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Introduction to Transport Phenomena

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Technical Presentation

In this lecture...



- · Types of species
 - momentum, energy and mass
- · Molecular transport of species
- · Microscopic transport of species
- · Macroscopic transport of species
- · Inter-relation between these levels
- · Construction of the rate equations





Introduction

In engineering systems we encounter transport of species Momentum - Energy - Mass

> Transport of species is brought by various "forces"/ " driving potentials"

(Net Change) $\propto \frac{\text{(Potential to change)}}{\sqrt{}}$ (Resistance to change)

The relative magnitude of one potential with respect to some other potential will decide which change will dominate

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Transport phenomena vs Thermodynamics



Thermodynamics

Global accounting of momentum, energy and mass Feasibility of events under equilibrium conditions

No consideration of the mechanisms of species transport Does not tell us how to compute the rate of species transport

> output input







!! Transport of species is inherently a non-equilibrium process !!





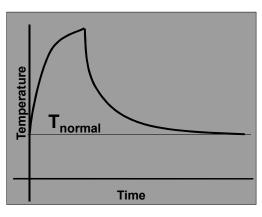
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Common experience: burning a finger





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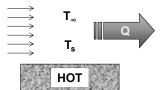


The Convection problem for interface transport

Typically we encounter solid-fluid boundaries

Net transport is linearly dependent on difference of driving potential at the interface

Newton's law of cooling



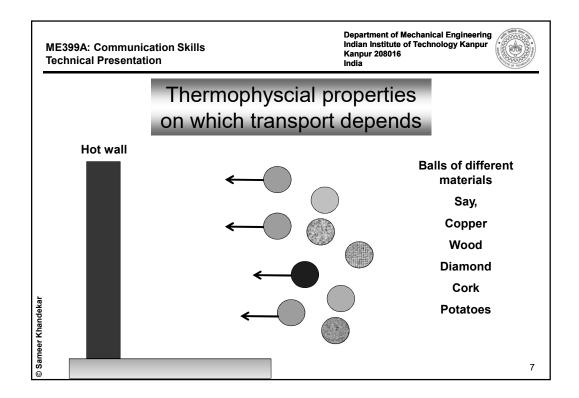
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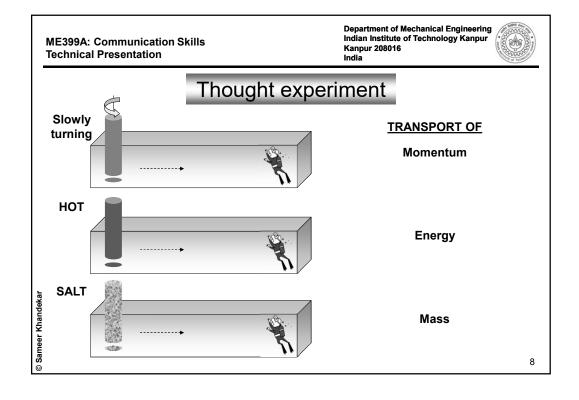
$$q'' = \frac{Q}{A_{cs}} = h \cdot (T_s - T_{\infty}) = -k_f \cdot \frac{\partial T}{\partial y}\Big|_{y=0}$$

Similarly for mass transfer

$$N_A'' = \frac{N}{A_{cs}} = h_m \cdot \left(C_{A,s} - C_{A,\infty} \right) = -D_{AB} \frac{\partial C_A}{\partial y} \bigg|_{y=0}$$

Heat/Mass transfer coefficients are 'fudge' factors





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Army of ants

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Transport phenomenon – holistic view



- · Length scales are different on the three levels
- Information must pass from molecular level to macroscopic level
- From molecular description we get viscosity thermal conductivity and diffusivity
- From microscopic description we find velocity, temperature and concentration,
- From macroscopic description we get bulk interactions and overall efficiency

Species conservation laws are applicable at all levels

Conservation of momentum

Conservation of energy

Conservation of mass

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Transport phenomenon – holistic view

Net Species Transport = \(\sum_{\text{interpolation}}\) (Molecular Transport + Convective Transport)

- Momentum Transport
- Energy Transport
- Mass Transport

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- # Molecular Momentum Transport + Convective Momentum Transport
- = Molecular Energy Transport + Convective Energy Transport



Diffusion terms

Advection terms

Rate equations

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How to solve problems?

