

## Heat transfer in case of Variable Cross-sectional area

At a radial distance  $r$ , a spherical shell of  $dr$  thickness is cut

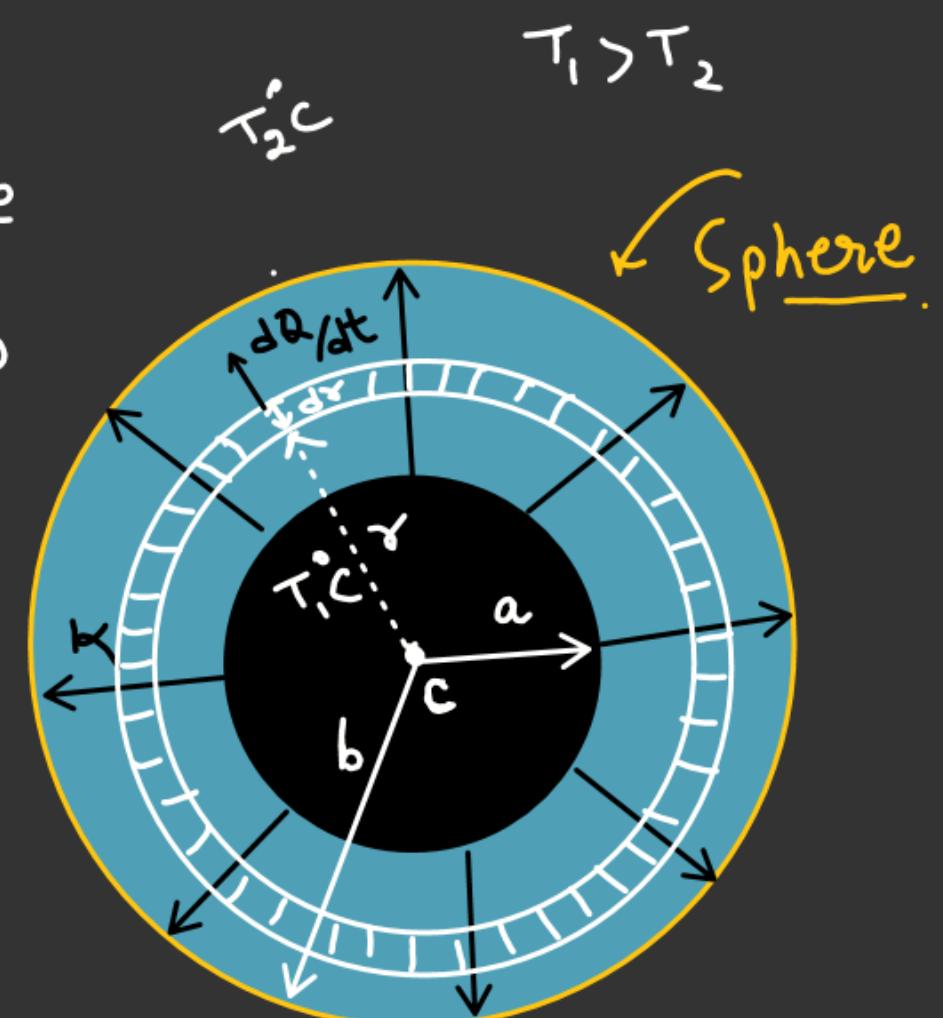
if  $\left(\frac{dQ}{dt}\right)$  be the heat flow at the time of Steady state

$$P \text{ J/s} \quad \left\langle \left( \frac{dQ}{dt} \right) = -K \cdot 4\pi r^2 \left( \frac{dT}{dr} \right) \right\rangle \quad \begin{array}{l} dT \text{ be the temp} \\ \text{difference for } dr \\ \text{thickness of the} \\ \text{shell.} \end{array}$$

↓  
??

$$P = -K \cdot 4\pi r^2 \left( \frac{dT}{dr} \right)$$

$$P \int_a^b \frac{dr}{r^2} = -4\pi K \int_{T_1}^{T_2} dT$$



Heat transfer in case of Variable Cross-sectional area

$$P \int_a^b \frac{dr}{r^2} = - 4\pi K \int_{T_1}^{T_2} dT \quad (i = \frac{\Delta V}{R})$$

$$P \left[ -\frac{1}{r} \right]_a^b = - 4\pi K (T_2 - T_1)$$

$$P \left[ -\frac{1}{b} + \frac{1}{a} \right] = 4\pi K (T_1 - T_2)$$

$$P = \left[ \frac{\frac{(T_1 - T_2)}{1}}{4\pi K \left( \frac{1}{a} - \frac{1}{b} \right)} \right] \quad R_{th} = \frac{1}{4\pi K} \left( \frac{1}{a} - \frac{1}{b} \right)$$

