

# **Foundations of Robotics**

**Lec 6: Inverse Kinematics** 



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# **\$** Outline

- 1. Inverse Kinematics
- 2. Analytic Approach (Trigonometry)
- 3. Numerical Approach (Newton's Method)
- 4. Homework

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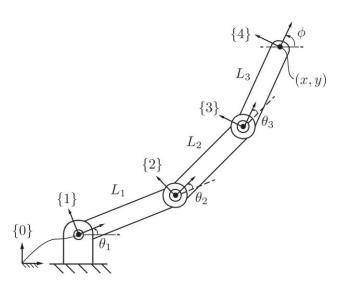
Consider a general *n* degree-of-freedom open chain.

#### **Forward Kinematics**

- $\theta \in \mathbb{R}^n \rightarrow T(\theta) \in SE(3)$
- Given joint coordinates  $\theta$ , calculate the configuration (position and orientation)  $T(\theta)$  of the end-effector frame.

#### **Inverse Kinematics**

- $T(\theta) \in SE(3) \rightarrow \theta \in \mathbb{R}^n$
- Given a homogeneous transform  $X \in SE(3)$  and forward kinematics  $T(\theta)$ , find solutions  $\theta$  that satisfy  $T(\theta) = X$ .





Example: a 2R planar open-chain manipulator

$$T(\theta) \in SE(2) \rightarrow \theta \in \mathbb{R}^2$$

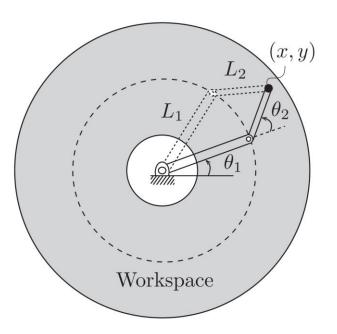
Considering only the position of end-effector and ignoring its orientation, the forward kinematics can be expressed as

$$x = L_1 \cos \theta_1 + L_2 \cos(\theta_1 + \theta_2)$$
  

$$y = L_1 \sin \theta_1 + L_2 \sin(\theta_1 + \theta_2)$$

Provided a desired end-effector position (x, y), there will be either zero, one or two solutions depending on where (x, y) lies.

## Assuming $L_1 > L_2$





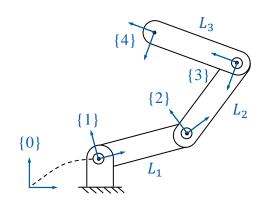
Example: a 3R planar open-chain manipulator

$$T(\theta) \in SE(2) \rightarrow \theta \in \mathbb{R}^3$$

Considering only the position of end-effector and ignoring its orientation, the forward kinematics can be expressed as

$$x = L_1 \cos \theta_1 + L_2 \cos(\theta_1 + \theta_2) + L_3 \cos(\theta_1 + \theta_2 + \theta_3)$$
  
$$y = L_1 \sin \theta_1 + L_2 \sin(\theta_1 + \theta_2) + L_3 \sin(\theta_1 + \theta_2 + \theta_3)$$

Provided a desired end-effector position (x, y), there will be either zero, one or multiple solutions depending on where (x, y) lies.



# **\$** Inverse Kinematics

Two ways to solve inverse kinematics:

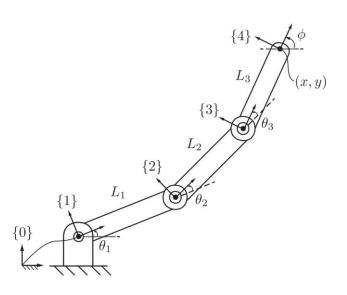
## Analytic Approach

- Derive equations based on the geometric structure (e.g., trigonometry) of the mechanism
- Provide zero, one or multiple solutions in closed-form

#### Numerical Approach

- Iteratively solve a non-linear optimization problem (e.g., by Newton-Raphson method)
- Require an initial guess; always produce one solution (best approximation, may not be optimal)

In practice, they both can be applied: analytic solution can serve as the initial guess for numerical methods.

