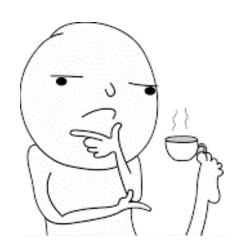
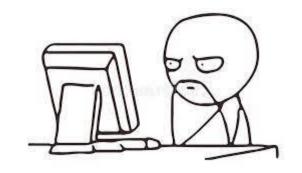




Dude, how do you build a Magneto - Optical Trap?



Workshop May 06, 2024 Sukhman K. S.



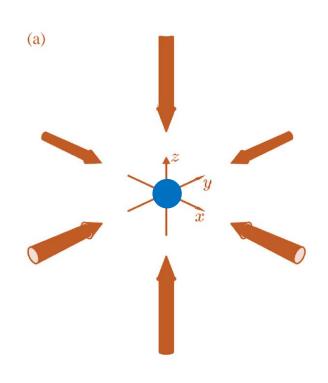




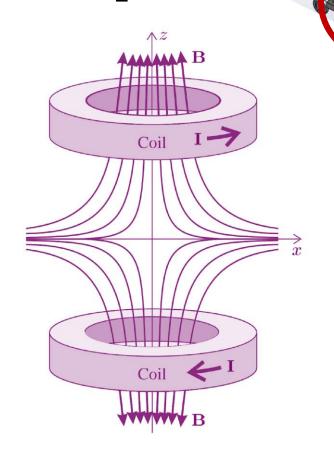
Outline

- Cooling and Trapping: MOT beams Optical Molasses
- Vacuum System
- Generating Quadrupole Magnetic Field
- Limitations of MOT: Temperature, Density
- Characterization and Optimization of MOTs: Thermometry, Imaging System

