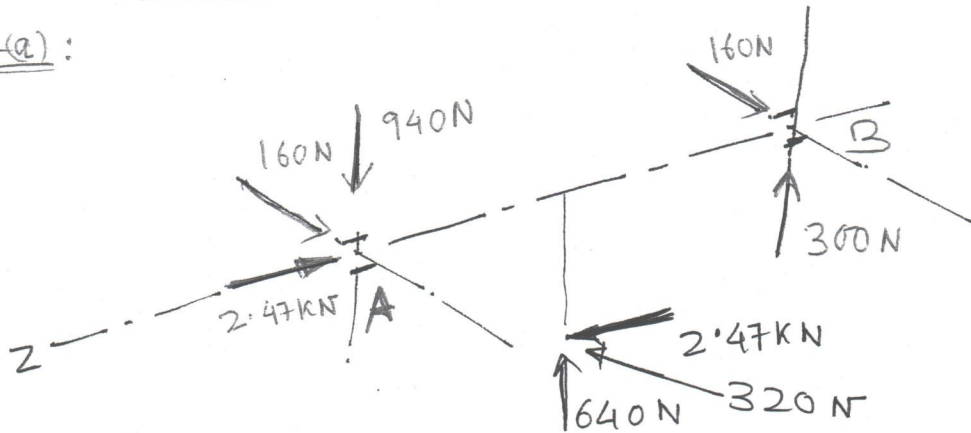


Part-(a):



- Bearing at A: Angular contact bearing. Takes all the thrust load.
- Bearing at B: Straight roller bearing
- Desired reliability:  $R_A = 0.99$ ,  $R_B = 1$

Selection of bearing at A:

$$F_r = (0.16^2 + 0.94^2)^{1/2} = 0.954 \text{ kN}$$

$$F_a = 2.47 \text{ kN}$$

Trial 1: Refer to table 11-1. Choose a starting  $F_a/C_0$  value at the middle of the table.

$$\Rightarrow \frac{F_a}{C_0} \approx 0.07 \Rightarrow C_0 = 35.3 \text{ kN}$$

Refer to 11-2 (table): select 02-60 mm angular contact bearing.

$$C_{10} = 55.9 \text{ kN}, C_0 = 35.5 \text{ kN}$$

$$\Rightarrow F_a/C_0 = 0.0696 \approx 0.07$$

Assume inner ring rotation. Rotation factor  $V = 1$ .

$$\Rightarrow \frac{F_a}{V F_r} = 2.59 > e \quad (e \approx 0.27 \text{ table 11-1})$$

$$\Rightarrow X_2 = 0.56, Y_2 = 1.632 \quad (\text{Table 11-1})$$

=> Equivalent radial load:  $F_e = X_2(V F_r) + Y_2 \cdot F_a$

$$\Rightarrow F_e = 4.57 \text{ kN} = (0.56(0.954) + 1.632 \times 2.47) \text{ kN}$$

Application factor  $a_f = 1.3$ . Desired load  $F_0 = F_e$

(2)

Life:  $L_D = 25 \text{ kh}$  (Desired),  $L_R = 10^6 \text{ cycles}$

$$\Rightarrow \boxed{X_D = \frac{25 \times 10^3 \times 600 \times 60}{10^6} = 900}$$

$$\Rightarrow C_{10} = a_f \cdot F_D \cdot \left[ \frac{X_D}{X_0 + (\theta - X_0) \left\{ \ln \frac{1}{R_0} \right\}^{1/b}} \right]^{1/a}$$

$a = 3$  (for ball bearing)

$$X_0 = 0.02, \theta - X_0 = 4.439, b = 1.483.$$

$$\Rightarrow C_{10} = 1.3 \times 4.57 \left[ \frac{900}{0.02 + 4.439 \left\{ \ln \left( \frac{1}{0.99} \right) \right\}^{1/1.483}} \right]^{1/3}$$

$$= 1.3 \times 4.57 \times [6.003]$$

$$\Rightarrow \boxed{C_{10} = 95.1 \text{ kN} > 55.9 \text{ kN}}$$

This will not work.

Trial-2: Select 02-90 mm bearing

$$\Rightarrow \boxed{C_{10} = 106 \text{ kN}, C_0 = 73.5 \text{ kN}} \quad (\text{Table 11-2})$$

$$\Rightarrow F_A / C_0 = 0.034, X_2 = 0.56, Y_2 = 1.93 \quad (\text{Table 11-1})$$

$$\Rightarrow \boxed{F_D = F_E = 5.3 \text{ kN}}$$

$$\Rightarrow C_{10} = 110.2 \text{ kN} > 106 \text{ kN}$$

Again, will not work.

Trial-3: Select 02-95 mm bearing.

$$\Rightarrow \boxed{C_{10} = 121 \text{ kN}, C_0 = 85 \text{ kN}} \quad (\text{Table 11-2})$$

$$\Rightarrow F_A / C_0 = 0.029, X_2 = 0.56, Y_2 = 1.98 \quad (\text{Table 11-1})$$

$$\Rightarrow F_D = F_E = 5.425 \text{ kN}$$

$$\Rightarrow \boxed{C_{10} = 112.88 \text{ kN} < 121 \text{ kN}}$$

Thus we select 02-series -95 mm angular contact bearing for A.

Bearing at B: (straight roller)

(3)

$$R_0 = 1, \quad F_r = F_D = (0.16^2 + 0.3^2)^{1/2} = 0.34 \text{ kN}$$

$$\Rightarrow C_{10} = a_f \cdot F_D \cdot \left[ \frac{900}{0.02} \right]^{1/a} \quad (a = 10/3 \text{ for roller bearing})$$
$$= 11 \text{ kN}$$

Refer to table 11-3: Even the smallest bore size straight roller bearing has  $C_{10} = 16.8 \text{ kN} > 11 \text{ kN}$ .

