

FLUID DYNAMICSQ4:Time to empty the tank

At  $t=t$ ,  $v = \sqrt{2gy}$

$$AV = av$$

$$V = \frac{a}{A} v$$

$$V = \frac{a}{A} \sqrt{2gy}$$

$$-\frac{dy}{dt} = \frac{a}{A} \sqrt{2gy}$$

$$\int_h^y \frac{dy}{\sqrt{y}} = -\frac{a}{A} \sqrt{2g} \int_0^t dt$$

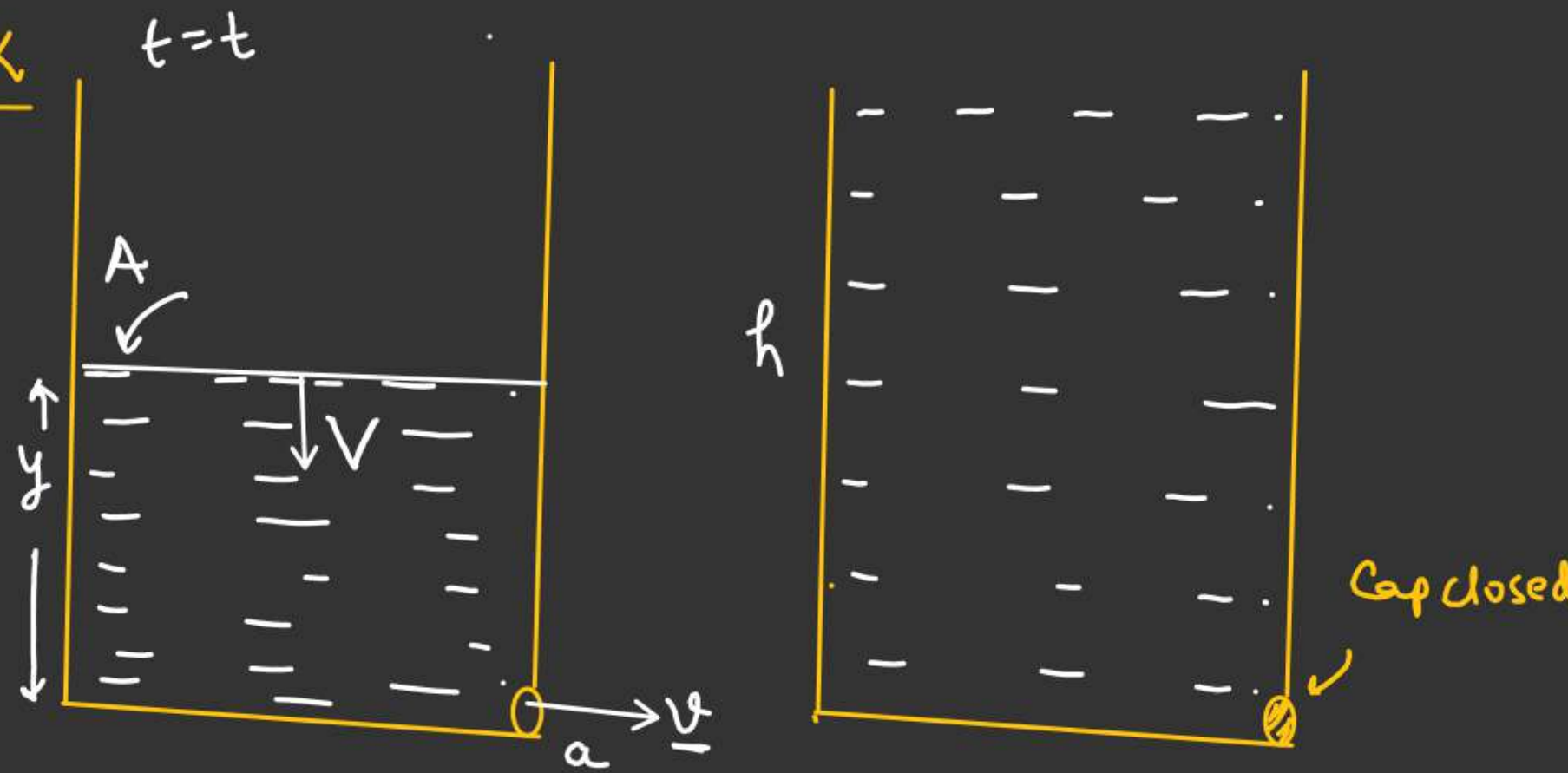
$$2 \left[ \sqrt{y} \right]_h^y = -\frac{a}{A} \sqrt{2g} t$$