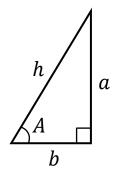


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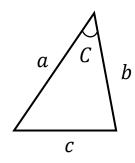


Math tools from trigonometry:



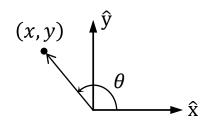
 $\sin A$ ,  $\cos A$ ,  $\tan A$  $\frac{a}{a}$ ,  $\frac{a}{b}$ ,  $\frac{a}{b}$ 

Trigonometric ratios



$$c^2 = a^2 + b^2 - 2ab\cos C$$

Law of cosines



$$\theta = \operatorname{atan2}(y, x) \in (-\pi, \pi]$$

Two-argument arctangent



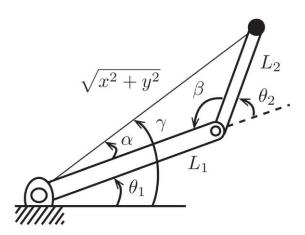
Example: A 2R planar open-chain manipulator

In the current "elbow-down" setup, as shown in the figure, joint angles can be obtained as follows.

- Compute  $\gamma = \operatorname{atan2}(y, x)$
- Compute  $\alpha$  from law of cosines
- Obtain  $\theta_1 = \gamma \alpha$
- Compute  $\beta$  from law of cosines
- Obtain  $\theta_2 = \pi \beta$

The other solution in the "elbow-up" setup can be obtained similarly:  $\theta_1 = \gamma + \alpha$ ,  $\theta_2 = \beta - \pi$ 

Again, no solution exists if (x, y) is not reachable, and exactly one solution exists if (x, y) lies on the boundary.

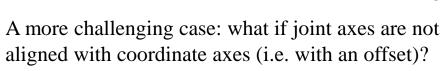


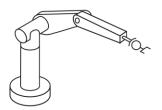


Example: A 3R spatial open-chain manipulator

One possible solution:

- Obtain  $\theta_1 = \operatorname{atan2}(p_y, p_x)$
- Compute  $\gamma = \operatorname{atan}(p_z/r)$
- Compute  $\alpha$  from law of cosines
- Obtain  $\theta_2 = \gamma \alpha$
- Compute  $\beta$  from law of cosines
- Obtain  $\theta_3 = \pi \beta$

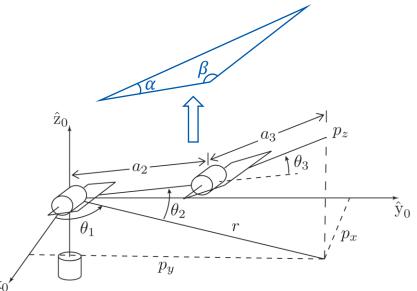












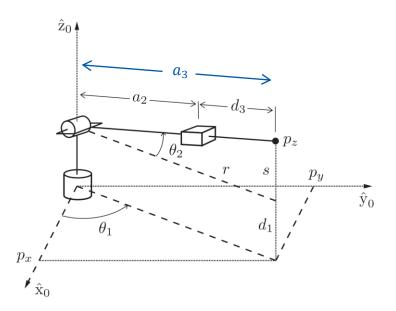


Example: An RRP spatial open-chain manipulator

One possible solution:

- Obtain  $\theta_1 = \operatorname{atan2}(p_y, p_x)$
- Compute  $s = p_z d_1$
- Compute  $r = \sqrt{p_x^2 + p_y^2}$
- Obtain  $\theta_2 = \operatorname{atan} s/r$
- Compute  $a_3 = \sqrt{r^2 + s^2}$
- Obtain  $d_3 = a_3 a_2$

Again, the solution can be more complicated if the shoulder joint is placed with an offset.





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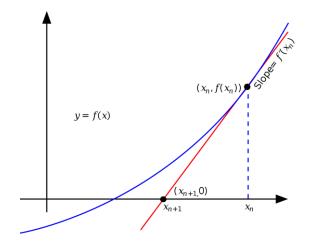


#### Newton-Raphson Method (a.k.a. Newton's Method)

 An iterative approach for finding the roots of a nonlinear equation.