$T_1 > T_2$   
Sphere

## Heat transfer in case of Variable Cross-sectional area

if K is Variable,  $K = \underline{K_0 r}$   $r \rightarrow$  radial distance

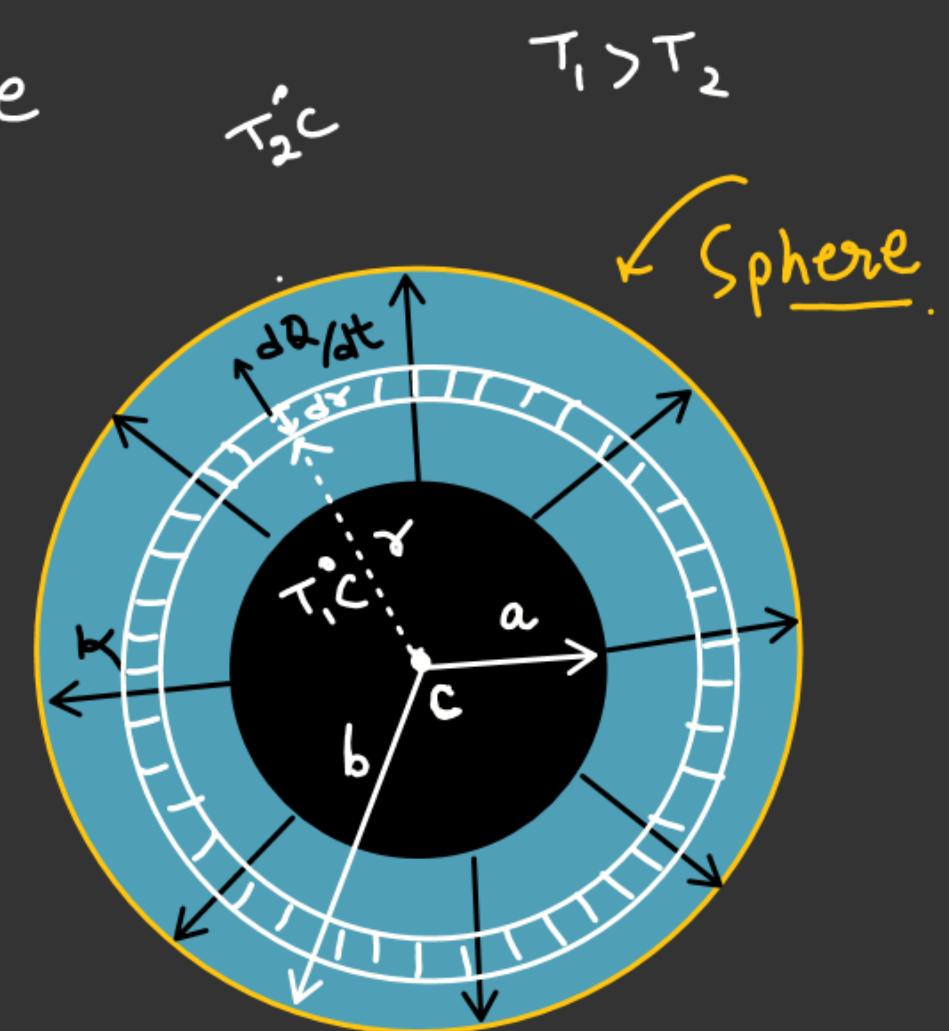
$$\frac{dQ}{dt} = - K_r 4\pi r^2 \left( \frac{dT}{dr} \right)$$



