



**SAVEETHA SCHOOL OF ENGINEERING,
SAVEETHA INSTITUTE OF MEDICAL AND TECHNICAL
SCIENCES**



**TRANSMISSION LINES
&
WAVEGUIDES**

ECA15

NAME:

REG.NO:

LAB MANUEL



**SAVEETHA SCHOOL OF ENGINEERING
SAVEETHA INSTITUTE OF TECHNICAL AND MEDICAL
SCIENCES**



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EXNO: 1	Estimation of Characteristic Impedance (Z_0), and Propagation Constant (γ) of a Transmission Line from Primary Constants
DATE:	

Test Case 1:

Investigating the significance of Characteristic Impedance (Z_0), and Propagation Constant (γ) of a Transmission Line using the following parameters

- a) Resistance = $10 \Omega/\text{Km}$
- b) Capacitance = $8 \mu\text{F}/\text{Km}$
- c) Inductance = $3.5 \text{ mH}/\text{Km}$
- d) Conductance = $4 \mu\text{mho}/\text{Km}$
- e) Frequency = 2 KHz

AIM: Investigating the significance of Characteristic Impedance (Z_0), and Propagation Constant (γ) of a Transmission Line with Resistance = $10 \Omega/\text{Km}$, Capacitance = $8 \mu\text{F}/\text{Km}$, Inductance = $3.5 \text{ mH}/\text{Km}$, Conductance = $4 \mu\text{mho}/\text{Km}$, Frequency = 2 KHz

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION:

$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}} = \sqrt{\frac{Z}{Y}}$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \sqrt{ZY}$$

PROGRAM:

```

clear; clc;
R=10;L=0.003;f=2*10^3;G=4*(10^-6);C=16*(10^-6);
w=2*pi*f;
Z=R+(%i*w*L);
Y=G+(%i*w*C);
Zo=sqrt(Z/Y);
C=round(real(Zo));
D=round(imag(Zo));
printf('-Zo = %f + j(%f)ohms\n',C,D);
P=sqrt(Z*Y);
a=real(P);
a1=round(a*10000)/10000;
printf('-Attenuation constant a = %f neper/km\n',a1);
b=imag(P);
b1=round(b*10000)/10000;
printf('-Phase constant b = %f radians/km',b1);

```

OUTPUT:

Constants L=3mH; f=2000; G=.4*(10⁻⁶); C=8*(10⁻⁶).

Simulation Results			Theoretical Results	
Z0(ohms)	α (neper/km)	β (radians/km)	α (neper/km)	β (radians/km)

RESULT:

The characteristic impedance and propagation constant of a transmission line is calculated using SCILAB and the impact of primary constants on secondary constants are investigated.

Test Case 2:

Examine the impact of resistance and inductance on the significance of Characteristic Impedance (Zo) and Propagation Constant (γ) of a Transmission Line at a frequency f=2.5 Khz. Vary the resistance value from 10 Ω to 50 Ω at the interval of 10 Ω with L,G and C values constant and calculate the Characteristic Impedance and Propagation Constant . Vary the inductance values from 3.5 mH to 11.5 mH at the interval of 2.5 mH with R,G and C values constant.

AIM: To examine the impact of resistance and inductance on the significance of

Characteristic Impedance (Z_0) and Propagation Constant (γ) of a Transmission Line at a frequency $f=2.5$ KHz. Vary the resistance value from $10\ \Omega$ to $50\ \Omega$ at the interval of $10\ \Omega$ with L,G and C values constant and calculate the Characteristic Impedance and Propagation Constant . Vary the inductance values from 3.5 mH to 11.5 mH at the interval of 2.5 mH with R,G and C values constant.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program
-

CALCULATION:

$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}} = \sqrt{\frac{Z}{Y}}$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \sqrt{ZY}$$

PROGRAM:

```
clear; clc;
R=10;L=0.003;f=2*10^3;G=4*(10^-6);C=16*(10^-6);
w=2*pi*f;
Z=R+(%i*w*L);
Y=G+(%i*w*C);
Zo=sqrt(Z/Y);
C=round(real(Zo));
D=round(imag(Zo));
printf('-Zo = %f + j(%f)ohms\n',C,D);
P=sqrt(Z*Y);
a=real(P);
a1=round(a*10000)/10000;
printf('-Attenuation constant a = %f neper/km\n',a1);
b=imag(P);
b1=round(b*10000)/10000;
printf('-Phase constant b = %f radians/km',b1);
```

OUTPUT:

Variable R

Constants $L=3\text{mH}$; $f=2000$; $G=.4*(10^{-6})$; $C=8*(10^{-6})$.

S. No.	Inputs (R)	Simulation Results			Theoretical Results	
		$Z_0(\text{ohms})$	$\alpha(\text{neper/km})$	$\beta(\text{radians/km})$	$\alpha(\text{neper/km})$	$\beta(\text{radians/km})$
1						
2						
3						
4						
5						

Variable L

Constants $R=10\Omega$; $f=2000$; $G=.4*(10^{-6})$; $C=8*(10^{-6})$.

S. No.	Inputs (L)	Simulation Results			Theoretical Results	
		$Z_0(\text{ohms})$	$\alpha(\text{neper/km})$	$\beta(\text{radians/km})$	$\alpha(\text{neper/km})$	$\beta(\text{radians/km})$
1						
2						
3						
4						
5						

RESULT:

The impact of resistance and inductance on the significance of Characteristic Impedance (Z_0) and Propagation Constant (γ) of a Transmission Line is examined at a frequency $f=2.5\text{ KHz}$.

Test Case 3:

Explore the impact of frequency and capacitance on the significance of Characteristic Impedance (Z_0) and Propagation Constant (γ) of a Transmission Line. Vary the frequency from 2KHz to 10 KHz at the interval of 2 KHz with L,R ,G and C values constant and calculate the Characteristic Impedance and Propagation Constant . Vary the capacitance values from 8 μF to 16 μF at the interval of 2 μF with R,G and L values constant.

AIM: To explore the impact of frequency and capacitance on the significance of Characteristic Impedance (Z_0) and Propagation Constant (γ) of a Transmission Line. Vary the frequency from 2KHz to 10 KHz at the interval of 2 KHz with L,R ,G and C values constant and calculate the Characteristic Impedance and Propagation Constant

CALCULATION:

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{Z}{Y}}$$

$$\gamma = \sqrt{(R+j\omega L)(G+j\omega C)} = \sqrt{ZY}$$

PROGRAM:

```
clear; clc;
R=10;L=0.003;f=2*10^3;G=4*(10^-6);C=16*(10^-6);
w=2*pi*f;
Z=R+(%i*w*L);
Y=G+(%i*w*C);
Zo=sqrt(Z/Y);
C=round(real(Zo));
D=round(imag(Zo));
printf('-Zo = %f + j(%f)ohms\n',C,D);
P=sqrt(Z*Y);
a=real(P);
a1=round(a*10000)/10000;
printf('-Attenuation constant a = %f neper/km\n',a1);
b=imag(P);
b1=round(b*10000)/10000;
printf('-Phase constant b = %f radians/km',b1);
```

OUTPUT:

Variable f
Constants L=3mH; f=2000; G=.4*(10^-6); C=8*(10^-6).
;

S. No.	Inputs (f) Hz	Simulation Results			Theoretical Results	
		Z0(ohms)	α (neper/km)	β (radians/km)	α (neper/km)	β (radians/km)
1						
2						
3						
4						
5						

Variable C
Constants R=10; L=.009; f=2500; G=.4*(10^-6);

S. No.	Inputs (C) F	Simulation Results			Theoretical Results	
		$Z_0(\text{ohms})$	α (neper/km)	β (radians/km)	α (neper/km)	β (radians/km)
1						
2						
3						
4						
5						

RESULT:

The impact of frequency and capacitance on the significance of Characteristic Impedance (Z_0) and Propagation Constant (γ) of a Transmission Line is investigated for various values of frequencies and capacitance values.

EXNO: 2	Estimation of Primary Constants (R,L,G &C) from Secondary Constants (Zo & γ) of an open wire transmission line
DATE:	

Test Case 1:

Find the primary constants R,L,G and C for the varying values of Characteristic Impedance (Zo) of a Transmission Line at a frequency f=2 KHz. Vary the Characteristic Impedance value from 100 Ω and take five readings at the interval of 20 Ω . Keep the Propagation Constant (γ) constant

AIM: To find the primary constants R,L,G and C for the varying values of Characteristic Impedance (Zo) of a Transmission Line at a frequency f=2 KHz. Vary the Characteristic Impedance value from 100 Ω and take five readings at the interval of 20 Ω . Keep the Propagation Constant (γ) constant

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$R + j\omega L = Z_0 \gamma$$

$$g + j\omega C = \gamma / Z_0$$

PROGRAM:

```
clear; clc;
Zo=100.6;f=2000; //value of Zo as taken in solution P=0.054* exp(%i*(%pi/(180/87.9)));
w=2*%pi*f;
Z=Zo*P;
R=real(Z);
```

```

printf('-Resistance R = %f ohms/km\n',R); L=(imag(Z))/w;
printf('-Inductance L = %f mH/km\n',L*(10^3)); Y=P/Zo;
G=real(Y);
printf('-Conductance G = %f micromhos/km\n',G*(10^6));
C=((imag(Y))/w)*(10^6);c=round(C*10000)/10000 printf('-Capacitance C = %f
microfarads/km\n',c);

```

OUTPUT:

Variable Zo; Constant f= 2000 Hz;

S. No	Input (Zo) ohms	Outputs			
		R(ohms/km)	L(mH/km)	G(microohms/km)	C(microfarads/km)
1					
2					
3					
4					
5					

RESULT:

Primary constants R,L,G and C are calculated by varying values of Characteristic Impedance (Zo) of a Transmission Line at a frequency f=2 Khz keeping the Propagation Constant (γ) constant.

Test Case 2:

Find the primary constants R,L,G and C for the varying values of Propagation constant of a Transmission Line at a frequency f=2 Khz. Vary the Propagation constant value from $200 \angle 30^\circ \Omega$ and take five readings at the interval of 50Ω . Keep the characteristic impedance $Z_o=100 \Omega$ constant

AIM: To find the primary constants R,L,G and C for the varying values of Propagation constant of a Transmission Line at a frequency f=2 Khz. Vary the Propagation constant value from $200 \angle 30^\circ \Omega$ and take five readings at the interval of 50Ω . Keep the characteristic impedance $Z_o=100 \Omega$ constant

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$R + j\omega L = Z_0 \gamma$$

$$G + j\omega C = \gamma / Z_0$$

PROGRAM:

```
clear; clc;
Zo=100.6;f=2000; //value of Zo as taken in solution P=0.054* exp(%i*(%pi/(180/87.9)));
w=2*%pi*f;
Z=Zo*P;
R=real(Z);
printf('-Resistance R = %f ohms/km\n',R); L=(imag(Z))/w;
printf('-Inductance L = %f mH/km\n',L*(10^3)); Y=P/Zo;
G=real(Y);
printf('-Conductance G = %f micromhos/km\n',G*(10^6));
C=((imag(Y))/w)*(10^6);c=round(C*10000)/10000 printf('-Capacitance C = %f
microfarads/km\n',c);
```

OUTPUT :

Variable γ ;
Constant $Z_0=100\Omega$;

S. No	Input (γ)	Outputs			
		R(ohms/km)	L(mH/km)	G(microohms/km)	C(microfarads/km)
1					
2					
3					
4					
5					

RESULT:

Primary constants R,L,G and C are calculated by varying values of Propagation Constant at a frequency $f=2$ Khz keeping the Characteristic Impedance constant.

