ESO 201A: Thermodynamics 2016-2017-I semester

Gas Power Cycle: part2

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Learning Objectives

- Evaluate the performance of gas power cycles for which the working fluid remains a gas throughout the entire cycle.
- Develop simplifying assumptions applicable to gas power cycles.
- Review the operation of reciprocating engines.
- Analyze both closed and open gas power cycles.
- Solve problems based on the Otto, Diesel, and Brayton cycles.

Reciprocating Engines

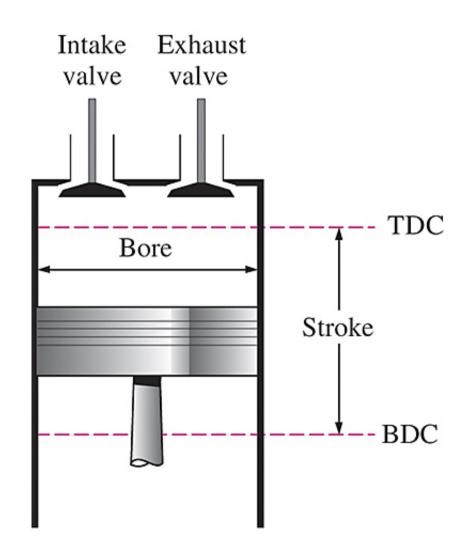
• The basic components of a reciprocating engine are shown to the right

Top Dead Center (TDC)

• The position of the piston when it forms the smallest volume in the cylinder

Bottom Dead Center (BDC)

• The position of the piston when it forms the largest volume in the cylinder



Stoke

- The distance between the TDC and BDC
- The largest distance the piston can travel in one direction

Bore

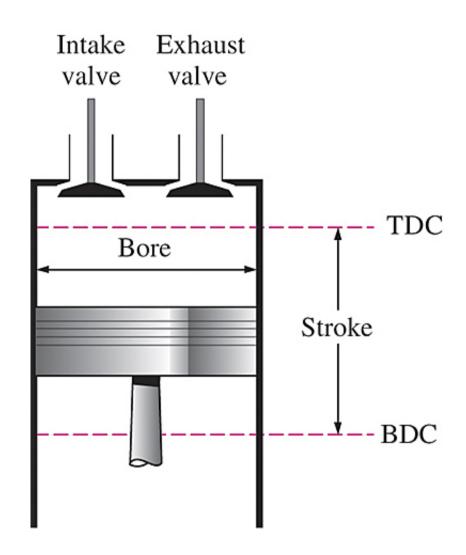
• The diameter of the piston

Intake Valve

• Where the air or air-fuel mixture is drawn into the cylinder

Exhaust Valve

• Where the combustion products are expelled from the cylinder

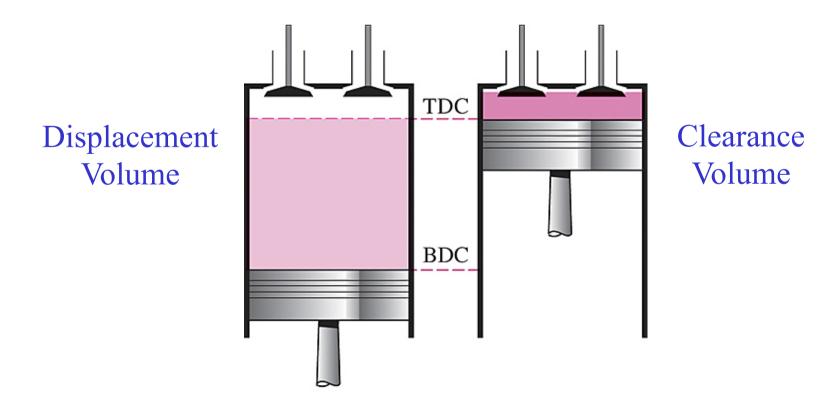


Clearance Volume

• The minimum volume formed in the cylinder, i.e., when the piston is at the TDC

Displacement Volume

• The volume displaced by the piston as it moves between the TDC and BDC



Compression Ratio (*r*)