$$P = - K_0 4\pi r^3 \frac{dT}{dr}$$

$$P \int_{a}^{b} \frac{dr}{r^3} = - K_0 4\pi \int_{T_1}^{T_2} dT$$

$$P = \checkmark$$



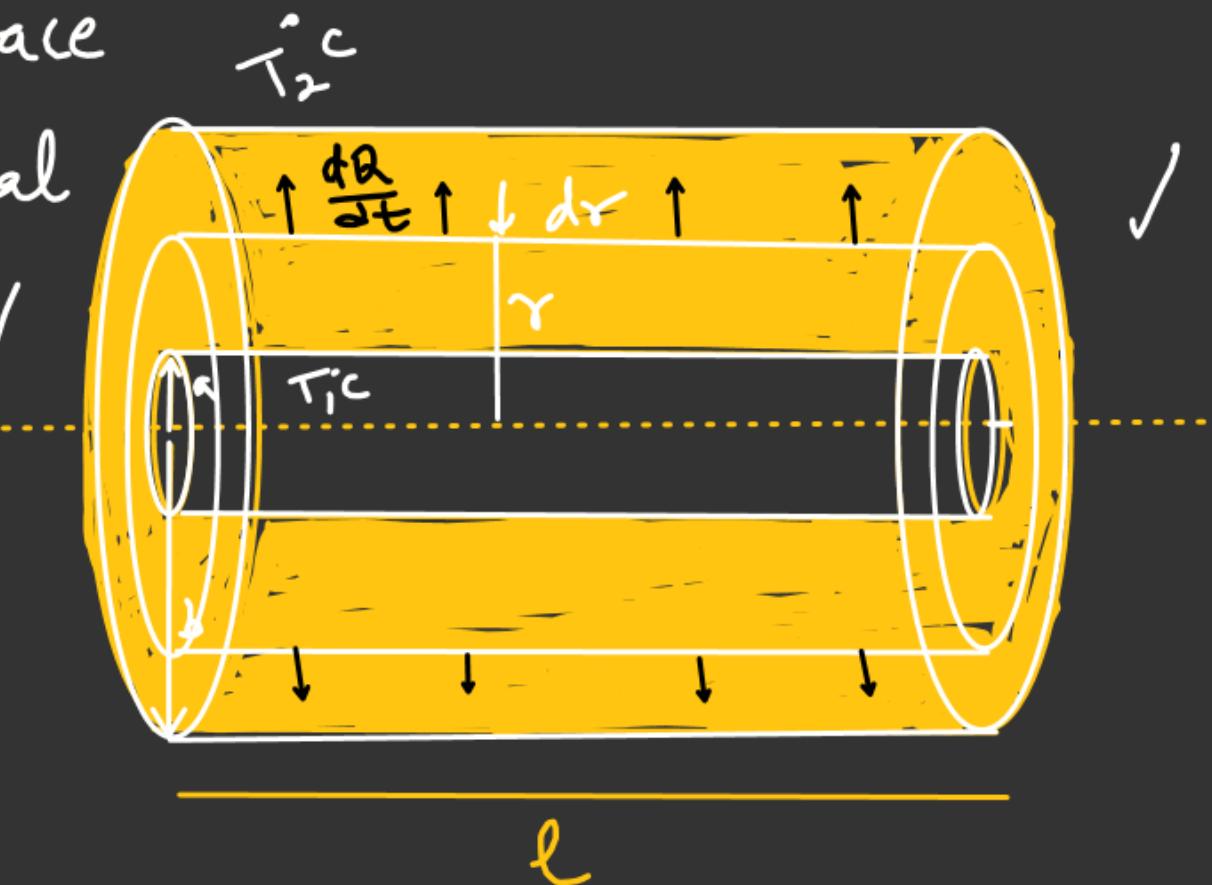


## Heat flow through Cylindrical Cross sectional area

$$P \text{ J/s} \leftarrow \frac{dQ}{dt} = -K(2\pi rl) \frac{dT}{dr}$$

A → Curve Surface  
area of  
Cylindrical  
Shell.

$dT \rightarrow$  temp difference for  $dr$   
thickness of shell.



$$P = -K2\pi l \left( \frac{T_2 - T_1}{r} \right) dT$$

$$P \int_a^b \frac{dr}{r} = - (2\pi l) K \int_{T_1}^{T_2} dT$$

$$P \int_a^b \frac{dr}{r} = - (2\pi l) \underbrace{k}_{K} \int_{T_1}^{T_2} dT$$

R-W

$K = K_0 r$	$r \rightarrow \text{radial distance}$
$K = k_0 / r$	
$K = K_0 + \alpha r$	

Find  $\frac{dQ}{dt} = ??$

$$P \ln\left(\frac{b}{a}\right) = - 2\pi k l (T_2 - T_1)$$

$P = \frac{(T_1 - T_2)}{\frac{1}{2\pi k l} \ln\left(\frac{b}{a}\right)}$

$i_{th}$

$R_{th}$

$$R_{th} = \frac{1}{2\pi k l} \ln\left(\frac{b}{a}\right)$$

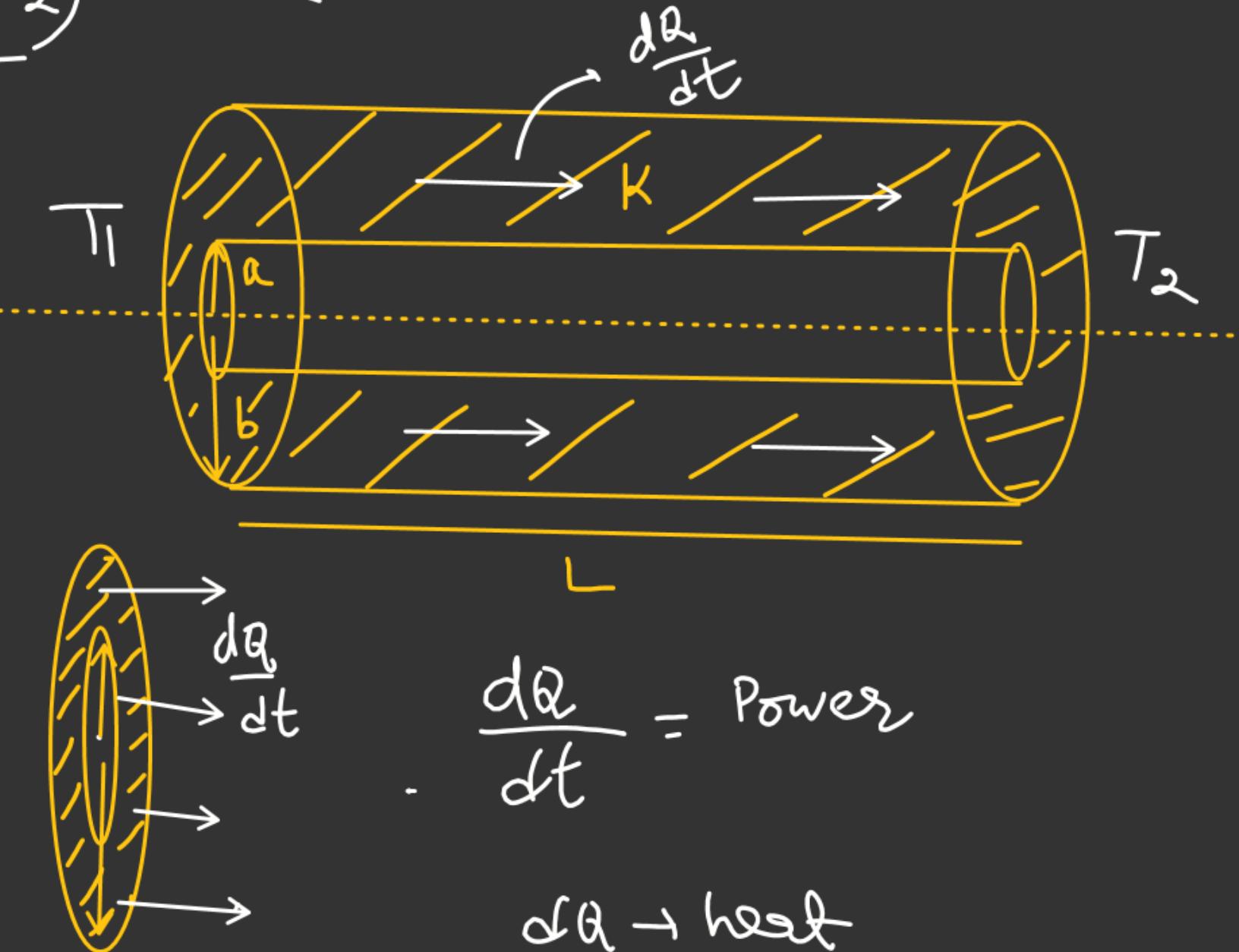
Thermal resistance of a  
Cylindrical conductor.