EXNO: 3	Evaluation of current in short circuited Lossless transmission line at the receiving end
DATE:	

Test Case 1:

Find the current at the receiving end for the varying values of the attenuation constant α from keeping the characteristic impedance Z_0 and the phase constant β constant

AIM: To find current at the receiving end for the varying values of the attenuation constant α from 0.1 to 0.4 N/Km keeping the characteristic impedance Z_0 and the phase constant β constant.

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$E_{SC} = j I_R \cdot R_0 \cdot \sin \frac{2\pi s}{\lambda}$$

$$I_{SC} = I_R \cos \frac{2\pi s}{\lambda}$$

PROGRAM:

```
clear;
clc;
Zo=600;a=0.1;b=0.05;x=10;Is=20*(10^-3);
```

```

Vr=0;
printf("-Receiving end voltage Vr=0 because the receiving end has been short
circuit\n");
P=a+(%i*b);
Ir=Is/(cosh(10*P));
A=real(Ir);
B=imag(Ir);
printf("-Received current is Ir = %f / _ %f mA
",round(abs(Ir)*(10^3)*100)/100,fix(atan(B,A)*180*10/%pi)/10);

```

OUTPUT:

Variable = α N/Km Constant parameters = $Z_0 \Omega$, β rad/Km

Sl.No	Simulation Results		Theoretical Results	
	α N/Km)	I_R (mA)	α N/Km)	I_R (mA)
1				
2				
3				
4				

RESULT:

The current at the receiving end for the varying values of the attenuation constant α is found while keeping the characteristic impedance Z_0 and the phase constant β constant

|

Test Case 2:

Find the current at the receiving end for the varying values of the phase constant β attenuation constant α from keeping the characteristic impedance Z_0 and the attenuation constant α constant

AIM: To find current at the receiving end for the varying values of the attenuation constant α from keeping the characteristic impedance Z_0 and the attenuation constant α constant

|

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$E_{SC} = j I_R \cdot R_0 \cdot \sin \frac{2\pi s}{\lambda}$$

$$I_{SC} = I_R \cos \frac{2\pi s}{\lambda}$$

PROGRAM:

```
clear;
clc;
Zo=600;a=0.1;b=0.05;x=10;Is=20*(10^-3);
Vr=0;
printf("-Receiving end voltage Vr=0 because the receiving end has been short
circuitied\n");
P=a+(%i*b);
Ir=Is/(cosh(10*P));
A=real(Ir);
B=imag(Ir);
printf("-Received current is Ir = %f / _ %f mA
",round(abs(Ir)*(10^3)*100)/100,fix(atan(B,A)*180*10/%pi)/10);
```

OUTPUT:

Variable = β rad/Km Constant parameters = Z_o Ω , α N/Km

Sl.No	Simulation Results		Theoretical Results	
	β rad/Km	I_R (mA)	β rad/Km	I_R (mA)
1				
2				
3				
4				

RESULT:

The current at the receiving end for the varying values of the phase constant β is found while keeping the characteristic impedance Z_o and the attenuation constant α constant.

|

EXNO: 4	Analysis of SWR (Standing Wave Ratio) Transmission Lines by varying a) load impedance b) characteristic impedance
DATE:	

Test Case 1:

Analyze the SWR of a transmission line for a fixed characteristic impedance (Z_0) of 50 ohms, as the load impedance (Z_L) is varied across 650 ohms to 850 ohms. Verify how the SWR changes with each value of Z_L . When $Z_L = Z_0$, the SWR should equal 1 (indicating no reflection).

AIM: To analyze the SWR of a transmission line for a fixed characteristic impedance (Z_0) of 50 ohms, as the load impedance (Z_L) is varied across the following values: 25 ohms, 50 ohms, 75 ohms, and 100 ohms. To verify how the SWR changes with each value of Z_L and when $Z_L = Z_0$.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$K = \frac{Z_R - Z_0}{Z_R + Z_0}$$

$$S = \frac{1 + |K|}{1 - |K|}$$

PROGRAM:

```
clc;clear;close;
Zo=200;ZR=650-(%i*475);
K=(ZR-Zo)/(ZR+Zo);
```

```
ampK=sqrt((real(K)^2)+(imag(K)^2));S=(1+ampK)/(1-ampK);
printf("(c)Standing wave ratio = %f",round(S*1000)/1000);
```

OUTPUT:

Zo=50 ohmsVariable:ZR

ZROhms	Simulation Results	Theoretical Results
	SWR	SWR

ZR=50/_40oohmsVariable:Zo

Zo Ohms	Simulation Results	Theoretical Results
	SWR	SWR

RESULT:

The SWR of a transmission line for a fixed characteristic impedance (Zo) of 50 ohms, is analyzed for various values of load impedance Z_L. SWR is also examined for the condition Z_L=Zo.

Test Case 2:

Analyze the SWR for a fixed load impedance (Z_L) of 50 ohms while varying the characteristic impedance (Z_0) of the transmission line to 250 ohms to 400 ohms. Verify how the SWR changes with each value Z_0 including $Z_0=Z_L$.

AIM: To analyze the SWR for a fixed load impedance (Z_L) of 75 ohms while varying the characteristic impedance (Z_0) of the transmission line to 25 ohms, 50 ohms, 75 ohms, and 100 ohms. To Verify how the SWR changes with each value Z_0 including $Z_0=Z_L$

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program
- End the program

CALCULATION

$$K = \frac{Z_R - Z_0}{Z_R + Z_0}$$

$$S = \frac{1 + |K|}{1 - |K|}$$

PROGRAM:

```
clc;clear;close;  
Zo=200;ZR=650-(%i*475);  
K=(ZR-Zo)/(ZR+Zo);  
ampK=sqrt((real(K)^2)+(imag(K)^2));S=(1+ampK)/(1-ampK);  
printf("(c) Standing wave ratio = %f",round(S*1000)/1000);
```

OUTPUT:

ZR=50/_40° ohms Variable: Zo

Zo Ohms	Simulation Results	Theoretical Results
	SWR	SWR

RESULT:

SWR for a fixed load impedance (Z_L) of 50 ohms is analyzed while varying the characteristic impedance (Z_0) of the transmission line to 250 ohms to 400 ohms. Impact of the condition $Z_0=Z_L$ on SWR is also examined for various values of Z_0 .

EXNO: 5	Exploration of the relationship between position of Voltage minima nearest to the load by varying magnitude of reflection coefficient K
DATE:	

Test Case 1:

For a fixed characteristic impedance (Z_0) of 50 ohms and varying reflection coefficient magnitudes ($K=|\Gamma|=\{0.1,0.3,0.5,0.7,0.9\}$), determine the position of the voltage minima (d_{\min}) relative to the load. The position of voltage minima should shift based on K and the corresponding phase of Γ . Compute d_{\min} using $d_{\min}=\lambda/2\pi\tan^{-1}(\text{Im}(\Gamma)/\text{Re}(\Gamma))$, where $\Gamma=Ke^{j\theta}$.

AIM: To explore the relationship between position of Voltage minima nearest to the load by varying magnitude of reflection coefficient K for the range of values ($K=|\Gamma|=\{0.1,0.3,0.5,0.7,0.9\}$).

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$K = \frac{Z_R - Z_0}{Z_R + Z_0}$$

$$S = \frac{1 + |K|}{1 - |K|}$$

PROGRAM:

```
Zo=50;f=300*(10^6);ZR=50+(%i*50);
```

```

lo=300/(f*(10^-6)); //where f is in megahertz
,lo=wavelength of wave in airK=(ZR-Zo)/(ZR+Zo);
ampK=sqrt((real
(K)^2)+(imag(K
)^2));S=(1+amp
K)/(1-ampK);
printf("-VSWR = %f\n",round(S*100)/100);
phi=atan(imag(K)/real(K));
ymax=phi*lo/(2*2*%pi);
ymin=ymax+(lo/4);
printf("-Position of voltage minimum nearest load = %f
metres",round(ymin*10000)/10000);

```

OUTPUT:

$Z_0=50\text{ ohms}$ Variable: Z_R

Z_R Ohms	SWR	Position of V_{\min}

$Z_R=50/_{40}\text{ohms}$ Variable: Z_0

Z_0 Ohms	SWR	Position of V_{\min}

RESULT:

The relationship between position of Voltage minima nearest to the load with Z_0 and Z_R is evaluated by varying magnitude of reflection coefficient K for the range of values ($K=|\Gamma|=\{0.1,0.3,0.5,0.7,0.9\}$).

.Test Case 2:

For a fixed reflection coefficient magnitude ($K=0.5$) and varying load impedances ($Z_L=\{25\ \Omega, 50\ \Omega, 100\ \Omega, 150\ \Omega\}$), calculate the position of voltage minima nearest to the load. Validate that the position of V_{\min} changes with the phase angle of Γ , which is influenced by the load impedance.

AIM: To calculate the position of voltage minima nearest to the load For a fixed reflection coefficient magnitude ($K=0.5$) and varying load impedance values.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program

- Execute the program
- End the program

CALCULATION

$$K = \frac{Z_R - R_0}{Z_R + R_0}$$

$$S = \frac{1 + |K|}{1 - |K|}$$

PROGRAM:

```
clear;clc;
Zo=50;f=300*(10^6);ZR=50+(%i*50);
lo=300/(f*(10^-6)); //where f is in megahertz
,lo=wavelength of wave in airK=(ZR-Zo)/(ZR+Zo);
ampK=sqrt((real
(K)^2)+(imag(K
)^2));S=(1+amp
K)/(1-ampK);

printf("-VSWR = %f\n",round(S*100)/100);
phi=atan(imag(K)/real(K));
ymax=phi*lo/(2*2*%pi);
ymin=ymax+(lo/4);
printf("-Position of voltage minimum nearest load = %f
metres",round(ymin*10000)/10000);
```


OUTPUT:

$Z_o = 50$ ohms Variable: Z_R

Z_R Ohms	SWR	Position of V_{min}

$Z_R = 50$ ohms Variable: Z_o

Z_o Ohms	SWR	Position of V_{min}

RESULT:

The position of voltage minima nearest to the load for a fixed reflection coefficient magnitude ($K=0.5$) is estimated for varying load impedance values. Variation of the position of V_{min} with the phase angle of Γ influenced by the load impedance is also validated.

