

Heat transfer in case of variable cross-sectional area

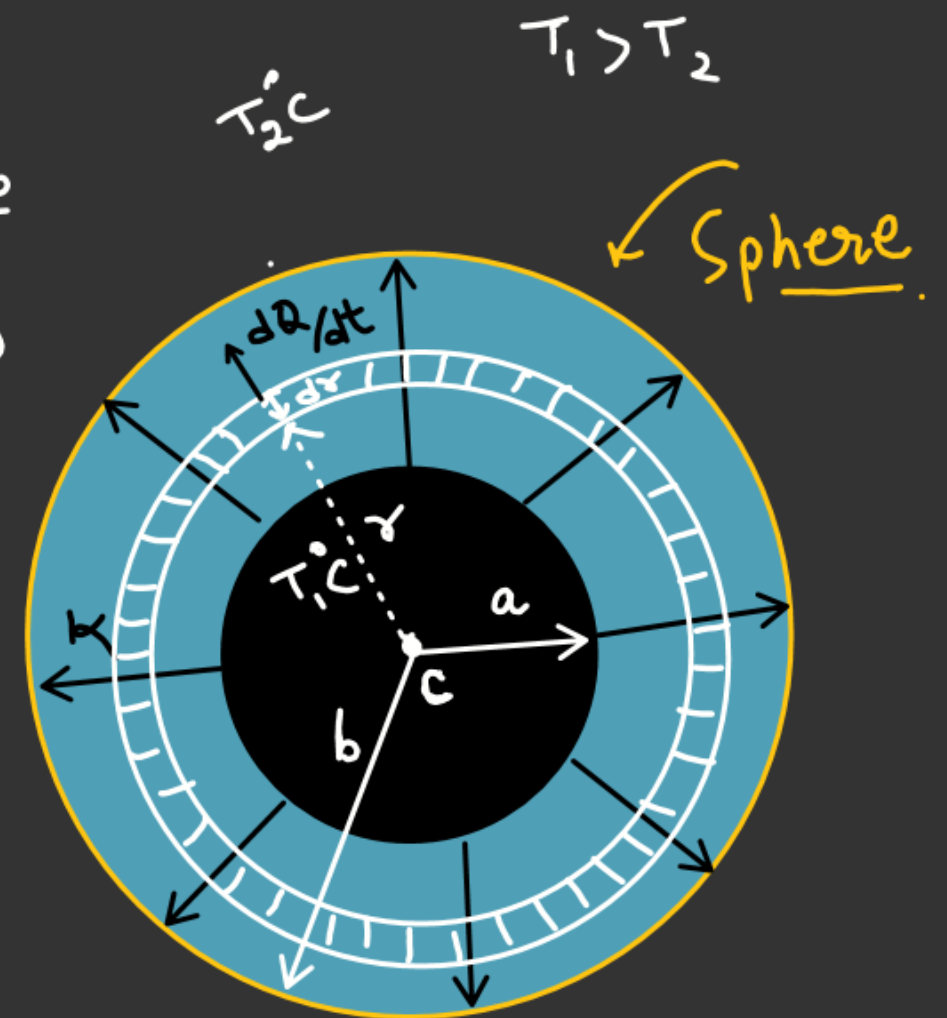
At a radial distance r , a spherical shell of 'dr' thickness is cut

if $\left(\frac{dQ}{dt}\right)$ be the heat flow at the time of Steady state

$$P \text{ J/s} \leftarrow \left(\frac{dQ}{dt}\right) = -K \underbrace{4\pi r^2}_A \left(\frac{dT}{dr}\right) \left[\begin{array}{l} dT \text{ be the temp} \\ \text{difference for } dr \\ \text{thickness of the} \\ \text{shell.} \end{array} \right]$$

$$P = -K \cdot 4\pi r^2 \left(\frac{dT}{dr}\right)$$

$$P \int_a^b \frac{dr}{r^2} = -4\pi K \int_{T_1}^{T_2} dT$$



Heat transfer in case of variable cross-sectional area

$$(i = \frac{\Delta V}{R})$$

$$P \int_a^b \frac{dr}{r^2} = -4\pi K \int_{T_1}^{T_2} dT$$

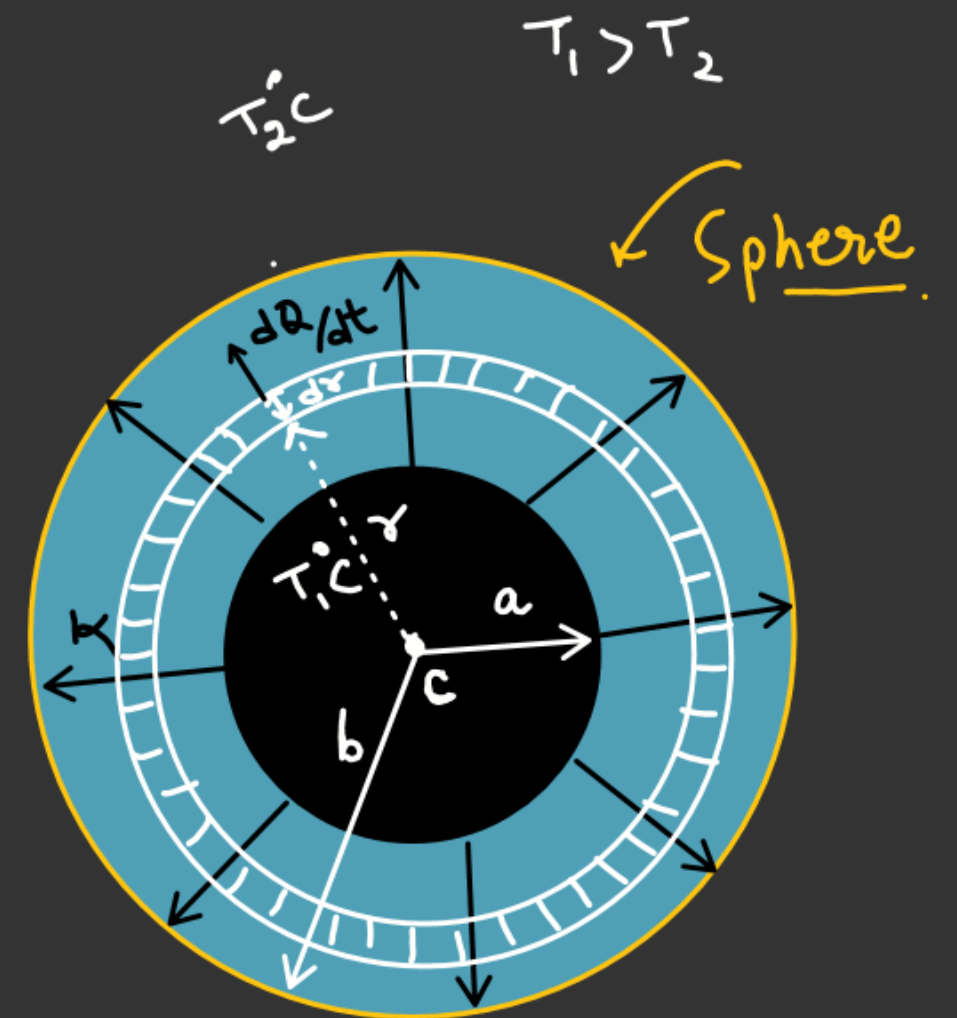
$$P \left[-\frac{1}{r} \right]_a^b = -4\pi K (T_2 - T_1)$$