$$\frac{\Delta Q}{\Delta t} = \frac{dQ}{dt} = \frac{K \pi (b^2 - a^2) (T_1 - T_2)}{L} \quad T_1 > T_2$$

↓  
P TS

$$P = \frac{T_1 - T_2}{\left( \frac{L}{K \pi (b^2 - a^2)} \right)}$$

↓  
R<sub>th</sub>





Case when one end of temperature of rod is a function of time

$$T_B = (20 + 2t)$$

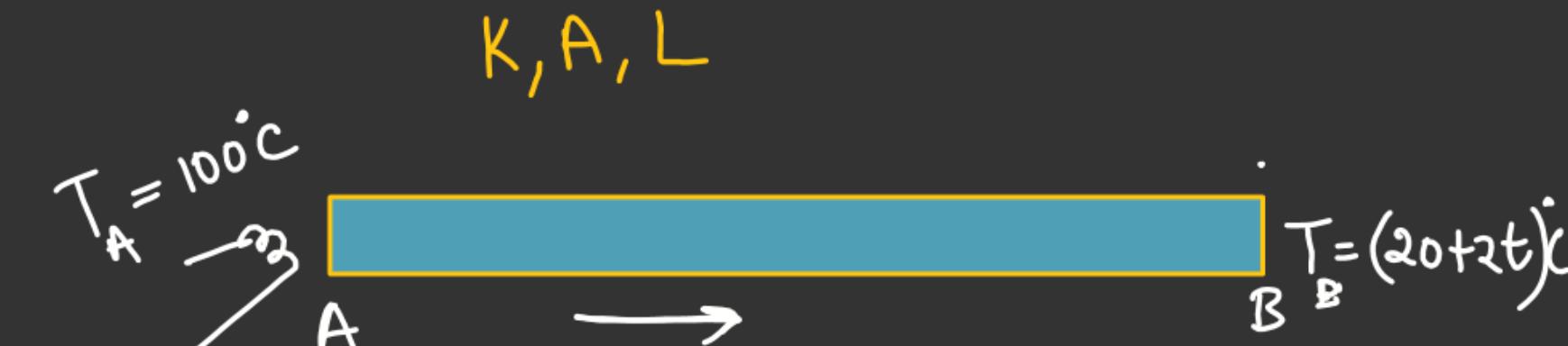
$t \rightarrow$  time.

Total heat flow from A to B

$$\left( \frac{dQ}{dt} \right) = KA \left( \frac{100 - (20 + 2t)}{L} \right)$$

$$Q \frac{dQ}{dt} = \frac{KA}{L} (80 - 2t)$$

$$\int_0^Q dQ = \frac{KA}{L} \int_0^{40} (80 - 2t) dt$$



Heat Continue to flow from A to B until & unless

$$T_A = T_B$$

$$100 = 20 + 2t$$

$$\frac{80}{2} = t$$

$$t = 40 \text{ sec. } \checkmark$$



$$\int_0^Q dQ = \frac{KA}{L} \int_0^{40} (80 - 2t) dt$$

$$Q = \frac{KA}{L} \left\{ 80[t]_0^{40} - \cancel{\frac{2[t^2]}{2}}_0^{40} \right\}$$

$$Q = \frac{KA}{L} \left\{ 3200 - 1600 \right\}$$

$$Q = \left( 1600 \frac{KA}{L} \right) J \quad \checkmark$$

 Case When Conductive of rod is a function of distance from end A.

