

Tutorial 5 - Solution

①

- ② General Constraints:
- $$4 \leq C \leq 12$$
- $$3 \leq N_a \leq 15$$
- $$\zeta \geq 0.15$$
- $$n_s \geq 1.2$$

Problem Specific Constraints:

$$L_o \leq 48 \text{ mm}$$
$$L_s \leq 31.5 \text{ mm}$$
$$n_1 \geq 1.5$$

- ⑥ Choose wire diameter $d = 2 \text{ mm}$
Free length $L_o = 48 \text{ mm}$.

\Rightarrow Maximum deflection (at service load $F_{\max} = 45 \text{ N}$)

$$y_{\max} = (48 - 37.5) = 10.5 \text{ mm}$$

\Rightarrow Spring rate $K = \frac{F_{\max}}{y_{\max}} = 4.286$

Size: Screw Thread $M10 \times 1.25$ g Clearance = 1.25 mm

$$\Rightarrow \begin{aligned} ID &= 10 + 1.25 = 11.25 \text{ mm} \\ OD &= ID + 2d = 13.25 \text{ mm} \\ D &= ID + d = 13.25 \text{ mm} \\ C &= D/d = 6.625 \text{ mm} \end{aligned}$$

Shear Modulus: $G = 79.3 \text{ MPa}$

(Table 10-5: d between 1.8-3 mm $\Rightarrow d \sim 0.064 - 0.125 \text{ in}$)

$$\Rightarrow N_a = \frac{d^4 G}{8 K D^3} = 15.9 \text{ turns (Not okay)}$$

$$N_t = N_a + 2 = 17.9 \text{ turns (Table 10-1)}$$

(for squared and ground ends)

Solid height: $L_s = d N_t = 35.8 \text{ mm}$ (Table 10-1)

\leftarrow (Not okay)

$$\Rightarrow y_s = 48 - 35.8 = 12.2 \text{ mm}$$

(deflection at solid length)

$$\Rightarrow F_s = K y_s = 52.289 \text{ N}$$

$$\Rightarrow \zeta = \frac{F_s}{F_{\max}} - 1 = 0.1627015$$

(Not okay)

(This is outside linear operating region)

continue with further calculations

(2)

$$K_B = \frac{4C+2}{4C-3} = 1.213$$

$$\Rightarrow \tau_s = K_B \left(\frac{8F_s D}{\pi d^3} \right) = 267.51 \text{ MPa}$$

Table 10-4: $A = 1783 \text{ MPa} \cdot (\text{mm})^m$, $m = 0.19$
relative cost = 1 (for A227-HD)

$$\Rightarrow S_{sy} = 0.45 S_{ut} = 0.45 \frac{A}{d^m}$$

$$\Rightarrow \boxed{S_{sy} = 703 \text{ MPa}}$$

$$\Rightarrow \boxed{n_s = \frac{S_{sy}}{\tau_s} = 2.63 > 1.2} \text{ (okay)}$$

$$\tau_{max} = K_B \left(\frac{8F_{max} D}{\pi d^3} \right) = 230 \text{ MPa}$$

$$\Rightarrow \boxed{n_t = \frac{S_{sy}}{\tau_{max}} = 3.054 > 1.5} \text{ (okay)}$$

$$\boxed{f_{om} = -\frac{\pi^2 d^2 D N_t}{4} = -2341}$$

Since we do not satisfy all the conditions, especially we are outside linear operation region. Need to reiterate.

d	1.8 mm	2 mm	2.2 mm
ID	11.25	11.25	11.25
OD	14.85	15.25	15.65
D	13.05	13.25	13.45
C	7.25	6.625	6.11
N_a	10.9	<u>15.9</u>	22.2
L_o	48	48	48
N_t	12.9	17.9	24.2
L_s	23.22	35.8	<u>53.24</u> $> L_o$
ξ	1.36	<u>0.139</u>	(not okay)
n_s	<u>0.994</u>	2.63	
n_t	2.3	3.054	
f_{om}	-1345	-2341	

Note: We do not need to iterate further. Observation

1. For $d = 2 \text{ mm}$: $\xi = 0.139 < 0.15$
 \Rightarrow outside linear regime

$N_a = 15.9$ may still be tolerated.

