# 热统习题的部分答案 (野生版)

## 2021年12月1日

## 目录

1	第一	<del>"</del> 章	1	
	1.1	习题 1.6	1	
	1.2	习题 1.8	1	
	1.3	习题 1.11	2	
	1.4	习题 1.13	3	
	1.5	习题 1.22	3	
	1.6	习题 1.23	3	
2	第二章			
	2.1	- 习题 2.2	5	
	2.2	习题 2.12	5	
	2.3	习题 2.15	5	
	2.4	习题 2.16	5	
	2.5	习题 2.17	7	
	2.6	习题 2.19	8	
3	第三章			
	3.1	-	9	
	3.2	习题 3.3	9	
	3.3	习题 3.7	9	
	3.4	· · -	10	
	3.5	习题 3.12		
	3.6	习题 3.15	10	
	3.7	か充 S1		
	3.8	补充 S2		
4	第四章			
	4.1	9年 - 习题 4.4		
	4.1	习题 4.14		
	4.3	习题 4.17		
	4.4	习题 4.19		
	4.4	フ脚 4.20		
	4.6	习题 4.25		
	4.0	7 /2 生.20	то	

### 1 第一章

#### 1.1 习题 1.6

$$\begin{split} \alpha &= \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{p V} \quad \Rightarrow \quad \left( \frac{\partial V}{\partial T} \right)_p = \frac{\nu R}{p} \\ &\Rightarrow \quad V = \frac{\nu R T}{p} + g(p) \quad \text{代入 } \kappa = \frac{1}{p} + \frac{a}{V} = -\frac{1}{V} \left( \frac{\partial V}{\partial p} \right)_T \\ &\Rightarrow \quad \mathrm{d}(p g(p)) = -\frac{a}{2} \mathrm{d}(p^2) \\ &\Rightarrow \quad p g(p) = -\frac{a}{2} p^2 + \mathrm{const} \quad \text{代入第二行式子并整理} \\ &\Rightarrow \quad p V = \nu R T - \frac{a}{2} p^2 + \mathrm{const} \; . \end{split}$$

#### 1.2 习题 1.8

1) 利用广延量假设,

$$S = Ns, V = Nv, U = Nu \quad \Rightarrow \quad s = A(vu)^{1/3}$$
 
$$\Rightarrow \quad T ds = TA \frac{v du + u dv}{3(vu)^{2/3}} = du + p dv$$
 
$$du, dv \text{ 前的系数对应相等并恢复广延量} \quad \Rightarrow \quad \begin{cases} T = \frac{3u^{2/3}}{Av^{1/3}} = \frac{3U^{2/3}}{A(NV)^{1/3}} & \text{易得: } U \sim T^{3/2} \\ p = \left(\frac{N}{V}\right)^{1/2} \left(\frac{AT}{3}\right)^{3/2} \end{cases}$$
 
$$C_V = \left(\frac{\partial U}{\partial T}\right)_V = \frac{1}{2} \sqrt{\frac{A^3 NVT}{3}} \quad \text{利用了前面的温度表达式.}$$

2) 对于每个热源而言, 我们有:

$$dQ = dU \sim T^{1/2} dT$$

由于高温热源放出热量 ( $\Delta Q_h < 0$ ) 必定大于等于低温热源吸热 ( $\Delta Q_c > 0$ ), 不失一般性, 我们假设  $T_1 > T_2$ ,

$$\Delta Q_h + \Delta Q_c \le 0 \implies \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) T^{1/2} dT \le 0$$

$$\Rightarrow T_f \le \left( \frac{T_1^{3/2} + T_2^{3/2}}{2} \right)^{2/3};$$

另一方面, 由热力学第二定律:  $\Delta S \geq 0$ ,

$$\Delta S = \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{dQ}{T} \sim \left( \int_{T_1}^{T_f} + \int_{T_2}^{T_f} \right) \frac{1}{T^{1/2}} dT \ge 0$$

$$\Rightarrow T_f \ge \left( \frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^2.$$

由第一题的温度表达式, 我们得到:

$$U = \left(\frac{AT(NV)^{1/3}}{3}\right)^{3/2} = CT^{3/2}.$$

对于整个系统而言,

$$W = -\Delta U_{\rm tot} = C \left( T_1^{3/2} + T_2^{3/2} - 2 T_f^{3/2} \right) \leq \sqrt{\frac{A^3 NV}{27}} \left[ T_1^{3/2} + T_2^{3/2} - 2 \left( \frac{T_1^{1/2} + T_2^{1/2}}{2} \right)^3 \right] \; .$$

#### 1.3 习题 1.11

首先,我们需要求出范氏气体的内能表达式,

由范氏气体的状态方程 
$$\Rightarrow$$
  $\left(\frac{\partial p}{\partial T}\right)_V = \frac{R}{V - b}$  代入书上式子 (1.9.16)  $\Rightarrow$   $\left(\frac{\partial U}{\partial V}\right)_T = -p + T\left(\frac{\partial p}{\partial T}\right)_V = \frac{a}{V^2}$   $\Rightarrow$   $\mathrm{d}U = C_V \mathrm{d}T + \left(\frac{\partial U}{\partial V}\right)_T \mathrm{d}V = C_V \mathrm{d}T + \frac{a}{V^2} \mathrm{d}V$   $\Rightarrow$   $U = C_V T - \frac{a}{V} + U_0$ .