$$P \left[-\frac{1}{b} + \frac{1}{a} \right] = 4\pi K (T_1 - T_2)$$

$$P = \left[\frac{(T_1 - T_2)}{\frac{1}{4\pi K} \left(\frac{1}{a} - \frac{1}{b} \right)} \right]$$

\Downarrow
 i_{th}
 \Downarrow
 R_{th}

$$R_{th} = \frac{1}{4\pi K} \left(\frac{1}{a} - \frac{1}{b} \right)$$



Heat transfer in case of variable cross-sectional area

if k is variable, $k = k_0 r$ $r \rightarrow$ radial distance

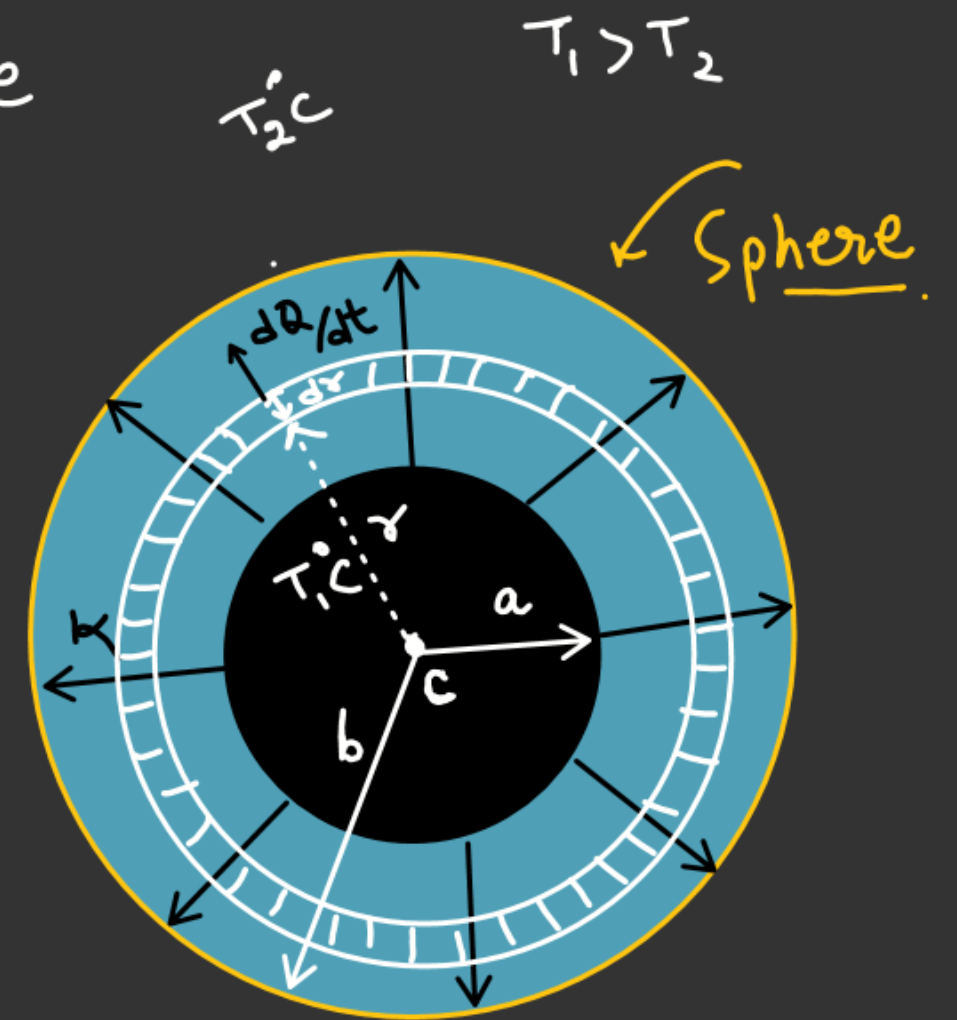
$$\frac{dQ}{dt} = -k_r 4\pi r^2 \left(\frac{dT}{dr} \right)$$

