Tutorial-6 Given: Gear ratio ma= No = 4 Pressure angle = 200. @ => To avoid interference: No. of teet in pinion:- Np  $N_p \geqslant \frac{2k}{(1+2m)\sin^2\phi} \left( m + \sqrt{m^2 + (1+2m)\sin^2\phi} \right)$ (K=1 full depth) = 15.49 => Choose [Np=16] => [NG=MGNP=64] Center to Center distance: C = (NP+NA). M = 200 MM => (M = 5 mm Diameters: dp= 80mm dg=320mm (b) Power rating: PH= 25 kW => Transmitted load: W1 = 60000 H = 60000 x 25 KN => Wt= 2.984 KN = 2984 N Pitch line velocity V= Idn x 103 m/s = 8.378 m/s.

Factors for Bending Stress and Strength calculation Factor [Ko = 2.0] (for Light Shock power Sounce and Heavy shock Liviven machine

Surface: Ks = 0.843 (bm Jy) 0.0535

=> 
$$(K_s)_p = 1.0964$$
 (Pinion)  
 $(K_s)_G = 1.1071$  (gear)

facebooks b = 50 mm, M = 5 mm,  $V_p = 0.296 \text{ (Pinion)}$   $= > [Ks]_p = 1.0964 \text{ (Pinion)}$  (Table 14-2 and linear interpolation)  $(Ks)_q = 1.1071 \text{ (gear)}$ 

```
\frac{14-27}{14-27} = \frac{14-27}{1
                                                                                                                                                                                                                                                                                                                 2
                                            => A B= 0.3969
                                                      A = 83.776
|K_{V} = 1.171
                                         KH = 1+ Cm. (Cpf Cpm + Cma Ce) (Eq-14-30)
                                                       Cmc = 10 (uncrowned teeth)
                                                        C_{pf} = \frac{b}{10d} - 0.0375 + 0.0125 b ( \geq q. 14.32)
                                                 =) (C_{pf})_{p} = 0.0496 (pinion)]

(C_{pf})_{q} = 0.0371 (gear) 4 = \frac{b}{100} = 0.0156 \le 0.05
                                                                                                                                                                                                                                                                   => 6 = 0.05 is chosen
                                                                     51/8=0 (See Fig 14-10)
                                                                  => [Cpm=01]
                                                                                               Ce = 1, Cma = 0.1 (curve-3 Fig 14-11, b= 50mm= 1.97 in)
                                              => (KH) = 1+1 (0.0496*1+0.1)
                                                                    = (K_{H})_{p} = 1.1496 (Pinion)

(K_{H})_{q} = 1.1371 (gear)
                                         Rim thickness - to - tooth treight retro. = 1.5

=> [KB = 1] (Figure 14-16)
                                      Geometry Factor: (Y_J) = 0.27 \text{ (Pinion)} (Fig. 14-6)

(Y_J)_q = 0.41 \text{ (gear)}
                                  Stress Cycle factor: Y_{\text{N}} = 1.3558 \times \text{N}^{-0.0178} (Fig 14-14)

\Rightarrow | (Y_{\text{N}})_{\text{P}} = 0.977 \text{ (Pinion, } N = 10^8 \text{ Cycles}) | (Y_{\text{N}})_{\text{G}} = 1.009 \text{ (Geov, } N = \frac{10^8 \text{ Cycles}}{4})
```

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(3)
Temperature factor: [Yo = 1]
 Reliability factor. = Yz = 1 (Reliability = 0.99)
```

Benoing Strength:

$$S_t = 0.7255 \, H_B + 153.63$$

(2.5% Chrome, Grade 2)

Figure 14-4

Brain (St)  $p = 335 \, MP_A$  (Pinion,  $HB = 250$ )

(St)  $q = 298.73 \, MP_A$  (Gear,  $HB = 200$ )

Bending stress failure

Pinion: 
$$\sqrt{\frac{W_L}{bm}} \times \sqrt{\frac{K_L}{V_J}} \times \sqrt{\frac{K_H \times K_B}{V_J}}$$

$$= \frac{2989}{50\times5} \times 2\times 10171\times 100969 \times \frac{101496\times1}{0.27}$$

$$\Rightarrow \sqrt{\frac{1}{P}} = 130.5 \text{ MPa}$$

Allowable storess: 
$$V_{all} = \frac{S_L}{S_F} \cdot \frac{Y_N}{V_0 V_2}$$

$$\Rightarrow (V_{all})_{pinion} = \frac{335 \times 0.977}{S_F \times 1 \times 1} = \frac{327.3}{(S_F)_p} MP_a$$

$$\Rightarrow Factor of Safety: (S_F)_p = 2.508$$

$$\Rightarrow$$
  $(S_F)_p = 2.508, (S_F)_q = 3.484$ 

```
4
B Factors for pilling-resistance & strength:
   Elasticly coefficient: ZE= 191 TMPa (Table 14-8)
      Sustace Condition Factor: Z_R = 1

Geometry factor: Z_I = \frac{\text{Cost}_{k} \sin \phi_{k}}{2 \text{ Mod}} \left( \frac{\text{Squalion 14-23}}{\text{mod}} \right)
                                          $ = $ = 20°, m_N=1, (spur gear)
                               Stress cycle factor: ZIN = 1.4488 N-0.023 (Fig 14-15)
                        \Rightarrow \left( \frac{2}{2} N \right)_{p} = 0.948 \text{ (pinion)}
\left( \frac{2}{2} N \right)_{q} = 0.979 \text{ (gear)}
        Haraness Ratro factor:

1.7 > HBP = 250 = 1.25 > 1.2
                  A' = \left(8.98 \left( \frac{HBP}{HeG} \right) - 8.29 \right) \times 10^{-3} \quad \left( = 2.935 \times 10^{-3} \right)
            => (Zw) = 1.0+ A'(m6-1) = 1.009. (20-14-36)
                   => (Z_N)_P = 1. (Pinion) (Z_W)_G = 1.009 (gear)
    Contact Strength: |Sc= 1350 MPa) for both pinion and gear.
      Pinion: (1) = ZE SWt Ko Kaks. KH ZR 1/2
                 = 191 \left\{ \frac{2984 \times 2 \times 1.171 \times 1.0964 \times \frac{1.1496}{80 \times 50} \times \frac{1}{0.1285} \right\}
= 790.68 \text{ MPa}
                   Allowable contact stress: Valan = Sc ZNZW
```

=> ( ( all) = 1350x 0.948x1 = 1279.8 Mpa

Allowable contact stress

$$Pimion: (SF) = 2.508, (SH)_p^2 = 2.621$$

Gear: 
$$(S_F)_{q} = 3.484$$
,  $(S_H)_{q}^2 = 2.849$ 

$$\Rightarrow \sqrt{p} = 327.3MPa.$$

$$\Rightarrow \sqrt{W_{t}} = 7.484 \text{ kN} \text{ at failure}$$

$$\Rightarrow \sqrt{H} = 62.7 \text{ kN} \text{ power rating at failure}$$

$$\text{This is 151\%. over load}$$