1) 对于等温过程,

$$\begin{split} \Delta U &= -\frac{a}{V_f} + \frac{a}{V_i} \\ W &= \int_{V_i}^{V_f} p \mathrm{d}V = \int_{V_i}^{V_f} \left( \frac{RT_i}{V - b} - \frac{a}{V^2} \right) \mathrm{d}V = RT_i \ln \left( \frac{V_f - b}{V_i - b} \right) + \frac{a}{V_f} - \frac{a}{V_i} \\ \Delta S &= \frac{\Delta U + W}{T_i} = R \ln \frac{V_f - b}{V_i - b} \,; \end{split}$$

2) 对于等压过程,

$$W = p_i(V_f - V_i) = \left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2}\right)(V_f - V_i)$$
利用状态方程  $\Rightarrow T_f = \left(p_i + \frac{a}{V_f^2}\right)(V_f - b)/R = \left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2} + \frac{a}{V_f^2}\right)(V_f - b)/R$ 

$$\Rightarrow \Delta U = C_V(T_f - T_i) - \frac{a}{V_f} + \frac{a}{V_i} = C_V\left[\left(\frac{RT_i}{V_i - b} - \frac{a}{V_i^2} + \frac{a}{V_f^2}\right)(V_f - b)/R - T_i\right] - \frac{a}{V_f} + \frac{a}{V_i}$$
由等压条件  $\Rightarrow TdS = dQ = C_pdT$ 

$$\Rightarrow dS = C_pd(\ln T)$$

$$\Rightarrow \Delta S = C_p \ln \frac{T_f}{T_i} = C_p \ln \left[\frac{V_f - b}{V_i - b} - a\left(\frac{1}{V_i^2} - \frac{1}{V_f^2}\right)\frac{V_f - b}{RT_i}\right];$$

3) 对于绝热过程,

$$dQ = dU + pdV = \left(\frac{\partial U}{\partial T}\right)_V dT + \left[\left(\frac{\partial U}{\partial V}\right)_T + p\right] dV = C_V dT + \left(\frac{a}{V^2} + p\right) dV = 0,$$
结合状态方程  $\Rightarrow C_V dT + \frac{RT}{V - b} dV = 0$ 
 $\Rightarrow C_V \ln T + R \ln(V - b) = 0$ 
 $\Rightarrow T^{C_V} (V - b)^R = \text{const}$ 
 $\Rightarrow T_f = T_i \left(\frac{V_i - b}{V_f - b}\right)^{R/C_V}$ 

因此, 我们容易得到:

$$\Delta U = C_V T_i \left[ \left( \frac{V_i - b}{V_f - b} \right)^{R/C_V} - 1 \right] - \frac{a}{V_f} + \frac{a}{V_i}$$

$$W = -\Delta U$$

$$\Delta S = 0.$$

#### 1.4 习题 1.13

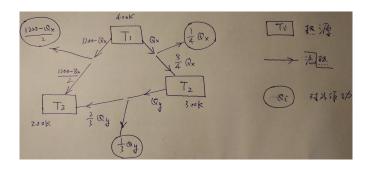
其中一个物体降温 (放热):  $T_1 \to T_2$ , 另一个物体升温 (吸热):  $T_1 \to T_x$ . 考虑整个体系, 由热力学第二定律,

$$\Delta S = \left( \int_{T_1}^{T_2} + \int_{T_1}^{T_x} \right) \frac{C_p \mathrm{d}T}{T} \ge 0 \quad \Rightarrow \quad T_x \ge \frac{T_1^2}{T_2} \,.$$

因此,

$$W \ge \Delta Q = C_p(T_x + T_2 - 2T_1) \ge C_p\left(\frac{T_1^2}{T_2} + T_2 - 2T_1\right) = C_p\frac{(T_1 - T_2)^2}{T_2}$$
.

#### 1.5 习题 1.22



由图, 我们有以下关系:

$$\frac{1200 - Q_x}{2} + \frac{Q_y}{3} + \frac{Q_x}{4} = 200 \quad \Rightarrow \quad \frac{3}{4}Q_x - Q_y = 1200$$

$$\Rightarrow \quad \begin{cases} Q_2 = \frac{3}{4}Q_x - Q_y = 1200 J \\ Q_3 = \frac{1200 - Q_x}{2} + \frac{2Q_y}{3} = -200 J \end{cases}$$

$$\Rightarrow \quad \begin{cases} \Delta S_1 = \frac{Q_1}{T_1} = \frac{-1200}{400} = -3J/K \\ \Delta S_2 = \frac{Q_2}{T_2} = \frac{1200}{300} = 4J/K \\ \Delta S_3 = \frac{Q_3}{T_3} = \frac{-200}{200} = -1J/K \end{cases}$$

$$\Delta S_{\frac{5}{10}} = \sum_{i=1}^{3} \Delta S_i = 0J/K.$$

#### 1.6 习题 1.23

考虑等熵过程  $(S = S_0)$ ,

$$W_{S_0} = \int_{V_0}^{V} p(S_0, V') dV' = RS_0 \ln \frac{V}{V_0} \quad \Rightarrow \quad p(S_0, V) = \frac{dW_{S_0}}{dV} = \frac{RS_0}{V}$$
$$U(S_0, V) - U(S_0, V_0) = -W_{S_0} \quad \Rightarrow \quad U(S_0, V) = U_0 - RS_0 \ln \frac{V}{V_0}.$$