\Leftarrow

$$P = -k_0 4\pi r^3 \frac{dT}{dr}$$

$$P \int_a^b \frac{dr}{r^3} = -k_0 4\pi \int_{T_1}^{T_2} dT$$

$P = \checkmark$



Heat flow through Cylindrical Crosssectional area

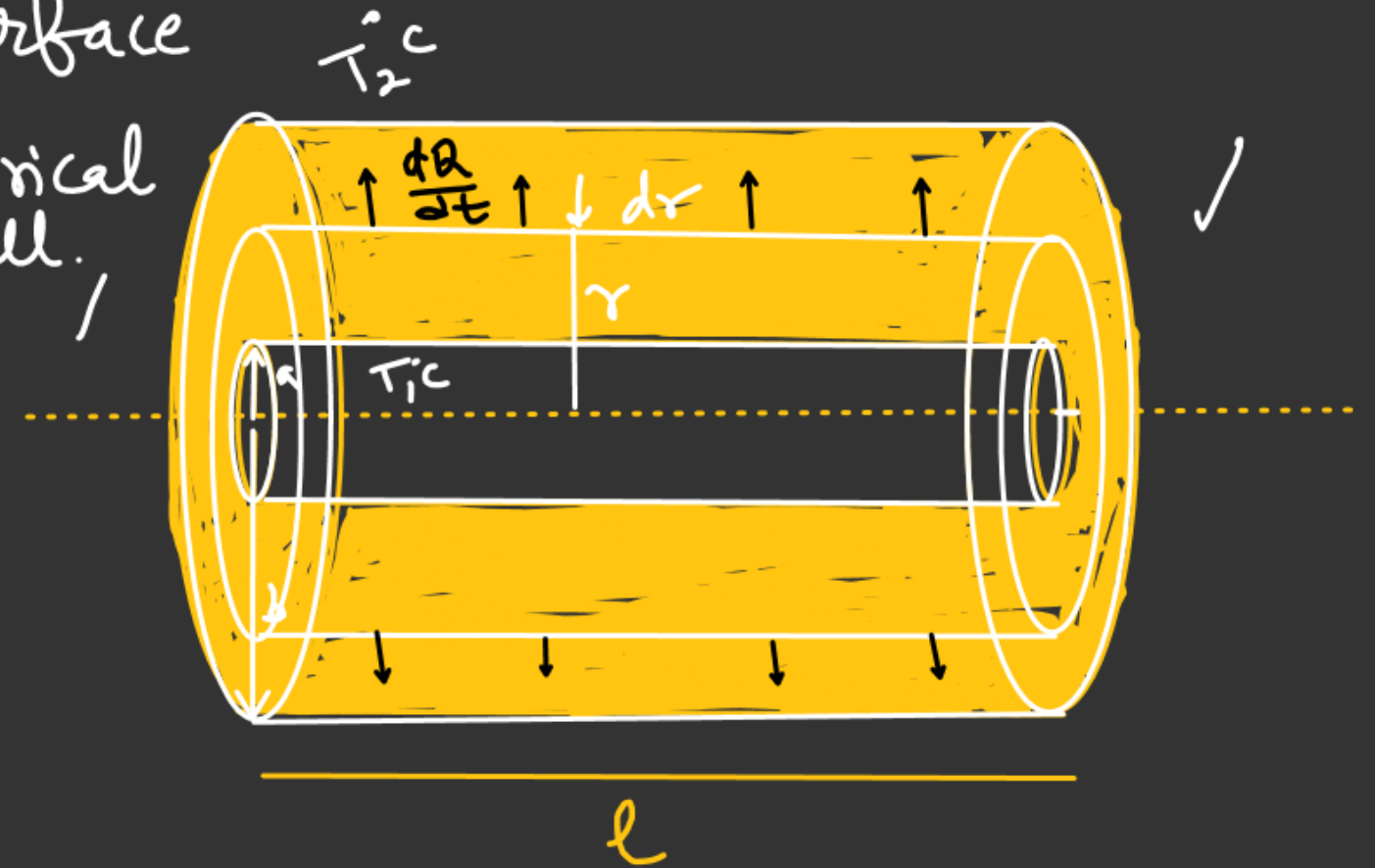
$$P \text{ J/s} \Leftarrow \frac{dQ}{dt} = -K(2\pi r l) \frac{dT}{dr}$$

A → Curve Surface area of Cylindrical Shell,

$dT \rightarrow$ temp difference for dr thickness of shell.

$$P = -K 2\pi l \left(\frac{r}{dr} \right) dT$$

$$P \int_a^b \frac{dr}{r} = - (2\pi l) K \int_{T_1}^{T_2} dT$$



$$P \int_a^b \frac{dr}{r} = - (2\pi l) \underbrace{K}_{\substack{\uparrow \\ T_2 \\ \downarrow \\ T_1}} \int_{T_1}^{T_2} dT$$

$$P \ln\left(\frac{b}{a}\right) = - 2\pi K l (T_2 - T_1)$$

$$P = \frac{(T_1 - T_2)}{\underbrace{\frac{1}{2\pi K l} \ln\left(\frac{b}{a}\right)}}_{\substack{\uparrow \\ i_{th} \\ \downarrow \\ R_{th}}}$$

$$\frac{1}{2\pi K l} \ln\left(\frac{b}{a}\right)$$

R_{th}

$$R_{th} = \frac{1}{2\pi K l} \ln\left(\frac{b}{a}\right)$$

Thermal resistance of a Cylindrical Conductor.

H.W

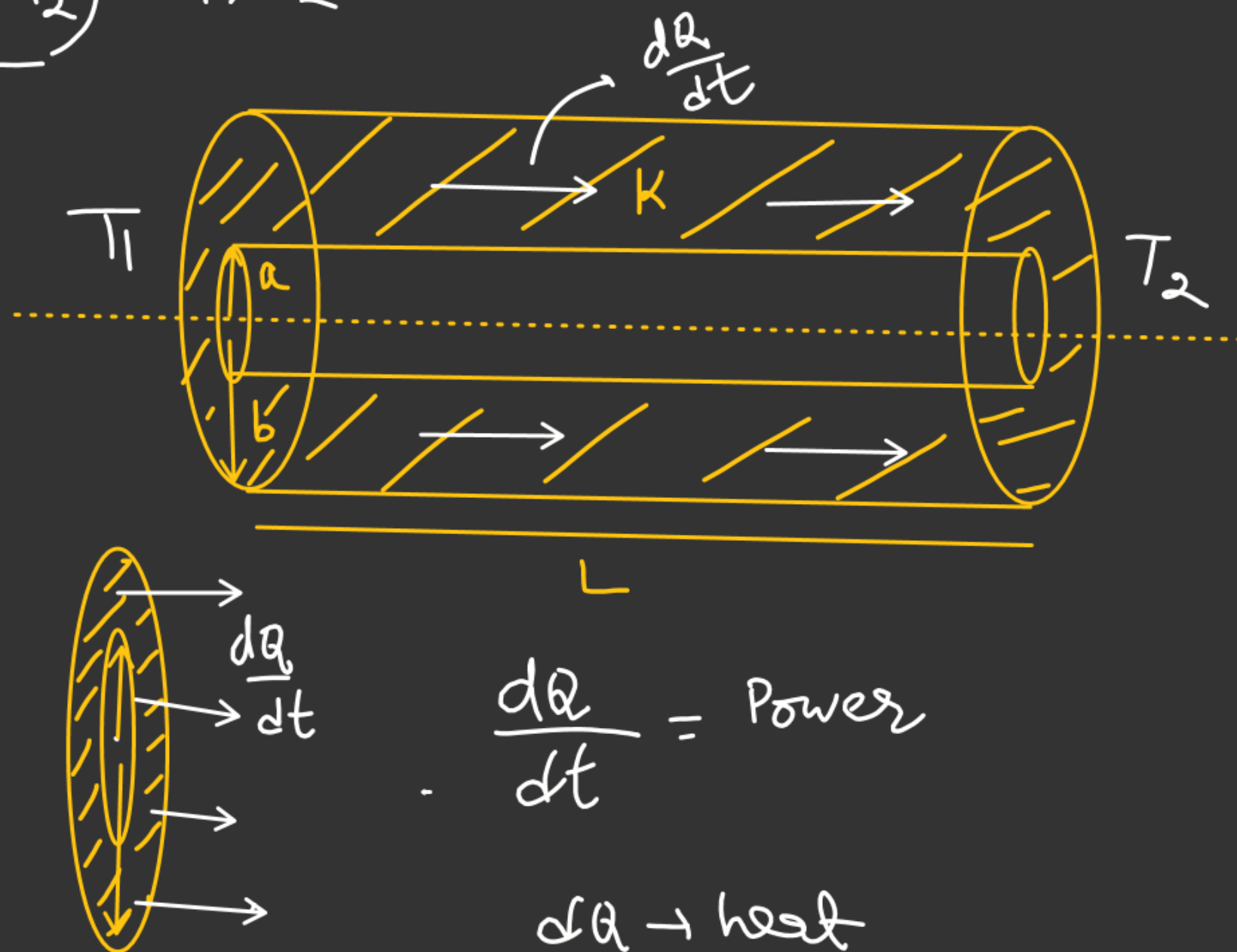
$$\begin{cases} K = K_0 r & r \rightarrow \text{radial distance} \\ K = K_0 / r \\ K = K_0 + \alpha r \end{cases}$$