EXNO: 6	Designing a Quarter wave transformer by varying following parameters a) frequency b) input impedance c) characteristic impedance
DATE:	

Designing a Quarter wave transformer by varying following parameters

- d) frequency**
- e) input impedance**
- f) characteristic impedance**

Experiment Number:7

Test Case 1:

Design a quarter-wave transformer for an input impedance (Z_{in}) of 50 ohms and a load impedance (Z_L) of 100 ohms. Analyze the transformer's performance as the operating frequency is varied across {100 MHz, 200 MHz, 300 MHz, 500 MHz}.

AIM: To design a quarter-wave transformer for an input impedance (Z_{in}) of 50 ohms and a load impedance (Z_L) of 100 ohms and to analyze the transformer's performance as the operating frequency is varied across {100 MHz, 200 MHz, 300 MHz, 500 MHz }.

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION:

$$R_0 = \sqrt{Z_R \cdot Z_{in}}$$

PROGRAM:

```
clear;clc;
Zr=100;s=9;d=0.1;
Zs=50;
Ro=sqrt(Zs*Zr);f=500*(10^6);r=d/2;
Zof=276*log10(s/r);
Zoq=sqrt(Zr*Zof);
L=300/(f*(10^-6));
printf("length of lambda/4 transformer = %f meters\n",L);
printf("characteristic impedance of quarter wave line = %f ",fix(Ro*10000)/10000);
```

OUTPUT:

Z_R=100 ohms Z_{in} =50 ohms

Z_S ohms	Z_R ohms	R_o ohms

Z_R=100 ohms Z_{in} =50 ohms

Frequency (MHz)	Length of λ/4 transformer (meters)

RESULT: A quarter-wave transformer for an input impedance (Z_{in}) of 50 ohms and a load impedance (Z_L) of 100 ohms is designed and the transformer's performance is analyzed for the varying operating frequency is varied across {100 MHz, 200 MHz, 300 MHz, 500 MHz }.

Test Case 2:

For a fixed operating frequency of 2 GHz and a load impedance (Z_L) of 100 ohms, design a quarter-wave transformer and evaluate its performance as the input impedance (Z_{in}) varies through {25 ohms, 50 ohms, 75 ohms, 100 ohms}. Validate that the transformer's characteristic impedance ($Z_{transformer} = R_0 = \sqrt{Z_{in} \cdot Z_L}$) changes with Z_{in} .

AIM: To design a quarter-wave transformer a fixed operating frequency of 2 GHz and a load impedance (Z_L) of 100 ohms and evaluate its performance as the input impedance (Z_{in}) varied .To validate that the transformer's characteristic impedance ($Z_{transformer} = R_0 = \sqrt{Z_{in} \cdot Z_L}$) changes with Z_{in} .

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$R_0 = \sqrt{Z_R \cdot Z_{in}}$$

PROGRAM:

```
clear;clc;  
Zr=100;s=9;d=0.1;  
Zs=50;
```

```

Ro=sqrt(Zs*Zr);f=100*(10^6);r=d/2;
Zof=276*log10(s/r);
Zoq=sqrt(Zr*Zof);
L=300/(f*(10^-6));
printf("length of lambda/4 transformer = %f lambda\n",L);
printf("characteristic impedance of quarter wave line = %f ",fix(Ro*10000)/10000);

```

OUTPUT:

ZR=100 ohms Variable :Zin

Z_{in}	R_o

RESULT: A quarter-wave transformer is designed at a fixed operating frequency of 2 GHz and load impedance (Z_L) of 100 ohms and its performance is evaluated for various input impedance values. The variation of transformer's characteristic impedance with Z_{in} is also validated..

EXNO: 7	Strategize impedance matching with characteristic impedance and load impedance through the measurement of a) Location of the stub b) Length of the stub
DATE:	

Test Case 1:

Optimize impedance matching using single stub matching by finding the location and length of the stub for the values of load impedance of $100 \angle 30^\circ$ to $350 \angle 30^\circ$ keeping the characteristic impedance $Z_0 = 60 \Omega$ constant.

AIM: To optimize impedance matching using single stub matching by finding the location and length of the stub for the values of load impedance of $100 \angle 30^\circ$ to $350 \angle 30^\circ$ keeping the characteristic impedance $Z_0 = 60 \Omega$ constant.

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$s_1 = \frac{\phi + \pi - \cos^{-1}(|K|)}{2\beta}$$

Length of the stub,

$$L = \frac{\lambda}{2\pi} \tan^{-1} \left[\frac{\sqrt{1-|K|^2}}{2|K|} \right]$$

PROGRAM:

```
clear; clear; clc;
ZR=100;Zo=600;f=100*(10^6);
lo=300/(f*(10^-6)); //lo=wavelength Ls=(lo/(2*pi))*(atan(sqrt(ZR/Zo)));
printf("-Point of attachment = %f cms\n",round(Ls*(10^2)*10)/10)
Lt=(lo/(2*pi))*(pi+atan((sqrt(ZR*Zo))/(ZR-Zo)));
printf("-Length of the short circuited stub = %f cms",round(Lt*(10^2)));
```

OUTPUT:

Variables Z_R ;
Constants $Z_o = 60\Omega$; $f=100*(10^6)$;

Input	Output	
ZR Ohms. angle 30°	Point of attachment	Length of short-circuited stub (cm)

RESULT:

Impedance matching using single stub matching is optimized by calculating the location and length of the stub or varying values of load impedance keeping the characteristic impedance $Z_o = 60\Omega$ constant .

Test Case 2:

Optimize impedance matching using single stub matching by finding the location and length of the stub for the values of characteristic impedance ranging from 600Ω to 1800Ω . Keeping the load impedance $Z_R = 100 \angle 30^\circ$ constant .

AIM: To optimize impedance matching using single stub matching by finding the location and length of the stub for the values of characteristic impedance ranging from 600Ω to 1800Ω . Keeping the load impedance $Z_R = 100 \angle 30^\circ$ constant .

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$s_1 = \frac{\phi + \pi - \cos^{-1}(|K|)}{2\beta}$$

Length of the stub,

$$L = \frac{\lambda}{2\pi} \tan^{-1} \left[\frac{\sqrt{1-|K|^2}}{2|K|} \right]$$

PROGRAM:

```
clear; clear; clc;
```

```
ZR=100;Zo=600;f=100*(10^6);
```

```
lo=300/(f*(10^-6)); //lo=wavelength Ls=(lo/(2*%pi))*(atan(sqrt(ZR/Zo)));
```

```
printf("-Point of attachment = %f cms\n",round(Ls*(10^2)*10)/10)
```

```
Lt=(lo/(2*%pi))*(%pi+(atan((sqrt(ZR*Zo))/(ZR-Zo))));
```

```
printf("-Length of the short circuited stub = %f cms",round(Lt*(10^2)));
```


OUTPUT:

Variables Z_0 ;

Constants $Z_R = 100 \angle 30^\circ \Omega$; $f = 100 \times (10^6)$;

Input	Output	
Z_0 Ohms.	Point of attachment	Length of short-circuited stub (cm)

RESULT:

Impedance matching using single stub matching is optimized by calculating the location and length of the stub for varying values of characteristic impedance keeping the load impedance constant .

EXNO: 8	Analysis of Electromagnetic Waves across the two parallel plates estimating the following a) Critical Wavelength b) Guide Wavelength
DATE:	

Test Case 1:

Analyze the variation of critical wavelength and guide wavelength of Electromagnetic waves between parallel plates with separation a ranging from 7.62 cm to 13 cm for TE1 mode.

AIM: To analyze the variation of critical wavelength and guide wavelength of Electromagnetic waves between parallel plates with separation a ranging from 7.62 cm to 13 cm for TE1 mode..

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

Critical wavelength $\lambda_c = V/f_c$

$$\text{Guide wavelength } \lambda_g = \frac{\lambda}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

PROGRAM:

```
clear;clc;
c=3*(10^8); f=3000*(10^8);
lo=c/f; l=lo*(10^4); m=1;n=0;a=7.62;
lc=2*a;
```

```
printf("-Critical wavelength = %f cm\n",lc); lg=sqrt((l*lc*lc)/((lc*lc)-(l*1)));
printf("-Guide wavelength = %f cm",round(lg*10)/10);
```

OUTPUT:

Spacing a(cm)	Critical wavelength (cm)	Guide wavelength (cm)

RESULT:

The variation of critical wavelength and guide wavelength of Electromagnetic waves propagated between parallel plates with separation a ranging from 7.62 cm to 13 cm is analyzed with SCILAB.

Test Case 2:

Analyze the variation of cutoff frequencies of Electromagnetic waves between parallel plates with for TE1, TE2, TE 3 and TE4 modes.

AIM: To analyze the variation of cutoff frequencies of Electromagnetic waves between parallel plates with for TE1, TE2, TE 3 and TE4 modes.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values

- Type the program
- Execute the program
- End the program

CALCULATION

Critical wavelength $\lambda_c = V/f_c$

$$\text{Guide wavelength } \lambda_g = \frac{\lambda}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

PROGRAM:

```
clc;
clear;
close;
//TE10 Mode
a=7.62*10^-2;
f=4*10^9;
V=3*10^8;
m=input("enter the value of m= ");
fc=(V/(2*3.14))*sqrt(m*3.14/a)^2;
disp("Cut off frequency in GHz=",fc*10^-9);
//let critical wavelength = lc
lc=(V/fc);
disp("critical wavelength in cm =",lc*10^2);
```

OUTPUT:

Modes	Cutoff frequency (GHz)	Critical wavelength (cm)

RESULT:

The variation of cutoff frequencies of Electromagnetic waves between parallel plates with for TE1, TE2, TE 3 and TE4 modes is examined using SCILAB.

EXNO: 9	Calculation of Group velocity, Phase velocity and phase constant of EM waves in rectangular waveguides
DATE:	

Test Case 1 :

You are experimenting with a rectangular waveguide to analyze the relationship between its dimensions and wave propagation. The waveguide dimensions are a=4.0 cm, b=2.0 cm and the operating frequency is f=8 GHz.

1. Calculate the cutoff frequencies for TE₁₀ modes.
2. Predict the phase and group velocities for the TE₁₀ mode at the given frequency.
3. If the width of the waveguide is reduced to a=3.0 cm, how does it affect the cutoff frequency and propagation characteristics?