MOT: Magneto-Optical Trap



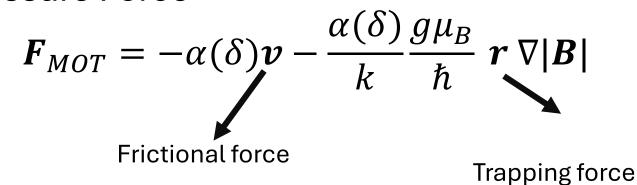
3 retro-reflected beams

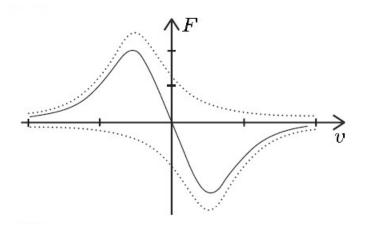


2 coils generating magnetic field

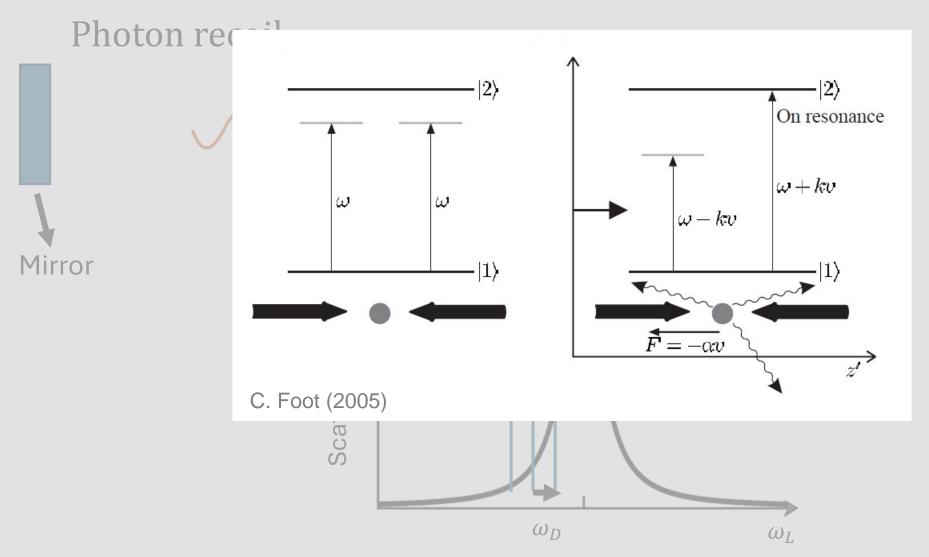
Cooling & Trapping forces

Radiation Pressure Force

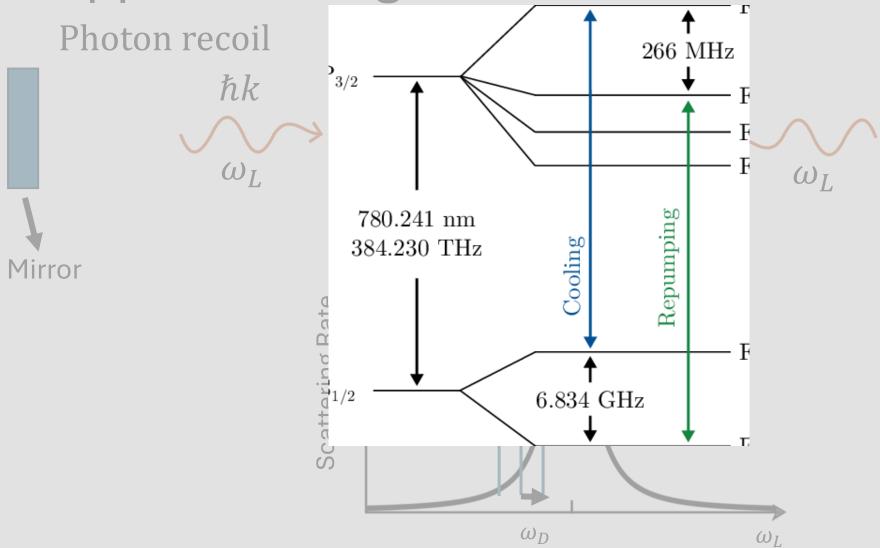




Doppler Cooling

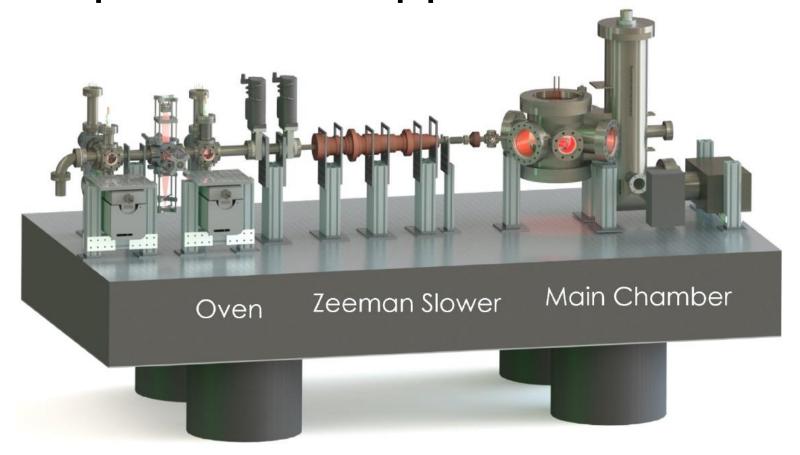


Doppler Cooling



Vacuum

Typical Experimental Apparatus

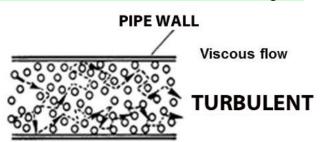


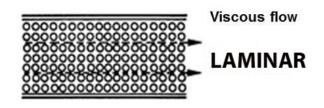
Ultracold Lithium University of California, Santa Barbara; PhD Thesis, C. Fujiwara (2019)

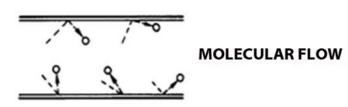
Mean free path $\lambda_{\text{mean}} \cong \frac{1}{n_0} \frac{1}{\sigma}$