现在考虑一个等体过程  $(V, S_0 \rightarrow V, S)$ ,

$$U(S, V) - U(S_0, V) = \int_{T(S_0, V)}^{T(S, V)} T(S', V) dS'$$
$$= \int_{S_0}^{S} \frac{RV_0}{V} \left(\frac{S'}{S_0}\right)^a dS'$$
$$= \frac{RV_0 S_0}{(a+1)V} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right]$$

因此,

$$U(S,V) = \frac{RV_0S_0}{(a+1)V} \left[ \left( \frac{S}{S_0} \right)^{a+1} - 1 \right] - RS_0 \ln \frac{V}{V_0} + U_0$$

又由:

$$\left(\frac{\partial p}{\partial S}\right)_V = -\left(\frac{\partial T}{\partial V}\right)_S = \frac{RV_0}{V^2} \left(\frac{S}{S_0}\right)^a$$

$$\Rightarrow \quad p(S,V) = \frac{RV_0S_0}{(a+1)V^2} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right] + \frac{RS_0}{V}$$

$$W(S,V_0 \to V) = \int_{V_0}^V p(S,V') dV' = \frac{RV_0S_0}{a+1} \left[\left(\frac{S}{S_0}\right)^{a+1} - 1\right] \left(\frac{1}{V_0} - \frac{1}{V}\right) + RS_0 \ln \frac{V}{V_0} .$$

## 2 第二章

#### 2.1 习题 2.2

$$\overline{v^n} = \frac{\int_0^{+\infty} v^{n+2} e^{-mv^2/2k_B T} dv}{\int_0^{+\infty} v^2 e^{-mv^2/2k_B T} dv} 
= \frac{\int_0^{+\infty} \left(\frac{2k_B T}{m}\right)^{\frac{n+3}{2}} s^{\frac{n+1}{2}} e^{-s} ds}{\int_0^{+\infty} \left(\frac{2k_B T}{m}\right)^{\frac{3}{2}} s^{\frac{1}{2}} e^{-s} ds} \quad \text{ 委量代换: } s = \frac{mv^2}{2k_B T} 
= \left(\frac{2k_B T}{m}\right)^{\frac{n}{2}} \frac{\Gamma(\frac{n+3}{2})}{\Gamma(\frac{3}{2})} \quad \text{ 利用 } \Gamma \text{ 函数的定义} 
= \frac{2}{\sqrt{\pi}} \left(\frac{2k_B T}{m}\right)^{\frac{n}{2}} \Gamma\left(\frac{n+3}{2}\right).$$

#### 2.2 习题 2.12

直接利用书上例 1 的结果,

$$F = -Nk_BT \ln Z = -Nk_BT \left( \ln V_1 + \frac{3}{2} \ln(2\pi m k_BT) \right),$$

$$S_{混前总} = Nk_B \left[ \ln V_1 V_2 + 3 \ln(2\pi m k_BT) + 3 \right] + 2S_0$$

$$= 2Nk_B \left[ \ln \sqrt{V_1 V_2} + \frac{3}{2} \ln(2\pi m k_BT) + \frac{3}{2} \right] + 2S_0,$$

$$S_{混后总} = 2Nk_B \left[ \ln(V_1 + V_2) + \frac{3}{2} \ln(2\pi m k_BT) + \frac{3}{2} \right] + 2S_0,$$

$$\Delta S = S_{混后总} - S_{混前总}$$

$$= 2Nk_B \ln \left( \frac{V_1 + V_2}{\sqrt{V_1 V_2}} \right)$$

$$= 2Nk_B \ln \left( \frac{p_1 + p_2}{\sqrt{p_1 p_2}} \right) \quad \text{利用理想气体的状态方程.}$$

#### 2.3 习题 2.15

利用书上式子 2.5.16 及 2.5.22:

$$\begin{cases} \left(\frac{\partial p}{\partial T}\right)_v = \left(\frac{\partial s}{\partial v}\right)_T = \frac{R}{v - b} \\ T\left(\frac{\partial p}{\partial T}\right)_v - p = \left(\frac{\partial u}{\partial v}\right)_T = \frac{a}{v^2} \end{cases} \Rightarrow \left(p + \frac{a}{v^2}\right)\left(v - b\right) = RT.$$