AIM: To find the group velocity, phase velocity and phase constant of Electromagnetic waves in Rectangular Waveguides whose dimensions are a=4.0 cm, b=2.0 cm and the operating frequency is f=8 GHz.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$\beta = \sqrt{\omega^2 \mu \epsilon - \left(\frac{\pi}{a}\right)^2} = \omega \sqrt{\mu \epsilon} \sqrt{1 - \left(\frac{f_c}{f}\right)^2}.$$

PROGRAM:

```

clc;
clear;
close;
//TE10 Mode
a=8.636*10^-2;
b=4.318*10^-2;
f=4*10^9;
V=3*10^8;
m=input("enter the value of m= "); n=input("enter the value of n= ");
fc=(V/(2*3.14))*sqrt((m*3.14/a)^2+(n*3.14/b)^2);
disp("Cut off frequency=",fc*10^-9);
//let phase velocity = A
A=V/sqrt(1-(fc/f)^2);
disp("Phase velocity in Mm/sec=",A*10^-6);
//let group velocity = B
B=V*A/A;
disp("Group velocity in Mm/sec =", B*10^-6);

```

OUTPUT:

Case 1:

Original Dimensions (a=4.0 cm,b=2.0 cm)

Inputs:

- m=1, n=0.
- f=8 GHz.

Outputs:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency (fc)		
Phase Velocity (vp)		
Group Velocity (vg)		

Test Case 2:

Reduced Width ($a=3.0$ cm, $b=2.0$ cm)

Inputs:

- $m=1$, $n=0$.
- $f=8$ GHz.

Outputs:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency (f_c)		
Phase Velocity (v_p)		
Group Velocity (v_g)		

Table: Variation of Phase and Group Velocities with a

Waveguide Width (a)	Simulation Results			Theoretical Results		
	Cutoff Frequency (f_c)	Phase Velocity (v_p)	Group Velocity (v_g)	Cutoff Frequency (f_c)	Phase Velocity (v_p)	Group Velocity (v_g)

RESULT:

The group velocity, phase velocity and phase constant of waves in a rectangular waveguide are estimated using SCILAB.

Test Case 2 :

In a radar system operating at $f=15$ GHz the waveguide dimensions are $a = 2.5$ and $b = 1.25$ cm

1. Compute the cutoff frequencies for TE_{10} modes.
2. Determine the phase and group velocities for the TE_{10} mode.
3. If dispersion is critical to radar signal accuracy, what strategies would you recommend maintaining signal fidelity?

AIM: To find the group velocity, phase velocity and phase constant of Electromagnetic waves in Rectangular Waveguides whose dimensions are $a = 2.5 \text{ cm}$, $b = 1.25 \text{ cm}$ and the operating frequency is $f = 15 \text{ GHz}$.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

PROGRAM:

```
clc;
clear;
close;
//TE10 Mode
a=8.636*10^-2;
b=4.318*10^-2;
f=4*10^9;
V=3*10^8;
m=input("enter the value of m= "); n=input("enter the value of n= ");
fc=(V/(2*3.14))*sqrt((m*3.14/a)^2+(n*3.14/b)^2);
disp("Cut off frequency=",fc*10^-9);
//let phase velocity = A
A=V/sqrt(1-(fc/f)^2);
disp("Phase velocity in Mm/sec=",A*10^-6);
```



```
//let group velocity = B
B=V*V/A;
disp("Group velocity in Mm/sec =", B*10^-6);
```

Program Output for TE₁₀ Mode:

Using the program with a=0.025 m b=0.0125 m and f=15 GHz:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency (f_c)		
Phase Velocity (v_p)		
Group Velocity (v_g)		

RESULT:

The group velocity, phase velocity and phase constant of waves in a rectangular waveguide are estimated using SCILAB.

Test Case 3 :

A waveguide with dimensions a=5.0 cm and b=2.5 cm is used to carry a signal at f=10 GHz

1. Determine the number of TE modes that can propagate at this frequency.
2. For the TE₁₀ mode, calculate the phase velocity and group velocity.
3. Discuss how the presence of multiple propagating modes affects the transmission quality and suggest practical solutions to limit multimode effects.

AIM:

To find the group velocity, phase velocity and phase constant of Electromagnetic waves in Rectangular Waveguides whose dimensions are a= 5.0 cm, b=2.5 cm and the operating frequency is f=10 GHz.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION**PROGRAM:**

```
clc;
clear;
close;
//TE10 Mode
a=8.636*10^-2;
b=4.318*10^-2;
f=4*10^9;
V=3*10^8;
m=input("enter the value of m= ");
n=input("enter the value of n= ");
fc=(V/(2*3.14))*sqrt((m*3.14/a)^2+(n*3.14/b)^2);
disp("Cut off frequency=",fc*10^-9);
//let phase velocity = A
A=V/sqrt(1-(fc/f)^2);
disp("Phase velocity in Mm/sec=",A*10^-6);
//let group velocity = B
B=V*V/A;
disp("Group velocity in Mm/sec =", B*10^-6);
```

OUTPUT:**Waveguide Parameters:**

- Width (a) = 5.0 cm=0.05m

- Height (b) = 2.5 cm=0.025 m
- Operating Frequency (f) = 10 GHz
- Speed of Light (V) = 3×10^8 m/s

1. Number of TE Modes that Can Propagate:

The cutoff frequency for a TE_{mn} mode is:

$$f_c(m,n) = V/2 \left(\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2} \right)$$

Modes propagate if $f > f_c(m,n)$. The number of modes can be determined by calculating f_c for different combinations of m and n.

	Simulation Results		Theoretical Results	
Mode (m,n)	Cutoff Frequency (fc)	Propagation (Yes/No)	Cutoff Frequency (fc)	Propagation (Yes/No)
TE ₁₀				
TE ₀₁				
TE ₁₁				
TE ₂₀				
TE ₂₁				
TE ₀₂				

- Result:

Five TE modes can propagate TE₁₀, TE₀₁, TE₁₁, TE₂₀, TE₂₁, TE₀₂

2. Output for TE₁₀ Mode:

Using the program with a=5 m b=2.5 m and f=10 GHz:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency (f_c)		
Phase Velocity (v_p)		
Group Velocity (v_g)		

RESULT:

The group velocity, phase velocity and phase constant of waves in a rectangular waveguide are estimated using SCILAB.

Test Case 4 :

A research lab is experimenting with high-order TE modes ($m,n>1$) in a waveguide with dimensions $a=3.0$ cm $b=1.5$ cm, and an operating frequency of $f=12$ GHz.

- 1. Calculate the cutoff frequencies for TE_{10} mode.**
- 2. Compute the phase and group velocities of this mode.**
- 3. Discuss how high-order modes can be utilized for advanced applications such as mode multiplexing in communications.**

AIM:

To find the group velocity, phase velocity and phase constant of Electromagnetic waves in Rectangular Waveguides whose dimensions are $a=3.0$ cm, $b=1.5$ cm and the operating frequency is $f=12$ GHz.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

PROGRAM:

```
clc;  
clear;  
close;  
//TE10 Mode  
a=8.636*10^-2;  
b=4.318*10^-2;  
f=4*10^9;
```

```

V=3*10^8;
m=input("enter the value of m= ");
n=input("enter the value of n= ");
fc=(V/(2*3.14))*sqrt((m*3.14/a)^2+(n*3.14/b)^2);
disp("Cut off frequency=",fc*10^-9);
//let phase velocity = A
A=V/sqrt(1-(fc/f)^2);
disp("Phase velocity in Mm/sec=",A*10^-6);
//let group velocity = B
B=V*A/A;
disp("Group velocity in Mm/sec =", B*10^-6);

```

OUTPUT:

Waveguide Parameters:

- Width (a) = 3.0 cm=0.03 m
- Height (b) = 1.5 cm=0.015 m
- Operating Frequency (f) = 12 GHz= 12×10^9 Hz
- Speed of Light (V) = 3×10^8 m/s

1. No. of Modes:

To analyze all modes, calculate f_c for other modes with $m,n > 1$.

OUTPUT:

Mode (m,n)	Simulation Results		Theoretical Results	
	Cutoff Frequency (fc)	Propagation (Yes/No)	Cutoff Frequency (fc)	Propagation (Yes/No)
TE ₁₀				
TE ₂₀				
TE ₀₁				
TE ₁₁				
TE ₂₁				
TE ₃₀	15.0 GHz	No	15.0 GHz	No

2. Program Output for TE₁₀ Mode:

Using the program with a=0.03 m b=0.015 m and f=12 GHz:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency (f_c)		
Phase Velocity (v_p)		
Group Velocity (v_g)		

RESULT:

The group velocity, phase velocity and phase constant of waves in a rectangular waveguide are estimated using SCILAB.

EXNO: 10	Examining the propagation characteristics of circular waveguide in terms of a) Cutoff wavelength d) Guide wavelength e) Characteristic impedance
DATE:	

Test Case 1:

Design a circular waveguide for the TE_{11} mode to transmit a signal at 10 GHz. The material is air, and the waveguide length is 2 meters.

- 1. Determine the minimum radius of the waveguide.**
- 2. Calculate the cutoff wavelength, guide wavelength, and characteristic impedance.**

AIM:

To determine the propagation characteristics of circular waveguide in terms of Cutoff wavelength. Guide wavelength and characteristic impedance.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

TE Mode

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - \left(\frac{p'_{nm}}{a}\right)^2},$$

with a cutoff frequency of

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p'_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TE} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta k}{\beta}.$$

TM Mode

The propagation constant of the TM_{nm} mode is

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - (p_{nm}/a)^2},$$

and the cutoff frequency is

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TM} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta\beta}{k}.$$

PROGRAM:

// Constants

c = 3e8; // Speed of light in m/s

f = 10e9; // Frequency in Hz

chi_11 = 1.841; // First root for TE11 mode

Z0 = 377; // Impedance of free space in ohms

// Calculations

lambda0 = c / f; // Free-space wavelength

r = (chi_11 * c) / (2 * %pi * f); // Minimum radius

lambda_c = 2 * %pi * r / chi_11; // Cutoff wavelength

lambda_g = lambda0 / sqrt(1 - (lambda0 / lambda_c)^2); // Guide wavelength

Z = Z0 / sqrt(1 - (lambda_c / lambda0)^2); // Characteristic impedance

// Output

disp("Minimum Radius (m): " + string(r));

disp("Cutoff Wavelength (m): " + string(lambda_c));

disp("Guide Wavelength (m): " + string(lambda_g));

disp("Characteristic Impedance (Ohms): " + string(Z));

OUTPUT:**Given Data:**

- Frequency $f=10\text{ GHz}=10\times 10^9\text{ Hz}$
- Speed of light $c=3\times 10^8\text{ m/s}$
- Material: Air (vacuum)
- Waveguide length = 2 meters
- For TE_{11} mode, the first root $\chi_{11}\approx 1.841$

Output Table:

Parameter	Simulation Results	Theoretical Results
	Value	Value
Minimum Radius (r)		
Cutoff Wavelength (λ_c)		
Guide Wavelength (λ_g)		
Characteristic Impedance (Z)		

RESULT:

The propagation characteristics of circular waveguide in terms of Cutoff wavelength Guide wavelength and characteristic impedance

Test Case 2:

You are designing a circular waveguide to operate in the TE_{11} mode at 12 GHz, and the waveguide is filled with a dielectric material with a relative permittivity of 2.5. The waveguide length is 3 meters.