Molecular Flow regime

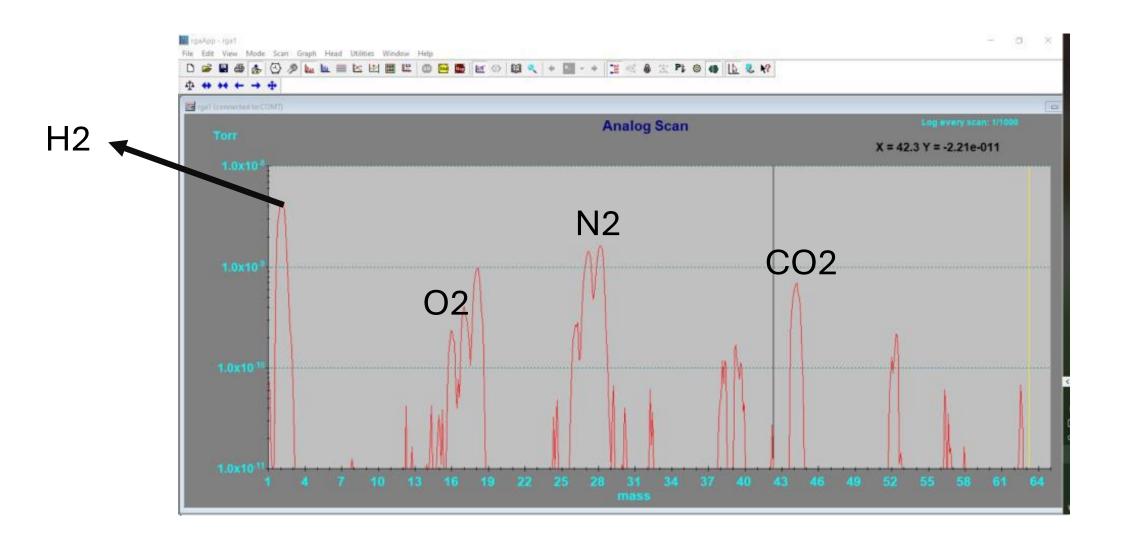
- Mean free path, for various pressure regimes:
 - $\lambda_{\text{mean}}(1 \text{ Torr}) \cong 30 \, \mu m$
 - $\lambda_{\text{mean}} (10^{-6} \text{ Torr}) \cong 30 \text{ } m$
 - $\lambda_{\text{mean}} (10^{-9} \text{ Torr}) \cong 30 \text{ km}$
- Throughput d/dt(PV) = Q
- Conductance $C = \frac{Q}{P_2 P_1}$ and $C = \alpha C_a$
 - Aperture: $C = 9.3 D^2$ Litre/s where diameter D in cm
 - Cylindrical tubes: $C=12.4 \frac{D^3}{L}$ L/s where length L in cm







Leaks? Residual Gas Analyzer (RGA)



Vacuum System: Pumps

• Roughing pump (best 0.01 Torr) → Turbo Pump (10⁻⁶-10⁻¹⁰ Torr)

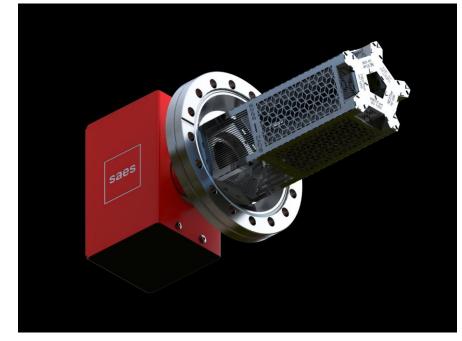
• Ion Pump: Main pump removes the noble gases, primarily Ar (6 L/s)

and $CH_4(15 L/s)$

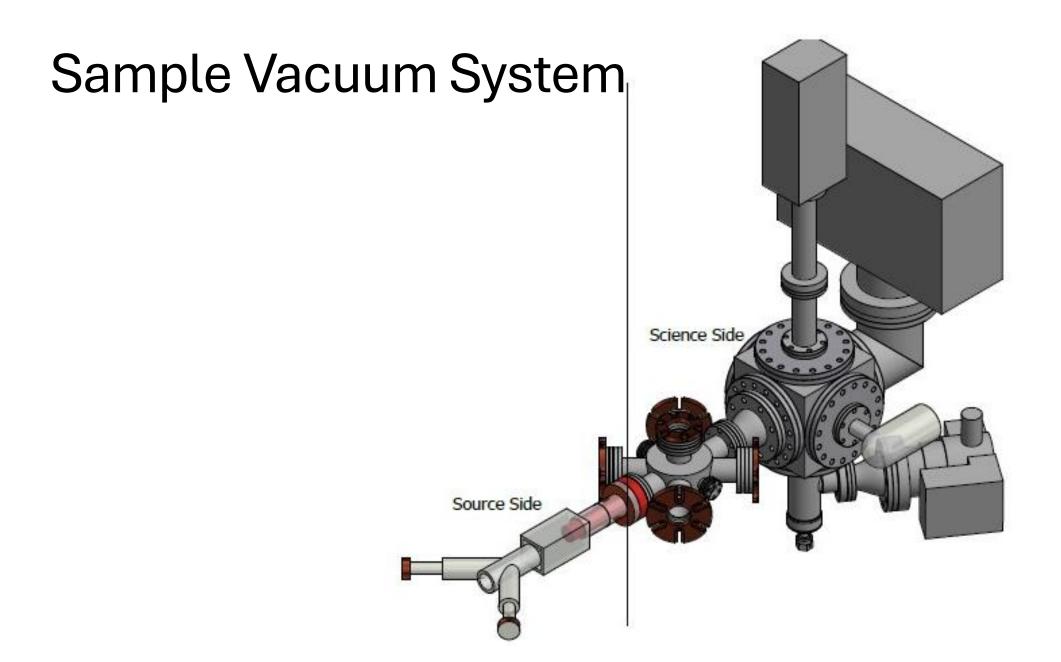
• Non-evaporative Getter (NEG): e.g. Ti-Sub