#### 2.4 习题 2.16

a,b)

$$\begin{split} \mathrm{d} U &= T \mathrm{d} S - p \mathrm{d} V = T \bigg( \frac{\partial S}{\partial p} \bigg)_V \mathrm{d} p + \left[ T \bigg( \frac{\partial S}{\partial V} \bigg)_p - p \right] \mathrm{d} V \\ \\ &\Rightarrow \quad \left\{ \left( \frac{\partial U}{\partial p} \right)_V = T \bigg( \frac{\partial S}{\partial p} \right)_V = -T \bigg( \frac{\partial V}{\partial T} \bigg)_S \, ; \\ &\left( \frac{\partial U}{\partial V} \right)_p = T \bigg( \frac{\partial S}{\partial V} \bigg)_p - p = T \bigg( \frac{\partial p}{\partial T} \bigg)_S - p \, . \end{split} \right. \end{split}$$

c)

d)

$$\begin{split} \mathrm{d}H &= T\mathrm{d}S + V\mathrm{d}p = T \left(\frac{\partial S}{\partial T}\right)_p \mathrm{d}T + \left[T \left(\frac{\partial S}{\partial p}\right)_T + V\right] \mathrm{d}p \\ &\Rightarrow T \left(\frac{\partial S}{\partial p}\right)_T + V = \left(\frac{\partial H}{\partial p}\right)_T \quad \mathrm{and} \quad \left(\frac{\partial H}{\partial T}\right)_p = T \left(\frac{\partial S}{\partial T}\right)_p \\ & = \mathrm{d}T \cdot \left(\frac{\partial T}{\partial p}\right)_H = \left(\frac{\partial T}{\partial p}\right)_S - V \left(\frac{\partial T}{\partial H}\right)_p; \\ & = \mathrm{d}H = T\mathrm{d}S + V\mathrm{d}p = T \left(\frac{\partial S}{\partial V}\right)_p \mathrm{d}V + \left[T \left(\frac{\partial S}{\partial p}\right)_V + V\right] \mathrm{d}p \\ & = \left(\frac{\partial H}{\partial V}\right)_p = T \left(\frac{\partial S}{\partial V}\right)_p = T \left(\frac{\partial P}{\partial T}\right)_S; \\ & = \left(\frac{\partial T}{\partial p}\right)_H = T \left(\frac{\partial V}{\partial H}\right)_p - V \left(\frac{\partial T}{\partial H}\right)_p. \end{split}$$

e)

$$\begin{split} \mathrm{d}H &= T\mathrm{d}S + V\mathrm{d}p = V\left(\frac{\partial p}{\partial T}\right)_S \mathrm{d}T + \left[V\left(\frac{\partial p}{\partial S}\right)_T + T\right] \mathrm{d}S \\ &\Rightarrow V\left(\frac{\partial p}{\partial S}\right)_T + T = \left(\frac{\partial H}{\partial S}\right)_T \quad \text{and} \quad \left(\frac{\partial H}{\partial T}\right)_S = V\left(\frac{\partial p}{\partial T}\right)_S \\ &\Rightarrow \left(\frac{\partial T}{\partial S}\right)_H = -\frac{\left(\frac{\partial H}{\partial S}\right)_T}{\left(\frac{\partial H}{\partial T}\right)_S} \\ &= -\frac{T}{V}\left(\frac{\partial T}{\partial p}\right)_S - \frac{\left(\frac{\partial p}{\partial S}\right)_T}{\left(\frac{\partial p}{\partial T}\right)_S} \\ &= -\frac{T}{V}\left(\frac{\partial T}{\partial p}\right)_S + \frac{T}{T\left(\frac{\partial S}{\partial T}\right)_p} \\ &= -\frac{T^2}{V}\left(\frac{\partial V}{\partial H}\right)_p + \frac{T}{C_p} \quad \text{利用了} \ d) \ \text{第 5 行}. \end{split}$$

#### 2.5 习题 2.17

a)

$$dU = TdS - pdV = T\left(\frac{\partial S}{\partial T}\right)_{V} dT + \left[T\left(\frac{\partial S}{\partial V}\right)_{T} - p\right] dV$$

$$= C_{V}dT + \left[T\left(\frac{\partial p}{\partial T}\right)_{V} - p\right] dV;$$

$$dH = TdS + Vdp = T\left(\frac{\partial S}{\partial T}\right)_{p} dT + \left[T\left(\frac{\partial S}{\partial p}\right)_{T} + V\right] dp$$

$$= C_{p}dT + \left[-T\left(\frac{\partial V}{\partial T}\right)_{p} + V\right] dp.$$

由全微分条件

$$\left( \frac{\partial C_V}{\partial V} \right)_T = \left( \frac{\partial \left[ T \left( \frac{\partial p}{\partial T} \right)_V - p \right]}{\partial T} \right)_V = T \left( \frac{\partial^2 p}{\partial T^2} \right)_V;$$

$$\left( \frac{\partial C_p}{\partial p} \right)_T = \left( \frac{\partial \left[ -T \left( \frac{\partial V}{\partial T} \right)_p + V \right]}{\partial T} \right)_p = -T \left( \frac{\partial^2 V}{\partial T^2} \right)_p.$$

对于理想气体而言:

$$\left(\frac{\partial C_V}{\partial V}\right)_T = 0 \quad \text{and} \quad \left(\frac{\partial C_p}{\partial p}\right)_T = 0,$$

因此, 其  $C_V, C_p$  均仅为温度的函数. 对于范氏气体而言:

$$\left(\frac{\partial C_V}{\partial V}\right)_T = 0,$$

因此, 其  $C_V$  仅为温度的函数.