1. Determine the minimum radius of the waveguide.
2. Calculate the cutoff wavelength and guide wavelength for the TE_{11} mode.
3. What would be the impact if the operating frequency is increased to 18 GHz? Would higher-order modes propagate?

AIM:

To determine the propagation characteristics of circular waveguide in terms of Cutoff wavelength. Guide wavelength and characteristic impedance

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

TE Mode

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - \left(\frac{p'_{nm}}{a}\right)^2},$$

with a cutoff frequency of

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p'_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TE} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta k}{\beta}.$$

TM Mode

The propagation constant of the TM_{nm} mode is

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - (p_{nm}/a)^2},$$

and the cutoff frequency is

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TM} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta\beta}{k}.$$

PROGRAM:

// Constants

c = 3e8; // Speed of light in m/s

f = 10e9; // Frequency in Hz

chi_11 = 1.841; // First root for TE11 mode

Z0 = 377; // Impedance of free space in ohms

// Calculations

lambda0 = c / f; // Free-space wavelength

r = (chi_11 * c) / (2 * %pi * f); // Minimum radius

lambda_c = 2 * %pi * r / chi_11; // Cutoff wavelength

lambda_g = lambda0 / sqrt(1 - (lambda0 / lambda_c)^2); // Guide wavelength

Z = Z0 / sqrt(1 - (lambda_c / lambda0)^2); // Characteristic impedance

// Output

disp("Minimum Radius (m): " + string(r));

disp("Cutoff Wavelength (m): " + string(lambda_c));

disp("Guide Wavelength (m): " + string(lambda_g));

disp("Characteristic Impedance (Ohms): " + string(Z));

OUTPUT:

Given Data:

- Operating Frequency $f=12$ GHz
- Relative permittivity $\epsilon_r=2.5$
- Speed of light in vacuum $c=3 \times 10^8$ m/s
- Waveguide length $L=3$ m
- For TE_{11} mode, the first root $\chi_{11} \approx 1.841$

1. Minimum Radius (r):

The cutoff wavelength (λ_c) for TE_{11} mode is given by:

$$\lambda_c = (2\pi r / \chi_{11})$$

r can be found using the above formula: $r = 22.7$ mm

2. Output

Parameter	Simulation Results	Theoretical Results
	Value	Value
Minimum Radius (r)		
Cutoff Wavelength (λ_c)		
Guide Wavelength (λ_g)		

RESULT

The propagation characteristics of circular waveguide in terms of Cutoff wavelength Guide wavelength and characteristic impedance

Test Case 3:

A circular waveguide with a radius of 5 cm is designed to transmit a signal at 8 GHz in the TE_{11} mode. Initially, the waveguide is filled with air, but it is later filled with a dielectric material of relative permittivity 4.

1. Calculate the cutoff wavelength and guide wavelength before and after the dielectric is added.
2. Determine the characteristic impedance in both cases.
3. Discuss how the material change affects the waveguide's ability to transmit signals and how to mitigate any undesired effects.

AIM:

To determine the propagation characteristics of circular waveguide in terms of Cutoff wavelength. Guide wavelength and characteristic impedance

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software

- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

TE Mode

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - \left(\frac{p'_{nm}}{a}\right)^2},$$

with a cutoff frequency of

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p'_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TE} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta k}{\beta}.$$

TM Mode

The propagation constant of the TM_{nm} mode is

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - (p_{nm}/a)^2},$$

and the cutoff frequency is

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TM} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta\beta}{k}.$$

PROGRAM:

```
// Constants
c = 3e8; // Speed of light in m/s
f = 10e9; // Frequency in Hz
chi_11 = 1.841; // First root for TE11 mode
Z0 = 377; // Impedance of free space in ohms

// Calculations
lambda0 = c / f; // Free-space wavelength
r = (chi_11 * c) / (2 * %pi * f); // Minimum radius
lambda_c = 2 * %pi * r / chi_11; // Cutoff wavelength
```

```
lambda_g = lambda0 / sqrt(1 - (lambda0 / lambda_c)^2); // Guide wavelength
Z = Z0 / sqrt(1 - (lambda_c / lambda0)^2); // Characteristic impedance
```

```
// Output
disp("Minimum Radius (m): " + string(r));
disp("Cutoff Wavelength (m): " + string(lambda_c));
disp("Guide Wavelength (m): " + string(lambda_g));
disp("Characteristic Impedance (Ohms): " + string(Z));
```

OUTPUT:

Given Data:

- Operating Frequency $f=8$ GHz
- Waveguide Radius $r=5$ cm= 0.05 m
- Relative Permittivity of Air $\epsilon_r=1$
- Relative Permittivity of Dielectric $\epsilon_r=4$
- For TE_{11} mode, the first root $\chi_{11} \approx 1.841$
- Speed of light in vacuum $c=3 \times 10^8$ m/s
-

Output

Parameter	Simulation Results		Theoretical Results	
	Before Dielectric (Air)	After Dielectric ($\epsilon_r = 4$)	Before Dielectric (Air)	After Dielectric ($\epsilon_r = 4$)
Cutoff Wavelength (λ_c)				
Guide Wavelength (λ_g)				
Characteristic Impedance (Z)				

RESULT:

The propagation characteristics of circular waveguide in terms of Cutoff wavelength Guide wavelength and characteristic impedance

Test Case 4:

A satellite communication system requires a circular waveguide to operate at 14 GHz in the TE_{11} mode. The waveguide's internal radius is 2.5 cm, and it is filled with air.

- Calculate the cutoff frequency for the TE_{11} mode.
- If the operating frequency is reduced to 12 GHz, will the TE_{11} mode still propagate?
- Design the waveguide parameters to ensure that only the TE_{11} mode propagates when operating between 10 GHz and 16 GHz.

AIM:

To determine the propagation characteristics of circular waveguide in terms of Cutoff wavelength, Guide wavelength and characteristic impedance

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

TE Mode

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - \left(\frac{p'_{nm}}{a}\right)^2},$$

with a cutoff frequency of

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p'_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TE} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta k}{\beta}.$$

TM Mode

The propagation constant of the TM_{nm} mode is

$$\beta_{nm} = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - (p_{nm}/a)^2},$$

and the cutoff frequency is

$$f_{c_{nm}} = \frac{k_c}{2\pi\sqrt{\mu\epsilon}} = \frac{p_{nm}}{2\pi a\sqrt{\mu\epsilon}}.$$

The wave impedance is

$$Z_{TM} = \frac{E_\rho}{H_\phi} = \frac{-E_\phi}{H_\rho} = \frac{\eta\beta}{k}.$$

PROGRAM:

```
// Constants
c = 3e8; // Speed of light in m/s
f = 10e9; // Frequency in Hz
chi_11 = 1.841; // First root for TE11 mode
Z0 = 377; // Impedance of free space in ohms

// Calculations
lambda0 = c / f; // Free-space wavelength
r = (chi_11 * c) / (2 * %pi * f); // Minimum radius
lambda_c = 2 * %pi * r / chi_11; // Cutoff wavelength
lambda_g = lambda0 / sqrt(1 - (lambda0 / lambda_c)^2); // Guide wavelength
Z = Z0 / sqrt(1 - (lambda_c / lambda0)^2); // Characteristic impedance

// Output
disp("Minimum Radius (m): " + string(r));
disp("Cutoff Wavelength (m): " + string(lambda_c));
disp("Guide Wavelength (m): " + string(lambda_g));
disp("Characteristic Impedance (Ohms): " + string(Z));
```

OUTPUT:**Given Data:**

- Operating Frequency $f=14$ GHz
- Waveguide Radius $r=2.5$ cm= 0.025 m
- Relative Permittivity of Air $\epsilon_r=1$
- Relative Permittivity of Dielectric $\epsilon_r=4$
- For TE_{11} mode, the first root $\chi_{11} \approx 1.841$
- Speed of light in vacuum $c=3 \times 10^8$ m/s

Output :

Parameter	Simulation Results	Theoretical Results
	Value	Value
Cutoff Frequency at 14 GHz		
TE_{11} Mode Propagation at 12 GHz		
Waveguide Radius for 10 GHz (minimum)		
Waveguide Radius for 16 GHz (maximum)		

RESULT:

The propagation characteristics of circular waveguide in terms of Cutoff wavelength Guide wavelength and characteristic impedance

EXNO: 11	Inference of Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mode with the following inputs a) Dimension a in x axis b) Dimension b in y axis c) Dimension p in z axis
DATE:	

Test Case 1:

You are tasked with designing a rectangular cavity resonator that operates in the TE₁₀₁ mode. The dimensions of the resonator are a=5 cm, b=4 cm, and c=10 cm. The cavity is made of copper (C=5.8×10⁷ S/m).

1. If the dimension a is increased to 7 cm while keeping b and c constant, how does the Q-factor change? Explain the relationship between a and the Q-factor.

Hint: Use the given formula for Q and compare the resulting values.

AIM:

To determine the Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mode by varying three dimensions

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$Q_{101} = \frac{\pi f_{101} \mu_0 a b d (a^2 + d^2)}{R_s [2b(a^3 + d^3) + ad(a^2 + d^2)]} \quad (\text{TE}_{101} \text{ mode}),$$

PROGRAM:

```
clear;
clc;
a=5*10^-2,b=4*10^-2,c=10*10^-2,C=5.8*10^7,Uo=4*%pi*10^-7;
f101=3.335*10^9;
```



```

d=sqrt(1/(%pi*f101*Uo*C));
Q=(a*a+c*c)*a*b*c/(d*(2*b*(a^3 + c^3)+a*c*(a*a+c*c)));
disp(Q,'Quality factor of TE101 = ');

```

OUTPUT:

a (cm)	b (cm)	c (cm)	Simulation Results	Theoretical Results
			Q Factor	Q Factor

RESULT: The Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mod by varying three dimensions is determined using Scilab

Test Case 2 :

You are asked to optimize the rectangular cavity resonator to achieve the highest possible Q-factor using the dimensions provided.

1. Based on the variation in a, b, and c, which combination of dimensions yields the maximum Q-factor?
2. Explain why this combination results in a higher Q-factor. Consider the relationship between a, b, and c and how they affect the Q-factor in the given formula.

AIM:

To determine the Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mode by varying three dimensions

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$Q_{101} = \frac{\pi f_{101} \mu_0 a b d (a^2 + d^2)}{R_s [2b(a^3 + d^3) + ad(a^2 + d^2)]} \quad (\text{TE}_{101} \text{ mode}),$$

PROGRAM:

```
clear;
clc;
a=5*10^-2, b=4*10^-2, c=10*10^-2, C=5.8*10^7, Uo=4*%pi*10^-7;
f101=3.335*10^9;
d=sqrt(1/(%pi*f101*Uo*C));
Q=(a*a+c*c)*a*b*c/(d*(2*b*(a^3 + c^3)+a*c*(a*a+c*c)));
disp(Q,'Quality factor of TE101 = ');
```

OUTPUT:

The combination of dimensions that yields the highest Q-factor is as follows:

a (cm)	b (cm)	c (cm)	Simulation Results	Theoretical Results
			Q Factor	Q Factor

RESULT:

The Q Factor of Rectangular Cavity Resonator for TE101 mode by varying three dimensions is determined using Scilab.