$$\frac{A}{a} \sqrt{\frac{2}{g}} \left[ \sqrt{h} - \sqrt{y} \right] = t$$

Q4

Total time to empty the tank,  $y=0, t=T$

$$T = \frac{A}{a} \sqrt{\frac{2h}{g}}$$



# Ratio of time taken to empty half of the tank to the time taken to empty the tank.

For half of tank

$$y = \frac{h}{2}$$

$$t_1 = \sqrt{\frac{2}{g}} \left[ \sqrt{h} - \sqrt{\frac{h}{2}} \right]$$

$$t_1 = \sqrt{\frac{2h}{g}} \frac{[\sqrt{2}-1]}{\sqrt{2}}$$

$$t_1 = \sqrt{\frac{h}{g}} (\sqrt{2}-1)$$

time taken to empty the tank completely

$$t_2 = \sqrt{\frac{2h}{g}}$$

$$\frac{t_1}{t_2} = \left( \frac{\sqrt{2}-1}{\sqrt{2}} \right)$$

By Law of Continuity

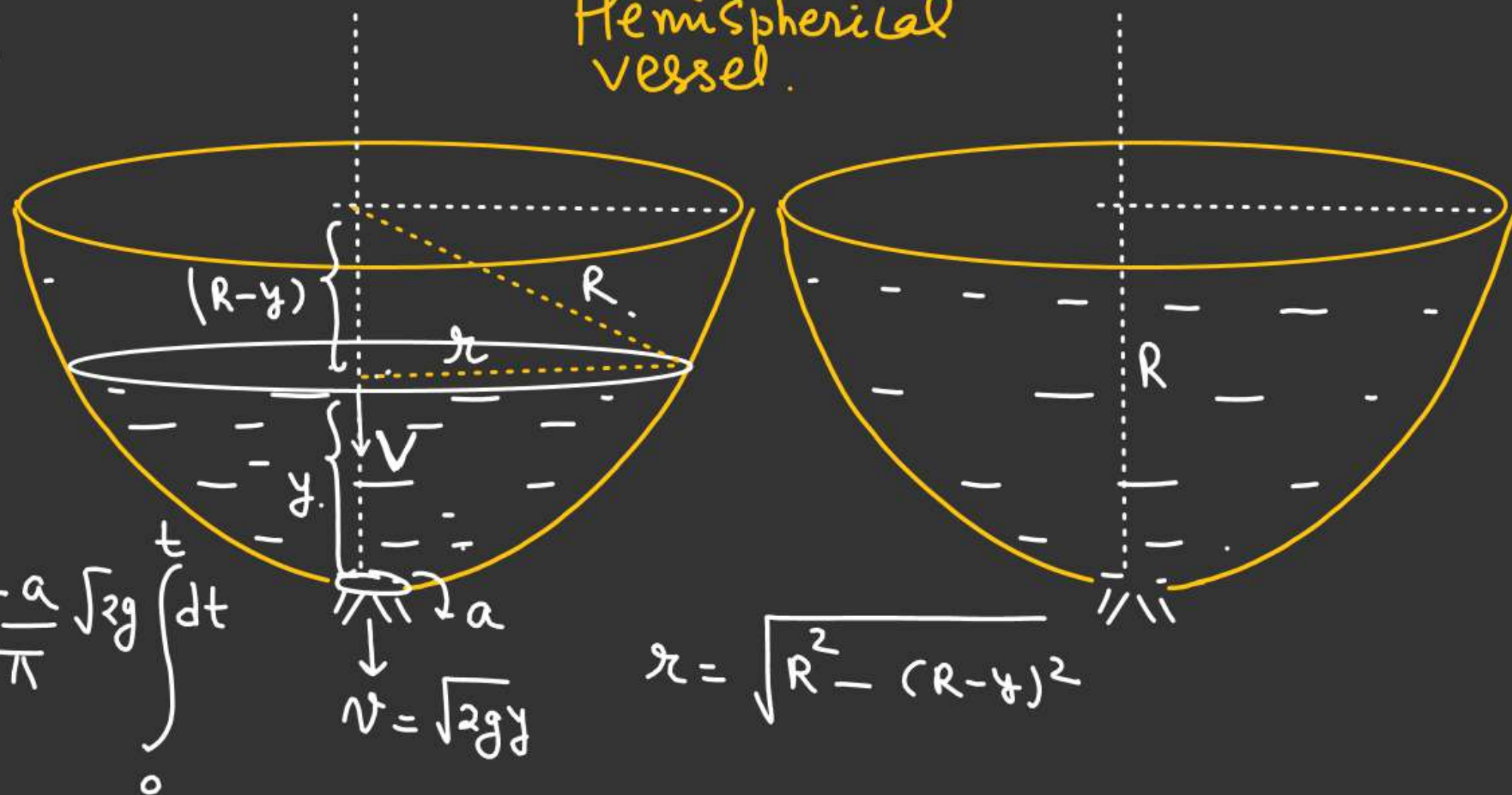
$$(\pi r^2) \underline{V} = a \underline{v}$$

$$\pi (R^2 - (R-y)^2) \left( -\frac{dy}{dt} \right) = a \sqrt{2gy}$$

$$\int_R^0 \frac{(R^2 - (R-y)^2)}{\sqrt{y}} \cdot dy = -\frac{a}{\pi} \sqrt{2g} \int_0^t dt$$

$$t = ??$$

Hemispherical vessel.



