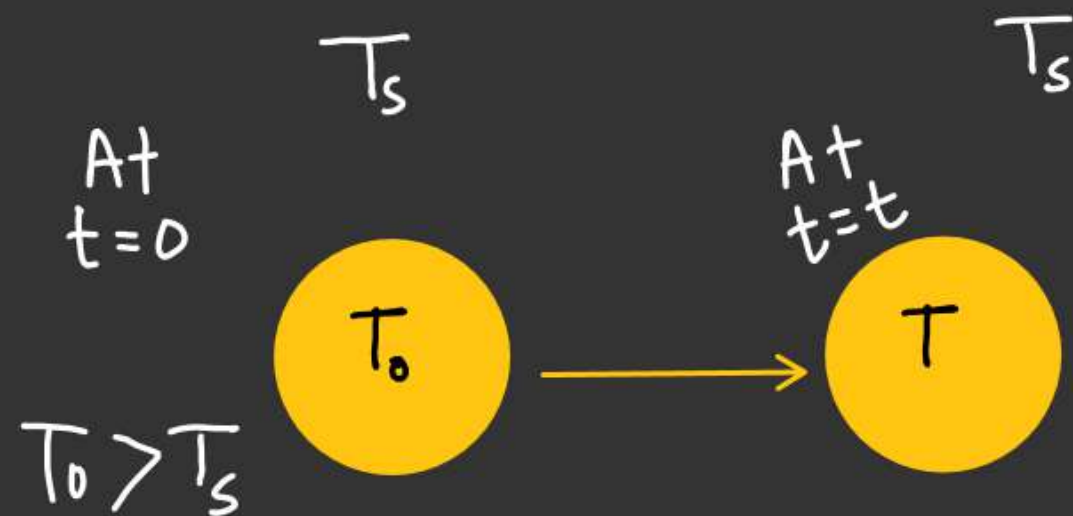


Newton's Law of Cooling

$$-\frac{dT}{dt} = K(T - T_s)$$



$$-\int_{T_0}^T \frac{dT}{T - T_s} = K \int_0^t dt$$

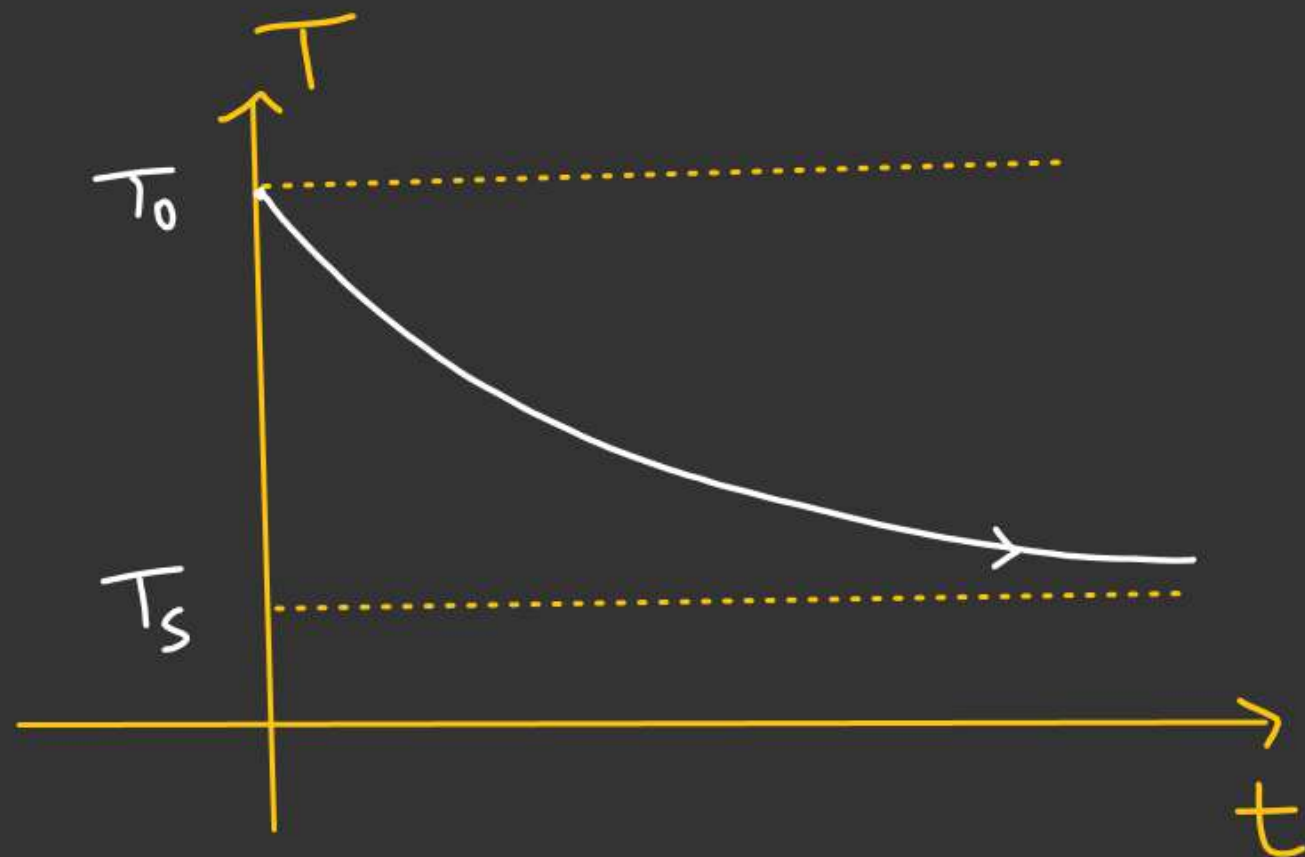
$$-\ln[T - T_s]_{T_0}^T = Kt$$

$$\ln\left(\frac{T - T_s}{T_0 - T_s}\right) = -Kt$$

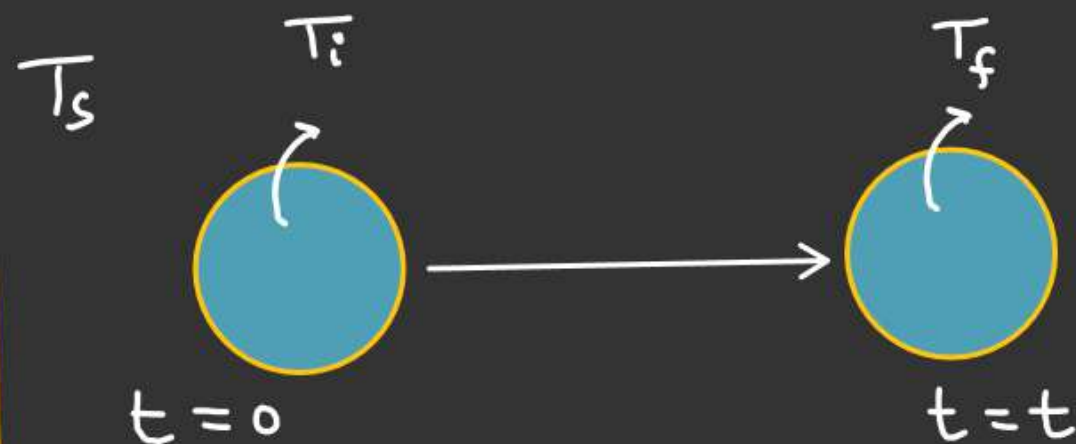
$$T - T_s = (T_0 - T_s)e^{-Kt}$$

$$T = T_s + (T_0 - T_s)e^{-Kt}$$

$$\underline{T = T_s} \text{ when } t \rightarrow \infty.$$



Avg form of Newton's Law of Colling



$$-\frac{dT}{dt} = K(T - T_s)$$

$$T = \left(\frac{T_i + T_f}{2} \right)$$

$$-\frac{\Delta T}{t} = K \left(\frac{T_i + T_f}{2} - T_s \right) \quad \begin{matrix} dT \rightarrow \Delta T \\ dt \rightarrow t \end{matrix}$$

$$\frac{T_i - T_f}{t} = K \left(\frac{T_i + T_f}{2} - T_s \right)$$

$$\frac{T_i - T_f}{t} = K \left(\frac{T_i + T_f}{2} - T_s \right)$$

↙
Avg. Method.

#

$$T_s = 16^\circ\text{C}$$



M-1

Integration Method. , At $t = t$, body temp be T

$$-\frac{dT}{dt} = K(T - T_s)$$

$$-\int_{40}^{36} \frac{dT}{T - T_s} = K \int_{0}^5 dt \rightarrow$$

\Downarrow
 $??$

$$T_s = 16^\circ\text{C}.$$

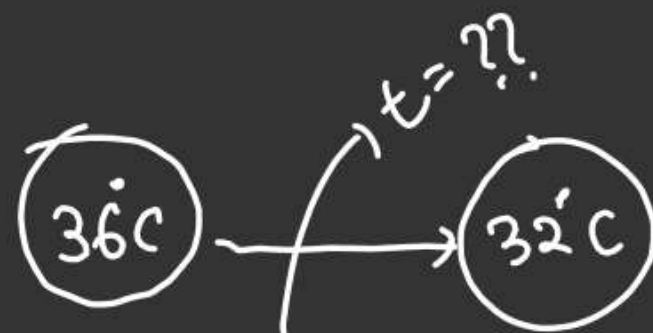
$$-\int_{40}^{36} \frac{dT}{T - T_s} = K \int_0^5 dt \rightarrow$$

$$-\ln[T - T_s]_{40}^{36} = 5K$$

$$-\ln\left[\frac{20}{24}\right] = 5K$$

$$-\ln\left(\frac{5}{6}\right) = 5K$$

$$K = \frac{1}{5} \ln\left(\frac{6}{5}\right) \checkmark$$



$$-\int_{36}^{32} \frac{dT}{T - T_s} = K \int_0^t dt$$

↓

$$t = ?? \checkmark$$

M-2

Avg. Method

$$\frac{dT}{dt} \rightarrow \frac{T_i - T_f}{t} = K \left[\left(\frac{T_i + T_f}{2} \right) - T_s \right]$$