Test Case 3 :

Your task is to assess how changes in a single dimension affect the resonator's performance.

1. Fix $b=4$ cm and $c=10$ cm and vary a between 4 cm and 6 cm. How does the Q-factor change? What does this tell you about the sensitivity of the Q-factor to the dimension a ?
2. In practical scenarios, which dimension is most critical to optimize for achieving a high Q-factor, and why?

AIM:

To determine the Q Factor of Rectangular Cavity Resonator for TE_{101} mode by varying three dimensions

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

$$Q_{101} = \frac{\pi f_{101} \mu_0 a b d (a^2 + d^2)}{R_s [2b(a^3 + d^3) + ad(a^2 + d^2)]} \quad (TE_{101} \text{ mode}),$$

PROGRAM:

```
clear;
clc;
a=5*10^-2, b=4*10^-2, c=10*10^-2, C=5.8*10^7, Uo=4*pi*10^-7;
f101=3.335*10^9;
d=sqrt(1/(pi*f101*Uo*C));
Q=(a*a+c*c)*a*b*c/(d*(2*b*(a^3 + c^3)+a*c*(a*a+c*c)));
disp(Q,'Quality factor of TE101 = ');
```

OUTPUT:

Below is the result of how changes in the dimension of 'a' affect the Q-factor, we can calculate the Q-factor for fixed values of $b=4$ cm and $c=10$ cm, while varying 'a' between 4 cm and 6 cm in equal steps.

1. Q-Factor Calculation for Varying a:

a (cm)	b (cm)	c (cm)	Simulation Results	Theoretical Results
			Q-Factor	Q-Factor

RESULT:

The Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mode by varying three dimensions is determined using Scilab.

Test Case 4 :

You are tasked with investigating how changes in b(the y-axis dimension) affect the Q-factor of the rectangular cavity resonator. Fix $a=5$ cm and $c=10$ cm and vary b between 3 cm and 5 cm. Analyze the Q-factor for these changes.

AIM:

To determine the Q Factor of Rectangular Cavity Resonator for TE₁₀₁ mode by varying three dimensions

SOFTWARE REQUIRED:

SCILAB

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values

- Type the program
- Execute the program
- End the program

CALCULATION

$$Q_{101} = \frac{\pi f_{101} \mu_0 a b d (a^2 + d^2)}{R_s [2b(a^3 + d^3) + a d (a^2 + d^2)]} \quad (\text{TE}_{101} \text{ mode}),$$

PROGRAM:

```
clear;
clc;
a=5*10^-2, b=4*10^-2, c=10*10^-2, C=5.8*10^7, Uo=4*%pi*10^-7;
f101=3.335*10^9;
d=sqrt(1/(%pi*f101*Uo*C));
Q=(a*a+c*c)*a*b*c/(d*(2*b*(a^3 + c^3)+a*c*(a*a+c*c)));
disp(Q,'Quality factor of TE101 = ');
```

OUTPUT:

Calculation of Q-Factor for Varying b

a (cm)	b (cm)	c (cm)	Simulation Results	Theoretical Results
			Q-Factor	Q-Factor

RESULT:

The Q Factor of Rectangular Cavity Resonator for TE101 mode by varying three dimensions is determined using Scilab.

EXNO: 12	Calculation of Resonant Frequency of Rectangular Cavity Resonator for TE and TM mode
DATE:	

Test Case 1: Construct a Rectangular Cavity Resonator with dimensions a= 5 cm, b=3 cm and height c= 9 cm. Find the resonant frequencies by varying the dimension a from 5 cm to 9 cm for 5 intervals keeping the other dimensions b and c constant for the modes TM₁₁₀ and TE₁₀₁.

AIM: To Construct a Rectangular Cavity Resonator with dimensions a= 5 cm, b=3 cm and height c= 9 cm. Find the resonant frequencies by varying the dimension a from 5 cm to 9 cm for 5 intervals keeping the other dimensions b and c constant for the modes TM₁₁₀ and TE₁₀₁

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program
- **CALCULATION**

The resonant frequency of the TE_{mnl} or TM_{mnl} mode is given by

$$f_{mnl} = \frac{ck_{mnl}}{2\pi\sqrt{\mu_r\epsilon_r}} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

•

PROGRAM:

```
clc; clear;
format('e',11); a=0.05; b=0.03; c=0.09;
v=3*10^8;
//for m=1; n=1; p=0;
m=1;n=1; p=0;
```

```

fr110=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr110,"fr110(in Hz)");
//for m=1,n=0. m=1; n=0;
m=1;n=0; p=1;
fr101=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr101,"fr101(in Hz)");

```

OUTPUT:

Variable: dimension a cm

a (cm)	Simulation Results		Theoretical Results	
	fr (TM110) GHz	fr (TE101) GHz	fr (TM110) GHz	fr (TE101) GHz

RESULT:

A Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. is constructed and the resonant frequencies are found by varying the dimension a from 5 cm to 9 cm for 5 intervals keeping the other dimensions b and c constant for the modes TM_{110} and TE_{101}

Test Case 2: Design a Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. Find the resonant frequencies by varying the dimension b from 3 cm to 6 cm for 5 intervals keeping the other dimensions a and c constant for the modes TM_{110} and TE_{101} .

AIM: To design a Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. Find the resonant frequencies by varying the dimension b from 3 cm to 6 cm for 5 intervals keeping the other dimensions a and c constant for the modes TM_{110} and TE_{101} .

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

The resonant frequency of the $TE_{mn\ell}$ or $TM_{mn\ell}$ mode is given by

$$f_{mn\ell} = \frac{ck_{mn\ell}}{2\pi\sqrt{\mu_r\epsilon_r}} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

PROGRAM:

```
clc; clear;
format('e',11); a=0.05; b=0.03; c=0.09;
v=3*10^8;
//for m=1; n=1; p=0;
m=1;n=1; p=0;
fr110=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr110,"fr110(in Hz)");
//for m=1,n=0. m=1; n=0;
m=1;n=0; p=1;
fr101=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr101,"fr101(in Hz)");
```

OUTPUT:

Variable: dimension b cm
constant a=5 cm , c=9 cm

b(cm)	Simulation Results		Theoretical Results	
	fr (TM ₁₁₀) GHz	fr (TE ₁₀₁) GHz	fr (TM ₁₁₀) GHz	fr (TE ₁₀₁) GHz
4.5	4.48	3.43	4.48	3.43
5	4.24	3.43	4.24	3.43
6	3.90	3.43	3.90	3.43

RESULT:

A Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. is constructed and the resonant frequencies are found by varying the dimension b from 3 cm to 6 cm for 5 intervals keeping the other dimensions a and c constant for the modes TM_{110} and TE_{101} . In TE_{101} mode, since $n=0$, the variations in the dimension b is not affecting the result , therefore the outcome remains the same.

Test Case 3: Design a Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. Find the resonant frequencies by varying the dimension c from 8 cm to 12 cm for 5 intervals keeping the other dimensions a and b constant for the modes TM_{110} and TE_{101} .

AIM: To design a Rectangular Cavity Resonator with dimensions $a = 5$ cm, $b = 3$ cm and height $c = 9$ cm. Find the resonant frequencies by varying the dimension c from 8 cm to 12 cm for 5 intervals keeping the other dimensions a and b constant for the modes TM_{110} and TE_{101} .

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values

- Type the program
- Execute the program
- End the program

c) CALCULATION

The resonant frequency of the $TE_{mn\ell}$ or $TM_{mn\ell}$ mode is given by

$$f_{mn\ell} = \frac{ck_{mn\ell}}{2\pi\sqrt{\mu_r\epsilon_r}} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

d)

PROGRAM:

```
clc; clear;
format('e',11); a=0.05; b=0.03; c=0.09;
v=3*10^8;
//for m=1; n=1; p=0;
m=1;n=1; p=0;
fr110=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr110,"fr110(in Hz)");
//for m=1,n=0. m=1; n=0;
m=1;n=0; p=1;
fr101=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr101,"fr101(in Hz)");
```

OUTPUT:

Variable: dimension c cm

c (cm)	Simulation Results		Theoretical Results	
	fr (TM110) GHz	fr (TE101) GHz	fr (TM110) GHz	fr (TE101) GHz

RESULT:

A Rectangular Cavity Resonator with dimensions $a=5$ cm, $b=3$ cm and height $c=9$ cm. is constructed and the resonant frequencies are found by varying the dimension c from 8 cm to 12 cm for 5 intervals keeping the other dimensions a and b constant for the modes TM_{110} and TE_{101} . In TM_{110} mode, $p=0$, therefore variation in C dimension does not affect the outcome.

Test Case 4: Design a cubic Cavity Resonator with dimension of 5 cm Find the resonant frequency by varying the dimension from 5 cm to 9 cm for 5 intervals for the modes TM_{110} and TE_{101} . Compare the results with that of Rectangular Cavity Resonator with dimension a assuming the same range of 5 cm to 9 cm for 5 intervals.

AIM: To design a cubic Cavity Resonator with dimension of 5 cm Find the resonant frequency by varying the dimension from 5 cm to 9 cm for 5 intervals for the modes TM_{110} and TE_{101} . Compare the results with that of Rectangular Cavity Resonator with dimension a assuming the same range of 5 cm to 9 cm for 5 intervals.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

The resonant frequency of the $TE_{mn\ell}$ or $TM_{mn\ell}$ mode is given by

$$f_{mn\ell} = \frac{ck_{mn\ell}}{2\pi\sqrt{\mu_r\epsilon_r}} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

PROGRAM:

```
clc; clear;
format('e',11); a=0.05; b=0.04; c=0.03;
v=3*10^8; p=1;
//for m=0,n=1. m=0; n=1;
fr011=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr011,"fr011(in Hz)");
//for m=1,n=0. m=1; n=0;
fr101=v/2*sqrt((m/a)^2+(n/b)^2+(p/c)^2); disp(fr101,"fr101(in Hz)");
```

OUTPUT:

a (cm)	fr (TM ₁₁₀) GHz – Rectangular cavity b= 3 cm, c=9 cm	fr (TM ₁₁₀) GHz Cubic cavity	fr (TE ₁₀₁) GHz Rectangular cavity b= 3 cm, c=9 cm	fr (TE ₁₀₁) GHz Cubic cavity

RESULT:

A cubic Cavity Resonator with dimension of 5 cm is designed and the resonant frequencies are calculated by varying the dimension from 5 cm to 9 cm for 5 intervals for the modes TM₁₁₀ and TE₁₀₁. The results are compared with that of Rectangular Cavity Resonator with dimension a assuming the same range of 5 cm to 9 cm for 5 intervals. In both modes, cubic cavity takes the dimension of a and since m=1 in these modes, the resonant frequencies remain the same for the two modes.

