}{\beta} \int_{\Omega} e^{-\Psi - \beta E} \mathrm{d}\Omega(E) \\ &= \frac{1}{\beta} \,; \end{split}$$

b) 由能量的概率分布

$$f(E)dE = e^{-\Psi - \beta E}d\Omega(E) = e^{-\Psi - \beta E}\Omega'(E)dE \quad \Rightarrow \quad f(E) = e^{-\Psi - \beta E}\Omega'(E),$$

我们有

$$\left. \frac{\partial f(E)}{\partial E} \right|_{E=E_p} = 0 \quad \Rightarrow \quad \frac{\Omega''(E_p)}{\Omega'(E_p)} = \beta \,.$$

3.7 补充 S1

先求体系的配分函数

$$P = Z^N = V^N \left[\frac{2\pi m}{\beta} \right]^{\frac{3N}{2}},$$

由此得到系统的状态方程, 内能和熵为

$$\begin{cases} p = \frac{1}{\beta} \frac{\partial \ln P}{\partial V} & \Rightarrow & pV = Nk_B T; \\ U = -\frac{\partial \ln P}{\partial \beta} = \frac{3}{2} Nk_B T; \\ S = S_0 + Nk_B \left[\ln V + \frac{3}{2} \ln(2\pi m k_B T) + \frac{3}{2} \right]. \end{cases}$$

3.8 补充 S2

先求体系的配分函数

$$Z_{g.c.} = e^{\zeta} = \sum_{N} \frac{e^{-N\alpha}}{N!} \int e^{-\beta E} d\Omega = \sum_{N} \frac{(e^{-\alpha})^N}{N!} V^N \left(\frac{2\pi m}{\beta}\right)^{\frac{3N}{2}} = \exp\left[e^{-\alpha} V \left(\frac{2\pi m}{\beta}\right)^{3/2}\right],$$

因此

$$\zeta = e^{-\alpha} V \left(\frac{2\pi m}{\beta}\right)^{3/2}.$$

由此我们能得到体系的状态方程,内能,熵,化学势和分子数的相对涨落

$$\begin{cases} \bar{N} = -\frac{\partial \zeta}{\partial \alpha} = \zeta; \\ p = \frac{1}{\beta} \frac{\partial \zeta}{\partial V} = \frac{\zeta}{\beta V} \quad \Rightarrow \quad pV = \bar{N}k_BT; \\ U = -\frac{\partial \zeta}{\partial \beta} = \frac{3}{2} \bar{N}k_BT; \\ S = S_0 + k_B \left(\zeta - \beta \frac{\partial \zeta}{\partial \beta} - \alpha \frac{\partial \zeta}{\partial \alpha}\right) = S_0 + \left(\frac{5}{2} + \alpha\right) \bar{N}k_B; \\ \mu = -\alpha k_BT; \\ \overline{N^2} = \sum_N \frac{e^{-\zeta - N\alpha} N^2}{N!} \int \dots = e^{-\zeta} \frac{\partial^2}{\partial \alpha^2} Z_{g.c.} = e^{-\zeta} \frac{\partial^2}{\partial \alpha^2} e^{\zeta} = \zeta + \zeta^2; \\ \overline{(\Delta N)^2} / \bar{N}^2 = \frac{\overline{N^2} - \bar{N}^2}{\bar{N}^2} = \frac{1}{\zeta} = \frac{1}{\bar{N}}. \end{cases}$$