Find $\frac{dQ}{dt} = ??$

$$\frac{\Delta Q}{\Delta t} = \frac{dQ}{dt} = \frac{k \pi (b^2 - a^2) (T_1 - T_2)}{L} \quad T_1 > T_2$$

↓
P T/s

$$P = \frac{T_1 - T_2}{\left(\frac{L}{k \pi (b^2 - a^2)} \right)} \quad \Downarrow \quad R_{th}$$



$$\frac{dQ}{dt} = \text{Power}$$

$dQ \rightarrow \text{heat}$



Case when one end of temperature of rod is a function of time

$$T_B = (20 + 2t)$$

$t \rightarrow$ time.

Total heat flow from A to B

$$\left(\frac{dQ}{dt} \right) = \frac{KA(100 - (20 + 2t))}{L}$$

$$Q \frac{dQ}{dt} = \frac{KA}{L} (80 - 2t)$$

$$\int_0^Q dQ = \frac{KA}{L} \int_0^{40} (80 - 2t) dt$$

$T_A = 100^\circ\text{C}$



Heat Continue to flow from A to B until & unless

$$T_A = T_B$$

$$100 = 20 + 2t$$

$$\frac{80}{2} = t$$

$$t = \underline{40 \text{ sec}} \checkmark$$



$$Q \int_0^{\infty} dQ = \frac{KA}{L} \int_0^{40} (80 - 2t) dt$$

$$Q = \frac{KA}{L} \left\{ 80[t]_0^{40} - \frac{2}{2}[t^2]_0^{40} \right\}$$

$$Q = \frac{KA}{L} \{ 3200 - 1600 \}$$

$$Q = \left(1600 \frac{KA}{L} \right) \text{ J } \checkmark$$

Case when conductive of rod is a function of distance from end A.

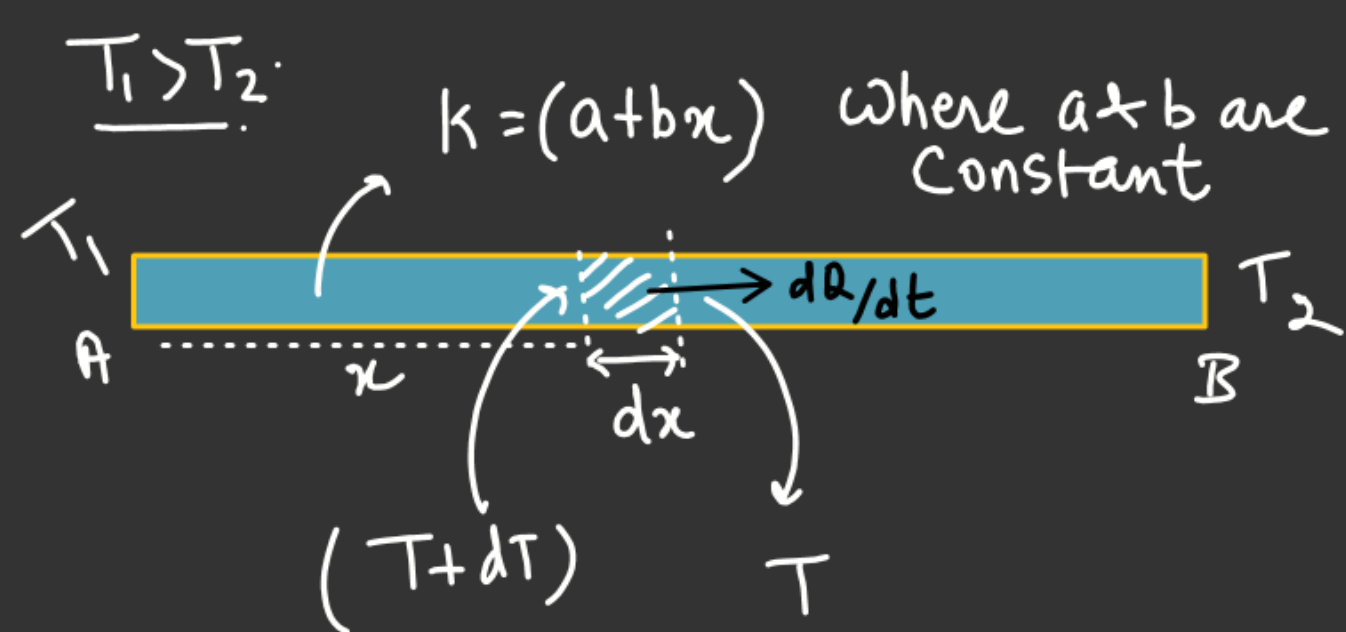
For dx length of rod.

$$\frac{dQ}{dt} = -k_x A \left(\frac{dT}{dx} \right)$$

\Downarrow

$$P = -(a+bx)A \cdot \left(\frac{dT}{dx} \right)$$

$$P \int_0^L \frac{dx}{a+bx} = -A \int_{T_1}^{T_2} dT$$



$$P \frac{\ln[a+bx]_0^L}{b} = -A(T_2 - T_1)$$

$$P = \left[\frac{bA(T_1 - T_2)}{\ln\left(\frac{a+bL}{a}\right)} \right] \left[\int \frac{dx}{a+bx} = \frac{\ln(a+bx)}{b} \right]$$

Total rate of heat flow =:

★★.