EXNO: 13	Estimation of Resonant Frequency in a Cylindrical Cavity Resonator for a) Transverse Electric mode b) Transverse Magnetic mode
DATE:	

Test Case 1: Design a Teflon filled Cylindrical Cavity Resonator with dimensions a= 3 cm, and height c= 10 cm. Find the resonant frequencies by varying the dimension a from 3 cm to 8 cm for 5 intervals with c at a constant value of 10 cm for the dominant mode.

AIM: To design a Teflon filled Cylindrical Cavity Resonator with dimensions a= 3 cm, and height c= 10 cm. Find the resonant frequencies by varying the dimension a from 3 cm to 8 cm for 5 intervals with c at a constant value of 10 cm for the dominant mode.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- **Open SCILAB software**
- **Open file-new**
- **Put the input values**
- **Type the program**
- **Execute the program**
- **End the program**

CALCULATION

the resonant frequency of the $TM_{nm\ell}$ mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

the resonant frequency of the $TE_{nm\ell}$ mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p'_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2},$$

PROGRAM:

TE Mode

```
clc; clear;  
a=0.0274;  
v=3*10^8;  
Xnm=3.832;  
d=2*a; TE011=v/2*%pi*sqrt((Xnm/a)^2+(%pi/d)^2)*10^-9; printf("TE011(in Hz)=%f  
GHZ",TE011);
```

TM Mode

```
clc; clear;  
a=0.0274;  
v=3*10^8;  
Xnm=2.405;  
d=2*a; TM011=v/(2*%pi^1.44)*sqrt((Xnm/a)^2+(%pi/d)^2)*10^-9; printf("TM011(in Hz)=%f  
GHZ",TM011);
```

OUTPUT :

Teflon, $\epsilon_r = 2.08$, $c = 10$ cm

a (cm)	Simulation Results	Theoretical Results
	fr (TE111) GHz	fr (TE111) GHz

RESULT:

A Teflon filled Cylindrical Cavity Resonator is designed with dimensions $a = 3$ cm, and height $c = 10$ cm. Resonant frequencies are estimated by varying the dimension a from 3 cm to 8 cm for 5 intervals with c at a constant value of 10 cm for the dominant mode.

Test Case 2: Design a hollow Cylindrical Cavity Resonator with dimensions a= 4.2 cm, and height c= 8 cm. Find the resonant frequencies by varying the dimension a from 4.2 cm to 8 cm for 5 intervals with a constant c value of 8 cm for TM₀₁₁ and TE₁₀₁ modes.

AIM: To design a hollow Cylindrical Cavity Resonator with dimensions a= 4.2 cm, and height c= 8 cm. Find the resonant frequencies by varying the dimension a from 4.2 cm to 8 cm for 5 intervals with a constant c value of 8 cm for TM₀₁₁ and TE₁₀₁ modes.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

the resonant frequency of the TM_{nmℓ} mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

the resonant frequency of the TE_{nmℓ} mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p'_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2},$$

PROGRAM:

TE01 Mode

```
clc; clear;  
a=0.042;
```

```
v=3*10^8;
Xnm=3.832;
d=2*a; TE101=v/2*pi*sqrt((Xnm/a)^2+(pi/d)^2)*10^-9; printf("TE101(in Hz)=%f
GHZ",TE101);
```

TE11 Mode

```
clc; clear;
a=0.0424;
v=3*10^8;
Xnm=1.83;
d=2*a; TE111=v/2*pi*sqrt((Xnm/a)^2+(pi/d)^2)*10^-9; printf("TE111(in Hz)=%f
GHZ",TM011);
```

OUTPUT:

Constant c= 10 cm

a (cm)	Simulation Results		Theoretical Results	
	fr (TE101) MHz	fr (TE111) MHz	fr (TE101) MHz	fr (TE111) MHz

RESULT:

A hollow Cylindrical Cavity Resonator is constructed with dimensions a= 4.2 cm, and height c= 8 cm. Resonant frequencies are found by varying the dimension a from 4.2 cm to 8 cm for 5 intervals with a constant c value of 8 cm for TM₀₁₁ and TE₁₀₁ modes.

Test Case 3: A hollow Cylindrical Cavity Resonator is constructed such that its length c is equal to its diameter 2a. Find a and c for the resonant frequency of 10 GHz and 12 GHz at the TM₀₁₀ mode.

AIM: To construct a hollow Cylindrical Cavity Resonator such that its length c is equal to its diameter $2a$. Find a and c for the resonant frequency of 10 GHz and 12 GHz at the TM_{010} mode.

SOFTWARE REQUIRED:

SCILAB Version 6.1.1

PROCEDURE:

- Open SCILAB software
- Open file-new
- Put the input values
- Type the program
- Execute the program
- End the program

CALCULATION

the resonant frequency of the $TM_{nm\ell}$ mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2}.$$

the resonant frequency of the $TE_{nm\ell}$ mode is

$$f_{nm\ell} = \frac{c}{2\pi\sqrt{\mu_r\epsilon_r}} \sqrt{\left(\frac{p'_{nm}}{a}\right)^2 + \left(\frac{\ell\pi}{d}\right)^2},$$

PROGRAM:

TM Mode

```
clc; clear;
v=3*10^8;
Xnm=2.405;
f= 10*10^9
a=v/2*%pi*((Xnm/f));
c=2*a;
printf("a(in cm)=%f ",a);
printf ("c ( in cm)=%f ",c);
```

OUTPUT :

fr (GHz)	Simulation Results		Theoretical Results	
	a (cm)	c=2a (cm)	a (cm)	c=2a (cm)

RESULT:

A hollow Cylindrical Cavity Resonator is constructed such that its length c is equal to its diameter $2a$. The dimensions a and c are calculated for the resonant frequencies of 10 GHz and 12 GHz at the TM_{011} mode.

EXNO: 14	Design a two conductor transmission line and Investigate the impact of Dielectric layer thickness on characteristic Impedance and Propagation Velocity
DATE:	

Test Case 1: Design a Two conductor transmission line with single ground plane and estimate the impact of varying the thickness of the dielectric layer on characteristic Impedance and Propagation Velocity. Thickness to be varied between 5 to 15mm,

AIM: To design a Two conductor transmission line with single ground plane and estimate the impact of varying the thickness of the dielectric layer on characteristic Impedance and Propagation Velocity. Thickness to be varied between 5 to 15mm,

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- **Open TNT 1.2.2 Tool**
- **Open file-new**
- **Create a two conductor transmission line**
- **Select the dielectric layer with specified material and dimensions**
- **Select the ground plane with specified dimensions**
- **Place the dielectric layer on top of the ground plane**
- **Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.**

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

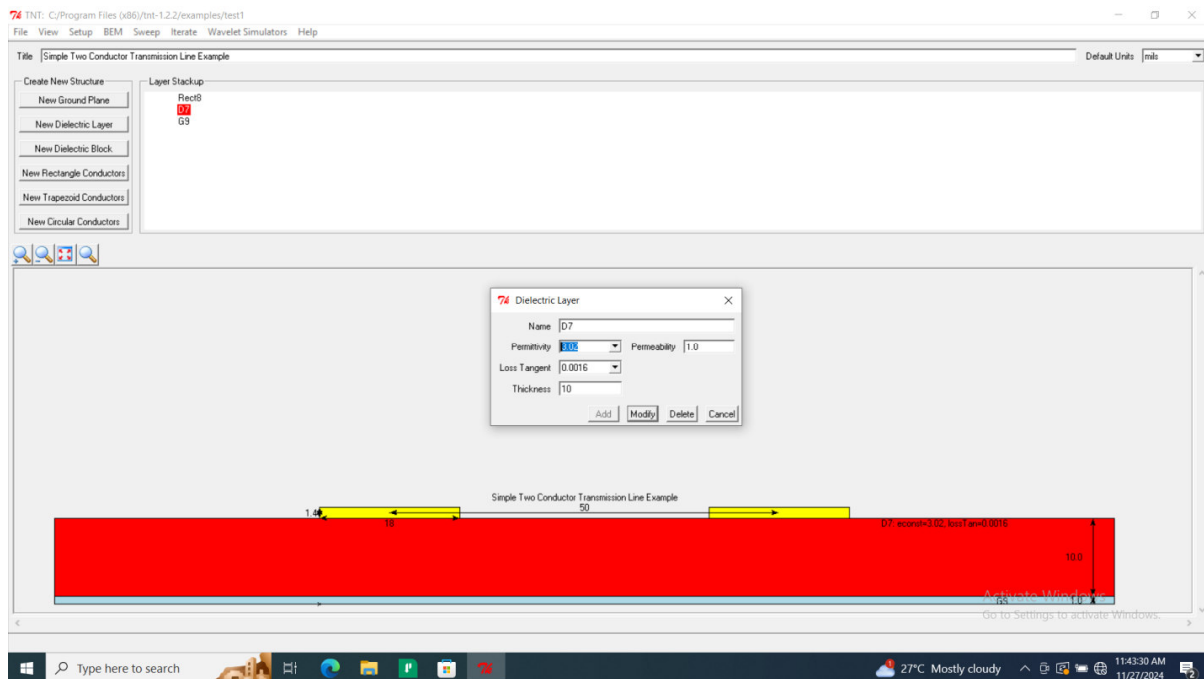
k = Relative permittivity of insulation between conductors

$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors



OUTPUT:

Thickness of Dielectric layer (mm)	Simulation Results		Theoretical Results	
	Characteristic Impedance (ohms)	Propagation Velocity (m/s)	Characteristic Impedance (ohms)	Propagation Velocity (m/s)

RESULT:

A Two conductor transmission line is designed with single ground plane and the impact of varying the thickness of the dielectric layer on characteristic Impedance and Propagation Velocity is estimated.

Test Case 2: Design a Two conductor transmission line with single ground plane and investigate the effect of far end cross talk and near end cross talk by varying the thickness of the dielectric layer .Thickness to be varied between 5 to 15mm

AIM: To design a Two conductor transmission line with single ground plane and estimate the impact of varying the thickness of the dielectric layer on characteristic Impedance and Propagation Velocity. Thickness to be varied between 5 to 15mm,

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- Open TNT 1.2.2 Tool
- Open file-new
- Create a two conductor transmission line
- Select the dielectric layer with specified material and dimensions
- Select the ground plane with specified dimensions
- Place the dielectric layer on top of the ground plane
- Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

k = Relative permittivity of insulation between conductors

$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors

OUTPUT:

Thickness of Dielectric layer	Simulation Results		Theoretical Results	
	Far end cross talk (dB)	Near end cross talk (dB)	Far end cross talk (dB)	Near end cross talk (dB)

RESULT:

A Two conductor transmission line is designed with single ground plane and the effect of far end cross talk and near end cross talk is investigated by varying the thickness of the dielectric layer .