One way to solve problems is to solve the (coupled) MOMENTUM, ENERGY AND MASS TRANSPORT RATE EQUATIONS

Only simple problems have analytical solutions

Others need CFD/CHT for solving the complex partial differential equations



The other way is "more" practical and also very useful

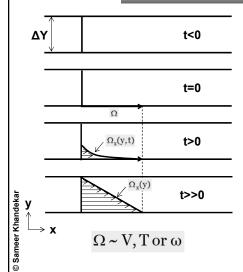
Use experimental data and dimensional analysis to formulate semi empirical/empirical equations

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Molecular transport of species



Momentum ►► Newton' Law of viscosity

Energy

► ► Fourier's Law of conductivity

Mass

► Fick's Law of diffusion

Basic forms of equation (One dimensional/incompressible)

$$\frac{F}{A} = \tau = -(\mu) \frac{\Delta V}{\Delta Y}$$

$$\frac{Q}{A} = q = -(k)\frac{\Delta T}{\Delta Y}$$

$$\frac{N_{Ay}}{A} = j_{Ay} = -(\rho D_{AB}) \frac{\Delta \omega_{Ay}}{\Delta Y}$$

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Molecular transport of species

Momentum diffusivity = μ/ρ also called v = $k/\rho C_p$ also called α Thermal diffusivity Mass diffusivity $= D_{AB}$

!! ALL HAVE THE SAME DIMENSIONS !! (length)²/ (time)

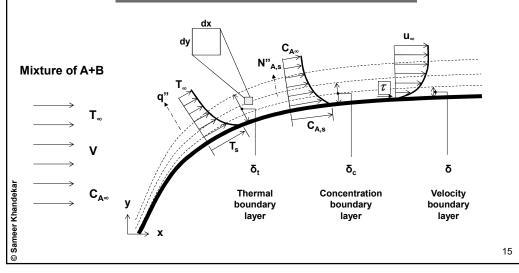
Taking any two at a time to form non-dimensional numbers

$$\begin{array}{ll} \text{The Prandtl Number} & = & Pr = \frac{\nu}{\alpha} = \frac{\mu C_p}{k} \\ \\ \text{The Schmidt Number} & = & Sc = \frac{\nu}{D_{AB}} = \frac{\mu}{\rho D_{AB}} \\ \\ \text{The Lewis Number} & = & Le = \frac{\alpha}{D_{AB}} = \frac{k}{\rho C_p D_{AB}} \\ \end{array}$$

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The concept of boundary layer



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Implications of the boundary layers

Velocity boundary layer Thermal boundary layer ▶ velocity gradients

▶ shear stress

Concentration boundary layer

► temperature gradients

► heat flux

▶ concentration gradients

► molar flux

For practical engineering design and applications the direct implications are:

Momentum transfer Energy transfer

► ► Friction Factor (non-dimensional shear stress)

► Nusselt Number (heat transfer coefficient)

Mass Transfer

► ► Sherwood Number (mass transfer coefficient)



Scaling Laws

Connecting the molecular level to microscopic level

$$\frac{\delta}{\delta_t} \approx \Pr^n \approx \frac{\text{Momentum diffusivity}}{\text{Thermal diffusivity}}$$

If Pr~1 $\blacktriangleright \blacktriangleright \delta \sim \delta_t$

(gases)

If Pr>>1 $\blacktriangleright \blacktriangleright \delta_t << \delta$

(Oils)

If Pr<<1 ▶▶ δ₁>>δ

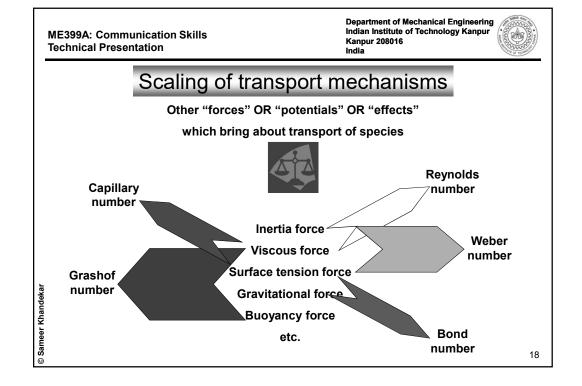
(liquid metals)