↓ T

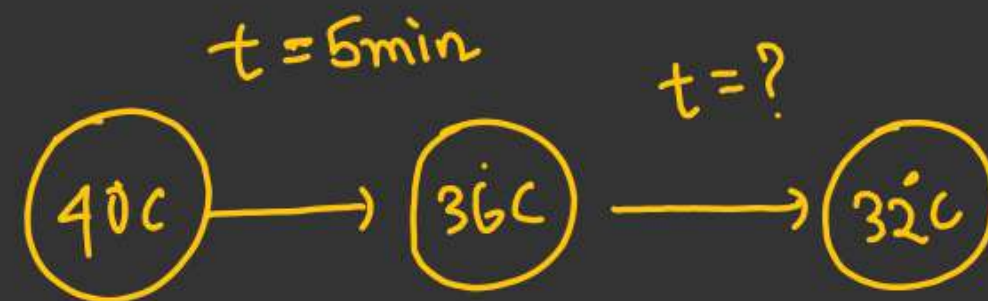
 $\frac{dT}{dt}$

← t

$$\left(\frac{40 - 36}{5} \right) = K \left[\left(\frac{40 + 36}{2} \right) - 16 \right]$$

$$K = \frac{0.8}{22} \text{ min}^{-1}$$

$$K = \frac{8}{220} = \frac{2}{55} \text{ min}^{-1}$$



$$\frac{36 - 32}{t} = \left(\frac{2}{55} \right) \left(\frac{36 + 32}{2} - 16 \right)$$

↓

t = ?? ✓

$$t = 6.1 \text{ min} \checkmark$$

THERMODYNAMICS

• System & Surrounding

↓
(The part under observation)

↓
(Other than System is surrounding)



→ (Cylinder + piston)
↓
System

THERMODYNAMICS

★ Thermodynamic Variables

⇒ By the help of which we can define state of any process

⇒ P, V, T, \rightarrow Three major thermodynamic variables.
 $(\Delta U, \Delta H)$

⇒ Thermodynamic variables are of two type —
State function
Path function

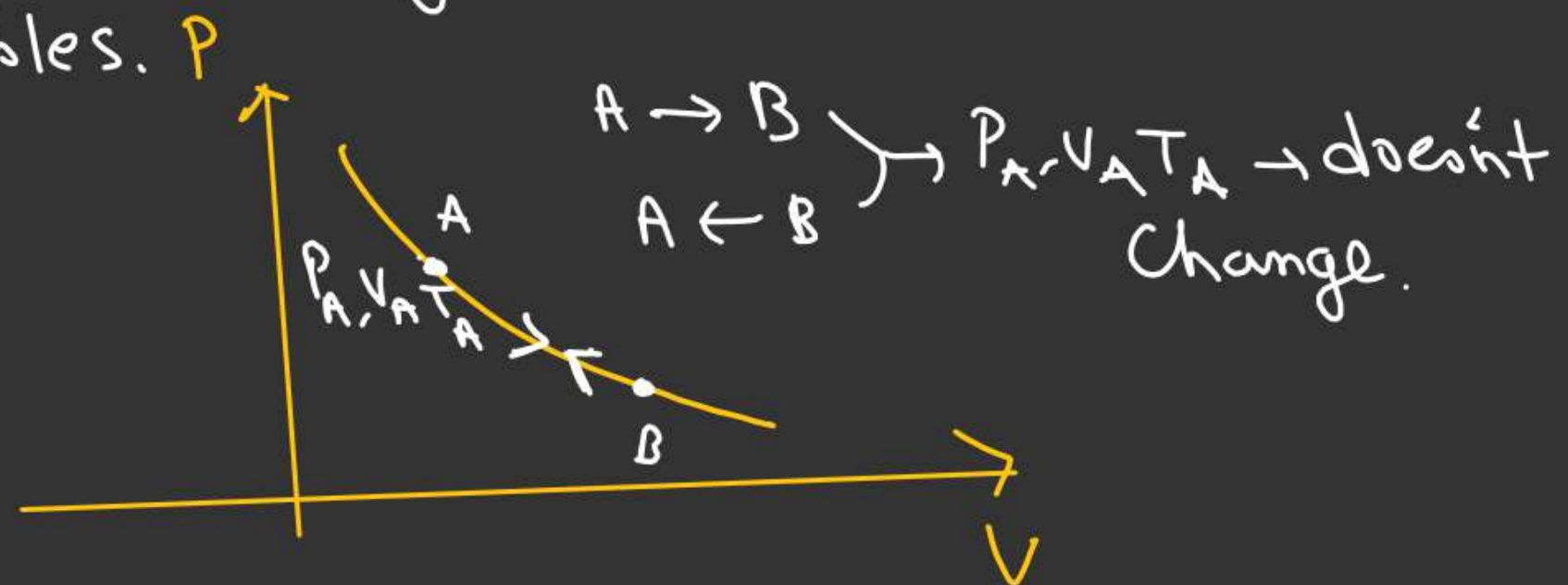
⇒ Variables which only depend on initial & final positions are called state function. Ex: $\Delta U,$

⇒ Variables which depend on the path. Ex $\rightarrow \Delta W$

THERMODYNAMICS

Reversible process

- Process occurs very slowly
- In Reversible process system is always in equilibrium with surrounding.
- In Reversible process we can again reach the thermodynamic variables.



THERMODYNAMICS

Internal Energy & Change in internal energy

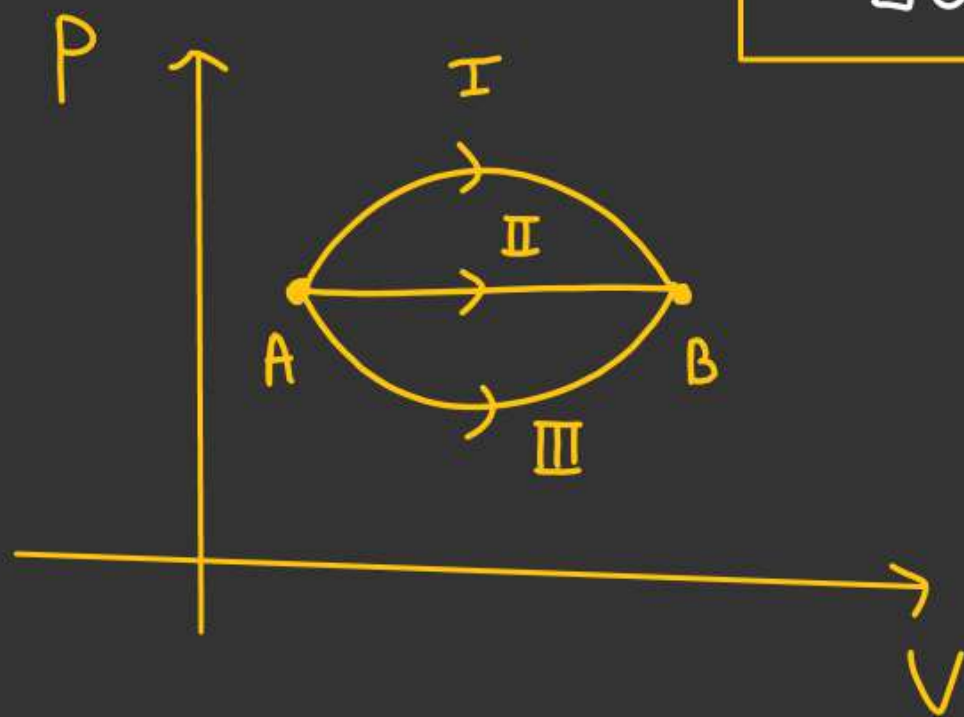
[Internal Energy of gas molecules is the sum of all the energy possess by gas molecules in the form of translational K-E, Rotational K-E & Vibrational energy]

[Internal Energy of a gas molecules is function of temperature].

$$\Delta U = (U_f - U_i) \rightarrow (\text{State function})$$

THERMODYNAMICS

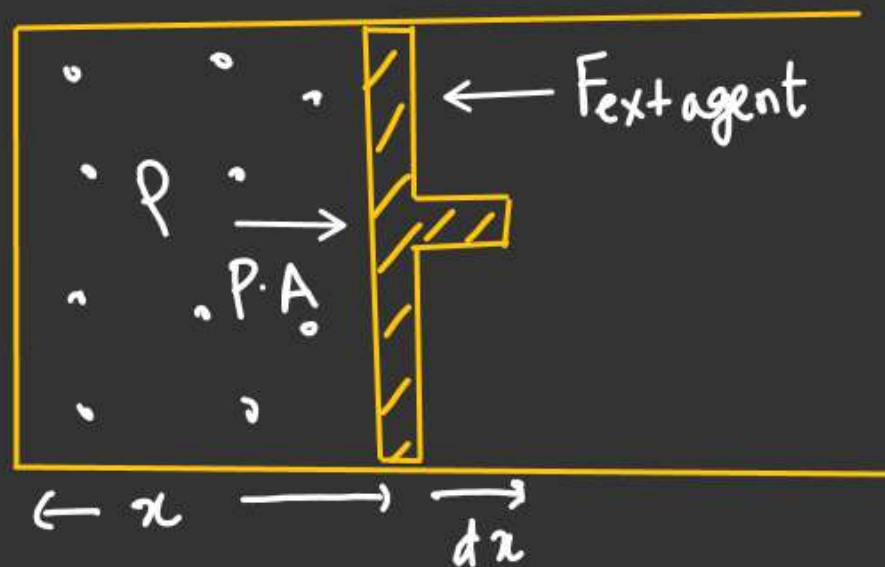
$$\Delta U_{\text{I}} = \Delta U_{\text{II}} = \Delta U_{\text{III}}$$



\Downarrow
 $\Delta U \rightarrow (\text{state function})$

THERMODYNAMICS

Work done (For reversible process)