b) 由前半小题, 我们有

$$\begin{split} \left(\frac{\partial S}{\partial V}\right)_T &= \left(\frac{\partial p}{\partial T}\right)_V = \int \frac{1}{T} \left(\frac{\partial C_V}{\partial V}\right)_T \mathrm{d}T \,; \\ \left(\frac{\partial S}{\partial p}\right)_T &= - \left(\frac{\partial V}{\partial T}\right)_p = \int \frac{1}{T} \left(\frac{\partial C_p}{\partial p}\right)_T \mathrm{d}T \,. \end{split}$$

易得,

$$\begin{split} S &= \int_{V} \mathrm{d}V \int_{T} \frac{1}{T} \left( \frac{\partial C_{V}}{\partial V} \right)_{T} \mathrm{d}T = \int_{T} \frac{1}{T} \mathrm{d}T \int_{V} \mathrm{d}V \left( \frac{\partial C_{V}}{\partial V} \right)_{T} = \int_{T} \frac{C_{V_{0}}}{T} \mathrm{d}T \,; \\ S &= \int_{p} \mathrm{d}p \int_{T} \frac{1}{T} \left( \frac{\partial C_{p}}{\partial p} \right)_{T} \mathrm{d}T = \int_{T} \frac{1}{T} \mathrm{d}T \int_{p} \mathrm{d}p \left( \frac{\partial C_{p}}{\partial p} \right)_{T} = \int_{T} \frac{C_{p_{0}}}{T} \mathrm{d}T \end{split}$$

因此,

$$\begin{split} F &= -\int p \mathrm{d}V - \int S \mathrm{d}T = -\int p \mathrm{d}V - \int \mathrm{d}T \int \frac{C_{V_0}}{T} \mathrm{d}T \,; \\ G &= \int V \mathrm{d}p - \int S \mathrm{d}T = \int V \mathrm{d}p - \int \mathrm{d}T \int \frac{C_{p_0}}{T} \mathrm{d}T \,. \end{split}$$

## 2.6 习题 2.19

能量由两部分组成,分别是平动动能  $\epsilon^t$  与转动动能  $\epsilon^r$ . 注意到我们的目标是求状态方程,因此我们只需要关心配分函数对 V 的依赖,

$$Z = Z^t \cdot Z^r = \int e^{-\beta \frac{p^2}{2m}} \mathrm{d}x \mathrm{d}y \mathrm{d}z \mathrm{d}p_x \mathrm{d}p_y \mathrm{d}p_z \times \int e^{-\frac{\beta}{2I} \left(p_\theta^2 + \frac{p_\varphi^2}{\sin^2 \theta}\right)} \mathrm{d}\theta \mathrm{d}\varphi \mathrm{d}p_\theta \mathrm{d}p_\varphi = V \times g(\overline{\wedge} \overleftrightarrow{\otimes} \overline{\mathcal{R}} \ V).$$

因此, 状态方程为:

$$p = \frac{N}{\beta} \frac{\partial \ln Z}{\partial V} = \frac{N}{\beta V},$$

即为理想气体的状态方程.

### 3 第三章

#### 3.1 习题 3.1

先计算体系的配分函数

$$P = Z^N = V^N \left[ \frac{2\pi m}{\beta} \right]^{\frac{3N}{2}},$$

a) 由此可得体系的平均能量

$$\bar{E} = -\frac{\partial \ln P}{\partial \beta} = \frac{3}{2} N k_B T;$$

b) 求最概然能量  $E_p$  需写出能量的概率分布

$$f(E)dE = e^{-\Psi - \beta E}d\Omega(E) = e^{-\Psi - \beta E}\Omega'(E)dE \propto e^{-\beta E}E^{\frac{3N}{2} - 1}dE \quad \Rightarrow \quad f(E) \propto e^{-\beta E}E^{\frac{3N}{2} - 1},$$

因此

$$\left. \frac{\partial f(E)}{\partial E} \right|_{E=E_p} = 0 \quad \Rightarrow \quad E_p = \left( \frac{3}{2} N - 1 \right) k_B T.$$

#### 3.2 习题 3.3

考虑到每个自旋有两种状态,记为: +1,-1,且分别对应了两个能量的取值:  $-\mu H$ , $+\mu H$ .体系的所有自旋的状态的选取确定了体系的一个构型 (configuration),例:  $\{s_i\} = \{+1,-1,-1,-1,+1,\cdots\}$ ,表示体系第 1 个自旋处于+1 的状态,第 2 个自旋处于-1 的状态,等等.为了求体系的配分函数,我们需要对体系的所有构型求和

$$P = \sum_{\{s_i\}} e^{-\beta \sum_{i=1}^{N} (-1)^{(s_i+1)/2} \mu H} = \sum_{\{s_i\}} \prod_{i=1}^{N} e^{-\beta (-1)^{(s_i+1)/2} \mu H}$$
$$= \prod_{i=1}^{N} \sum_{s_i = \pm 1} e^{-\beta (-1)^{(s_i+1)/2} \mu H} = \prod_{i=1}^{N} \left( e^{-\beta \mu H} + e^{\beta \mu H} \right)$$
$$= \left( 2 \cosh(\beta \mu H) \right)^{N},$$