#### Example of a scalar function

- Problem to solve: f(x) = 0
- Initial guess:  $x = x_0$
- At the *n*th iteration:  $x = x_n$
- Taylor expansion of f(x) at  $x_n$ :  $f(x) = f(x_n) + f'(x_n)(x - x_n) + h.o.t.$
- Ignore higher-order terms, set f(x) = 0 and solve for x to obtain  $x_{n+1} = x_n \frac{f(x_n)}{f'(x_n)}$
- Repeat until some stopping criterion is satisfied



<sup>\*</sup> Figure taken from wikipedia: https://en.wikipedia.org/wiki/Newton's\_method



#### Newton's Method in Optimization

• Find the roots of the derivative of a twice-differentiable function (solution to f'(x) = 0).

#### Example of a scalar function

Problem to solve

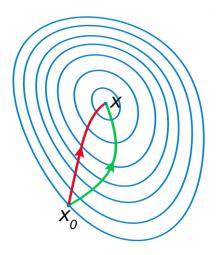
$$\min f(x)$$

• In each iteration, Taylor expansion of f(x) at  $x_n$  up to second order terms

$$f'(x) = f'(x_n) + f''(x_n)(x - x_n) = 0$$

Update equation

$$x_{n+1} = x_n - \frac{f'(x_n)}{f''(x_n)}$$



Green: Gradient Descent; Red: Newton's Method

\* Figure taken from wikipedia: https://en.wikipedia.org/wiki/Newton's\_method\_in\_ optimization



#### Newton's Method in Inverse Kinematics

- Inverse kinematics: find solution to  $T(\theta) = X$
- Define  $g(\theta) = x_d f(\theta) = X T(\theta)$
- Solve  $g(\theta) = 0$  using Newton's method

#### Example of a vector function

Problem to solve

$$g(\theta) = x_d - f(\theta) = 0$$

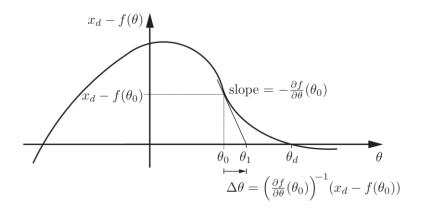
Taylor expansion

$$x_d = f(\theta) = f(\theta^k) + J(\theta^k)(\theta - \theta^k) + h.o.t.$$

• Update equation

$$\theta^{k+1} = \theta^k + J^{-1}(\theta^k)(x_d - f(\theta^k))$$

Note:  $J^{-1}$  exists only when J is square and nonsingular!



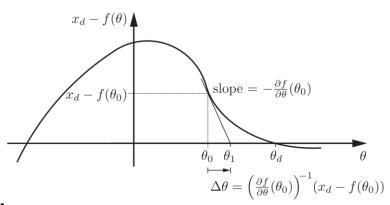
$$J(\theta^{k}) = \begin{bmatrix} \frac{\partial f_{1}}{\partial \theta_{1}^{k}} & \cdots & \frac{\partial f_{1}}{\partial \theta_{n}^{k}} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_{m}}{\partial \theta_{1}^{k}} & \cdots & \frac{\partial f_{m}}{\partial \theta_{n}^{k}} \end{bmatrix} \in \mathbb{R}^{m \times n}$$



In cases where J is not invertible, we can apply pseudoinverse  $J^{\dagger}$  instead.

- 1. The robot has more joints n than the end-effector coordinates m ("fat" Jacobian)
  - $J^{\dagger} = J^{\mathsf{T}} (JJ^{\mathsf{T}})^{-1}$
  - Called a right inverse since  $II^{\dagger} = I$
- 2. The robot has fewer joints n than the end-effector coordinates m ("tall" Jacobian)
  - $J^{\dagger} = (J^{\mathsf{T}}J)^{-1}J^{\mathsf{T}}$
  - Called a left inverse since  $I^{\dagger}I = I$

In practice, we often use linear solvers to avoid the computation of inverse matrices.