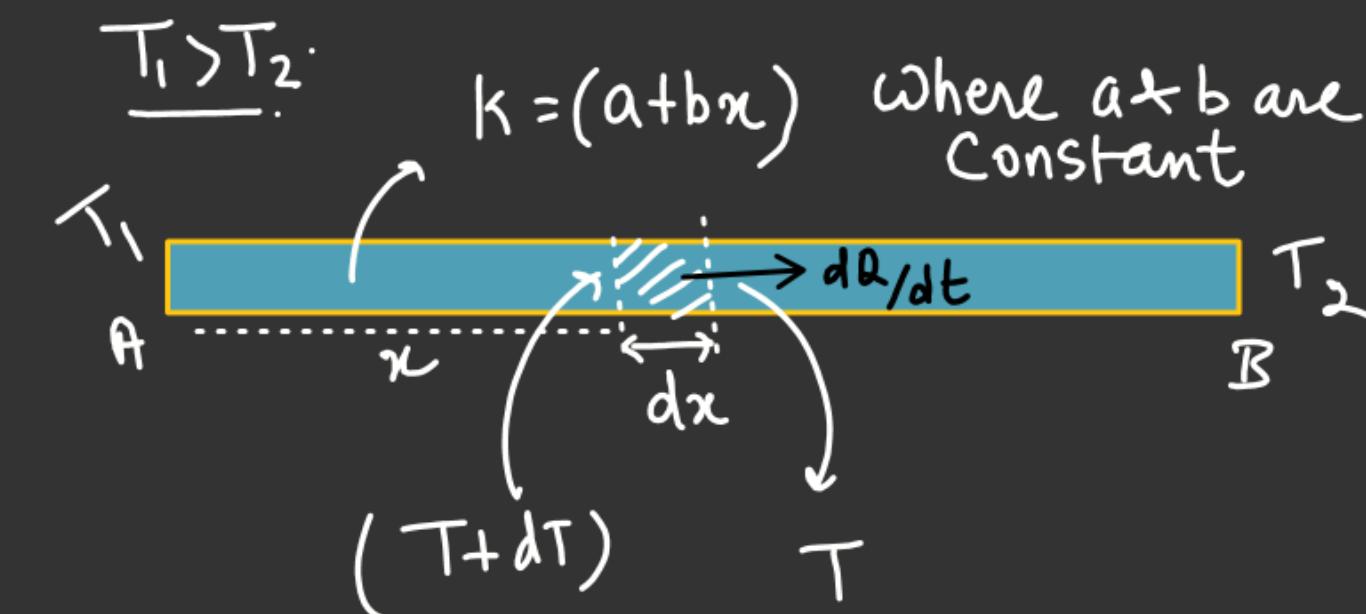
For  $dx$  length of rod.

$$\frac{dQ}{dt} = -\frac{K_x A}{dx} \left( \frac{dT}{dx} \right)$$

||

$$P = -(a+bx)A \cdot \left( \frac{dT}{dx} \right)$$

$$P \int_0^L \frac{dx}{a+bx} = -A \int_{T_1}^{T_2} dT$$



$$P \frac{\ln[a+bx]_0^L}{b} = -A(T_2 - T_1)$$

$$P = \left[ \frac{bA(T_1 - T_2)}{\ln(a+bx)_0^L} \right] \left[ \int \frac{dx}{a+bx} = \ln(a+bx) \frac{0}{b} \right]$$

Total rate  
of heat flow = :



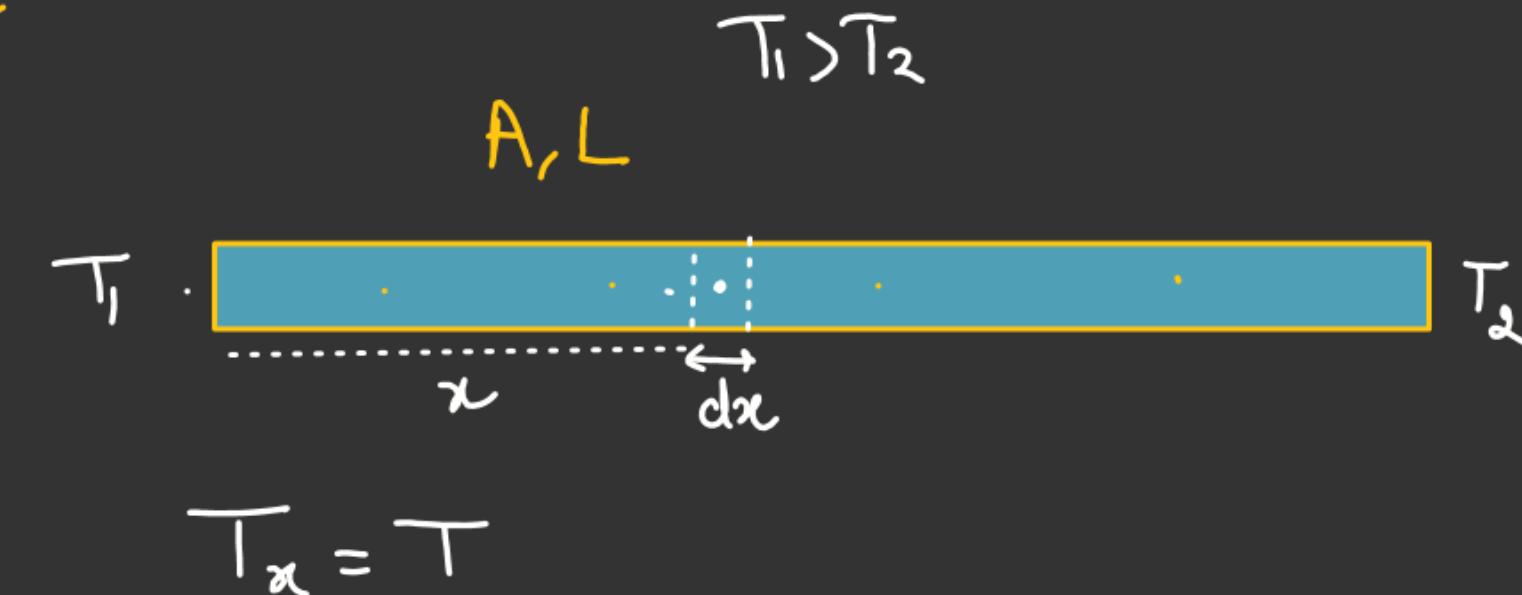
Case when thermal conductivity of rod as a function of temp of the rod