to boost H2 pumping (byproduct: H2O, CO2, O2 and N2.)

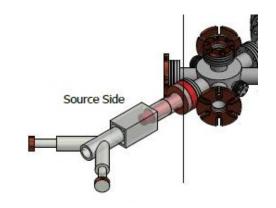
Getters do not pump noble gases as they are not chemically reactive.

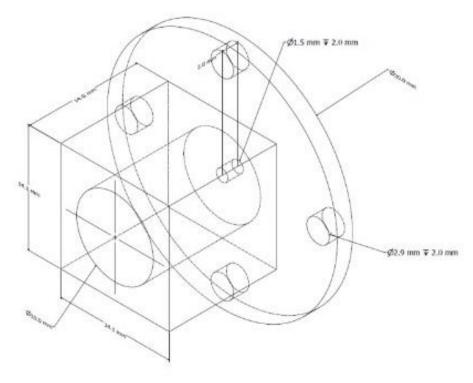


SAES

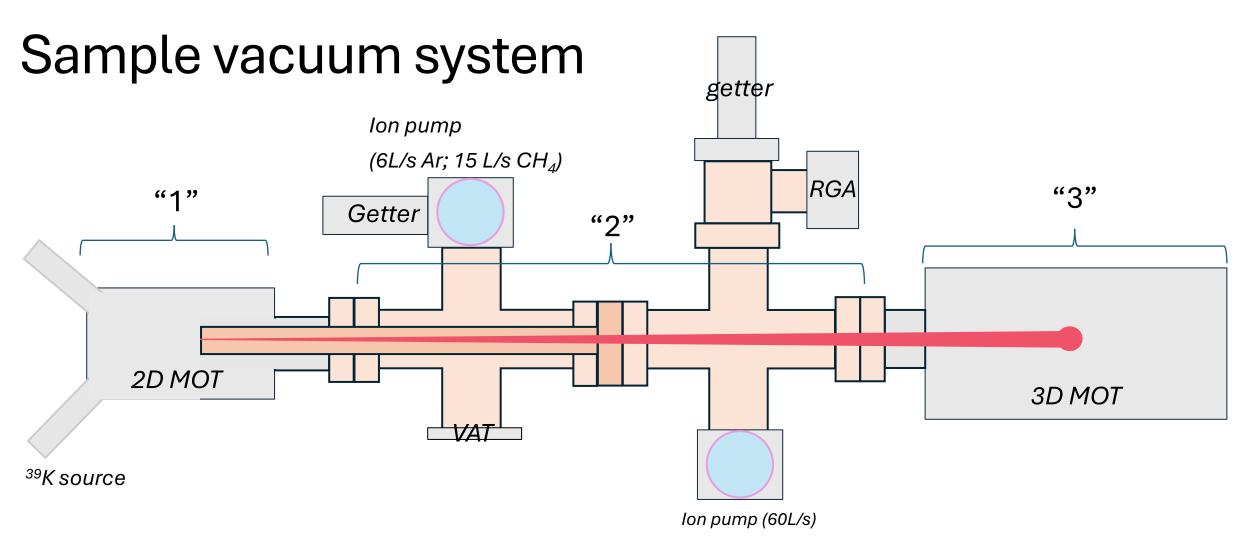


Differential Pumping Stage





Current differential pumping tube with a 1.5mm opening



- 1. Isolation: C_{12} , C_{23} 'small' $\rightarrow P_3 \sim 10^{-3} P_2 \sim 10^{-3} P_1$
- 2. Adequate pumping of 2, 3: $C_{P2, 2}$, $C_{P3, 3}$ 'large' i.e. low pressure & high pumping speed