因此可得体系的内能, 熵, 热容和总磁矩分别为

$$\begin{cases} U = -\frac{\partial}{\partial \beta} \ln P = -N\mu H \tanh(\beta \mu H); \\ S = S_0 + k_B \left( \ln P - \beta \frac{\partial}{\partial \beta} \ln P \right) = S_0 + Nk_B \left( \ln(2\cosh\beta \mu H) - \beta \mu H \tanh\beta \mu H \right); \\ C_H = \left( \frac{\partial U}{\partial T} \right)_H = -k_B \beta^2 \left( \frac{\partial U}{\partial \beta} \right)_H = Nk_B \frac{(\beta \mu H)^2}{\cosh^2(\beta \mu H)}; \\ M = \frac{1}{\beta} \frac{\partial \ln P}{\partial H} = N\mu \tanh(\beta \mu H). \end{cases}$$

#### 3.3 习题 3.7

先求体系的配分函数

$$P = V^N \left[ 4\pi \int_0^{+\infty} e^{-\beta cp} p^2 dp \right]^N = \left[ \frac{8\pi V}{(c\beta)^3} \right]^N,$$

由此可得体系的状态方程与内能

$$\begin{cases} p = \frac{1}{\beta} \frac{\partial \ln P}{\partial V} = \frac{N}{\beta V} & \Rightarrow & pV = Nk_B T; \\ U = -\frac{\partial \ln P}{\partial \beta} = 3Nk_B T. \end{cases}$$

#### 3.4 习题 3.11

由能均分定理

$$\overline{\frac{1}{2}mv_i^2} = \frac{1}{2}k_BT \quad \Rightarrow \quad \overline{v_i^2} = \frac{k_BT}{m},$$

a)

$$\overline{v_x^3} \propto \int_{-\infty}^{+\infty} e^{-\beta m v_x^2/2} v_x^3 \mathrm{d}v_x = 0;$$

b)

$$\overline{v_x^3 v_y} \propto \int_{-\infty}^{+\infty} e^{-\beta m v_x^2/2} v_x^3 dv_x \times \int_{-\infty}^{+\infty} e^{-\beta m v_y^2/2} v_y dv_y = 0;$$

c)

$$\overline{v_x^2 v_y^2} = \overline{v_x^2} \times \overline{v_y^2} = \left(\frac{k_B T}{m}\right)^2;$$

d)

$$\overline{(v_x + av_y)^2} = \overline{v_x^2 + 2av_xv_y + a^2v_y^2} = \overline{v_x^2} + 0 + a^2\overline{v_y^2} = (a^2 + 1)\frac{k_BT}{m};$$

e)

$$\overline{v^2v_x} = \overline{v_x^3} + \overline{v_y^2v_x} + \overline{v_z^2v_x} = 0.$$

#### 3.5 习题 3.12

a)

由能均分定理 
$$\Rightarrow$$
  $\bar{\epsilon} = \frac{5}{2}k_BT$ ;

b)

$$\frac{1}{2}m(v_y - v_0)^2 = \frac{1}{2}mv_y^2 + \frac{1}{2}mv_0^2 - mv_yv_0 = \frac{1}{2}mv_y^2 - \frac{1}{2}mv_0^2 = \frac{1}{2}k_BT,$$

$$\frac{1}{2}mv_y^2 = \frac{1}{2}k_BT + \frac{1}{2}mv_0^2.$$

因此, 我们有

#### 3.6 习题 3.15

a)

$$\begin{split} \left\langle \frac{\Omega(E)}{\Omega'(E)} \right\rangle_{\text{c.e.}} &= \int_{\Omega} e^{-\Psi - \beta E} \frac{\Omega(E)}{\Omega'(E)} \mathrm{d}\Omega(E) \\ &= \int_{0}^{+\infty} e^{-\Psi - \beta E} \Omega(E) \mathrm{d}E \\ &= -\frac{1}{\beta} \int e^{-\Psi} \Omega(E) \mathrm{d}e^{-\beta E} \\ &= -\frac{1}{\beta} e^{-\Psi - \beta E} \Omega(E) \bigg|_{E=0}^{E=+\infty} + \frac{1}{\beta} \int_{\Omega} e^{-\Psi - \beta E} \mathrm{d}\Omega(E) \\ &= \frac{1}{\beta} \,; \end{split}$$

b) 由能量的概率分布

$$f(E)dE = e^{-\Psi - \beta E}d\Omega(E) = e^{-\Psi - \beta E}\Omega'(E)dE \quad \Rightarrow \quad f(E) = e^{-\Psi - \beta E}\Omega'(E),$$

我们有

$$\frac{\partial f(E)}{\partial E}\Big|_{E=E_p} = 0 \quad \Rightarrow \quad \frac{\Omega''(E_p)}{\Omega'(E_p)} = \beta.$$

#### 3.7 补充 S1

先求体系的配分函数

$$P = Z^N = V^N \left[ \frac{2\pi m}{\beta} \right]^{\frac{3N}{2}},$$

由此得到系统的状态方程,内能,熵和热容量为

$$\begin{cases} p = \frac{1}{\beta} \frac{\partial \ln P}{\partial V} & \Rightarrow pV = Nk_B T; \\ U = -\frac{\partial \ln P}{\partial \beta} = \frac{3}{2} Nk_B T; \\ S = S_0 + Nk_B \left[ \ln V + \frac{3}{2} \ln(2\pi m k_B T) + \frac{3}{2} \right]; \\ C_v = \frac{\partial U}{\partial T} = \frac{3}{2} Nk_B. \end{cases}$$