Sign - Convention

$W_{\text{by the gas}} \rightarrow +ve$

$W_{\text{on the gas}} \rightarrow -ve$

$$\int dW_{\text{gas}} = \int P A dx$$

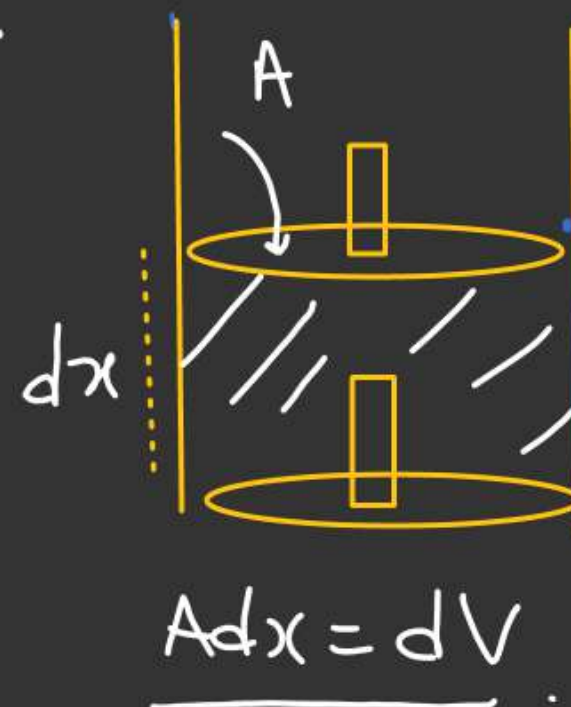
\Downarrow
 $dV \rightarrow \text{Change in Volume}$

$$W_{\text{gas}} = \int P dV$$

Since process is reversible

So, $P.A = F_{\text{ext agent}}$

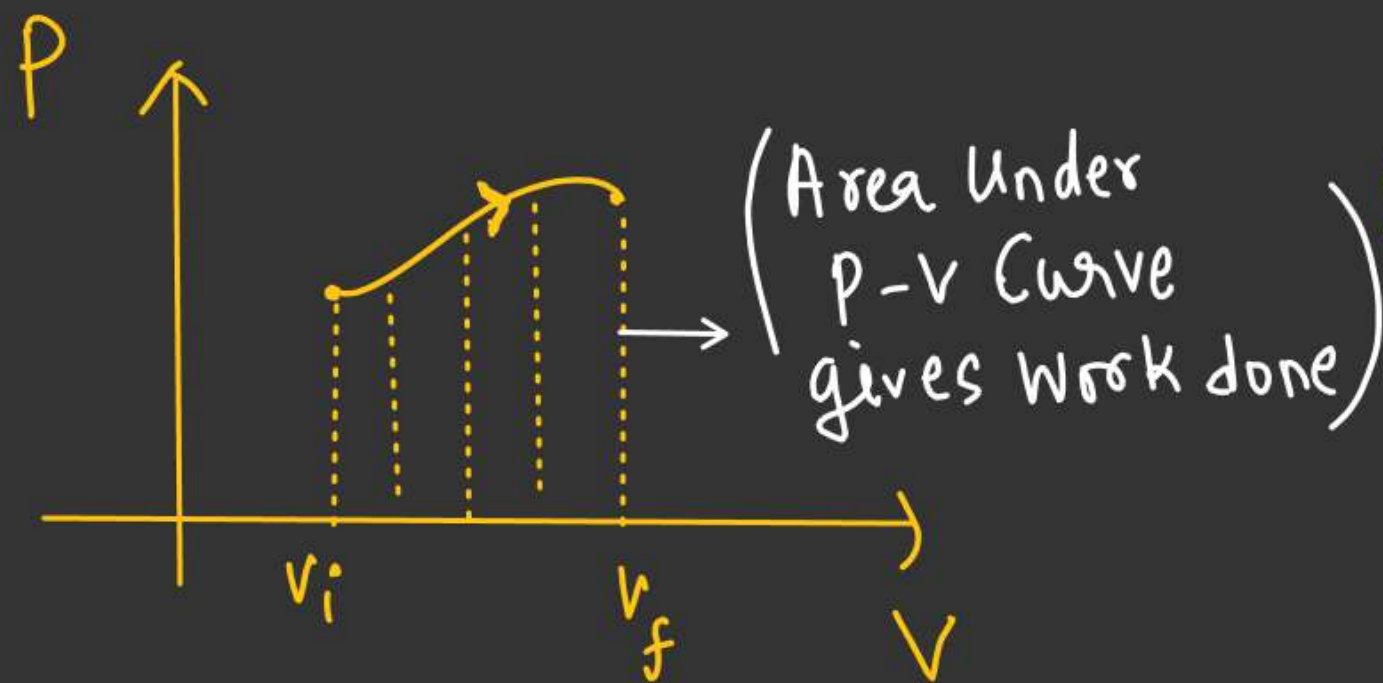
$$\begin{aligned} W_{\text{ext agent}} &= \int F_{\text{ext agent}} \cdot dx \cos \pi \\ &= - \int P A dx = \ominus \int P \cdot dV \end{aligned}$$



THERMODYNAMICS

$$W = \int_{V_i}^{V_f} P \cdot dV$$

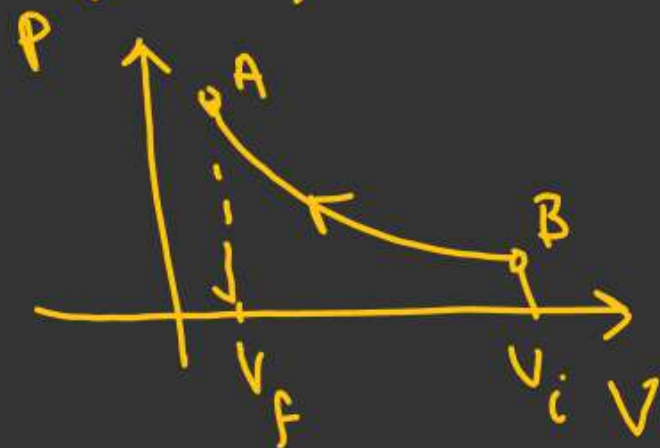
(*) During Expansion
 $V_f > V_i \Rightarrow$ gas is doing work
 or
 Work done by the gas \rightarrow +ve.



(*) During Compression
 $V_f < V_i \Rightarrow$ Work done on the gas
 (-ve)



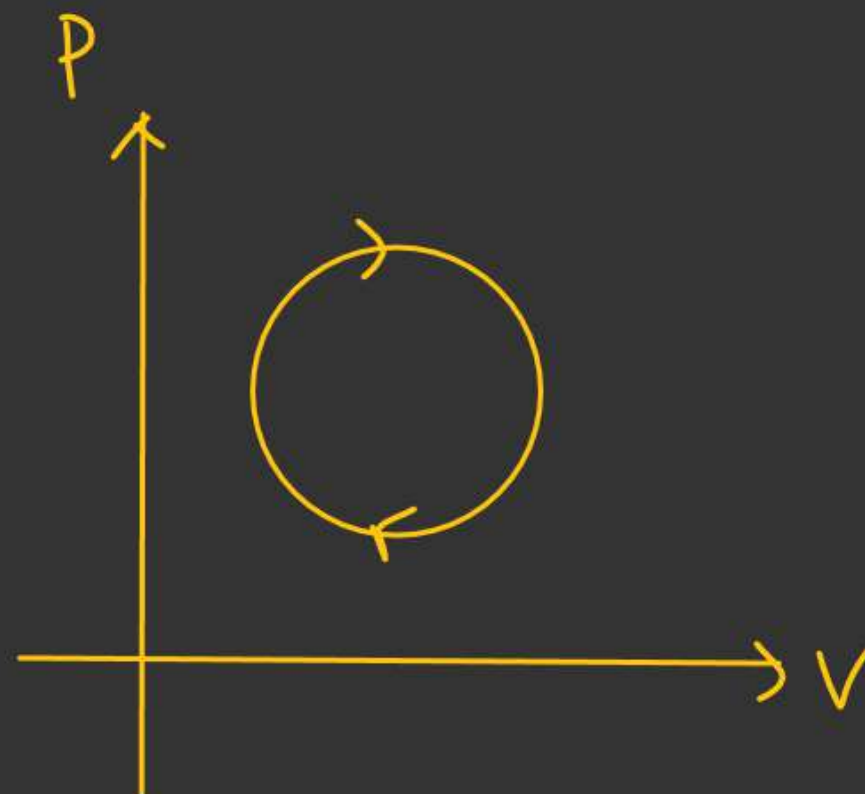
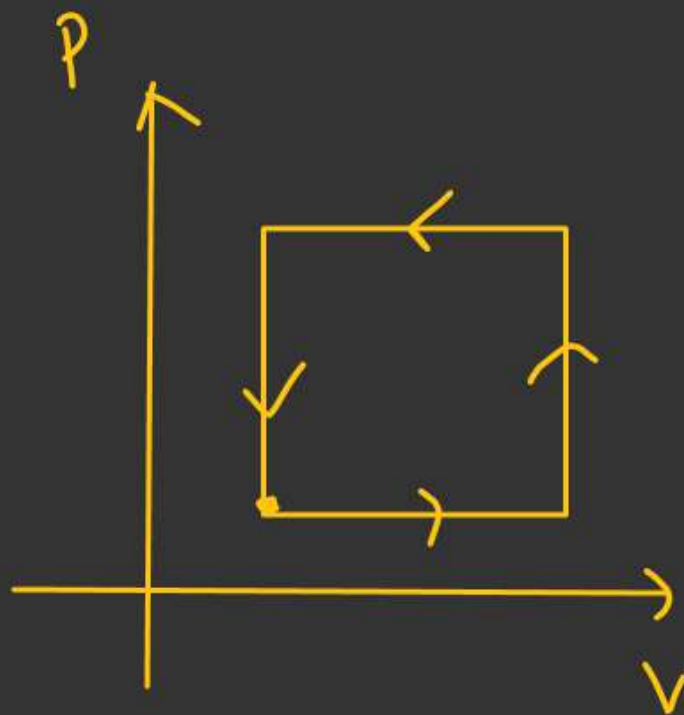
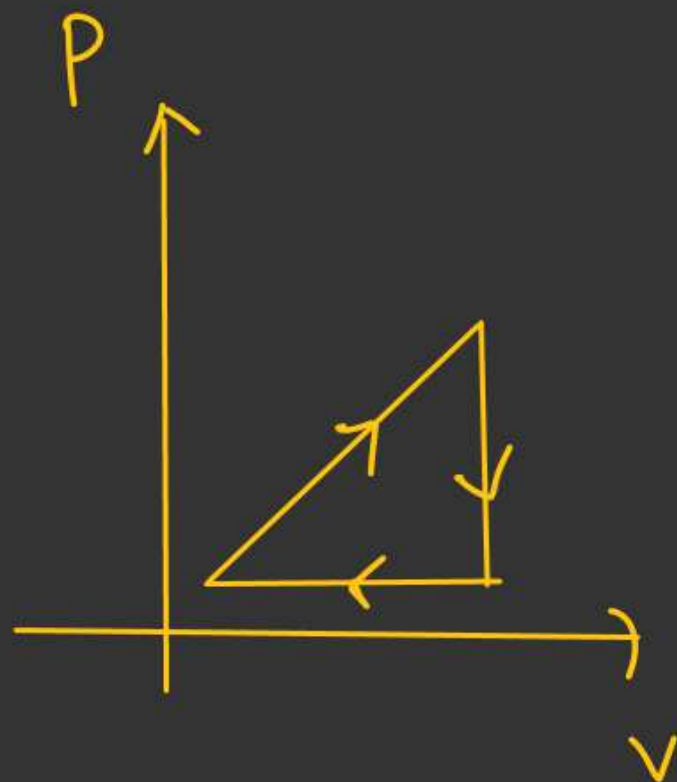
$$V_f > V_i \Rightarrow W \rightarrow +ve$$