$$r = \sqrt{R^2 - (R-y)^2}$$



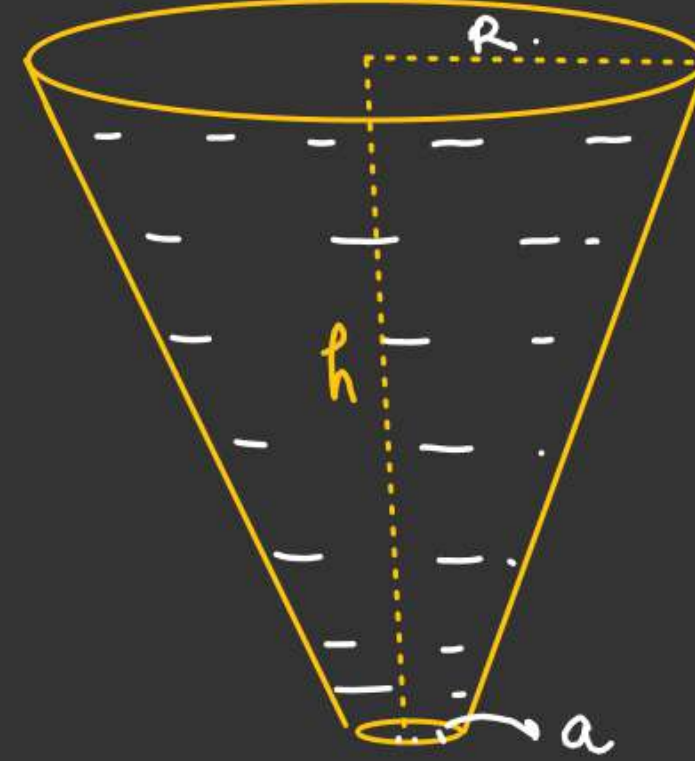
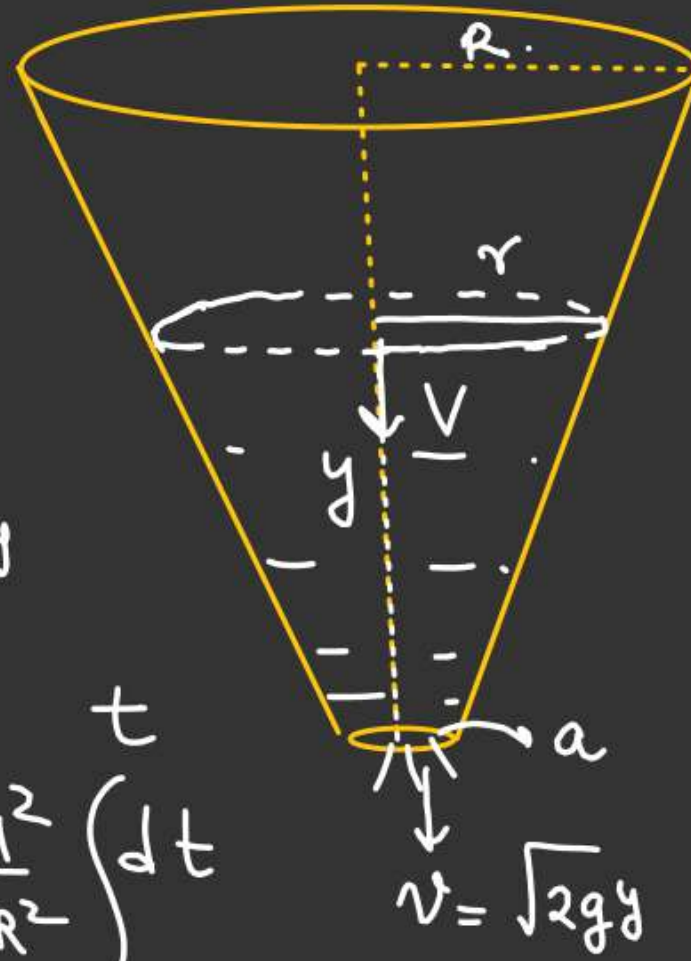
$$\frac{r}{y} = \frac{R}{H}$$

$$r = \left(\frac{R}{H} y\right)$$

$$(\pi r^2) \underline{v} = a \sqrt{2gy}$$

$$\pi \left(\frac{R}{H} y\right)^2 \left(-\frac{dy}{dt}\right) = a \sqrt{2gy}$$

$$\int_R^0 \frac{y^2}{\sqrt{y}} dy = -\frac{a \sqrt{2g}}{\pi} \frac{H^2}{R^2} \int_0^t dt$$



# Velocity of efflux in rotating frame

1 & 2 are points just inside and outside the hole.