$$J(\theta^k) = \begin{bmatrix} \frac{\partial f_1}{\partial \theta_1^k} & \cdots & \frac{\partial f_1}{\partial \theta_n^k} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_m}{\partial \theta_1^k} & \cdots & \frac{\partial f_m}{\partial \theta_n^k} \end{bmatrix} \in \mathbb{R}^{m \times n}$$



## Algorithm to reach a provided 3D point

- 1. Initialization
  - Given an end-effector position  $x_d \in \mathbb{R}^m$
  - Given an initial guess  $\theta^0 \in \mathbb{R}^n$
  - Set k=0
- 2. While  $||x_d f(\theta^k)|| > \epsilon$  for some small  $\epsilon$ :
  - Compute  $\Delta \theta = J^{\dagger}(\theta^k) (x_d f(\theta^k))$
  - Update  $\theta^{k+1} = \theta^k + \Delta \theta$
  - Increment *k*

Right inverse:  $J^{\dagger} = J^{\mathsf{T}} (JJ^{\mathsf{T}})^{-1}$ 

Left inverse:  $J^{\dagger} = (J^{\mathsf{T}}J)^{-1}J^{\mathsf{T}}$ 

$$J(\theta^{k}) = \begin{bmatrix} \frac{\partial f_{1}}{\partial \theta_{1}^{k}} & \cdots & \frac{\partial f_{1}}{\partial \theta_{n}^{k}} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_{m}}{\partial \theta_{1}^{k}} & \cdots & \frac{\partial f_{m}}{\partial \theta_{n}^{k}} \end{bmatrix} \in \mathbb{R}^{m \times n}$$



## Algorithm to reach a provided 6D pose

- Initialization
  - Given an end-effector pose  $T_{sd} \in SE(3)$
  - Given an initial guess  $\theta^0 \in \mathbb{R}^n$
  - Set k = 0
- While  $\|\omega_h\| > \epsilon_{\omega}$  or  $\|v_h\| > \epsilon_v$  for some small  $\epsilon_{\omega}$  and  $\epsilon_{v}$ :
  - Compute  $[\mathcal{V}_b] = \log(T_{sb}^{-1}(\theta^k)T_{sd})$
  - Compute  $\Delta \theta = J^{\dagger}(\theta^{k})\mathcal{V}_{b}$  Update  $\theta^{k+1} = \theta^{k} + \Delta \theta$  Increment k

Jacobian should act on body twist

Right inverse: 
$$J^{\dagger} = J^{\top} (JJ^{\top})^{-1}$$

Left inverse: 
$$J^{\dagger} = (J^{\mathsf{T}}J)^{-1}J^{\mathsf{T}}$$

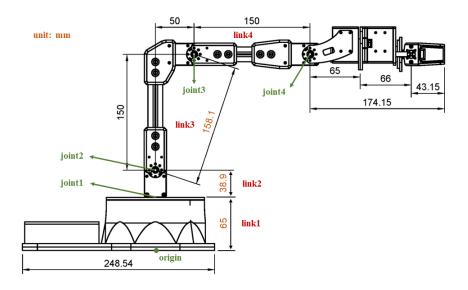
$$J(\theta^k) = \begin{bmatrix} \frac{\partial f_1}{\partial \theta_1^k} & \dots & \frac{\partial f_1}{\partial \theta_n^k} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_m}{\partial \theta_1^k} & \dots & \frac{\partial f_m}{\partial \theta_n^k} \end{bmatrix} \in \mathbb{R}^{m \times n}$$

desired state: 
$$T_{sd}$$
 current state:  $T_{sb}(\theta^k)$  difference:  $T_{bd}(\theta^k) = T_{bs}(\theta^k)T_{sd} = T_{sb}^{-1}(\theta^k)T_{sd}$ 

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#### (1) Lab Assignments: Inverse Kinematics

- Provided the schematic of a 3R manipulator, write two scripts (in C++ or Python) to implement analytic and numerical methods to solve the inverse kinematics.
- The scripts will be tested using a few test cases (input: the position of the end effector; expected output: joint variables)



# Thanks for Listening