$$V_f < V_i \Rightarrow W = -ve$$

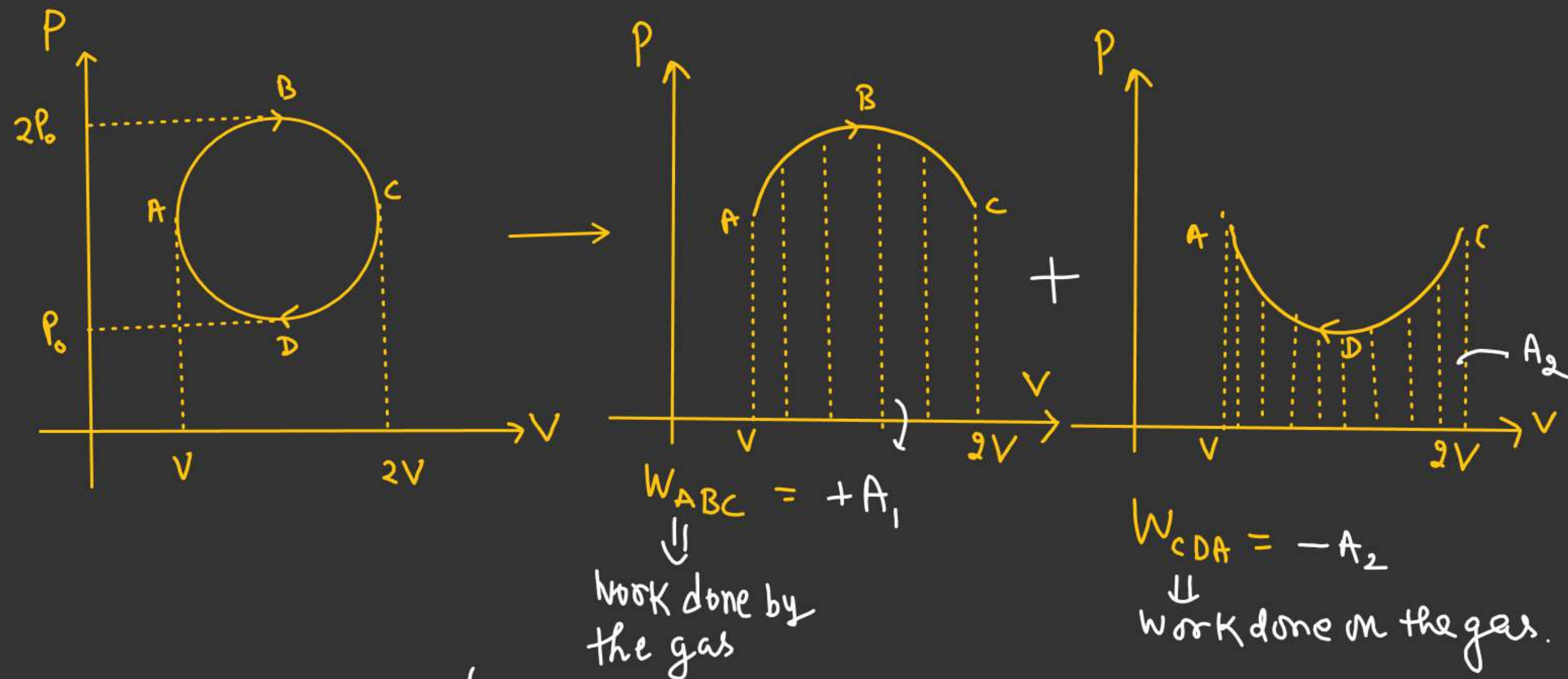
THERMODYNAMICS

Work done in a Cyclic process



$\Rightarrow \Delta U$ for all the cyclic process is zero.

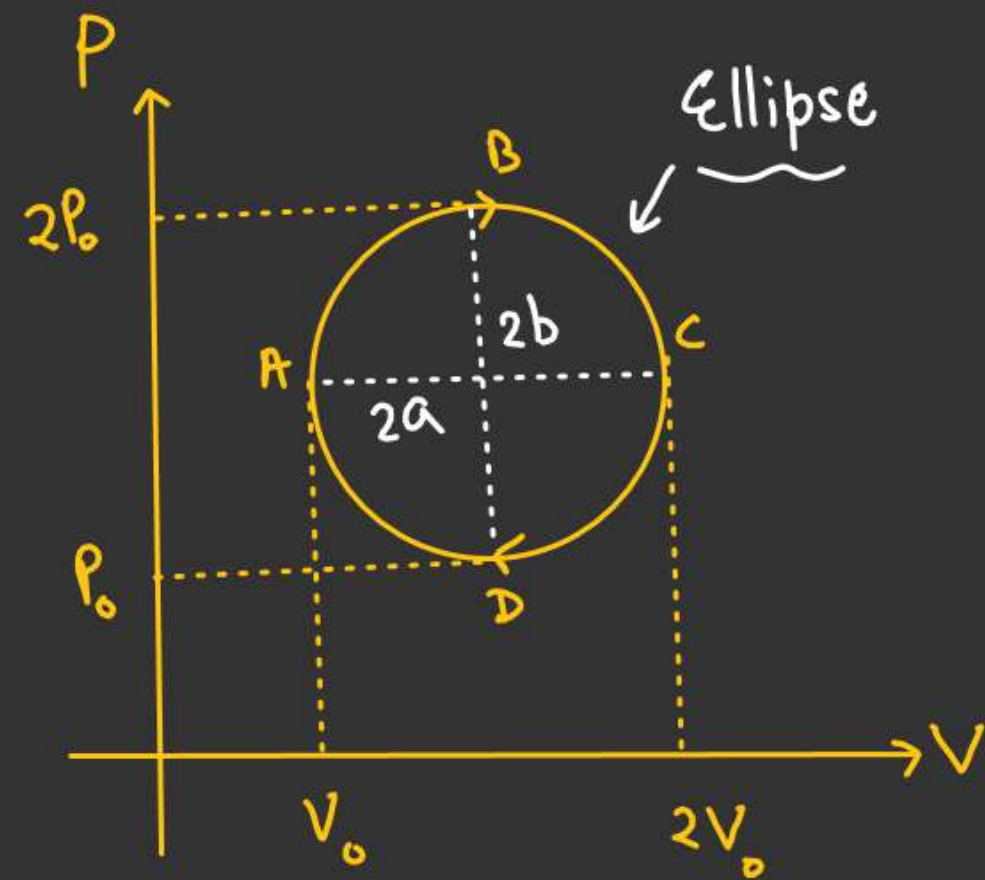
(As its initial & final state is same)

THERMODYNAMICS

$$W_{\text{net}} = (A_1 - A_2) = (\text{Area of cyclic fig.})$$

$W_{\text{net}} > 0 \Rightarrow$ If cycle is clockwise.