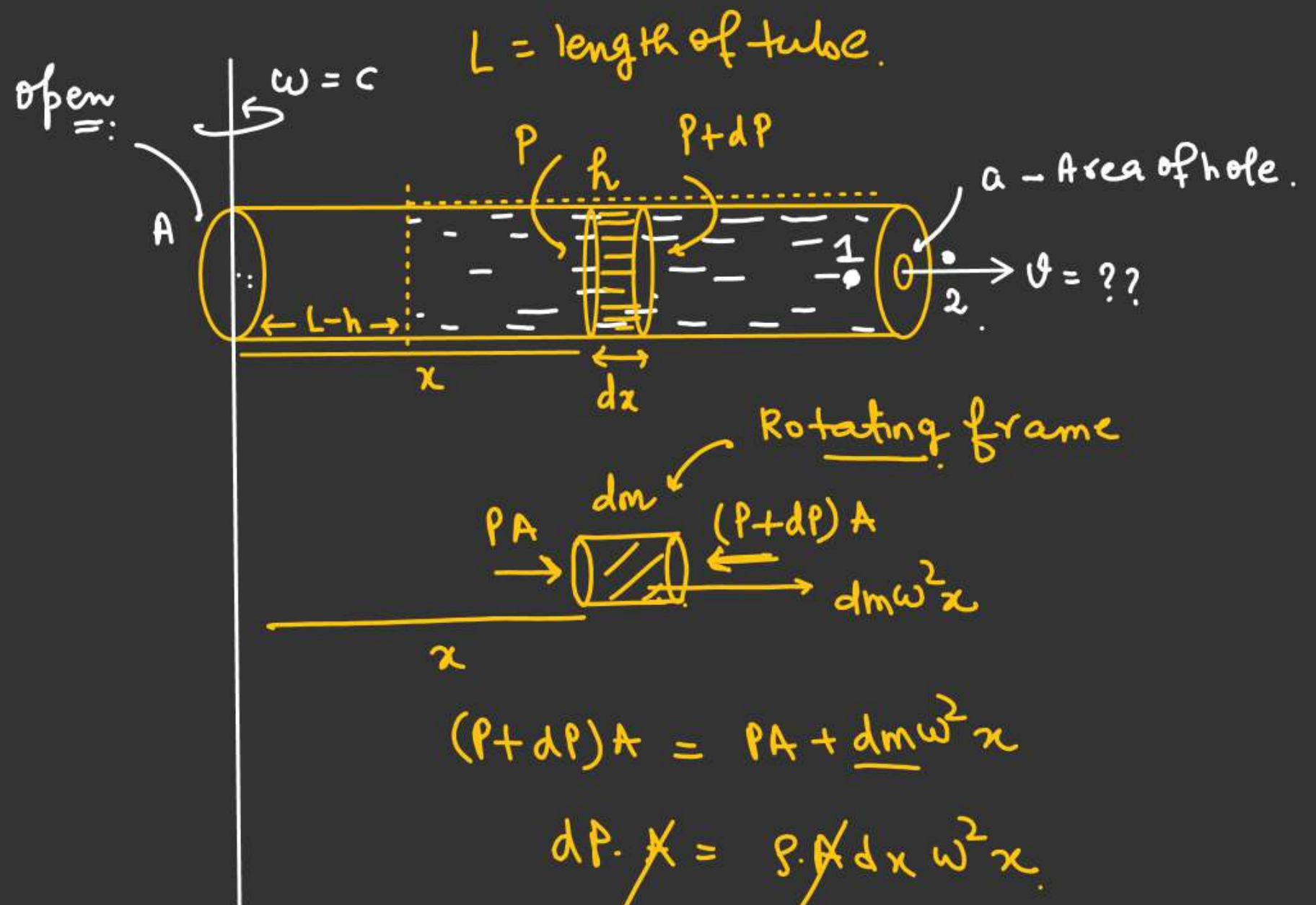
$$\frac{dP}{dx} = \rho \omega^2 x$$

$$\int_{P_{atm}}^{P_1} dP = \rho \omega^2 \int_{(L-h)}^L x dx$$

$$P_1 - P_{atm} = \frac{\rho \omega^2 [L^2 - (L-h)^2]}{2}$$

$$P_1 = P_{atm} + \frac{\rho \omega^2 [L^2 - (L^2 + h^2 - 2Lh)]}{2}$$

$$P_1 = P_{atm} + \frac{\rho \omega^2 [2Lh - h^2]}{2}$$



$$(P+dP)A = PA + dm\omega^2 x$$

$$dP \cdot A = \rho \cdot A dx \omega^2 x$$

$$\int dP = \rho \omega^2 \int x dx$$



$$P_1 = P_{atm} + \frac{\rho \omega^2}{2} [2Lh - h^2] \quad \text{open} =$$

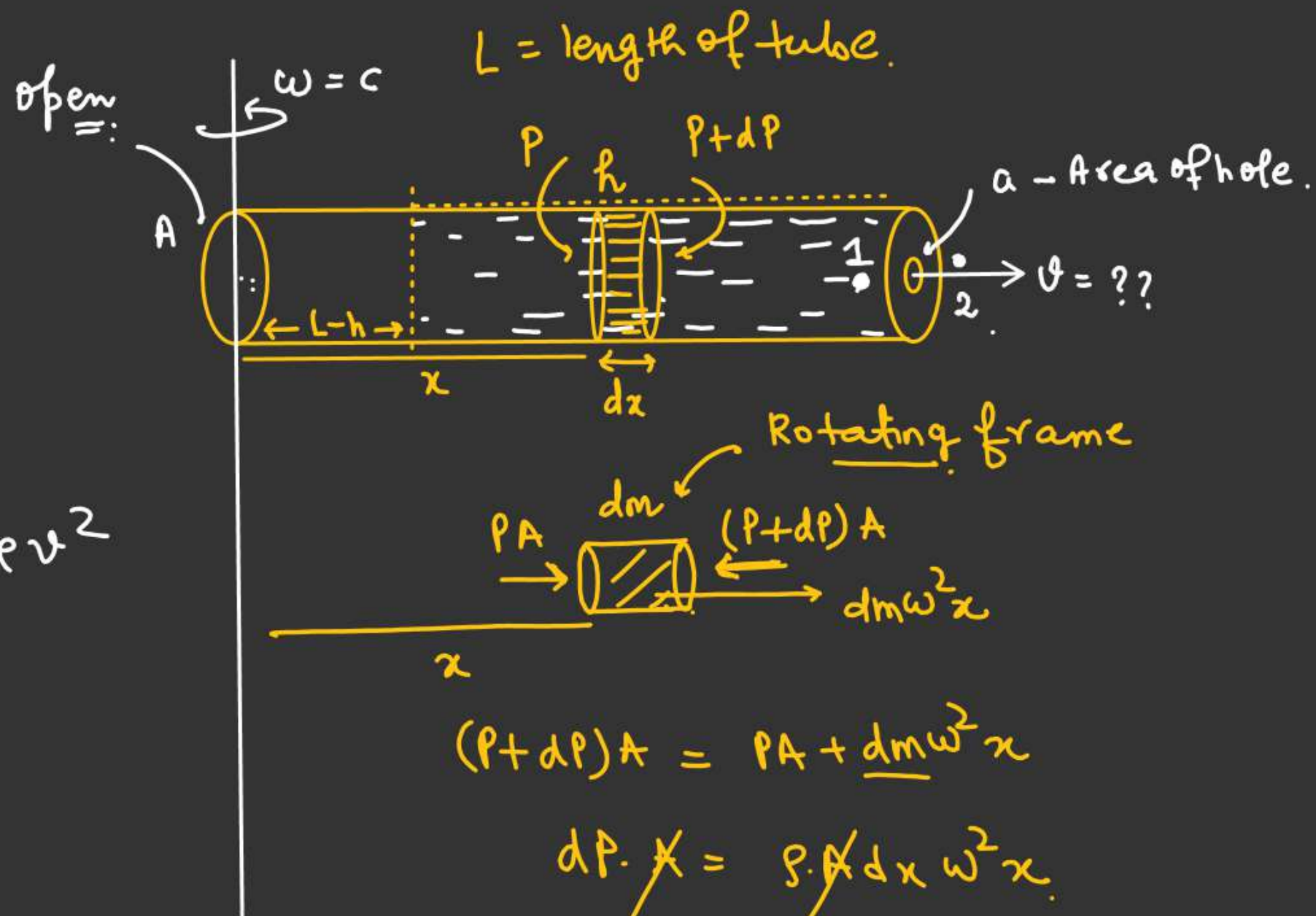
Bernoulli's b/w 1 & 2.