2. $d = 1.8 \text{ mm}$: $n_s = 0.974 < 1$
This is not ~~at~~ all desirable

3. $d = 2.2$ and higher:
 $L_s > L_o = \text{free length}$
Can not be manufactured.

\Rightarrow Need to iterate again.

(3)

③ One more parameter that we can play with is L_0 , satisfying $L_0 < 48 \text{ mm}$.

\Rightarrow Choose $L_0 = 45 \text{ mm}$.

$$\Rightarrow y_{\max} = (45 - 37.5) = 7.5 \text{ mm}$$

$$\Rightarrow k = \frac{45}{7.5} = 6 \text{ N/mm} = 6000 \text{ N/m}$$

\Rightarrow For $L_0 = 45 \text{ mm}$

d	1.8 mm	2 mm	2.2 mm
ID	11.25 mm	11.25 mm	11.25
OD	14.85	15.25	15.65
D	13.05	13.25	13.45
C	7.25	6.625	6.11
N_a	7.8	11.36	15.9
L_0	45	45	45
N_t	9.8	13.36	17.9
L_s	19.04	26.72	39.38
ξ	3.528	1.437	
n_s	0.534	1.288	
n_1	2.3	3.054	
f_{om}	-1022.4	-17.47	

$37.5 = \text{workpiece thickness}$
(not feasible)

\Rightarrow Only the wire diameter $d = 2 \text{ mm}$ satisfy all the criteria.

\Rightarrow This should be chosen.

④ Buckling: $L_0 < \frac{2.63 D}{\alpha} = 5.26 D = 69.7 \text{ mm}$ (Table 10-2: $\alpha = 0.5$)
(safe)

Critical frequency: $f = \frac{1}{2} \sqrt{\frac{k_y}{W}}$, $W = \frac{\gamma \pi^2 d^2 D N_a}{4} = 0.13 \text{ N}$

(Table-A5) $\gamma = 76 \text{ kN/m}^3$

$\Rightarrow f = 361 \text{ Hertz}$

Since, operating frequency is $\approx 5 \text{ Hz}$, the spring is safe.

Fatigue factor of safety:

Zimmerli Data (unpeened) :

$$S_{ca} = 241 \text{ MPa}, \quad S_{sm} = 379 \text{ MPa}$$

Table 10-4: $S_{ut} = \frac{A}{d_u} = 1563 \text{ MPa}$

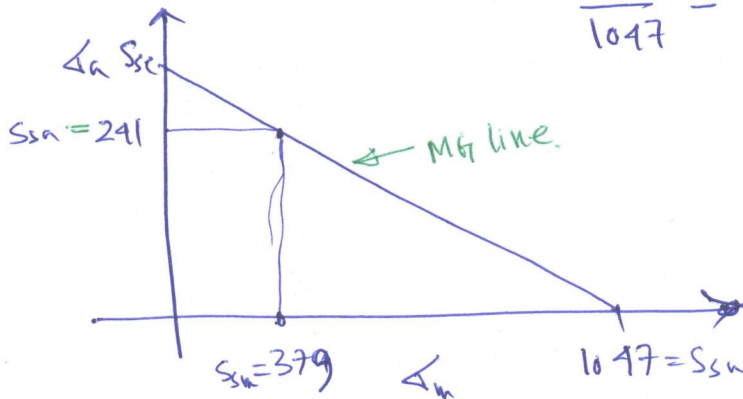
$$\Rightarrow S_{sn} = 0.67 S_{ut} = 1047 \text{ MPa}$$

Using Goodman Criterion

$$\Rightarrow \frac{S_{se}}{1047} = \frac{S_{ca}}{(1047 - S_{sm})} = \frac{241}{(1047 - 379)}$$

$$\Rightarrow \boxed{S_{se} = 377.7 \text{ MPa}}$$

$$\Rightarrow \eta_f = \frac{1}{\frac{\tau_a}{S_{sn}} + \frac{\tau_m}{S_{sn}}}$$



$$\tau_{max} = 230.00 \text{ MPa} \Rightarrow \tau_a = \tau_m = 115 \text{ MPa}$$

$$\tau_{min} = 0 \text{ MPa}$$

$$\Rightarrow \boxed{\eta_f = 2.414}$$

Using Sines Criteria : $S_{se} = S_{ca} = 241 \text{ MPa}$

$$\Rightarrow \boxed{\eta_f = \frac{S_{ca}}{\tau_a} = 2.10}$$