$W_{\text{net}} < 0 \Rightarrow$ If cycle is anticlockwise

THERMODYNAMICS

$$W_{\text{net}} = \text{Area of cyclic fig.}$$

$$= \text{Area of Ellipse}$$

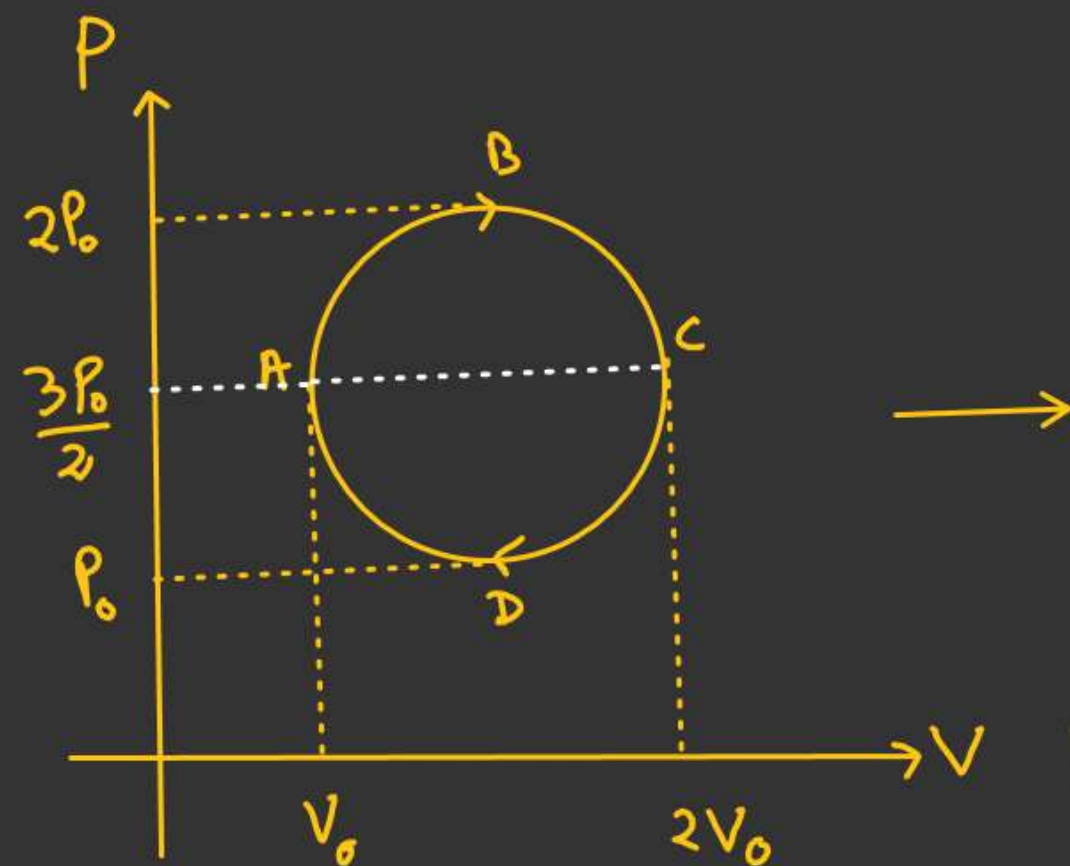
$$= \pi a b$$

$$= \oplus \left(\frac{\pi P_0 V_0}{4} \right) \checkmark$$

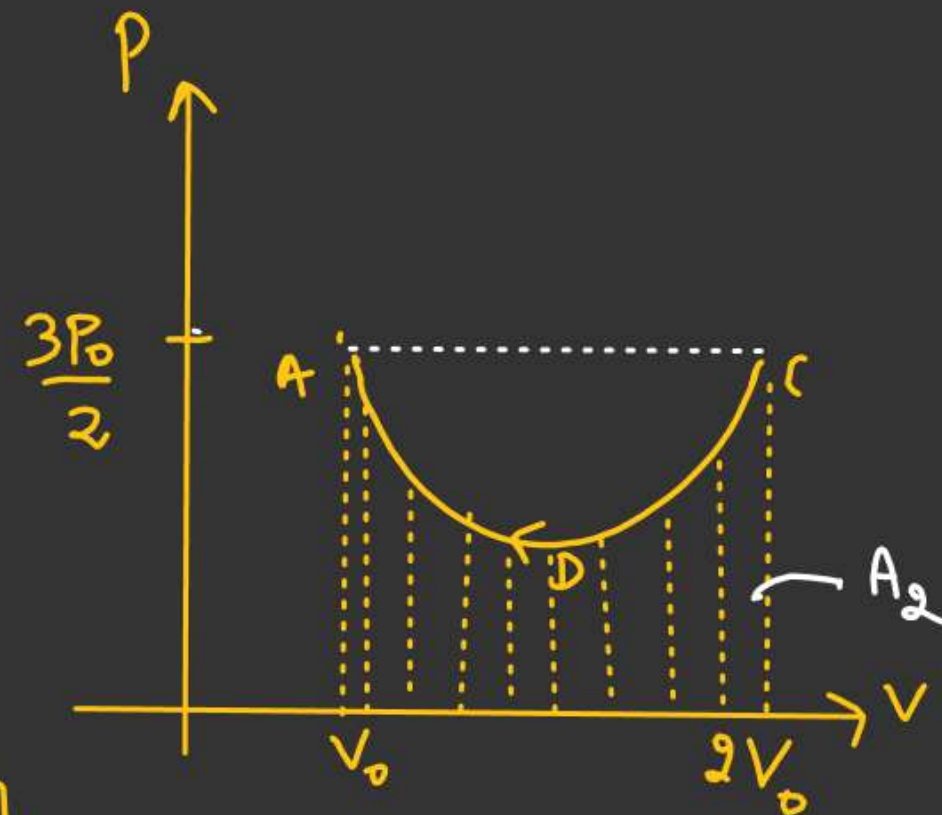
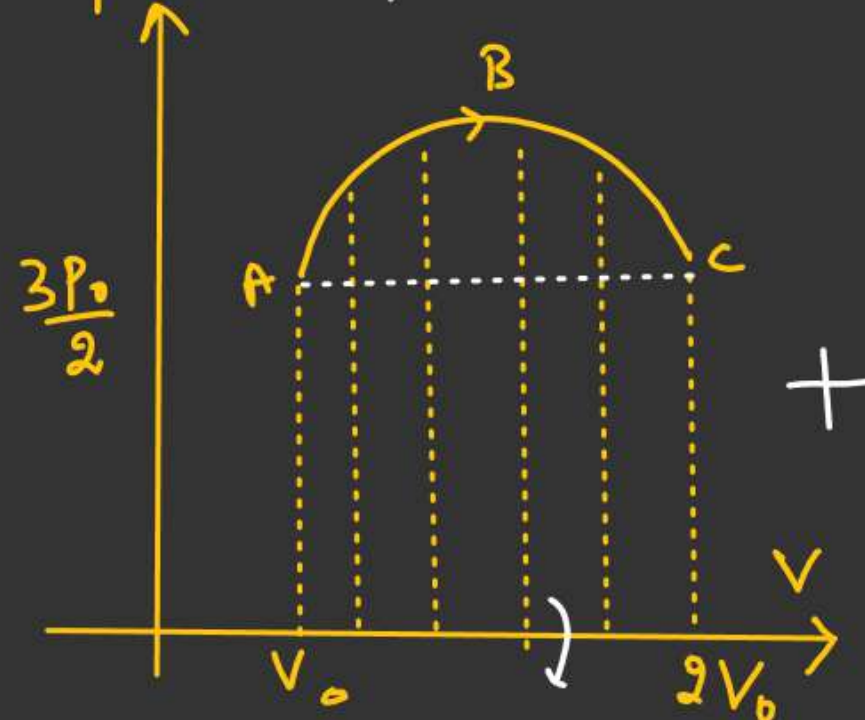
(Cycle is clockwise)

$$\begin{array}{l|l} 2a = V_0 & 2b = P_0 \\ a = \frac{V_0}{2} & b = \frac{P_0}{2} \end{array}$$

THERMODYNAMICS



Expansion.



$$W_{\text{expansional work}} = \left[\text{Area of Semiellipse} + \text{Area of rectangle} \right]$$

(+ve)

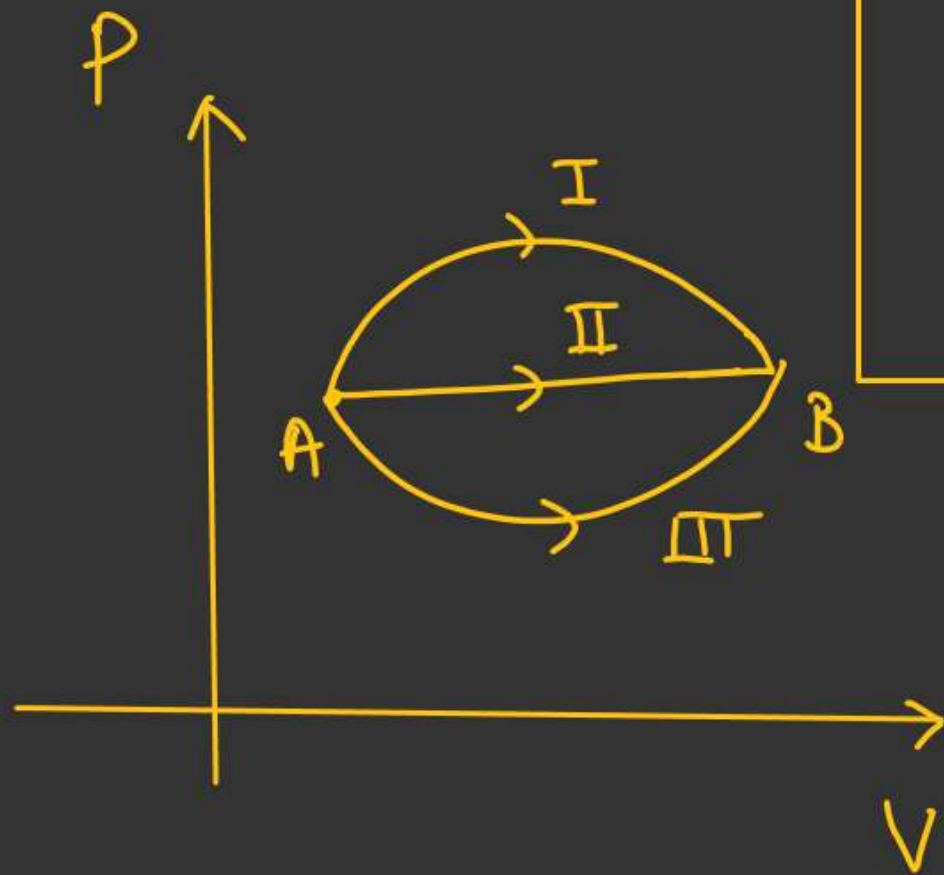
$$= \frac{1}{2} \left(\frac{\pi P_0 V_0}{4} \right) + \left(\frac{3 P_0 V_0}{2} \right)$$