$$P_1 = P_{atm} + \frac{1}{2} \rho v^2$$

$$\cancel{P_{atm}} + \frac{\rho \omega^2}{2} (2Lh - h^2) = \cancel{P_{atm}} + \frac{1}{2} \rho v^2$$

$$\sqrt{\omega^2 (2Lh - h^2)} = v$$

$$\left[ v = \omega h \sqrt{\frac{2L}{h} - 1} \right]$$



$$(P + dP)A = PA + \underline{dm\omega^2 x}$$

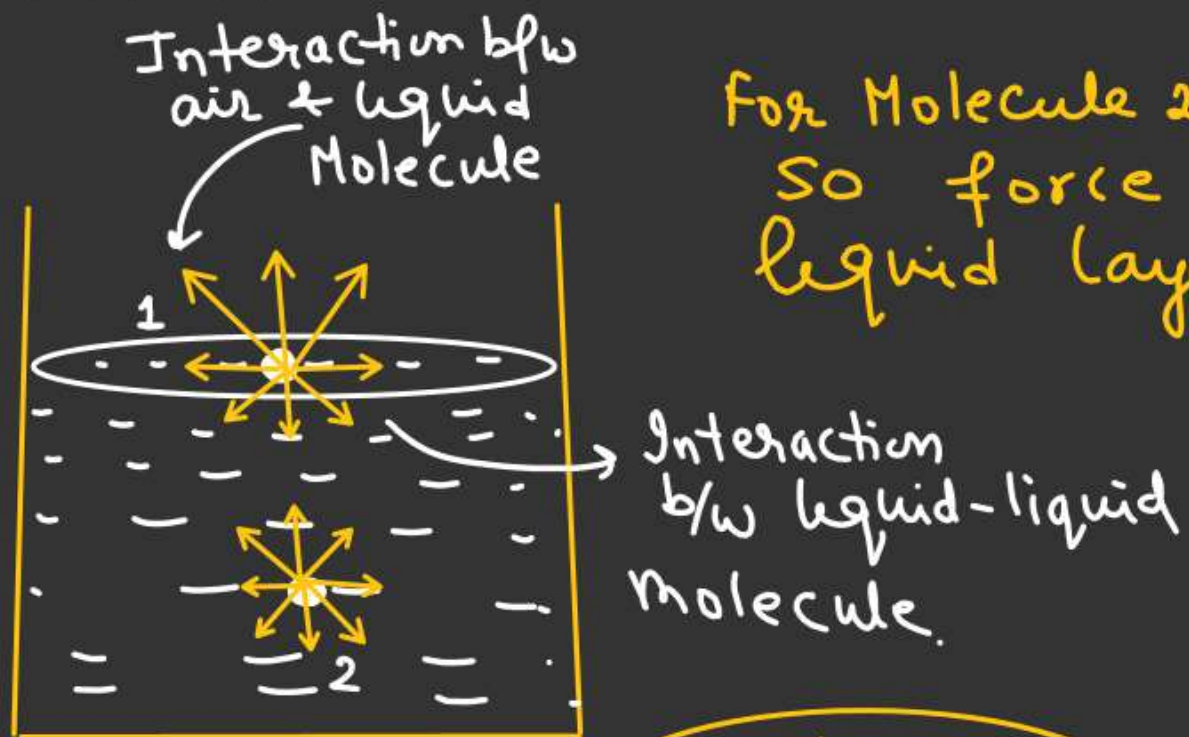
$$\cancel{dP \cdot A} = \cancel{P \cdot A} dx \omega^2 x$$

$$\int dP = \rho \omega^2 \int x dx$$

# SURFACE TENSION

Two type of forces.