$$K = \left( \frac{\alpha}{T} \right) \quad \alpha = \text{Constant}$$

$$\left( \frac{dQ}{dt} \right) = - K A \left( \frac{dT}{dx} \right)$$

$$P = - \frac{\alpha}{T} A \frac{dT}{dx}$$

$$P \int dx = - \alpha A \int_{T_1}^{T_2} \left( \frac{dT}{T} \right)$$



$$P(L) = - \alpha A \ln \left( \frac{T_2}{T_1} \right)$$

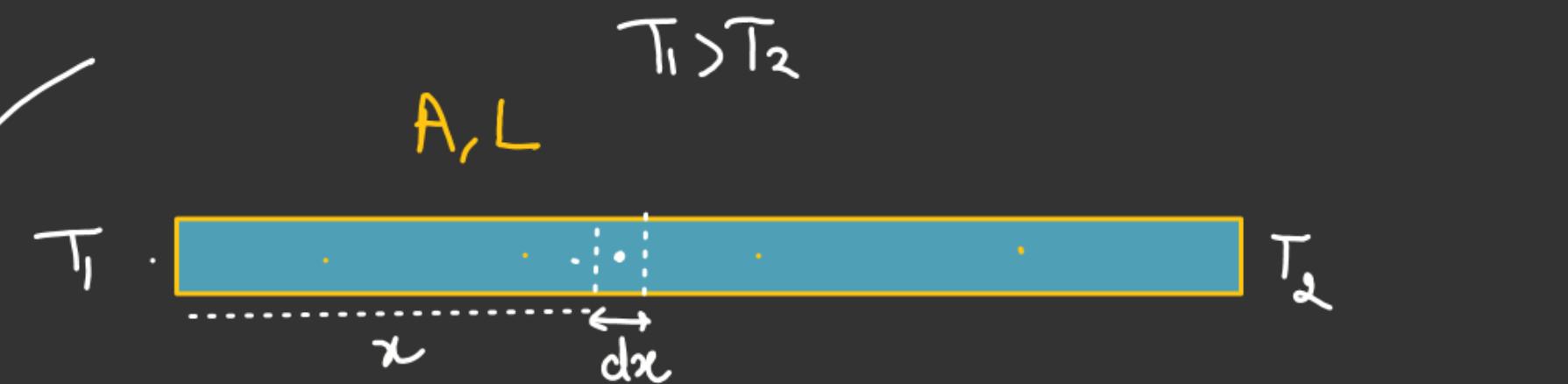
$$P = \frac{\alpha A}{L} \ln \left( \frac{T_1}{T_2} \right)$$



Case when thermal conductivity of rod as a function of temp of the rod

$$\checkmark K = \left( \frac{\alpha}{T} \right) \quad \alpha = \text{constant}, \quad \checkmark$$

$T \rightarrow f(x) = ??$



$$\left( \frac{dQ}{dt} \right) = -K A \left( \frac{dT}{dx} \right)$$

$$P = -\frac{\alpha}{T} A \frac{dT}{dx}$$

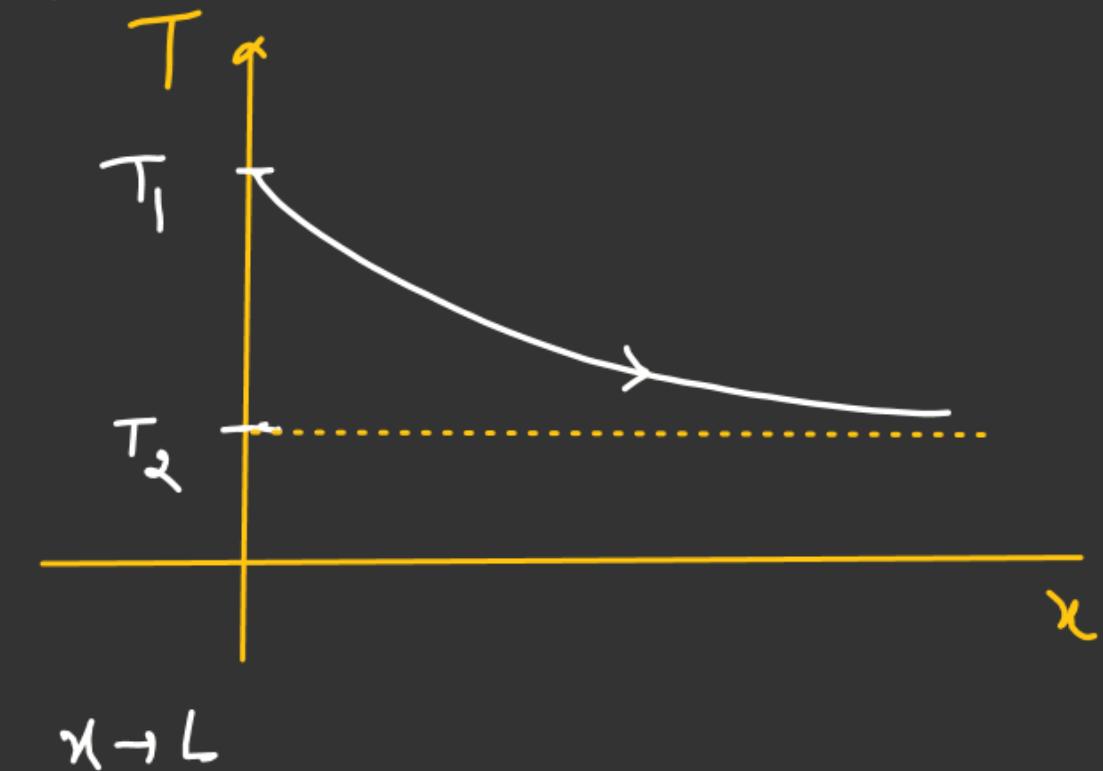
$$P \int_0^x dx = -\alpha A \int_{T_1}^T \left( \frac{dT}{T} \right)$$