$W_{\text{compressional}}$

$$= - \left[\left(\text{Area of Rectangle} \right) - \left(\text{Area of Semiellipse} \right) \right]$$

$$= - \left[\left(\frac{3 P_0 V_0}{2} - \frac{\pi P_0 V_0}{8} \right) \right]$$

THERMODYNAMICS



$$\Delta U_I = \Delta U_{II} = \Delta U_{III}$$

$$\Delta W_I > \Delta W_{II} > \Delta W_{III}$$

THERMODYNAMICS

BREAK

6:30 → 6:40

First Law of Thermodynamics

(Based on Conservation of Energy)

$$dQ = dU + dW$$

$$\Delta Q = \Delta U + \Delta W$$

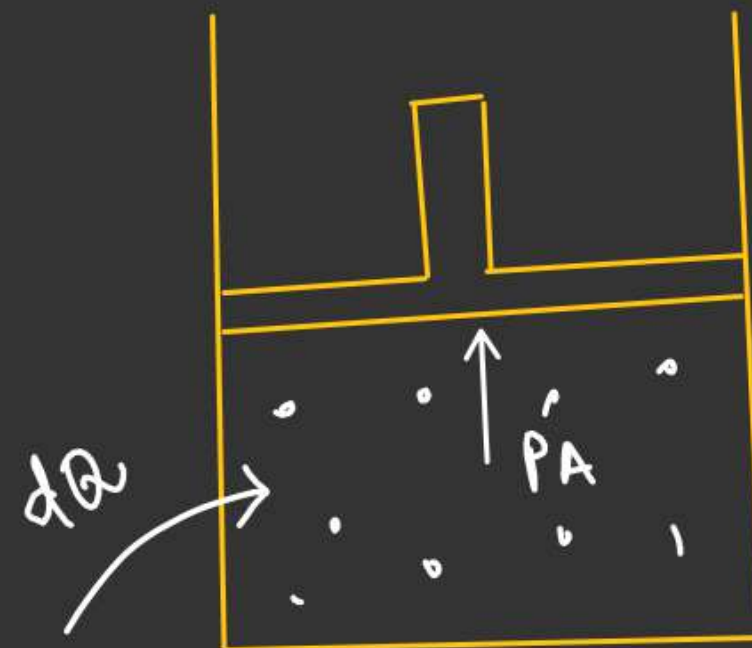
Sign-Convention

$dQ \rightarrow +ve$ (heat given to the system)

$dQ \rightarrow (-ve)$ (heat released)

$dW \rightarrow +ve$ (work done by the gas)

$dW \rightarrow -ve$ (work done on the gas)



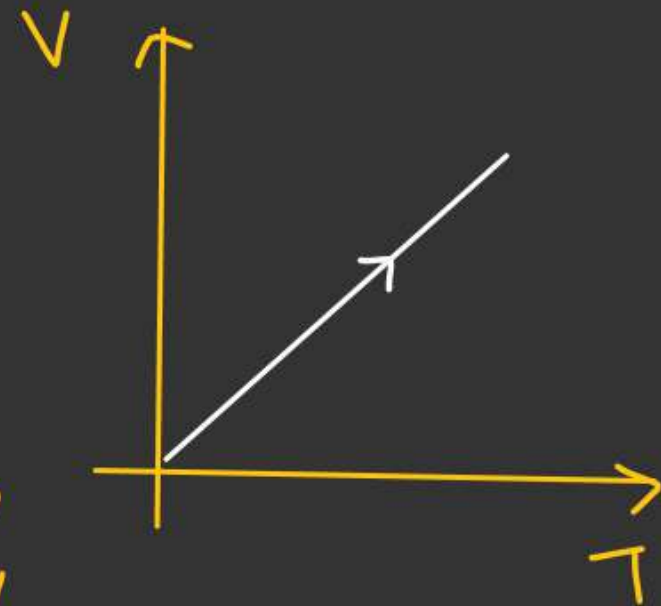
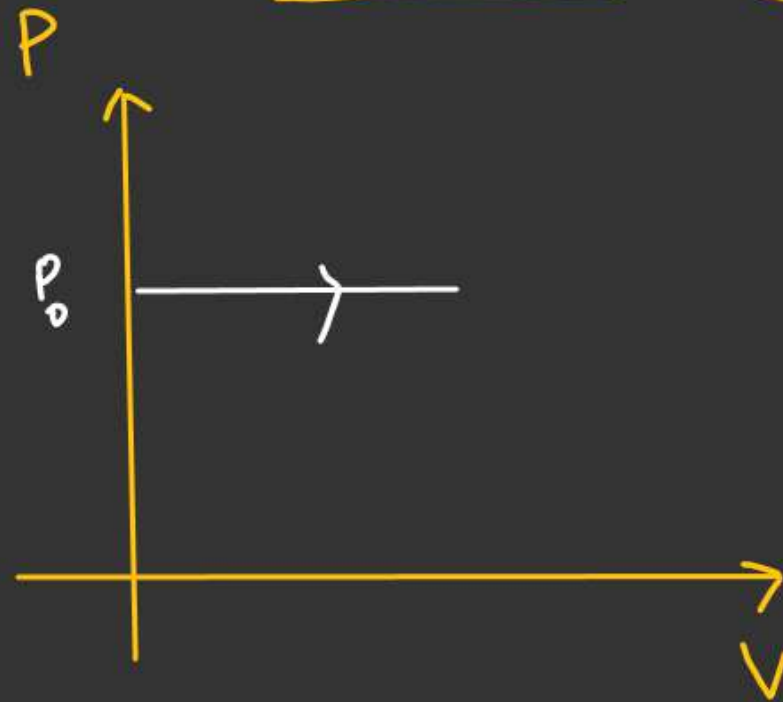
THERMODYNAMICS

Process

- Isobaric ($P = c$)
- Isochoric ($V = c$)
- Isothermal ($T = c$)
- Adiabatic ($\Delta Q = 0$)
- Polytropic

THERMODYNAMICS

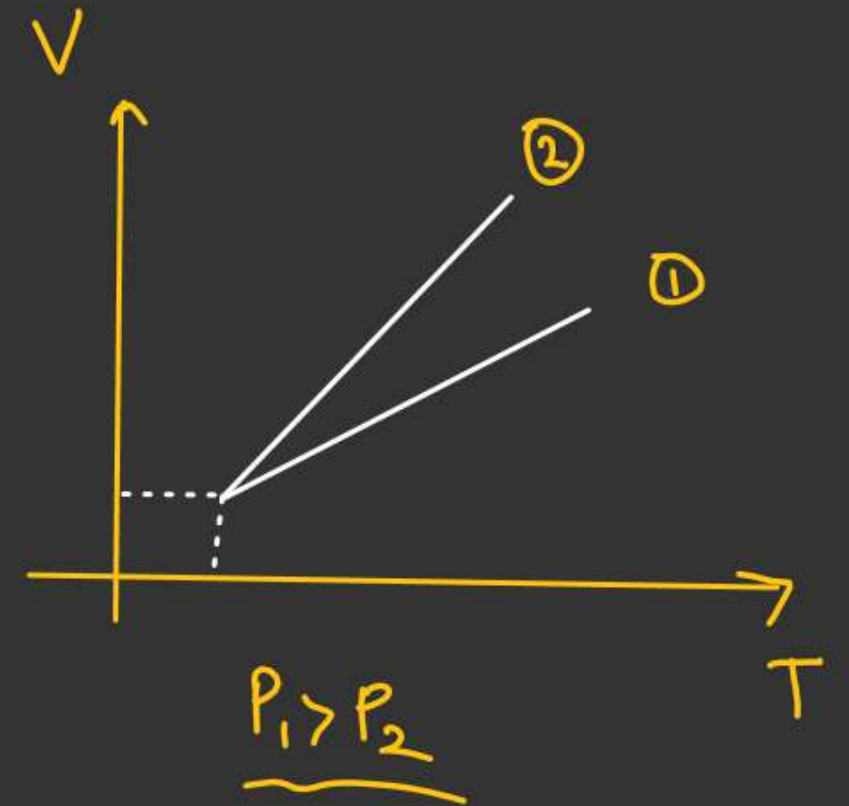
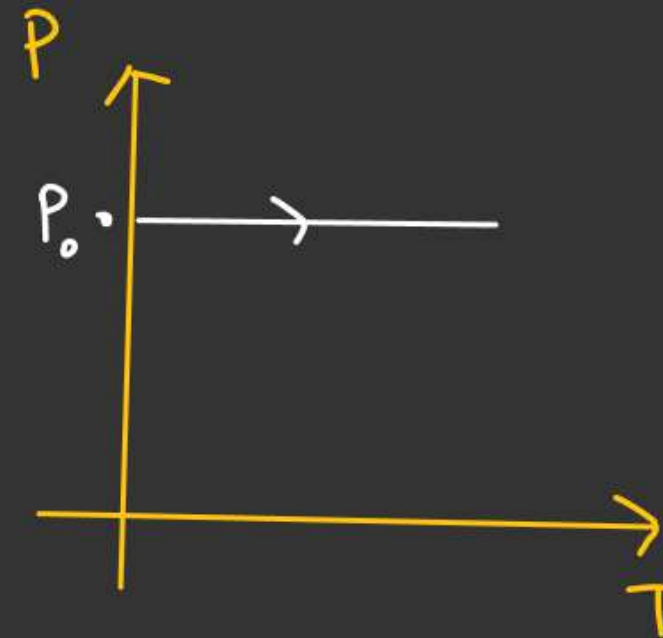
Isobaric ($P = C$)



$$PV = nRT$$

$$V = \left(\frac{nR}{P} \right) T$$

↓
Slope



\Rightarrow Molar heat Capacity \rightarrow (Heat given to raise the temp of 1 mole of gas by 1°C)

$$C = \frac{1}{n} \left(\frac{dQ}{dt} \right) \quad n = \text{Mole}$$

$C \rightarrow C_p$ for Constant pressure.