- 1) Cohesive :- force of attraction b/w molecules of same nature.
- 2) Adhesive :- force of attraction b/w Molecules of different nature.



For Molecule 2 it is surrounded by liquid molecule so force of cohesion. No net force on the liquid layer containing molecule-2.

For Molecule 1 it is interacted with air molecule as well as liquid-molecule. So there is net force on surface layer, & it acts like a stretch membrane.

Surface tension  $T = \left( \frac{F_T}{L} \right)$





$$F = T \cdot L_{\text{eff}}$$

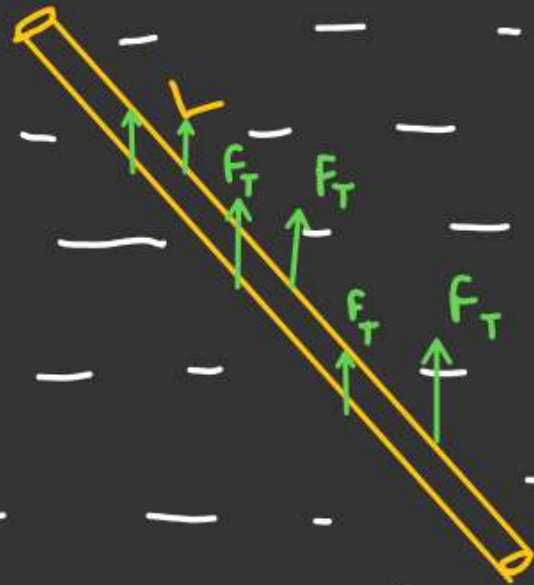
$L_{\text{eff}}$  = Effective length

$$L_{\text{eff}} = (n \times L)$$

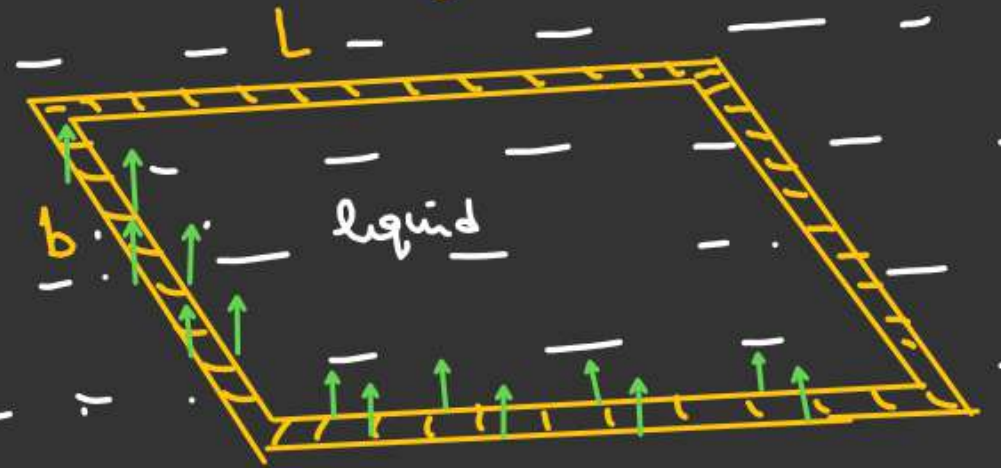
$n$  = No of Contact  
b/w body and liquid.

$L$  = length of body in  
contact with liquid

$$F_T = (2TL)$$



Rectangular  
wire frame.