EXNO: 15	Design a two conductor transmission line and examine the impact of conductor dimensions on characteristic Impedance and Propagation Velocity
DATE:	

Test Case 1: Design a Two conductor transmission line with single ground plane and investigate the impact of the width of the rectangular conductor on Characteristic Impedance and Propagation Velocity .Thickness to be varied between 10 to 20 mm.

AIM: To design a Two conductor transmission line with single ground plane and investigate the impact of the width of the rectangular conductor on Characteristic Impedance and Propagation Velocity .Thickness to be varied between 10 to 20 mm.

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- Open TNT 1.2.2 Tool
- Open file-new
- Create a two conductor transmission line
- Select the dielectric layer with specified material and dimensions
- Select the ground plane with specified dimensions
- Place the dielectric layer on top of the ground plane
- Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

k = Relative permittivity of insulation between conductors

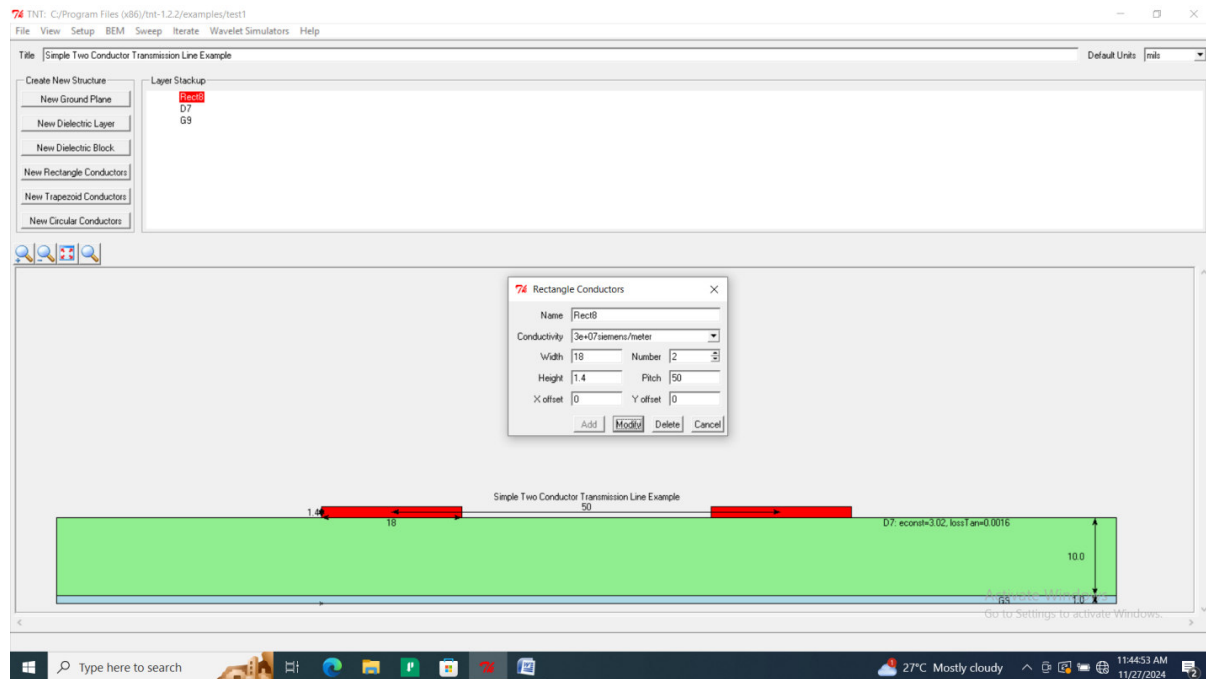
$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors

OUTPUT:



Width of the Conductor (mm)	Simulation Results		Theoretical Results	
	Characteristic Impedance (ohms)	Propagation Velocity (m/s)	Characteristic Impedance (ohms)	Propagation Velocity (m/s)

RESULT:

A Two conductor transmission line with single ground plane is designed and the impact of the width of the rectangular conductor on Characteristic Impedance and Propagation Velocity is investigated.

Test Case 2: Examine the effect of Characteristic Impedance and Propagation Velocity by varying the height of the rectangular conductor .Height to be varied between 1 to 1.4 mm.

AIM: To examine the effect of Characteristic Impedance and Propagation Velocity by varying the height of the rectangular conductor .Height to be varied between 1 to 1.4 mm.

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- Open TNT 1.2.2 Tool
- Open file-new
- Create a two conductor transmission line
- Select the dielectric layer with specified material and dimensions
- Select the ground plane with specified dimensions
- Place the dielectric layer on top of the ground plane
- Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

k = Relative permittivity of insulation between conductors

$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors

OUTPUT:

Height of the Conductor (mm)	Simulation Results		Theoretical Results	
	Characteristic Impedance (ohms)	Propagation Velocity (m/s)	Characteristic Impedance (ohms)	Propagation Velocity (m/s)

RESULT:

The effect of Characteristic Impedance and Propagation Velocity is examined by varying the height of the rectangular conductor between 1 to 1.4 mm.

EXNO: 16	Design a two conductor transmission line and examine the impact of Dielectric layer material on characteristic Impedance and Propagation Velocity
DATE:	

Test Case 1: Design a Two conductor transmission line with single ground plane and investigate the impact of the Dielectric layer material on characteristic Impedance and Propagation Velocity. Materials to be tested - GETEK ,FR 404, ADS995 and RO3203 .

AIM: To design a Two conductor transmission line with single ground plane and investigate the impact of the Dielectric layer material on characteristic Impedance and Propagation Velocity. Materials to be tested - GETEK ,FR 404, ADS995 and RO3203 .

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- Open TNT 1.2.2 Tool
- Open file-new
- Create a two conductor transmission line
- Select the dielectric layer with specified material and dimensions
- Select the ground plane with specified dimensions
- Place the dielectric layer on top of the ground plane
- Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

k = Relative permittivity of insulation between conductors

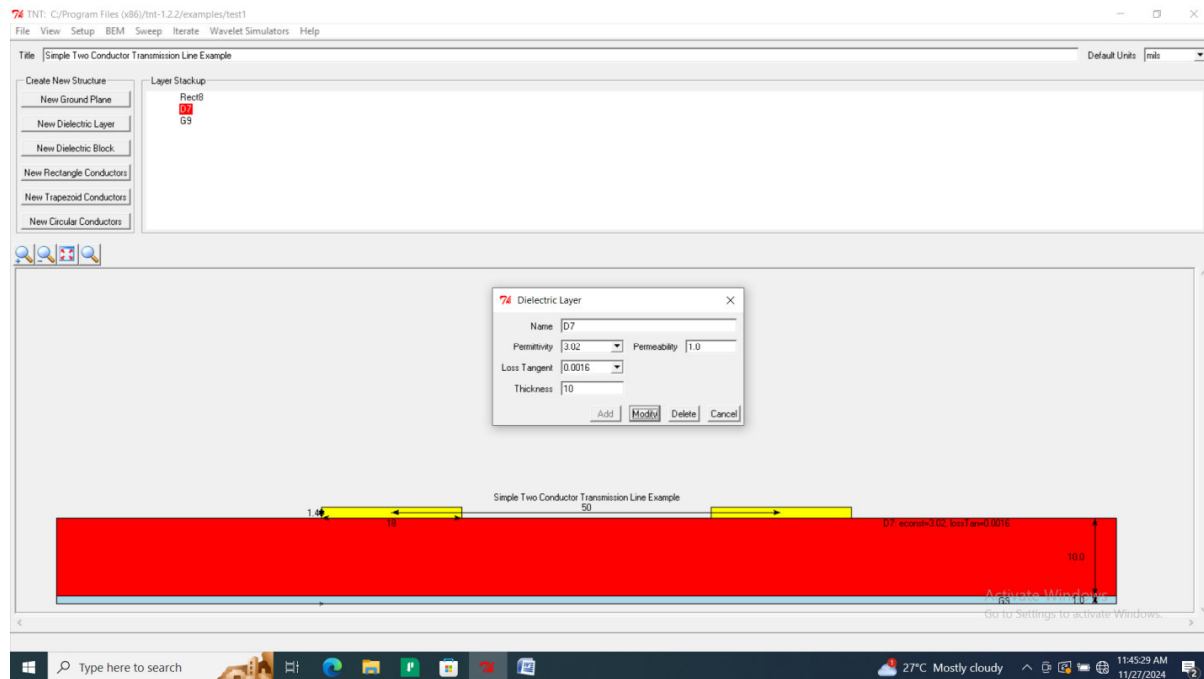
$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors

OUTPUT:



Dielectric layer material	Permittivity	Loss tangent	Simulation Results		Theoretical Results	
			Characteristic Impedance (ohms)	Propagation Velocity (m/s)	Characteristic Impedance (ohms)	Propagation Velocity (m/s)

RESULT:

A Two conductor transmission line with single ground plane is constructed and the impact of the Dielectric layer material like GETEK, FR 404, ADS995 and RO3203 on characteristic

Impedance and Propagation Velocity is examined. Materials to be tested -

Test Case 2: Design a Two conductor transmission line with single ground plane and investigate the impact of the conductor material on Rdc parameters. Width of the conductor is 18 mm and the height is 1.4 mm. Conductor is placed on a 10 mm thickness dielectric layer.

AIM: To design a Two conductor transmission line with single ground plane and investigate the impact of the conductor material on Rdc parameters. Width of the conductor is 18 mm and the height is 1.4 mm. Conductor is placed on a 10 mm thickness dielectric layer.

TOOL REQUIRED:

TNT 1.2.2

PROCEDURE:

- Open TNT 1.2.2 Tool
- Open file-new
- Create a two conductor transmission line
- Select the dielectric layer with specified material and dimensions
- Select the ground plane with specified dimensions
- Place the dielectric layer on top of the ground plane
- Select two rectangular conductors with specified material and dimensions and place on the top of dielectric layer.

CALCULATION

$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Z_0 = Characteristic impedance of line

d = Distance between conductor centers

r = Conductor radius

k = Relative permittivity of insulation between conductors

$$\text{Velocity factor} = \frac{v}{c} = \frac{1}{\sqrt{k}}$$

v = Velocity of wave propagation

c = Velocity of light in a vacuum

k = Relative permittivity of insulation between conductors

OUTPUT:

Conductor material	Conductivity S/m	Rdc R1 R1	Rdc R1 R0	Rdc R0 R1	Rdc R0 R0
Tungston	1×10^7				
Aluminium	3×10^7				
Copper	5×10^7				
Silver	6×10^7				

RESULT:

A Two conductor transmission line with single ground plane is designed and the impact of the conductor material on Rdc parameters is evaluated.