$$\left(C_p = \frac{1}{n} \frac{(dQ)_{\text{at } P=C}}{dt} \right)$$

Work done in isobaric process

$$P, V_i, T_i \rightarrow P, V_f, T_f \quad (P = C)$$

$$PV_f = nRT_f$$

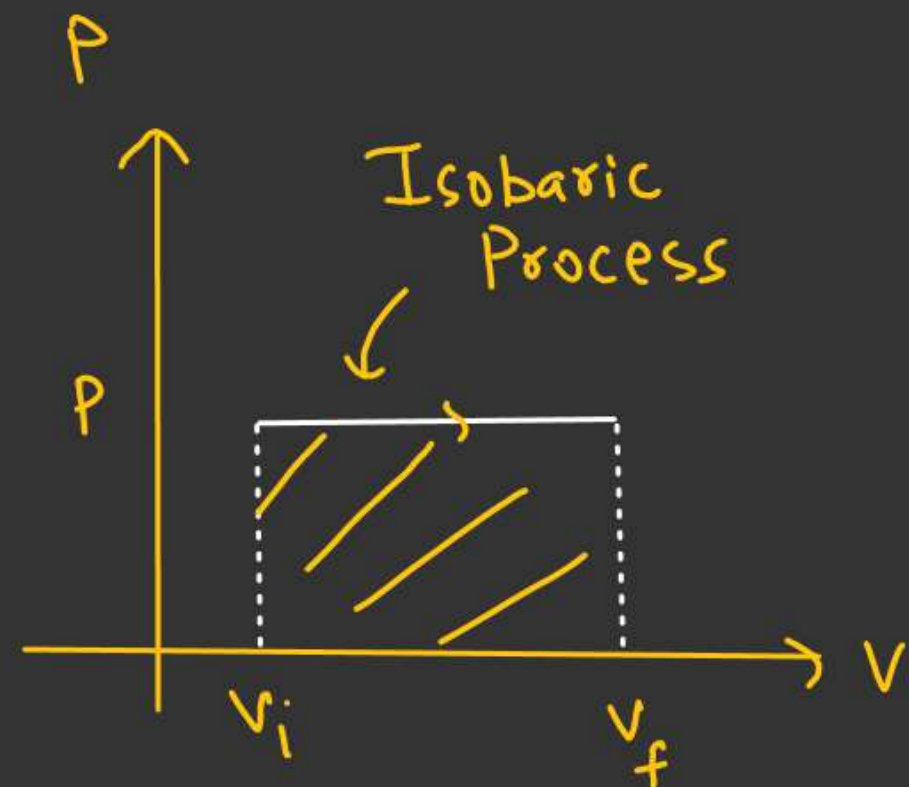
$$PV_i = nRT_i$$

$$\int_0^W dW = \int_{V_i}^{V_f} P \cdot dV$$

$$W = P \int_{V_i}^{V_f} dV$$

$$W = nR(T_f - T_i)$$

$$W = P(V_f - V_i)$$



$$W_{\text{isobaric}} = \text{Area of Rectangle} \\ = P(V_f - V_i) \quad \checkmark$$

First law in isobaric process

$$(dQ) = dU + dW$$

↓

↓

$$nC_p dT = nC_v dT + PdV$$

$$nC_p dT = nC_v dT + nRdT$$

$$C_p = \frac{1}{n} \frac{dQ}{dT} \quad \left| \quad PdV = nRdT \right.$$

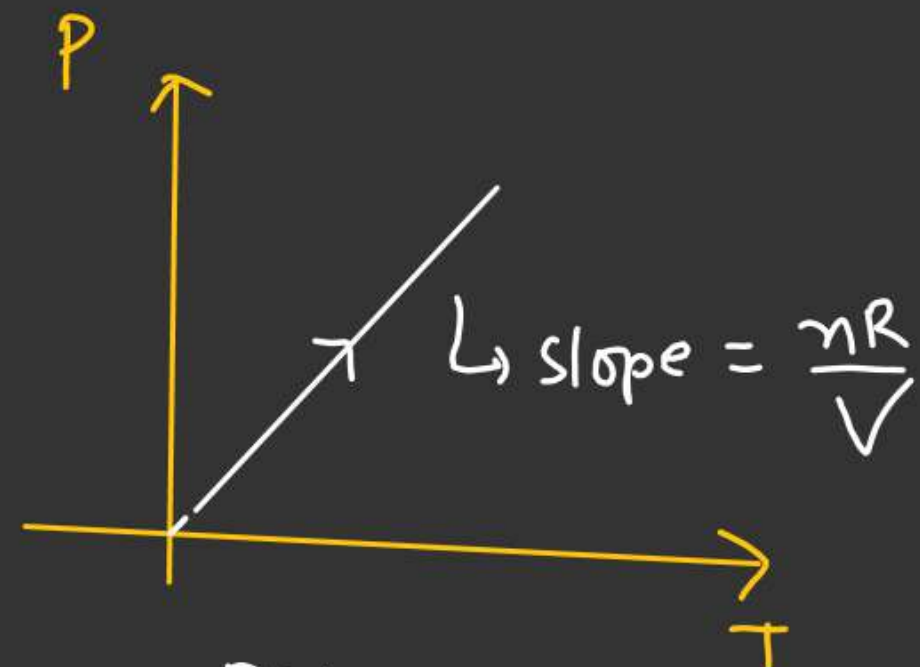
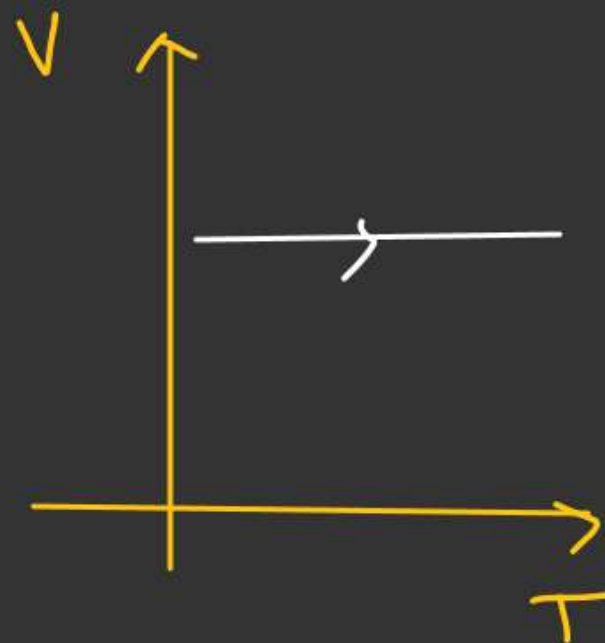
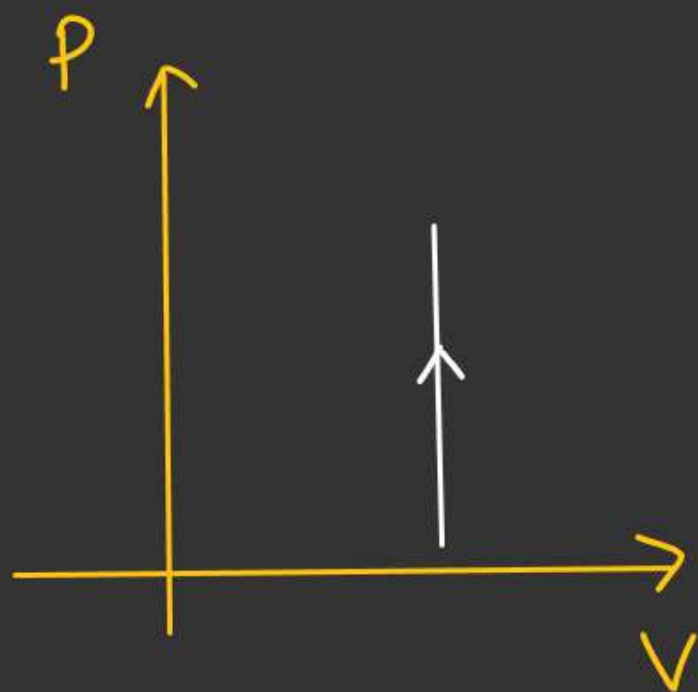
$$dQ = nC_p dT$$

Note

 dU For any process = $nC_v dT$
 $C_v \rightarrow$ Molar heat Capacity at Constant volume

$$C_p = C_v + R$$

ISOTHERM PROCESS ($V=C$)