$$P x = -\alpha A \ln\left(\frac{T}{T_1}\right)$$

$$-\frac{P}{\alpha A} x = \ln\left(\frac{T}{T_1}\right)$$

$$\frac{T}{T_1} = e^{-\frac{P}{\alpha A} x}$$

$$T = T_1 e^{-\frac{P}{\alpha A} x}$$





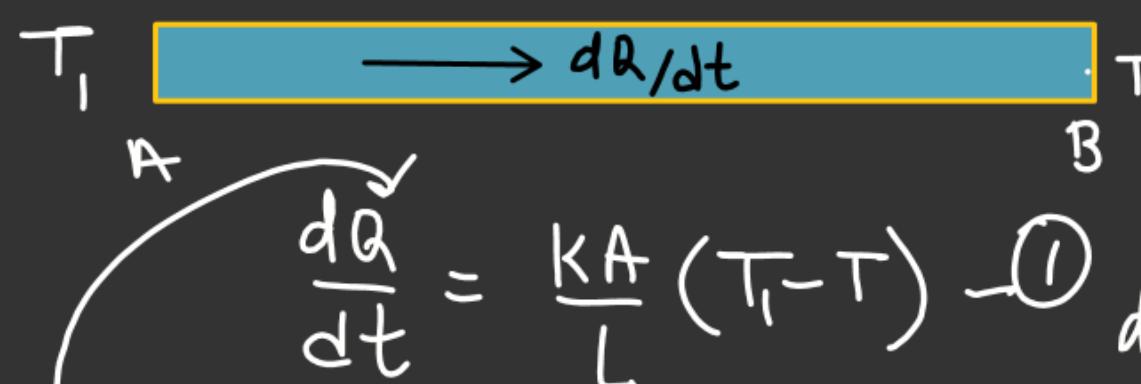
## Heat flow in a Sink

At  $t=0$ ,  $T_1$  &  $T_2$  be the temp of end A & B.

Let, at any time 't' temp of end B or sink be  $T$ .