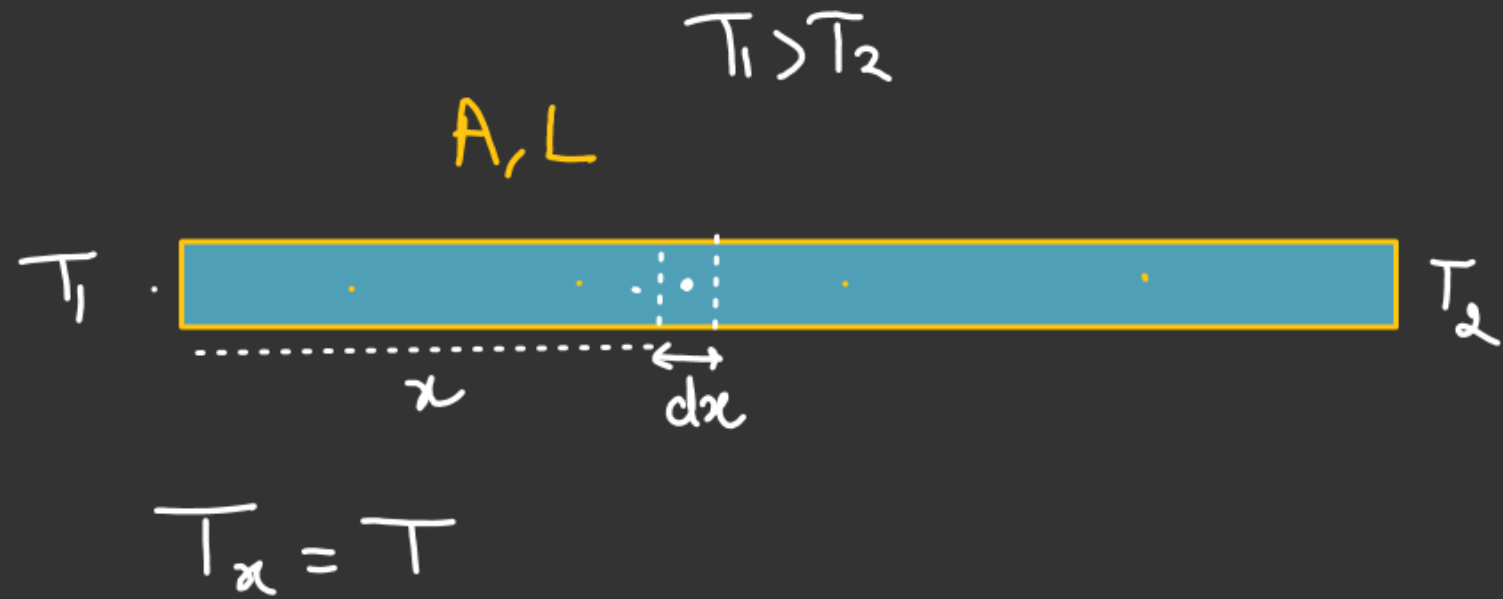
Case when thermal conductivity of rod as a function of temp of the rod

$$K = \left(\frac{\alpha}{T} \right) \quad \alpha = \text{Constant}$$

$$\left(\frac{dQ}{dt} \right) = -KA \left(\frac{dT}{dx} \right)$$

$$P = -\frac{\alpha}{T} A \frac{dT}{dx}$$

$$P \int_0^L dx = -\alpha A \int_{T_1}^{T_2} \left(\frac{dT}{T} \right)$$



$$P(L) = -\alpha A \ln \left(\frac{T_2}{T_1} \right)$$

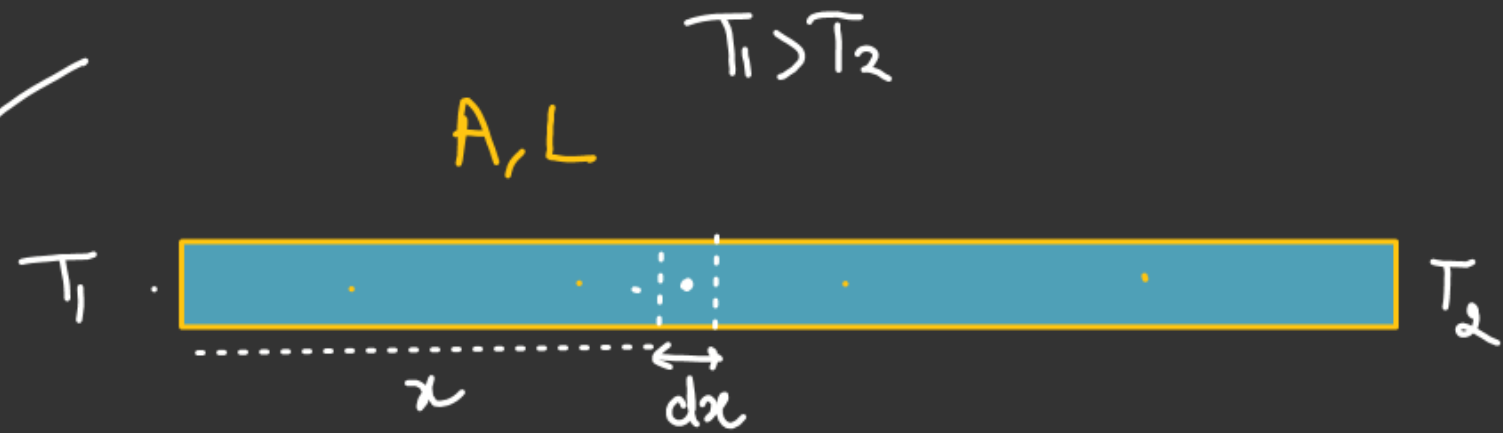
$$P = \frac{\alpha A}{L} \ln \left(\frac{T_1}{T_2} \right)$$