Similarly

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 $\frac{\delta}{\delta_c} \approx Sc^n \approx \frac{\text{Momentum diffusivity}}{\text{Mass diffusivity}}$

$$\frac{\delta}{\delta_t} \approx Le^n \approx \frac{\text{Thermal diffusivity}}{\text{Mass diffusivity}}$$



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Rate Equations

$$\left(\frac{\partial v_i}{\partial t} + v_x \frac{\partial v_i}{\partial x} + v_y \frac{\partial v_i}{\partial y} + v_z \frac{\partial v_i}{\partial z} \right) \\ = \mu \left(\frac{\partial^2 v_i}{\partial x^2} + \frac{\partial^2 v_i}{\partial y^2} + \frac{\partial^2 v_i}{\partial z^2} \right) - \frac{\partial p}{\partial x} \\ \left| i = x, y, z \right|$$

$$\rho C_p \! \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) \\ = k \! \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right)$$

$$\rho - \left(\frac{\partial C_{_A}}{\partial t} + v_{_X}\frac{\partial C_{_A}}{\partial x} + v_{_Y}\frac{\partial C_{_A}}{\partial y} + v_{_Z}\frac{\partial C_{_A}}{\partial z}\right) = \rho D_{AB} \left(\frac{\partial^2 C_{_A}}{\partial x^2} + \frac{\partial^2 C_{_A}}{\partial y^2} + \frac{\partial^2 C_{_A}}{\partial z^2}\right)$$



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Summary and Conclusions

- · A holistic view of transport phenomena was provided
- "Thermodynamics" and "Transport Phenomena" are complimentary
- · Momentum, energy and mass transport are guided by very similar laws
- · Conservation of species is applicable in all cases
- Information at all levels: molecular, microscopic and macroscopic is needed
- · Understanding can be improved by a unified study of specie transport
- Thermal/fluid management and design of thermal/fluid systems is indeed vital for the success of critical technologies and systems

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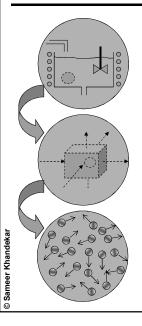
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In this lecture...

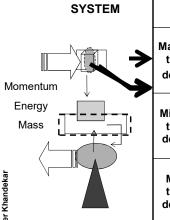
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Transport phenomenon – holistic view



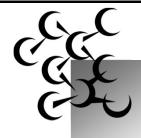
	Momentum	Energy	Mass
	transport	transport	transport
Macroscopic transport/ description	Macroscopic balances (isothermal)	Macroscopic balances (non- isothermal)	Macroscopic balances (mixtures)
Microscopic	Friction	Heat transfer coefficient (empirical)	Mass transfer
transport/	factor		coefficient
description	(empirical)		(empirical)
Molecular transport/ description	Dynamic Viscosity (momentum flux tensor)	Thermal Conductivity (Heat flux vector)	Mass Diffusivity (Mass flux vector)

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Molecular transport

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Microscopic transport

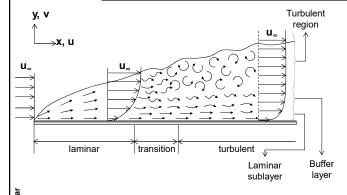
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Microscopic transport parameters



Reynolds Number

Inertia force
Viscous force

$$Re = \frac{(\rho \cdot V^2)}{(\mu \cdot V/L)} = \frac{\rho \cdot V \cdot L}{\mu}$$

Criterion for flow transition

LAMINAR ▶TURBULENT

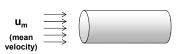
Laminar region ► Highly ordered flow ► streamlines

Turbulent region ► highly irregular, 3D ► enhanced species transport ► increased boundary layer thickness ► mixing ► flatter velocity profile



Microscopic transport parameters

In engineering practice we usually encounter two types of flow



Internal flows:

flow confined in a conduit, pipe, duct, etc. of constant cross section

External flows:

Flow past a flat plate, submerged bodies aerofoils, bluff bodies, etc.