$\Rightarrow$  Any bearing can be chosen.

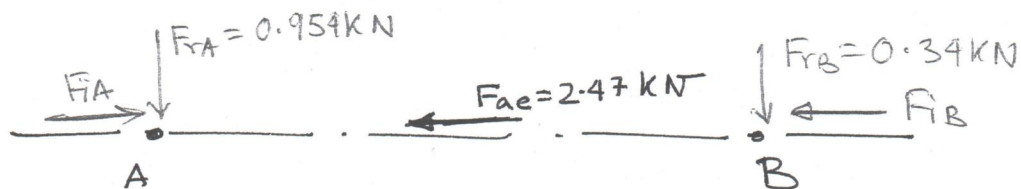
- Choose bearing with same bore size.

$\Rightarrow$  For B: 02-series 95mm roller bearing.

$$\boxed{C_{10} = 165 \text{ kN}, C_0 = 112 \text{ kN}}$$

— x — x — x —

Part - b: The modified FBD looks like the following



- Consider direct mounting.
- $F_{ae}$  is positive as per convention (retowards A).
- Induced Thrust  $F_i = \frac{0.47 F_r}{k}$ . Starting guess for  $k = 1.5$ .

$$\Rightarrow \boxed{F_{tA} = 0.30 \text{ kN}, F_{tB} = 0.107 \text{ kN}}$$

Since  $F_{tA} < (F_{tB} + F_{ae}) = 2.577 \text{ kN}$ , bearing A takes thrust load.

$\Rightarrow$  Equivalent loads are:

$$\left. \begin{aligned} F_{eA} &= 0.4 F_{rA} + k_A (F_{tB} + F_{ae}) = 4.25 \text{ kN} \\ F_{eB} &= F_{rB} = 0.34 \text{ kN} \end{aligned} \right\} \text{(Eq 11-16)}$$

Reliability:  $R_A = R_B = \sqrt{0.9} = 0.949$

Rated life:  $L_{10} = 3000 \times 500 \times 60 = 90 \times 10^6 \text{ revs.}$

$$\Rightarrow \boxed{x_D = \frac{900 \times 10^6}{90 \times 10^6} = 10}$$

$$C_{10} = a_f F_D \cdot \left[ \frac{x_0}{x_0 + (\theta - x_0) \left\{ \ln \left( \frac{1}{R_D} \right) \right\}^{1/b}} \right]^{1/a} \cdot \left( a = \frac{10}{3} \text{ for roller bearings} \right)$$

$$x_0 = 0, \theta = 4.48, b = 1.5$$

$$\Rightarrow C_{10} = 1.3 \times 4.25 \left[ \frac{10}{4.48 \times \left\{ \ln \left( \frac{1}{0.949} \right) \right\}^{1/1.5}} \right]^{3/10}$$

$$= 1.3 \times 4.25 \times [2.295]$$

$$\Rightarrow \boxed{C_{10} = 12.68 \text{ kN}}$$

Refer to Fig 11-15:

Select ~~33205~~ Cone }  $\Rightarrow C_{10} = 13 \text{ kN (radial)}$   
~~33205~~ Cap. }  $C_{10} = 7.96 \text{ kN (axial)}$   
~~33205~~

$$\boxed{K = 1.66}$$

Note: 30305 Cup and Cone had lower  $C_{10}$  (13 kN), However this was chosen because  $K$  value is closer to initial guess.

~~33205~~

Trial-2:  $F_{1A} = \frac{0.47 \times F_{ra}}{1.66} = 0.27 \text{ kN}$

Bearing at B:  $C_{10} = 1.01 \text{ kN.}$

$\Rightarrow$  Select 30205 Cup and 30205 Cone (has lowest  $C_{10}$  rating and same bore size as bearing A)

$$\Rightarrow \boxed{K = 1.56}$$

$$\Rightarrow F_{1B} = \frac{0.47 F_{rB}}{1.56} = 0.102 \text{ kN}$$

Again:  $F_{1A} < (F_{1B} + F_{ae}) = 2.572 \text{ kN}$

$$\Rightarrow \boxed{F_{eA} = 4.65 \text{ kN}, F_{eB} = 0.34 \text{ kN}}$$

$\Rightarrow C_{10} = 13.88 \text{ kN}$  (Bearing A) — will not work.

$C_{10} = 1.01 \text{ kN}$  (Bearing B) — will work.



(5)

Trial-3: Select Cone — 32305 } Bearing A  
 Cup — 32305,

$$\Rightarrow C_{10} = 17.4 \text{ kN (radial)}$$

$$K = 1.95$$

Bearing B: no change.

$$\Rightarrow F_A = 0.23 \text{ kN} < (F_B + F_{ae}) = 2.572 \text{ kN}$$

$$\Rightarrow \boxed{F_A = 5.397 \text{ kN}, F_B = 0.34 \text{ kN}}$$

$$\Rightarrow C_{10} = 16.1 \text{ kN (Bearing A)} < 17.4 \text{ kN}$$

This will work. Hence the selected bearings are.

For A: Cone — 32305 }  $C_{10} = 17.4 \text{ kN (radial)}$   
 Cup — 32305 }  $K = 1.95$

For B: Cone — 30205 }  $C_{10} = 8.19 \text{ kN (radial)}$   
 Cup — 30205 }  $K = 1.56$