### Equation of Rod

$K, A, L$

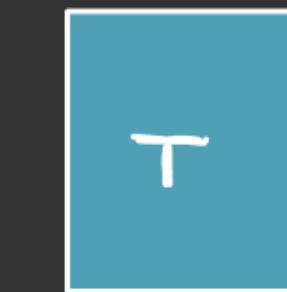


$$\frac{dQ}{dt} = \frac{KA}{L} (T_1 - T) \quad \text{--- (1)}$$

### Equation of Sink

$$dQ = (msdT) \quad \text{--- (2)}$$

$m, s(t)$



$$dQ \rightarrow (T + dT) \quad (t + dt)$$

$T_1 > T_2$

$t=0$

$K, A, L$

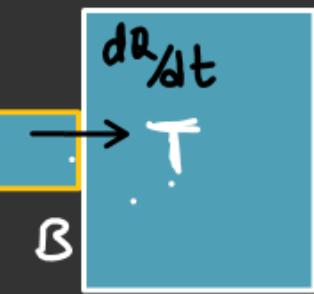


$m, s$



$t=t$

$K, A, L$



$\uparrow$   
Sink

$$\checkmark \quad (dQ = msdT)$$

↓  
Specific heat  
 $ms \rightarrow \text{heat capacity}$



$$\frac{dQ}{dt} = \frac{KA}{L} (T_1 - T) \quad \textcircled{1}$$

Equation of Sink

$$dQ = (m_s dT) \quad \textcircled{2}$$

From ① & ②

$$\frac{\ln [T_1 - T]_T}{(-1)} = \frac{KA}{m_s L} t$$

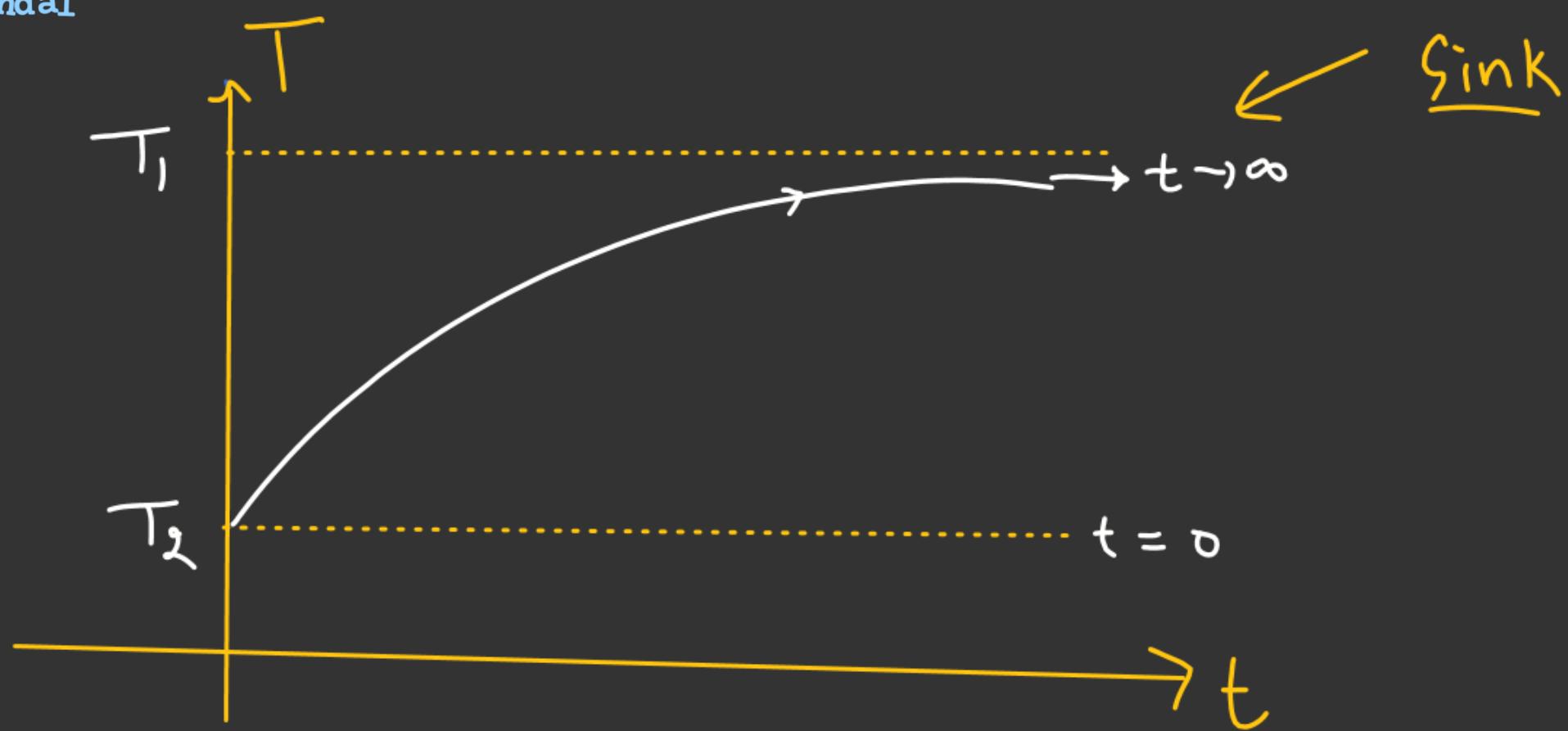
$$\ln (T_1 - T) - \ln (T_1 - T_2) = \frac{-KA}{m_s L} t$$

$$\int_{T_2}^T \frac{dT}{T_1 - T} = \frac{KA}{m_s L} \int_0^t dt$$

$$\ln \left( \frac{T_1 - T}{T_1 - T_2} \right) = - \frac{KA}{m_s L} t$$

$$T_1 - T = (T_1 - T_2) e^{-\frac{KA}{m_s L} t}$$

$T = T_1 - (T_1 - T_2) e^{-\frac{KA}{m_s L} t}$

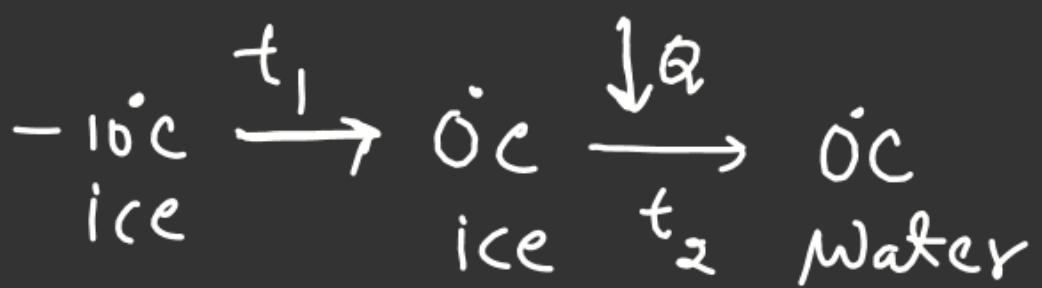




Find time 't' to melt  
the ice Cube.



$$t = \left( t_1 + t_2 \right)$$



$$(Q = m L_f)$$