✓✓

Case when thermal conductivity of rod as a function of temp of the rod

✓✓ $K = \left(\frac{\alpha}{T} \right)$ $\alpha = \text{Constant}$, ✓

$T \rightarrow f(x) = ??$



$\left(\frac{dQ}{dt} \right) = -KA \left(\frac{dT}{dx} \right)$

$P = -\frac{\alpha}{T} A \frac{dT}{dx}$

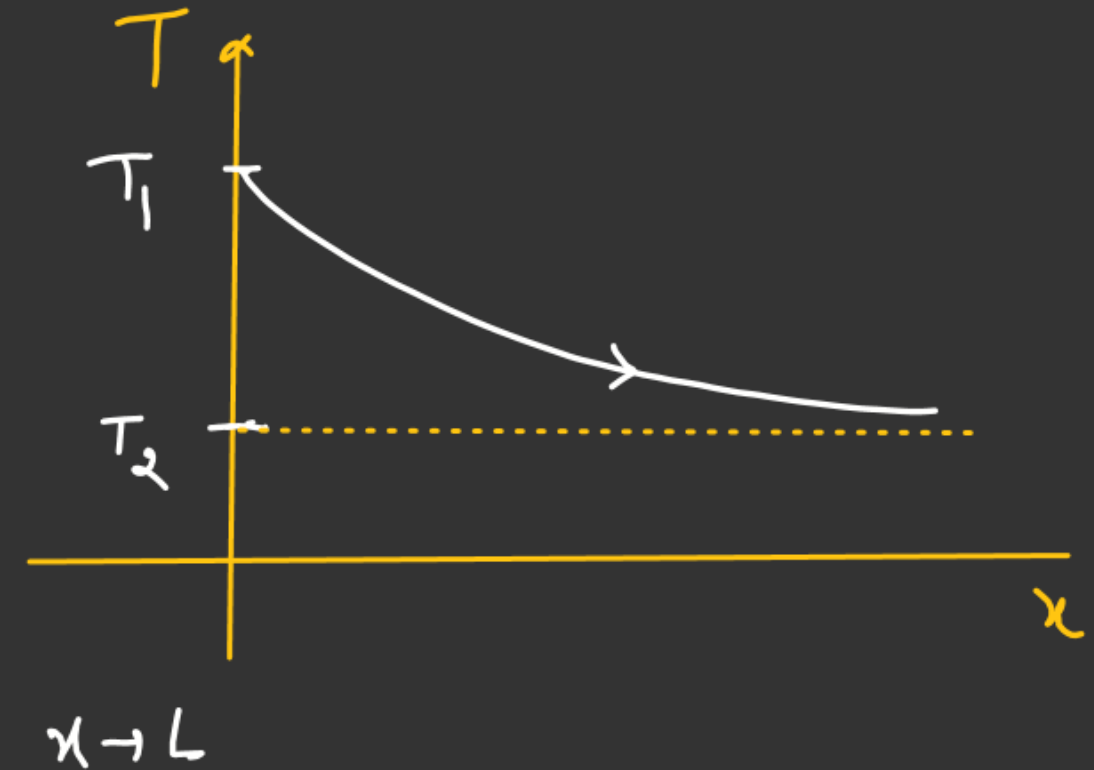
$P \int_0^x dx = -\alpha A \int_{T_1}^T \left(\frac{dT}{T} \right)$