最后, 我们来算体系的能量涨落:

$$\begin{split} \bar{E^2} &= \int E^2 e^{-\Psi - \beta E} \mathrm{d}\Omega = e^{-\Psi} \frac{\partial^2 e^{\Psi}}{\partial \beta^2} = \frac{\partial^2 \Psi}{\partial \beta^2} + \left(\frac{\partial \Psi}{\partial \beta}\right)^2 \\ &\downarrow \\ (E - \bar{E})^2 &= \bar{E^2} - \bar{E}^2 = \frac{\partial^2 \Psi}{\partial \beta^2} = \frac{3}{2} N k_B^2 T^2 \;. \end{split}$$

#### 3.8 补充 S2

先求体系的配分函数

$$Z_{g.c.} = e^{\zeta} = \sum_{N} \frac{e^{-N\alpha}}{N!} \int e^{-\beta E} d\Omega = \sum_{N} \frac{(e^{-\alpha})^{N}}{N!} V^{N} \left(\frac{2\pi m}{\beta}\right)^{\frac{3N}{2}} = \exp\left[e^{-\alpha}V\left(\frac{2\pi m}{\beta}\right)^{3/2}\right],$$

因此

$$\zeta = e^{-\alpha} V \left(\frac{2\pi m}{\beta}\right)^{3/2}.$$

由此我们能得到体系的状态方程,内能,熵,化学势和分子数的相对涨落

$$\begin{cases} \bar{N} = -\frac{\partial \zeta}{\partial \alpha} = \zeta; \\ p = \frac{1}{\beta} \frac{\partial \zeta}{\partial V} = \frac{\zeta}{\beta V} \quad \Rightarrow \quad pV = \bar{N}k_BT; \\ U = -\frac{\partial \zeta}{\partial \beta} = \frac{3}{2}\bar{N}k_BT; \\ S = S_0 + k_B \left(\zeta - \beta \frac{\partial \zeta}{\partial \beta} - \alpha \frac{\partial \zeta}{\partial \alpha}\right) = S_0 + \left(\frac{5}{2} + \alpha\right)\bar{N}k_B; \\ \mu = -\alpha k_BT; \\ \overline{N^2} = \sum_N \frac{e^{-\zeta - N\alpha}N^2}{N!} \int \dots = e^{-\zeta} \frac{\partial^2}{\partial \alpha^2} Z_{g.c.} = e^{-\zeta} \frac{\partial^2}{\partial \alpha^2} e^{\zeta} = \zeta + \zeta^2; \\ \overline{(\Delta N)^2}/\bar{N}^2 = \overline{\frac{N^2 - \bar{N}^2}{\bar{N}^2}} = \frac{1}{\zeta} = \frac{1}{\bar{N}}. \end{cases}$$

## 4 第四章

#### 4.1 习题 4.4

a) 由书 P216 的 (4.14.3):  $p_F \propto n^{1/3}$ , 可知三个铜块的费米球半径相同.

b)

$$\begin{split} \bar{\epsilon} &= \frac{3}{5} \mu_0 \,; \\ \bar{\epsilon^2} &= \frac{8\pi V}{h^3 N} \int_{|p| \le \sqrt{2m\mu_0}} \epsilon^2 p^2 \mathrm{d}p = \frac{8\pi V}{h^3 N} \sqrt{2} m^{3/2} \int_0^{\mu_0} \epsilon^{5/2} \mathrm{d}\epsilon = \frac{8\pi V}{h^3 N} \sqrt{2} m^{3/2} \frac{2}{7} \mu_0^{7/2} = \frac{3}{7} \mu_0^2 \,; \\ & \qquad \qquad \downarrow \\ \overline{(\epsilon - \bar{\epsilon})^2} &= \bar{\epsilon^2} - \bar{\epsilon}^2 = \frac{12}{175} \mu_0^2 \,. \end{split}$$

#### 4.2 习题 4.14

$$f(v) \mathrm{d}v = \frac{4\pi g V}{h^3} \frac{p^2 \mathrm{d}p}{e^{(\epsilon - \mu)/k_B T} - 1} = \frac{4\pi g m^3 V}{h^3} \frac{v^2 \mathrm{d}v}{\exp[(mv^2/2 - \mu)/k_B T] - 1};$$
 易得最概然速率  $v_p$  满足的方程 
$$\frac{\mathrm{d}}{\mathrm{d}v} \left( \frac{v^2}{\exp[(mv^2/2 - \mu)/k_B T] - 1} \right) \Big|_{v = v_p} = 0;$$
 
$$\Rightarrow v_p^2 = \frac{2k_B T}{m} \frac{\exp[(mv_p^2/2 - \mu)/k_B T] - 1}{\exp[(mv_p^2/2 - \mu)/k_B T]};$$
 在  $T > T_c$  时,有  $\exp[(mv_p^2/2 - \mu)/k_B T] \gg 1$  
$$\Rightarrow v_p = \sqrt{\frac{2k_B T}{m}}.$$