• The ratio of the maximum volume formed in the cylinder to the minimum volume

$$r = \frac{V_{\text{max}}}{V_{\text{min}}} = \frac{V_{\text{BDC}}}{V_{\text{TDC}}}$$

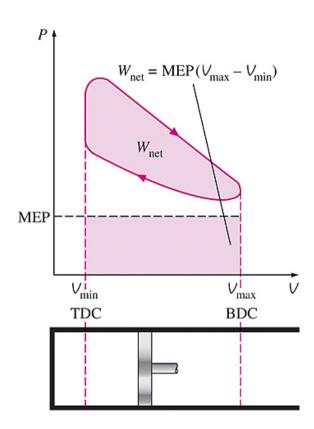
Mean Effective Pressure (MEP)

• A fictitious pressure that, if it acted on the piston during the entire power stoke, would produce the same amount of net work as that produced during the actual cycle

$$W_{\text{net}} = \text{MEP} \times \text{Piston Area} \times \text{Stoke}$$

= MEP \times Displacement Volume

$$MEP = \frac{W_{\text{net}}}{V_{\text{max}} - V_{\text{min}}}$$



Spark-Ignition Engines

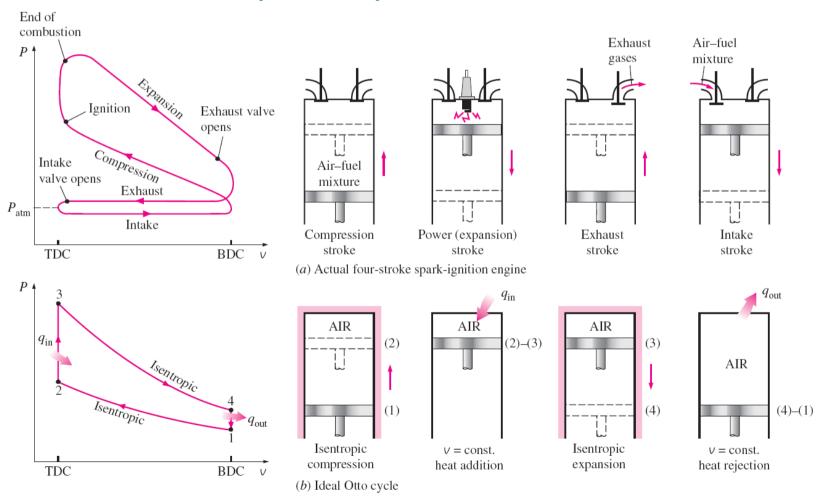
- The combustion of the air-fuel mixture is initiated by a spark plug
- E.g., engines in most cars

Compression-Ignition Engines (CI)

- The air-fuel mixture is self-ignited as a result of compressing the mixture above its self ignition temperature
- E.g., Diesel engines

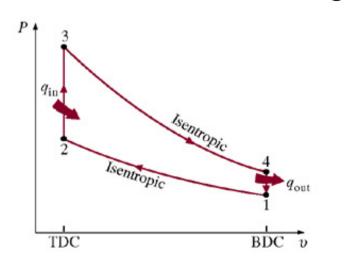
Four-Stroke Internal Combustion Engines

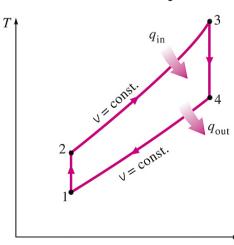
• An engine in which the piston executes four complete stokes within the cylinder, and the crankshaft completes two revolutions for each thermodynamic cycle



Simplification and Analysis

- The analysis of the four-stoke engine can be simplified significantly if the air-standard assumptions are utilized
- The resulting cycle is the ideal *Otto Cycle*, which consists of four internally reversible processes
 - 1→2 Isentropic compression
 - $2 \rightarrow 3$ Constant-volume heat addition
 - 3→4 Isentropic expansion
 - 4→1 Constant-volume heat rejection
- Here are the *P-v* and *T-s* diagrams for the Otto cycle