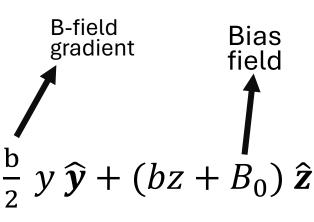
- 3. High solid angle of 3D MOT
- 4. Optical access

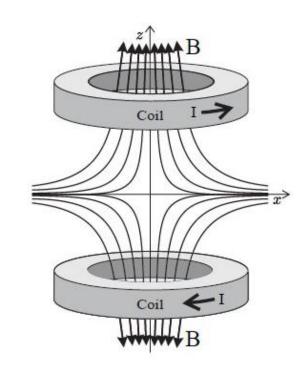
Magneto-Optical Trap

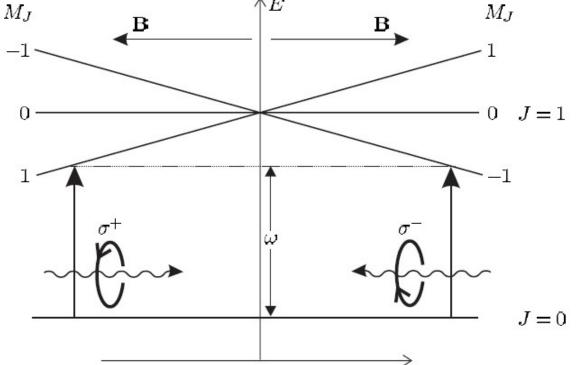
Magnetic Field

Quadroupole field

$$\mathbf{B}(\mathbf{x}, \mathbf{y}, \mathbf{z}) = -\frac{\mathbf{b}}{2} x \hat{\mathbf{x}} - \frac{\mathbf{b}}{2} y \hat{\mathbf{y}} + (bz + B_0) \hat{\mathbf{z}}$$







 Zeeman shift at displacement z provided by the magnetic field is

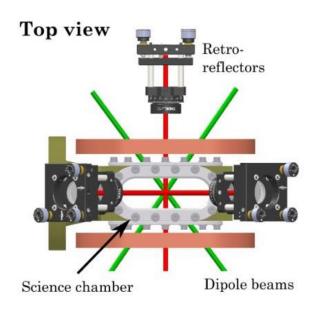
$$U_Z = \frac{g\mu_B}{\hbar} \frac{dB}{dz} Z$$

Magnetic Field – Design Considerations

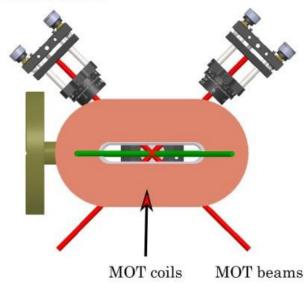
- 1. Uniformity
- 2. Dynamic response: Self- & Mutual-Inductance
- 3. Power Dissipation: depends on RT copper resistivity, wire cross-section, length
 - E.g. Total resistance of 77 $m\Omega$ requires 10 V power supply with 130 A anticipated power-dissipation: $I^2R=1.3~kW$
- 4. Hydrodynamic conductivity: determined by length & no of windings (limitations on cooling)
- 5. Feshbach fields: high fractional stability $\delta B/B_0$
- 6. Geometry: Hollow-core VS EDM

Electromagnets: Hollow-core

- Insulated copper wire with hollow-core
- Homogeneous field gradient upto distance r $r \leq \sqrt{3}r_{\rm eff}$
- Vacuum chamber constraint:
 - Separation distance d bw coils $\sim O(r_{\rm eff})$ $d \leq r_{\rm eff}$
- Issues: High water pressure, inefficient cooling, expansive, hard to recreate the same coils