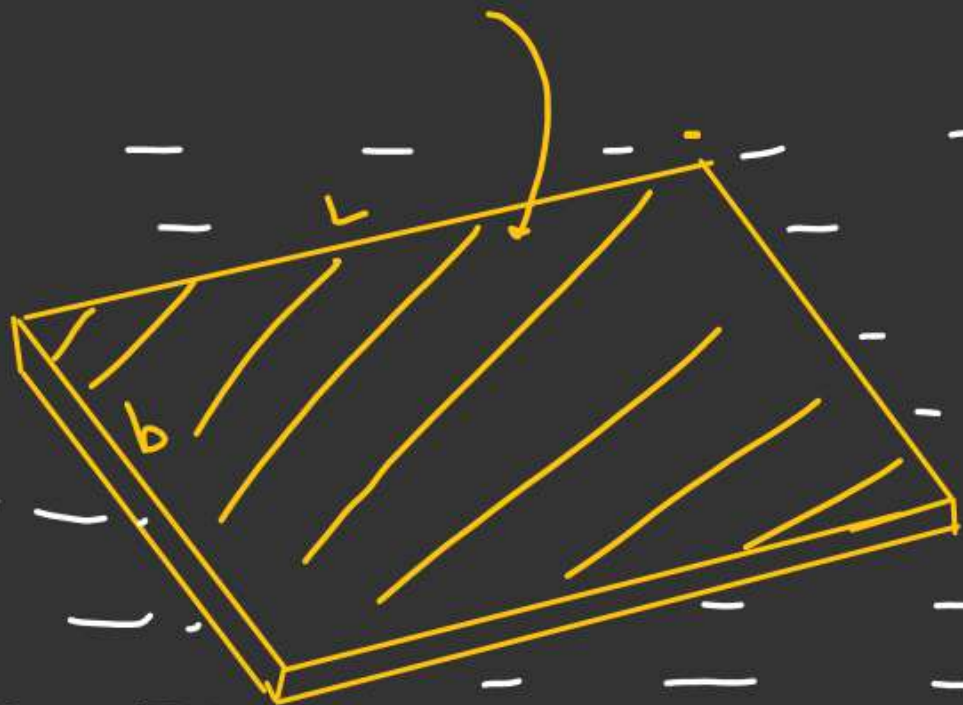
$$F = T[2(L+b)] \times 2$$

$$F = 4T(L+b)$$

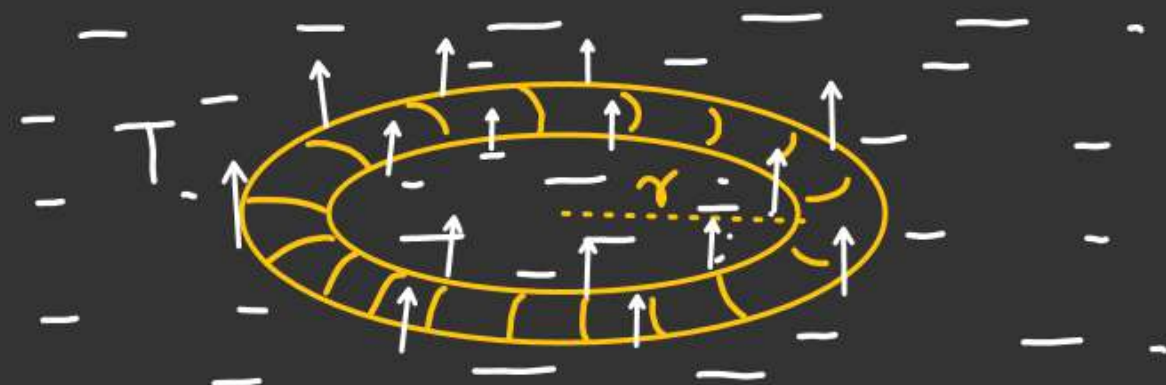




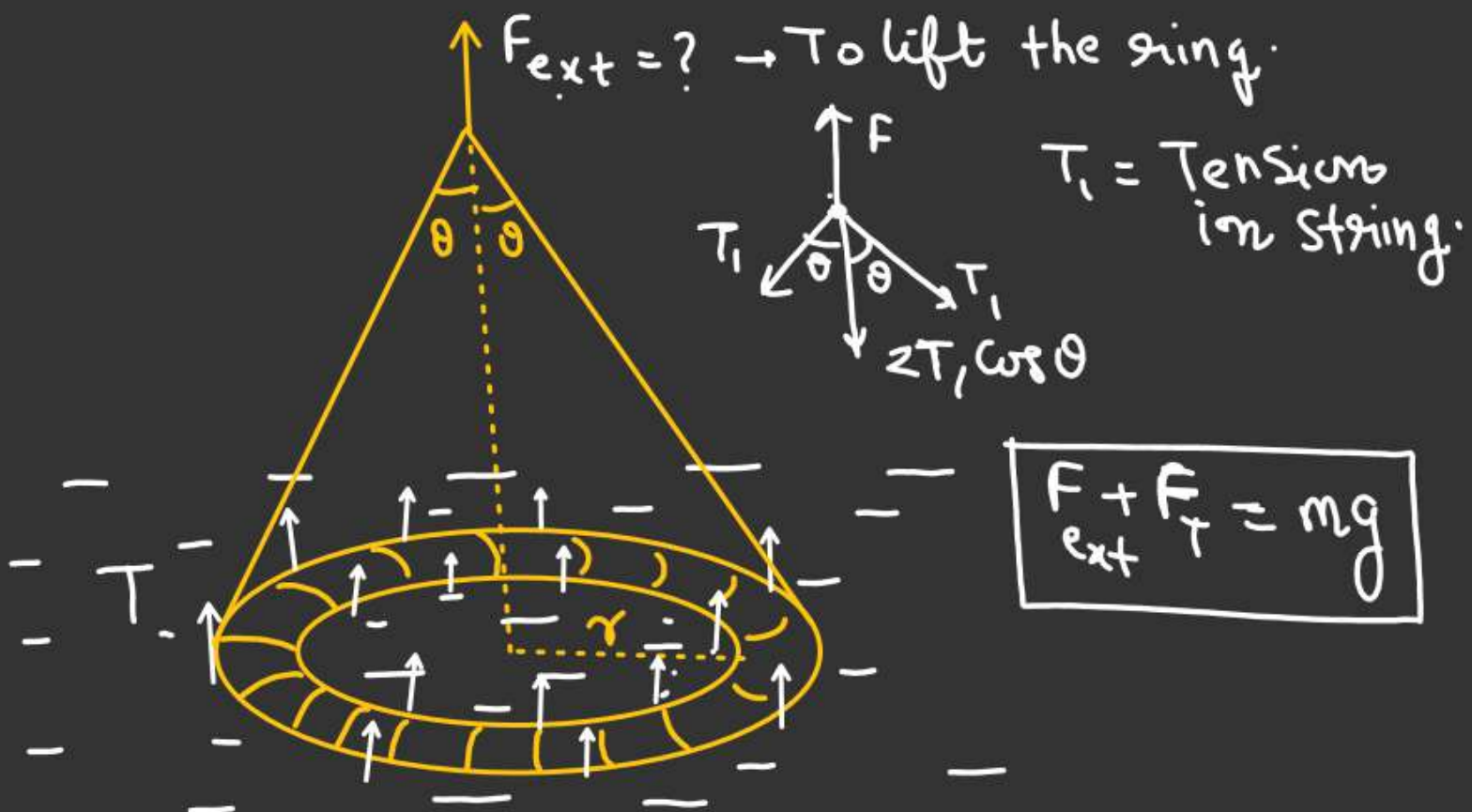
Sheet.