$$PV = nRT$$

$$P = \left(\frac{nR}{V} \right) T$$

\Downarrow
Constant

Molar heat Capacity at Constant volume

$$C_V = \frac{1}{n} \left(\frac{dQ}{dT} \right)_{\text{at constant volume}}$$

Work done = 0

$$V = \text{Constant}$$

$$\Delta V = 0$$

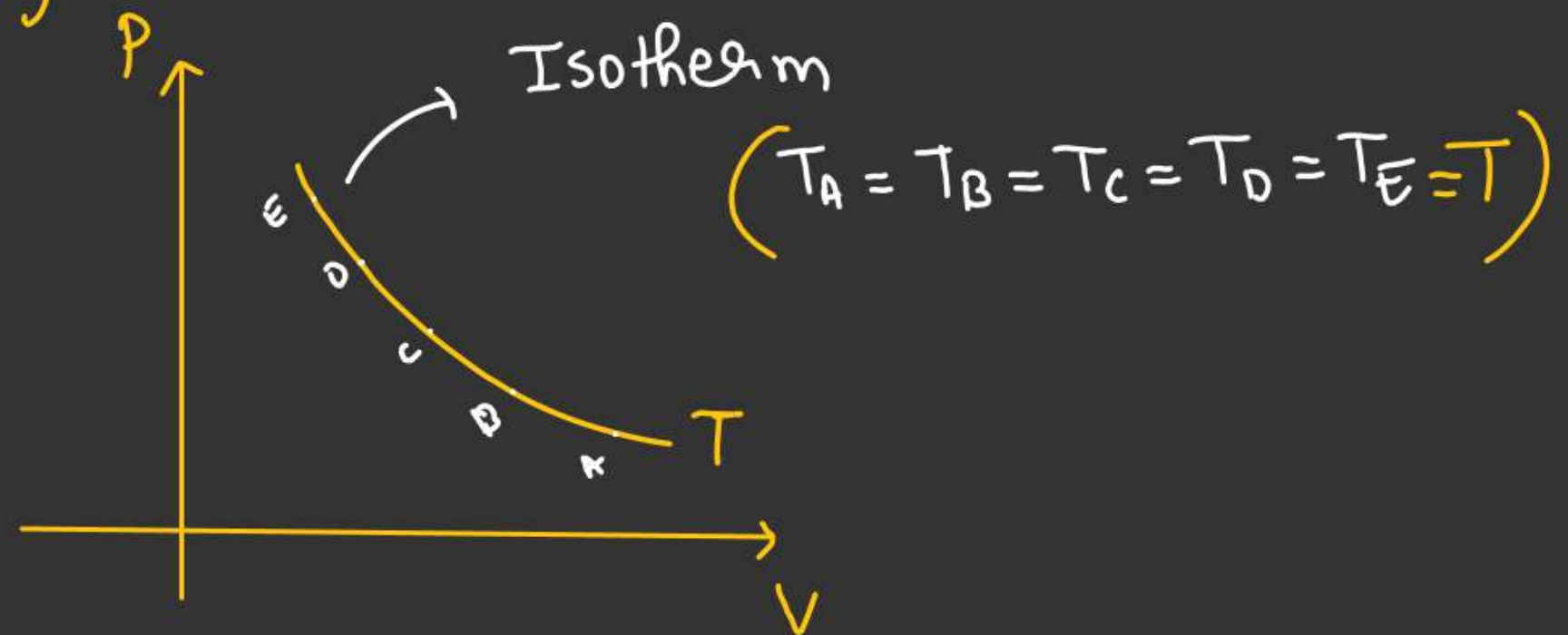
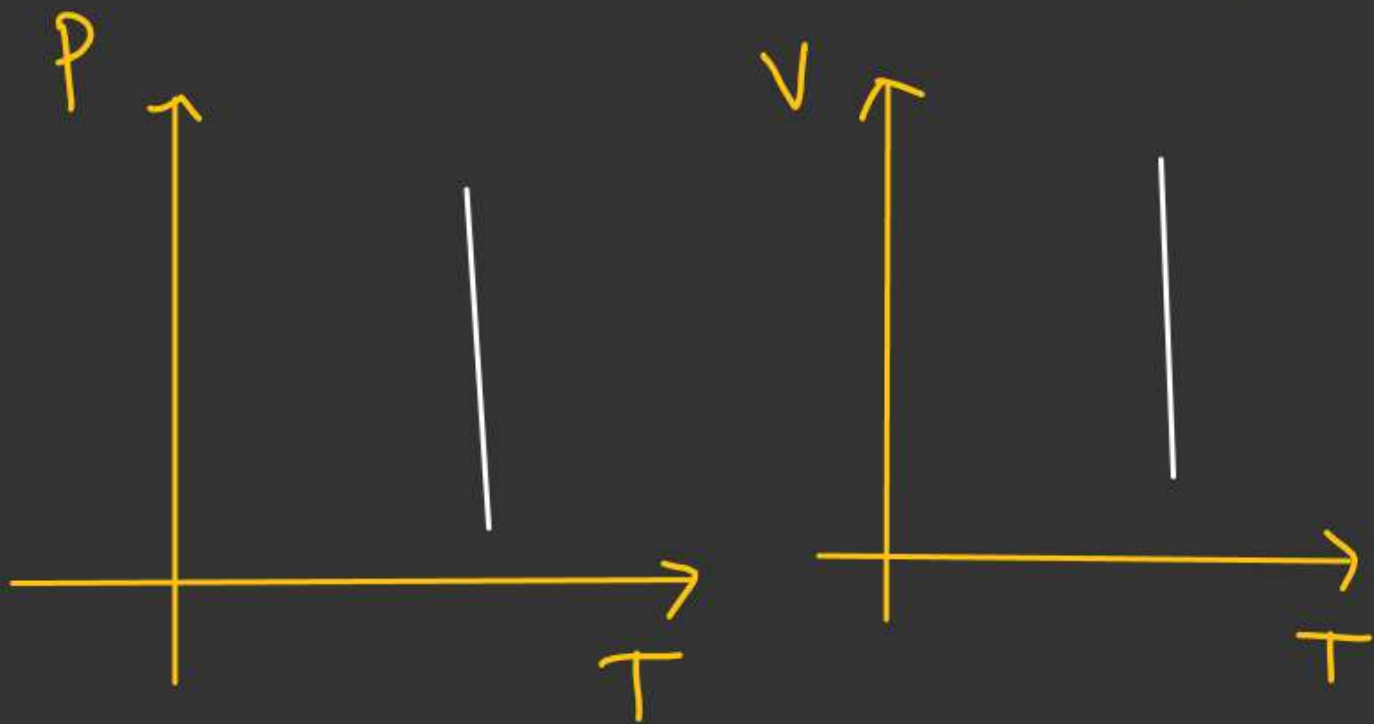
First Law

$$dQ = dU + dW \rightarrow 0$$

$$dQ = dU$$

$$nC_V dT = dU$$

(Valid for all process)

Isothermal process ($T = C$)

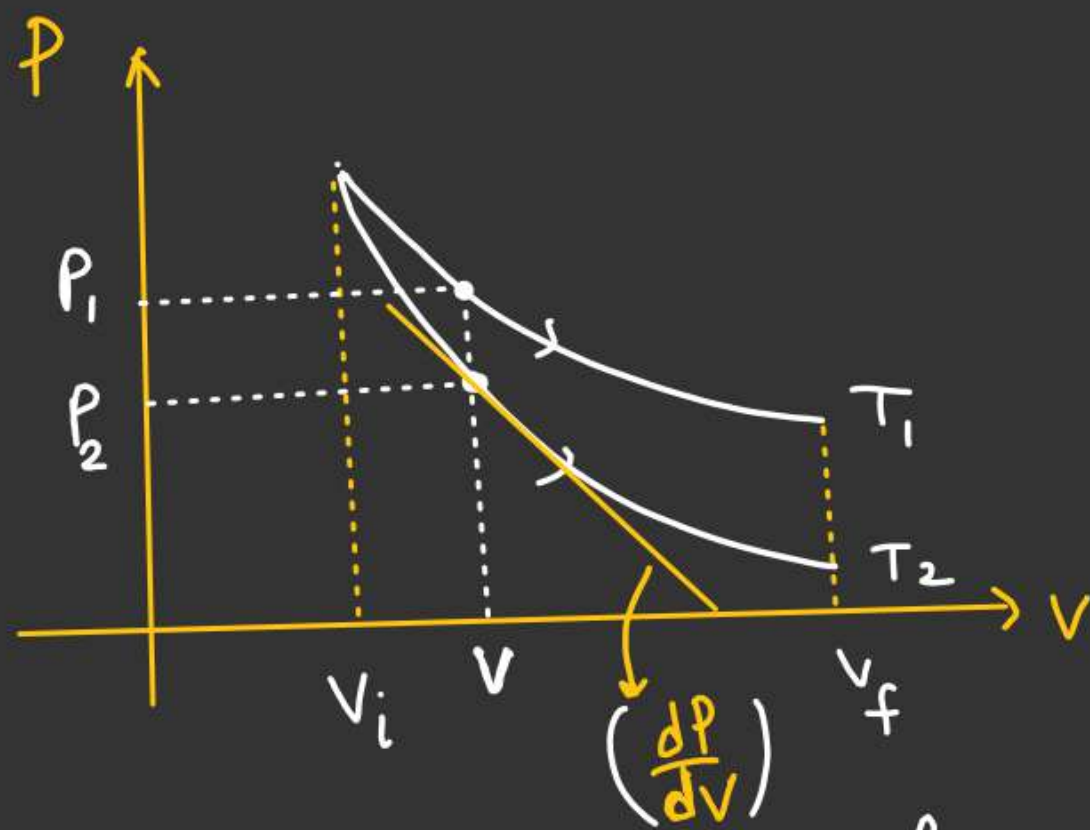
$$PV = \textcircled{nRT} \rightarrow \text{Constant}$$

$$\left(P = \frac{C}{V}\right)$$

$xy = C \rightarrow$ Rectangular hyperbola



Higher isotherm are at higher temp. ✓



$$P_1 V = nRT_1 \quad \frac{P_1}{P_2} = \frac{T_1}{T_2}$$

$$P_2 V = nRT_2 \quad P_1 > P_2$$

$$\Rightarrow T_1 > T_2$$

(*) Slope of isotherm

$$PV = nRT$$

Differentiating both side w.r.t
Volume

$$\frac{d}{dV}(PV) = \frac{d}{dV}(nRT) \quad \downarrow \text{Constant}$$

$$P \frac{d(V)}{dV} + V \frac{dP}{dV} = 0$$

$$P = -V \frac{dP}{dV}$$

$$\frac{dP}{dV} = \left(-\frac{P}{V} \right)$$

∴

Slope of isotherm

B is isothermal process

$$B = - \frac{dP}{\left(\frac{dV}{V}\right)}$$

$$B_{\text{isothermal}} = P$$

$$B = \left(- \frac{dP}{\frac{dV}{V}} \right) \times V$$

$$B = \frac{P}{V} \times V$$

Molar heat Capacity in isothermal process

$$C = \frac{1}{n} \left(\frac{dQ}{dT} \right)$$

for isothermal $dT \rightarrow 0$

$$C_{\text{isothermal}} \rightarrow \infty$$

→ A very large reservoir have ∞ heat capacity.

Work-done in isothermal process

$$PV = nRT$$

$$P = \left(\frac{nRT}{V} \right)$$

$$W = \int_{V_i}^{V_f} P \cdot dV = nRT \int_{V_i}^{V_f} \frac{dV}{V}$$

$$W = nRT \ln\left(\frac{V_f}{V_i}\right)$$

$$W = nRT \ln\left(\frac{P_i}{P_f}\right)$$

$$P_i, V_i, T \rightarrow P_f, V_f, T$$

$$P_i V_i = nRT$$

$$P_f V_f = nRT$$

$$P_i V_i = P_f V_f$$

$$\frac{P_i}{P_f} = \frac{V_f}{V_i}$$

$$\Delta U_{\text{isothermal}} = 0$$

For any process

$$\Delta U = nC_v \Delta T$$

$\downarrow \qquad \qquad \downarrow$
 $0 \qquad \qquad \qquad 0$

First Law in isothermal process

$$dQ = \cancel{dU} + dW$$

$\nearrow 0$

$dQ = dW$