$Px = -\alpha A \ln \left(\frac{T}{T_1} \right)$

$-\frac{P}{\alpha A} x = \ln \left(\frac{T}{T_1} \right)$

$\frac{T}{T_1} = e^{-\frac{P}{\alpha A} x}$

$T = T_1 e^{-\frac{P}{\alpha A} x}$

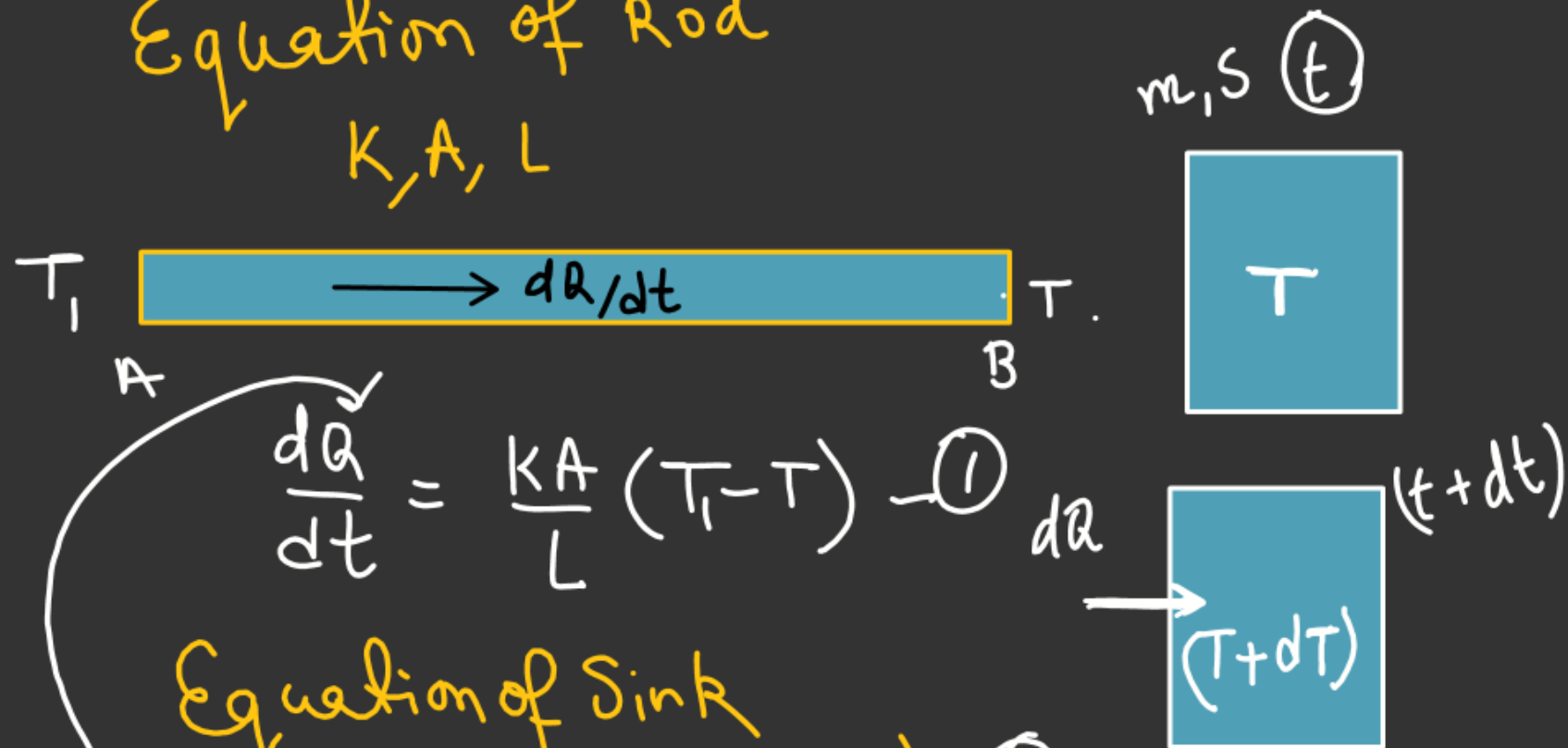


Heat flow in a Sink

At $t=0$, T_1 & T_2 be the temp of end A & B.

let, at any time 't' temp of end B or Sink be T .

Equation of Rod
 K, A, L

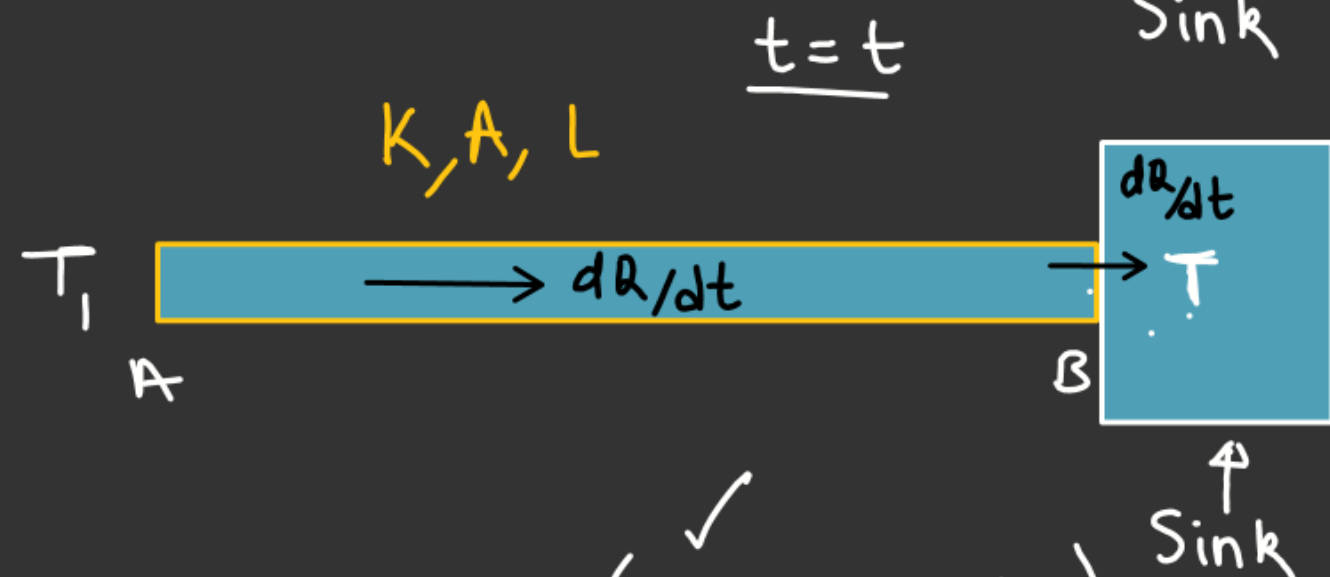
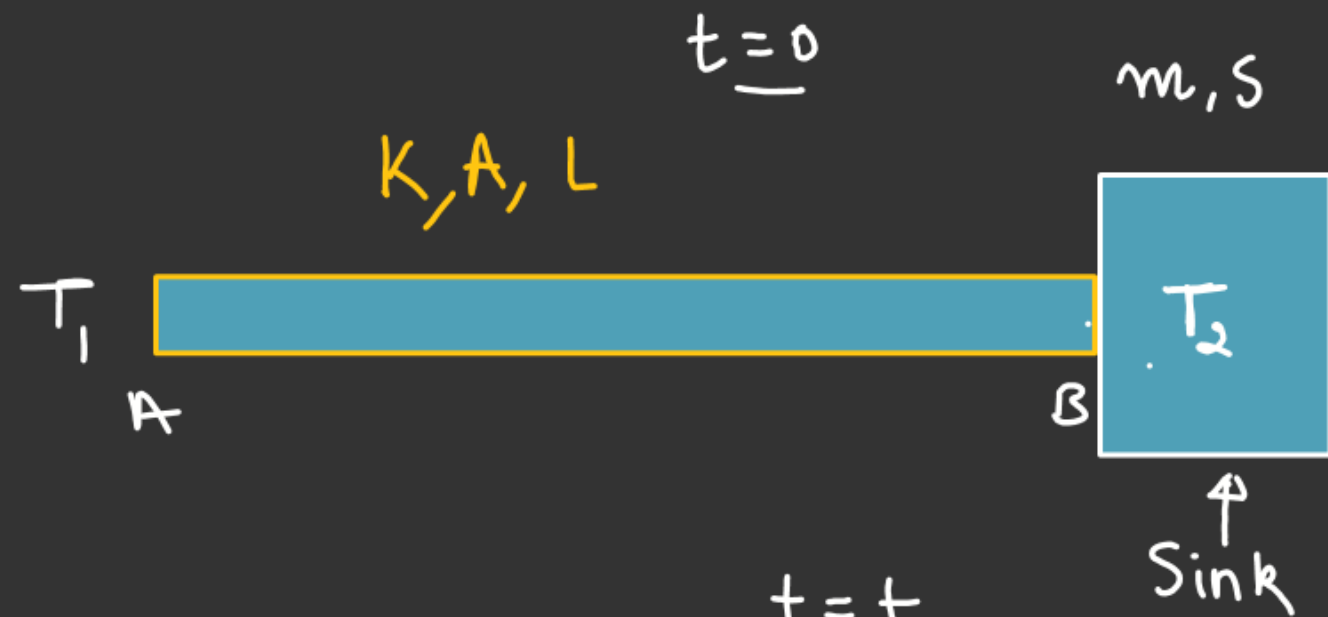