Nikolaus

Otto

Thermodynamic Analysis

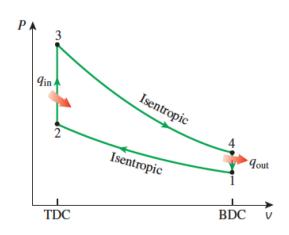
- The Otto cycle occurs in a closed system
- To simplify, kinetic and potential energy changes will be disregarded
- The energy balance for any of the processes on a unit-mass basis is expressed as

$$(q_{\rm in} - q_{\rm out}) - (w_{\rm out} - w_{\rm in}) = \Delta u$$

• No work is involved during the heat transfer process since both take place at constant volume

$$q_{\rm in} = u_3 - u_2 = c_v (T_3 - T_2)$$

$$q_{\text{out}} = u_4 - u_1 = c_v (T_4 - T_1)$$



Thermal Efficiency

• The thermal efficiency of the ideal Otto cycle under the cold-airstandard assumptions becomes

$$\eta_{\text{th, Otto}} = \frac{w_{\text{net}}}{q_{\text{in}}} = 1 - \frac{q_{\text{out}}}{q_{\text{in}}}$$

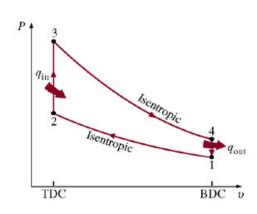
$$= 1 - \frac{T_4 - T_1}{T_3 - T_2}$$

$$= 1 - \frac{T_1(T_4/T_1 - 1)}{T_2(T_3/T_2 - 1)}$$

• Processes $1 \rightarrow 2$ and $3 \rightarrow 4$ are isentropic, and $v_2 = v_3$ and $v_4 = v_1$

$$\frac{T_1}{T_2} = \left(\frac{v_2}{v_1}\right)^{k-1} = \left(\frac{v_3}{v_4}\right)^{k-1} = \frac{T_4}{T_3}$$

$$\frac{T_4}{T_1} = \frac{T_3}{T_2} \implies \frac{(T_4/T_1-1)}{(T_3/T_2-1)} = 1$$



Thermal Efficiency (cont.)

• Combining the previous expressions yields the following expression for the thermal efficiency

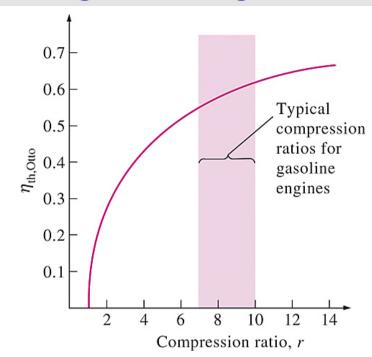
$$\left| \eta_{\text{th, Otto}} = 1 - \frac{1}{r^{k-1}} \right|$$

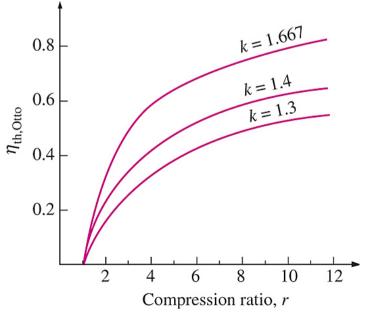
• Where *r* is the compression ratio

$$r = \frac{V_{\text{max}}}{V_{\text{min}}} = \frac{v_1}{v_2}$$

Thermal Efficiency (cont.)

- The thermal efficiency increases with both the compression ratio (r) and the specific heat ratio (k)
- The plot to the upper right shows the thermal efficiency as a function of the compression ratio
- In practice, when high compression ratios are used, premature ignition of the fuel, called *autoignition* may occur
- Autoignition produces an audible noise called *engine knock*
- The efficiency of the Otto cycle can also be improved by using a working fluid with a high specific heat ratio (see diagram at lower right)





Example

The compression ratio of an air-standard Otto cycle is 9.5. Prior to the isentropic compression process, the air is at 100 kPa, 35 °C, and 600 cm³. The temperature at the end of the isentropic expansion process is 800 K. Using specific heat values at room temperature, determine

- (a) The highest temperature and pressure in the cycle.
- (b) The amount of heat transferred, in kJ.
- (c) The thermal efficiency.
- (d) The mean effective pressure.