#### 4.3 习题 4.17

考虑到膨胀前后的粒子数不变,  $N_1 = N_2 = N$ 

$$\begin{split} N_1 &= \frac{8\pi V_1}{3h^3} (2m)^{3/2} \mu_0^{3/2} \; ; \\ N_2 &= \frac{8\pi V_2}{3h^3} (2m)^{3/2} \mu^{3/2} \left[ 1 + \frac{\pi^2}{8} \left( \frac{k_B T}{\mu} \right)^2 + \cdots \right] \; , \\ \\ &\Rightarrow \quad \mu^{3/2} \approx \frac{V_1}{V_2} \mu_0^{3/2} \left[ 1 - \frac{\pi^2}{8} \left( \frac{k_B T}{\mu} \right)^2 \right] \; , \\ \\ \Rightarrow \quad \mu^{5/2} &\approx \left( \frac{V_1}{V_2} \right)^{5/3} \mu_0^{5/2} \left[ 1 - \frac{5\pi^2}{24} \left( \frac{k_B T}{\mu} \right)^2 \right] \end{split}$$

显然, 膨胀前后内能也不发生改变,  $E_1 = E_2 = E$ 

$$\begin{split} E_1 &= \frac{8\pi V_1}{h^3} \sqrt{2} m^{3/2} \frac{2}{5} \mu_0^{5/2} \,; \\ E_2 &= \frac{8\pi V_2}{h^3} \sqrt{2} m^{3/2} \frac{2}{5} \mu^{5/2} \left[ 1 + \frac{5\pi^2}{8} \left( \frac{k_B T}{\mu} \right)^2 + \cdots \right] \\ &\approx \frac{8\pi V_2}{h^3} \sqrt{2} m^{3/2} \frac{2}{5} \left( \frac{V_1}{V_2} \right)^{5/3} \mu_0^{5/2} \left[ 1 - \frac{5\pi^2}{24} \left( \frac{k_B T}{\mu} \right)^2 \right] \left[ 1 + \frac{5\pi^2}{8} \left( \frac{k_B T}{\mu} \right)^2 + \cdots \right] \\ &\approx \frac{8\pi V_2}{h^3} \sqrt{2} m^{3/2} \frac{2}{5} \left( \frac{V_1}{V_2} \right)^{5/3} \mu_0^{5/2} \left[ 1 + \frac{5\pi^2}{12} \left( \frac{k_B T}{\mu} \right)^2 \right] \,, \\ &\Rightarrow V_1 \mu_0^{5/2} = V_2 \left( \frac{V_1}{V_2} \right)^{5/3} \mu_0^{5/2} \left[ 1 + \frac{5\pi^2}{12} \left( \frac{k_B T}{\mu} \right)^2 \right] \,, \\ &\Rightarrow \frac{k_B T}{\mu} = \sqrt{\frac{12}{5\pi^2} \left[ \left( \frac{V_2}{V_1} \right)^{3/2} - 1 \right] \,. \end{split}$$

最后再利用一下 μ 粗的近似

$$\mu \approx \left(\frac{3}{8\pi}\right)^{2/3} \frac{h^2}{2m} \left(\frac{N}{V_2}\right)^{2/3} ,$$

$$\Rightarrow T = \left(\frac{3}{8\pi}\right)^{2/3} \frac{h^2}{2mk_B} \left(\frac{N}{V_2}\right)^{2/3} \sqrt{\frac{12}{5\pi^2} \left[\left(\frac{V_2}{V_1}\right)^{3/2} - 1\right]} .$$

#### 4.4 习题 4.19

利用可逆绝热条件及黑体辐射的相关结论

$$\begin{split} 0 &= T\mathrm{d}S = \mathrm{d}U + p\mathrm{d}V\,;\\ p &= \frac{1}{3}u = \frac{1}{3}aT^4\,;\\ U &= uV = aT^4V\,, \end{split}$$

将 p 与 U 代入热一公式后整理得到

$$d(3 \log T + \log V) = 0 \implies VT^3 = \text{const} \implies T_f = 500 \text{K}.$$

#### 4.5 习题 4.20

由苏书 (4.14.9) 及 (4.14.4)

$$\left(\frac{\partial p}{\partial V}\right)_{T=0} = -\frac{h^2}{3mV} \left(\frac{3}{8\pi}\right)^{2/3} \left(\frac{N}{V}\right)^{5/3} = -\frac{2}{3V} \epsilon_F n,$$

$$\Rightarrow \quad \kappa|_{T=0} = -\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_{T=0} = \frac{3}{2} \frac{1}{n \epsilon_F}.$$

#### 4.6 习题 4.25

a) 
$$\phi_{\vec{p}} \propto \exp{(i\vec{p} \cdot \vec{r})}/\hbar$$
 由周期边界条件  $\Rightarrow p_{\alpha}L = 2\pi\hbar n_{\alpha} \quad (\alpha = x, y, z)$   $\Rightarrow \epsilon = c|\vec{p}| = \frac{2\pi c\hbar}{V^{1/3}} \sqrt{n_x^2 + n_y^2 + n_z^2}$ .

b) 由习题 3.7, 
$$p = \frac{U}{3V}, p_{s} = \frac{U}{3NV}$$
.

## 4.7 习题 4.26