$$\frac{dQ}{dt} = \frac{KA}{L} (T_1 - T) \quad (1)$$

Equation of Sink

$$dQ = (msdT) \quad (2)$$

$$T_1 > T_2$$



$$(dQ = msdT)$$

Specific heat
 $ms \rightarrow$ heat capacity

★ ★

$$\frac{dQ}{dt} = \frac{KA}{L} (T_1 - T) \quad \text{--- (1)}$$

Equation of Sink

$$dQ = (msdT) \quad \text{--- (2)}$$

From (1) & (2)

$$ms \frac{dT}{dt} = \frac{KA}{L} (T_1 - T)$$

$$\int_{T_2}^T \frac{dT}{T_1 - T} = \frac{KA}{msL} \int_0^t dt$$

$$\frac{\ln [T_1 - T]_{T_2}^T}{(-1)} = \frac{KA}{msL} t$$

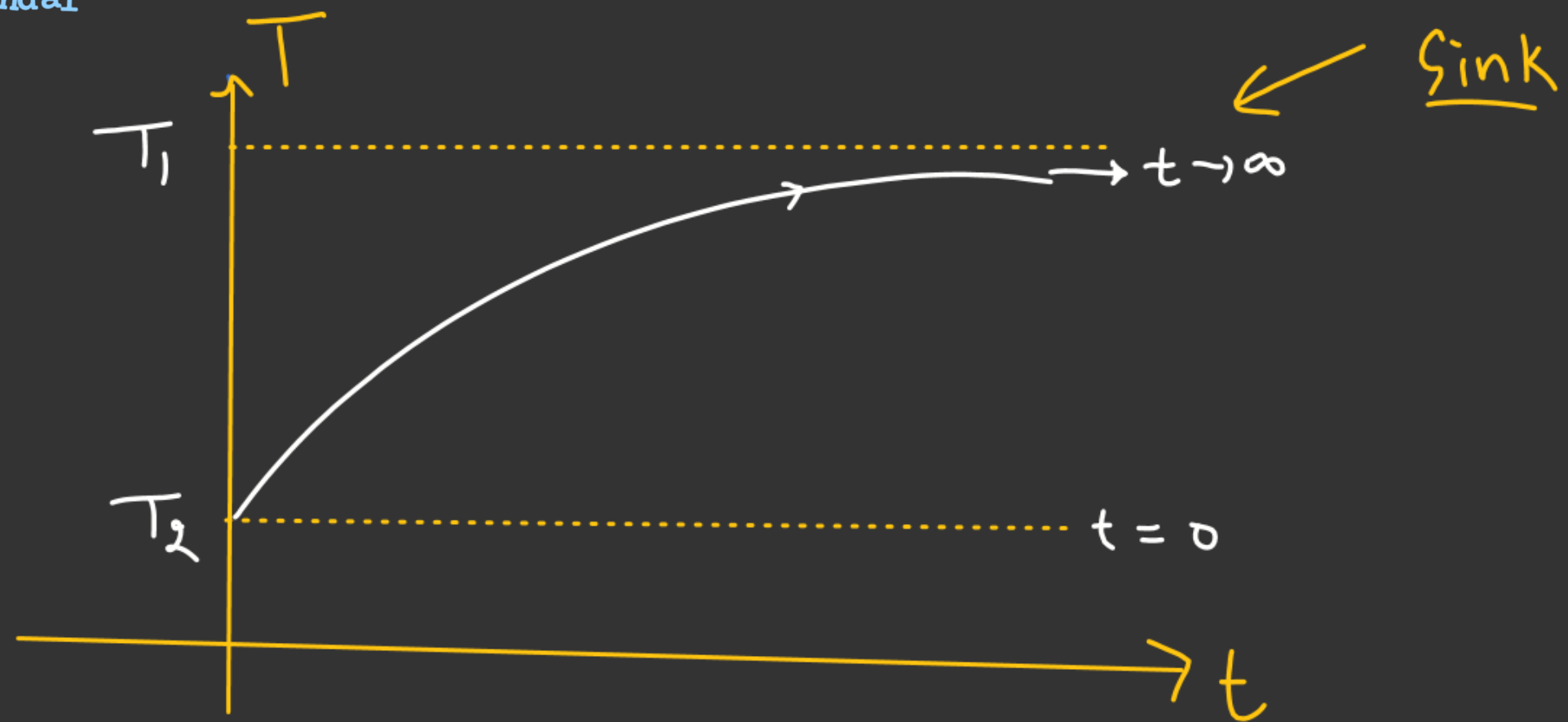
$$\ln (T_1 - T) - \ln (T_1 - T_2) = \frac{-KA}{msL} t$$

$$\ln \left(\frac{T_1 - T}{T_1 - T_2} \right) = \frac{-KA}{msL} t$$

$$T_1 - T = (T_1 - T_2) e^{\frac{-KA}{msL} t}$$

$$T = T_1 - (T_1 - T_2) e^{\frac{-KA}{msL} t}$$

★ ★

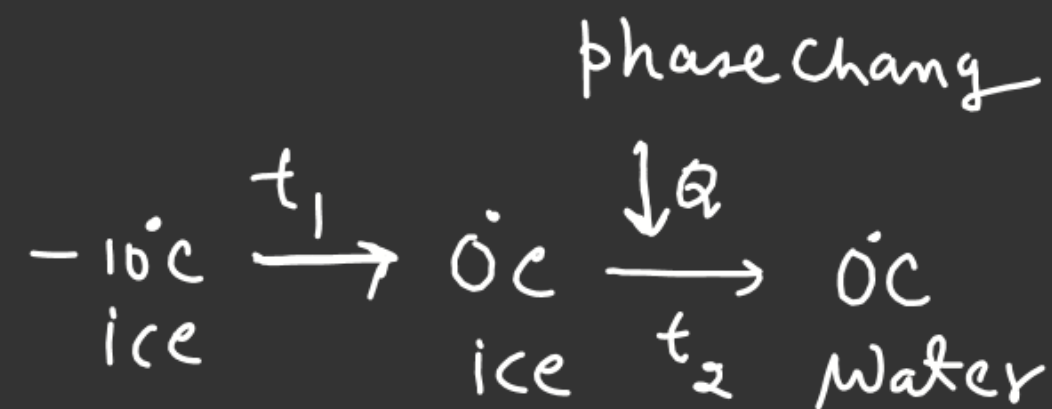


H.W

Find time 't' to melt the ice Cube.



$$t = (t_1 + t_2)$$



$$(Q = mL_f)$$