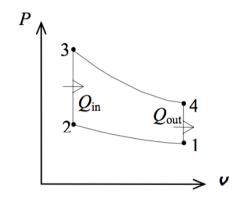
Example

Assumptions 1 The air-standard assumptions are applicable. 2 Kinetic and potential energy changes are negligible. 3 Air is an ideal gas with constant specific heats.

(a) Process 1-2: isentropic compression.

$$T_2 = T_1 \left(\frac{\mathbf{v}_1}{\mathbf{v}_2}\right)^{k-1} = (308 \text{ K})(9.5)^{0.4} = 757.9 \text{ K}$$

$$\frac{P_2 \mathbf{v}_2}{T_2} = \frac{P_1 \mathbf{v}_1}{T_1} \longrightarrow P_2 = \frac{\mathbf{v}_1}{\mathbf{v}_2} \frac{T_2}{T_1} P_1 = (9.5) \left(\frac{757.9 \text{ K}}{308 \text{ K}}\right) (100 \text{ kPa}) = 2338 \text{ kPa}$$



Process 3-4: isentropic expansion.

$$T_3 = T_4 \left(\frac{\mathbf{v}_4}{\mathbf{v}_3}\right)^{k-1} = (800 \text{ K})(9.5)^{0.4} = 1969 \text{ K}$$

Process 2-3: v =constant heat addition.

$$\frac{P_3 \mathbf{v}_3}{T_3} = \frac{P_2 \mathbf{v}_2}{T_2} \longrightarrow P_3 = \frac{T_3}{T_2} P_2 = \left(\frac{1969 \text{ K}}{757.9 \text{ K}}\right) (2338 \text{ kPa}) = \mathbf{6072 \text{ kPa}}$$

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Example

(b)
$$m = \frac{P_1 V_1}{RT_1} = \frac{\left(100 \text{ kPa}\right) \left(0.0006 \text{ m}^3\right)}{\left(0.287 \text{ kPa} \cdot \text{m}^3/\text{kg} \cdot \text{K}\right) \left(308 \text{ K}\right)} = 6.788 \times 10^{-4} \text{ kg}$$

$$Q_{\text{in}} = m \left(u_3 - u_2\right) = m c_v \left(T_3 - T_2\right) = \left(6.788 \times 10^{-4} \text{ kg}\right) \left(0.718 \text{ kJ/kg} \cdot \text{K}\right) \left(1969 - 757.9\right) \text{K} = \textbf{0.590 kJ}$$

(c) Process 4-1: \mathbf{v} = constant heat rejection.

$$Q_{\text{out}} = m(u_4 - u_1) = mc_v (T_4 - T_1) = -(6.788 \times 10^{-4} \text{ kg})(0.718 \text{ kJ/kg} \cdot \text{K})(800 - 308) \text{K} = 0.240 \text{ kJ}$$

$$W_{\text{net}} = Q_{\text{in}} - Q_{\text{out}} = 0.590 - 0.240 = 0.350 \text{ kJ}$$

$$\eta_{\text{th}} = \frac{W_{\text{net,out}}}{Q_{\text{in}}} = \frac{0.350 \text{ kJ}}{0.590 \text{ kJ}} = 59.4\%$$

(d)
$$V_{\min} = V_2 = \frac{V_{\max}}{r}$$

$$MEP = \frac{W_{\text{net,out}}}{V_1 - V_2} = \frac{W_{\text{net,out}}}{V_1(1 - 1/r)} = \frac{0.350 \text{ kJ}}{(0.0006 \text{ m}^3)(1 - 1/9.5)} \left(\frac{\text{kPa} \cdot \text{m}^3}{\text{kJ}}\right) = 652 \text{ kPa}$$

Next lecture

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