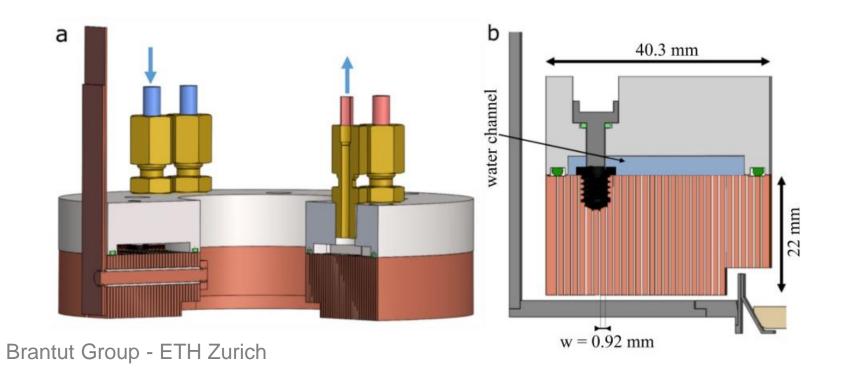


Side view



Electromagnets

 Bulk-machined electromagnet (EDM 6Ethylene Propylene Diene Methylene rubber)



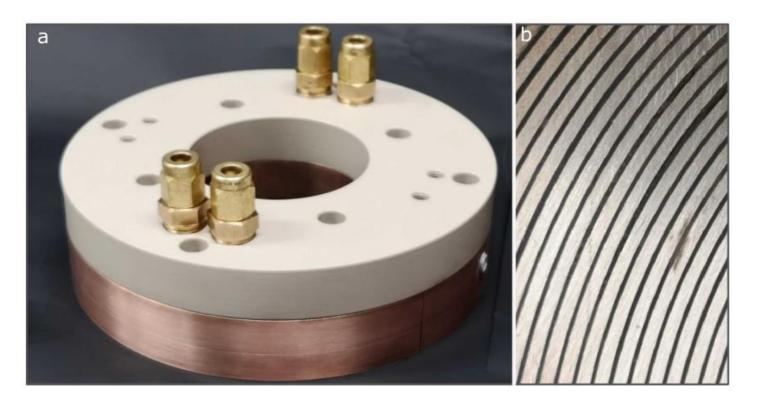


Figure 2: **a**: Photograph of the assembled electromagnet, showing the PEEK cap attached to the coil body, with coolant connections from the top. **b**: Close view of the top surface of the coil after glueing and machining on a standard lathe, showing the successive windings separated by the electrically insulating epoxy. The width of a copper winding is 0.92 mm.

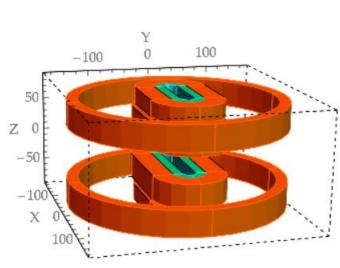
Radia: Quadroupole Magnet

Introduction & Theory

In this example, we model a simple iron-dominated quadrupole magnet. The pole-tips have hyperbolic faces with a flat chamfer at each end.

Field computations in the case of iron-dominated geometries present specific difficulties that usually make them less accurate t the case of structures dominated by coils or permanent magnets. Nevertheless, Radia includes special methods that enable one reasonable precision with a reasonable amount of computational effort—cpu time and memory usage.

Because this example bears some similarities to that of Example 5, all the remarks made there also apply here. We recommend to least review the introduction of that example before playing with this one. But, as a brief reminder for those in a hurry, the following recommendations will help you achieve an acceptable level of precision within a reasonable time frame:



SC Wiggler

Credits: github.com/ochubar/Radia

Radia

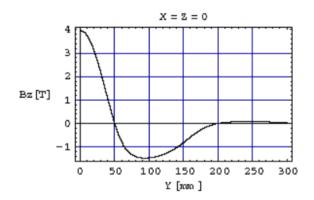
Plot the Field Integrals

```
Plot[radFldInt[Grp,"inf","ibz",{x,-300,0},{x,300,0}]
,{x,-400,400}
,FrameLabel->{"X [mm]","IBz [T mm]","Z = 0",""}];
```

IBz[T mm] -100 -150 -200 0 200 400 X [mm]