Force exerted by fluid on the object

- (a) Forces present even if the fluid is stationary (Buoyancy)
- (b) Forces due to fluid motion (frictional drag and form drag)

The motion of fluid is due to kinetic energy and we are interested to know how much of this kinetic energy is manifested as pressure drop/shear stress

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Microscopic transport parameters

Internal flows = Darcy friction factor $f = \frac{-\left(dp \, / \, dx\right)D}{\frac{1}{2} \, \rho \cdot u_{\scriptscriptstyle m}^2}$

External flows = Coefficient of friction $C_f = \frac{\tau_s}{\frac{1}{2} \, \rho \cdot u_\infty^2} = \frac{(\text{Drag force per unit area})}{\frac{1}{2} \, \rho \cdot u^2}$

(note the difference between basis velocities for kinetic energy scaling)

We can see that the functional form of these equations are in the form:

$$f \text{ or } C_f = \frac{2}{\text{Re}} \frac{\partial u^*}{\partial y^*} \Big|_{y^*=0} \approx F^{\underline{n}}(\text{Re})$$

!! The significance of this result should not be overlooked !!

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Microscopic transport parameters

Now coming back to the definition of heat and mass transfer coefficients

$$h \cdot (T_s - T_{\infty}) = -k_f \cdot \frac{\partial T}{\partial y} \bigg|_{y=0}$$

$$h_m \cdot (C_{A,s} - C_{A,\infty}) = -D_{AB} \frac{\partial C_A}{\partial y} \bigg|_{y=0}$$

Again, it can be shown that the functional form of these equations are in the form:

$$h = \frac{k_f}{L} \frac{\partial T^*}{\partial y^*} \bigg|_{y^* = 0} \qquad OR \qquad Nu = \frac{hL}{k_f} = \frac{\partial T^*}{\partial y^*} \bigg|_{y^* = 0}$$

$$h_{m} = \frac{D_{AB}}{L} \frac{\partial C_{A}^{*}}{\partial y^{*}} \bigg|_{y^{*}=0} \qquad OR \qquad Sh = \frac{h_{m}L}{D_{AB}} = \frac{\partial C_{AB}^{*}}{\partial y^{*}} \bigg|_{y^{*}=0}$$

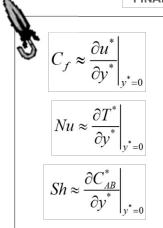
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Microscopic transport parameters

FINAL PICTURE WHICH EMERGES



The Nusselt Number is to the thermal boundary layer what the friction factor is to the velocity boundary layer

The Sherwood Number is to the concentration boundary layer what the Nusselt Number is to the thermal boundary layer

All three quantities manifest the nondimensional gradients at the interface of the particular specie they respectively represent

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Rate Equations

$$\rho = \left(\frac{\partial v_i}{\partial t} + v_x \frac{\partial v_i}{\partial x} + v_y \frac{\partial v_i}{\partial y} + v_z \frac{\partial v_i}{\partial z} \right) = \mu \left(\frac{\partial^2 v_i}{\partial x^2} + \frac{\partial^2 v_i}{\partial y^2} + \frac{\partial^2 v_i}{\partial z^2} \right) - \frac{\partial p}{\partial x}$$
 | $i = x, y, z$

$$\rho C_{\mathfrak{p}}\!\!\left(\frac{\partial T}{\partial t} + v_{x}\frac{\partial T}{\partial x} + v_{y}\frac{\partial T}{\partial y} + v_{z}\frac{\partial T}{\partial z}\right) \\ = k\!\!\left(\frac{\partial^{2}T}{\partial x^{2}} + \frac{\partial^{2}T}{\partial y^{2}} + \frac{\partial^{2}T}{\partial z^{2}}\right)$$

$$\rho - \left(\frac{\partial C_{_A}}{\partial t} + v_{_X}\frac{\partial C_{_A}}{\partial x} + v_{_Y}\frac{\partial C_{_A}}{\partial y} + v_{_Z}\frac{\partial C_{_A}}{\partial z}\right) = \rho D_{_{AB}}\!\!\left(\frac{\partial^2 C_{_A}}{\partial x^2} + \frac{\partial^2 C_{_A}}{\partial y^2} + \frac{\partial^2 C_{_A}}{\partial z^2}\right)$$









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End of Lecture