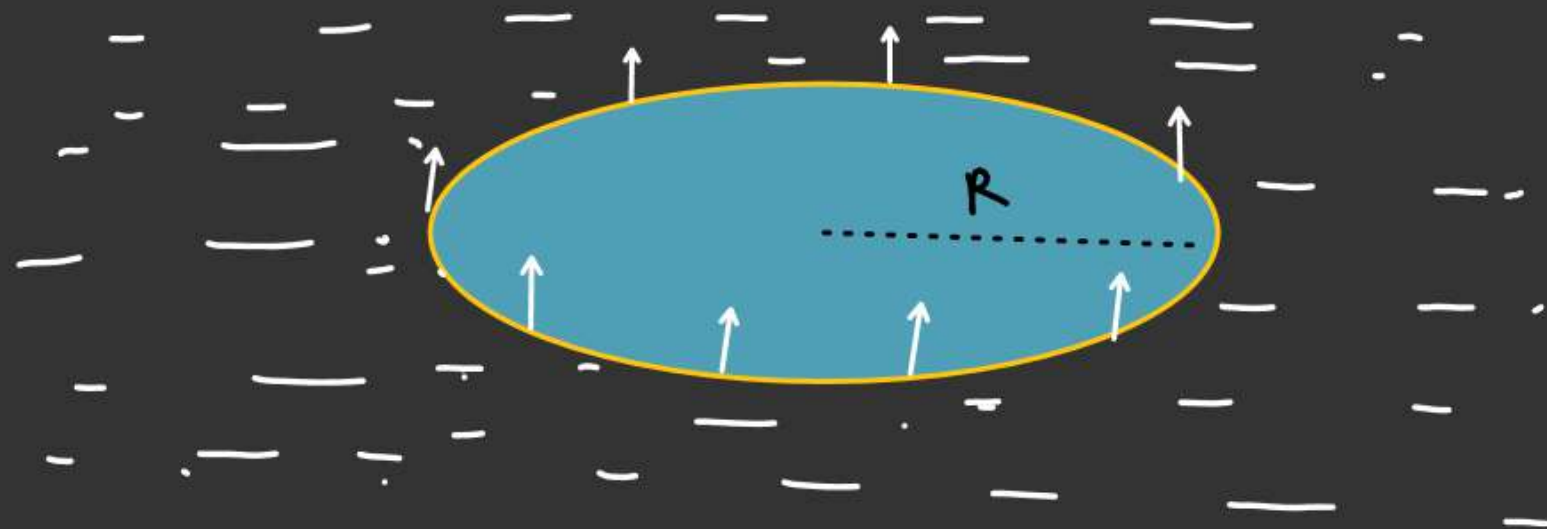


$$F = 2T(L+b)$$

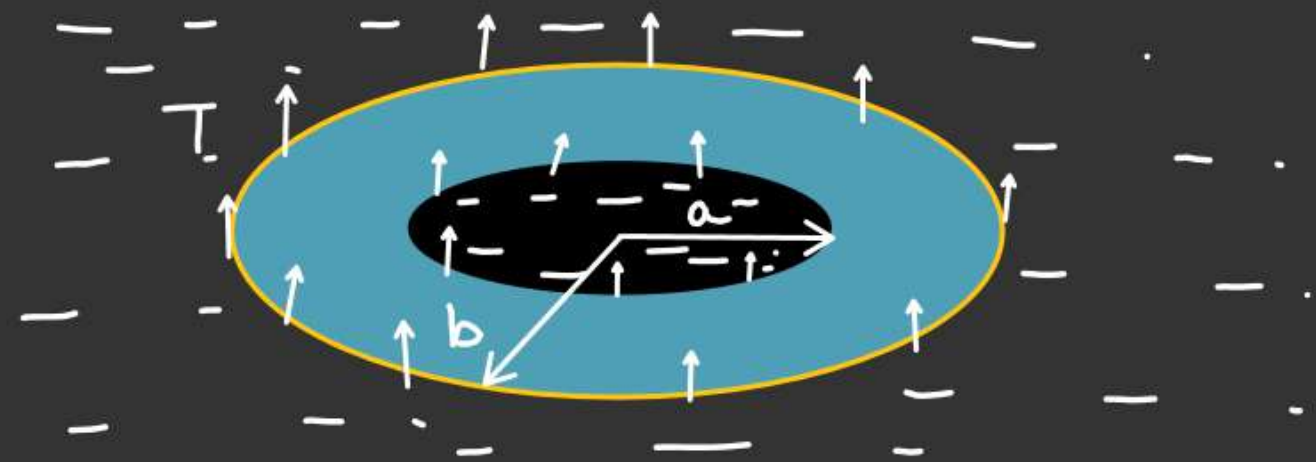


$$F_T = [T \times 2\pi r \times 2]$$





$$F_T = T \times 2\pi R$$



$$F_T = T 2\pi b + T \times 2\pi a$$

$$F_T = \underline{T 2\pi \cdot (b+a)} \checkmark$$