Plot the Magnetic Field

```
RadPlotOptions[];
Plot[radFld[Grp,"Bz",{0,y,0}],{y,0,300}
,AxesOrigin->{0,0}
,FrameLabel->{"Y [mm]","Bz [T]","X = Z = 0",""}];
```



Credits: github.com/ochubar/Radia

Limitations: n, T

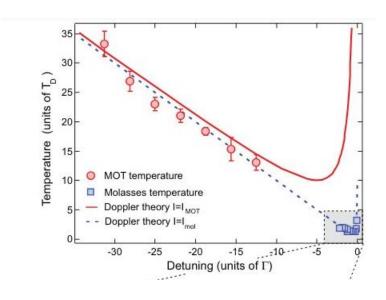
Limitations of a MOT: Temperature, T

• Temperature:

• Doppler Limit (Foot)

$$T_D = \frac{\hbar\Gamma}{2~k_B}$$
 (alkali T_D ~100µK) T_D = 146 µK

• Recoil limit (alkali $T_{rec} \sim 1 \mu K$) $T_{rec} = 362 \text{ nK} \rightarrow v_{rec} \cong 6 \text{mm/s}$ (typically 0.3-10cm/s)



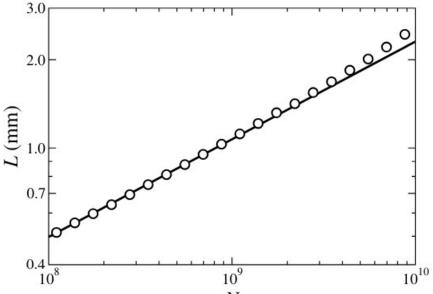
R. Chang et al. (2014)

Limitations of a MOT: Density, n

- $n \approx 10^{10} 10^{11} cm^{-3}$
- MOT size (L) scaling $L \propto N^{1/3}$

Standard MOT parameters

MOT detuning MOT intensity per beam MOT beam waist	$\delta_{ ext{MOT}} = -2.5\Gamma$ $I_{ ext{MOT}} pprox 1.2 ext{mW cm}^{-2}$ $w_{ ext{MOT}} pprox 2.4 ext{ cm}$
Repumper detuning Repumper intensity per beam	$\delta_{\mathrm{rep}} = 0$ $I_{\mathrm{rep}} \approx 0.5 \mathrm{mW cm^{-2}}$
Repumper beam diameter Magnetic field gradient	$L_{\rm rep} \approx 5 {\rm cm \ FWHM}$ $\nabla B = 10 {\rm G \ cm^{-1}}$



MOT size versus atom number calculated (circles) compared to the N $\sim L^{1/3}$ power law (solid line).

G. L. Gattobigio et al. (2010)

Measurement & Optimization: n, temp

Imaging System: Absorption Imaging

Absorption imaging

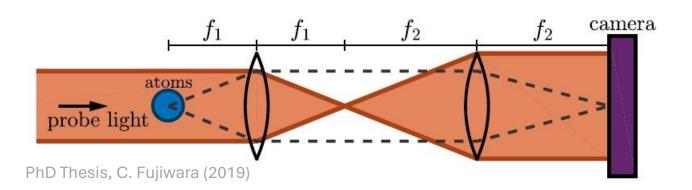
$$I_f = I_i e^{-OD} \qquad OD = n\sigma_0$$

• Discretization of OD yields the number of atoms for a given pixel N_{px}

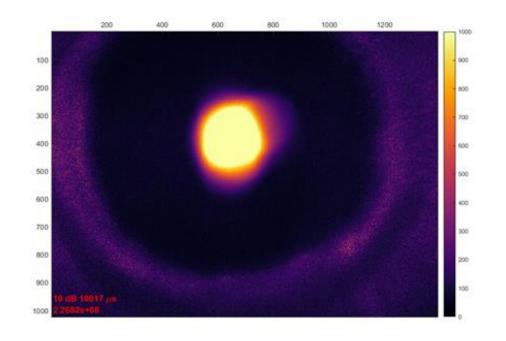
Physical area at location of atoms
$$N_{px} = \frac{A_{px}}{\sigma_0} \text{ OD} = \frac{A_{px}}{\sigma_0} \ln \left(\frac{I_{i,px} - I_{d,px}}{I_{f,px} - I_{d,px}} \right)$$

• Map atomic spatial distribution: 4F imaging system

Measured bg pixel intensity per pixel (common mode noise)



Fluorescence Image





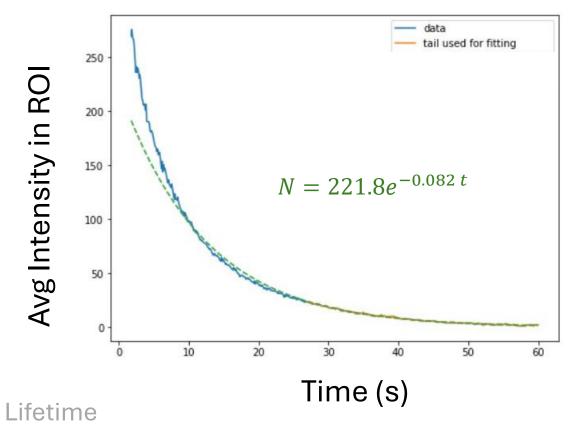
The number of atoms N within the MOT is obtained by

$$N\gamma_{sc} = \frac{4\pi}{\Omega} P_{\text{optical}}$$

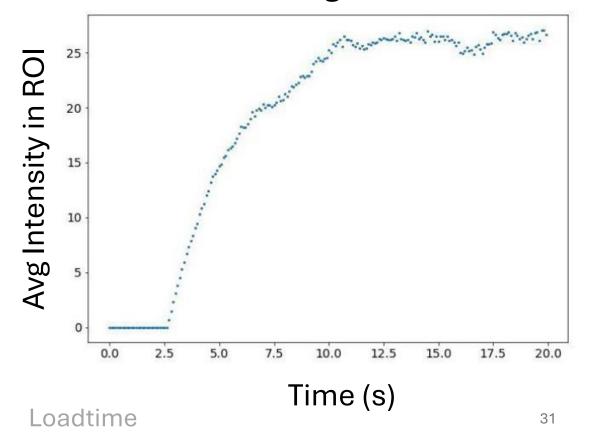
Characterization – Trap Dynamics:

$$\frac{dN}{dt} = R - \gamma N - \beta \int n^2(\boldsymbol{r}, t) d^3 \boldsymbol{r}$$

After blocking 2D MOT beams

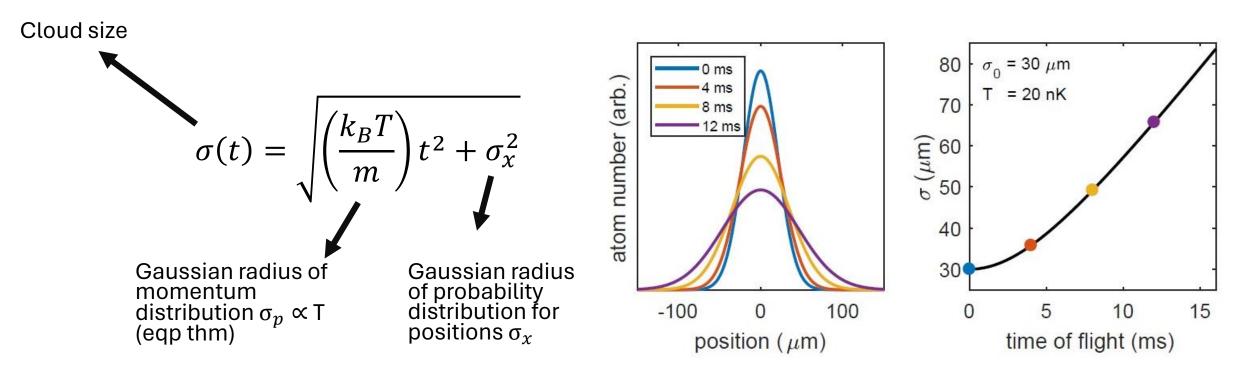


After unblocking 3D MOT beams



Ballistic Time-of-flight (TOF) thermometry: insitu x and p distribution

• Temperature of initial cloud σ_{χ} is related to the cloud size



Laboratoire Kastler Brossel Physique quantique et applications

scientific visualizations. Let's proceed with this idea.



Here is the artistic representation of rubidium atoms at a few hundred microkelvin. The image features an ethereal cloud of atoms inside a vacuum chamber, highlighted with blue and violet hues to suggest extreme coldness. You can view the image above.