

## EE210: HW-8Z Solution

Date: 05/03/2019

**Q1.** Consider the BJT circuit show in the Fig. 1. Determine the values of  $R_C$  and  $R_B$  that would make the transistor Q operate at the bias point of  $I_C = 0.5 \text{ mA}$  and  $V_{CE} = 3 \text{ V}$ . Assume  $V_{CC} = V_B = 5 \text{ V}$ , and  $\beta = 100$ . Keeping the value of  $R_B$  unchanged, determine the new value of  $R_C$  that would make the transistor operate at the onset of saturation. Now, assume that this value of  $R_C$  is further doubled. What is the new mode of operation of Q, and what is its degree of saturation (DoS) under this condition?

**Solution:**

$$R_C = \frac{V_{CC} - V_{CE}}{I_C} = \frac{5 - 3}{0.5 \text{ mA}} = 4 \text{ k}\Omega$$

$$I_B = \frac{I_C}{\beta} = \frac{0.5 \text{ mA}}{100} = 5 \mu\text{A}$$

$$R_B = \frac{V_B - V_{BE}}{I_B} = \frac{5 - 0.7}{5 \mu\text{A}} = 860 \text{ k}\Omega$$

At onset of saturation,  $V_{CE} = 0.7 \text{ V}$

With  $I_B$  unchanged,  $I_C$  will remain unchanged, then

$$R_C = \frac{V_{CC} - V_{CE}}{I_C} = \frac{5 - 0.7}{0.5 \text{ mA}} = 8.6 \text{ k}\Omega$$

With  $R_C$  further doubled to  $17.2 \text{ k}\Omega$ , the potential drop across it will drive of into hard saturation, with  $V_{CE}(\text{sat}) = 0.2 \text{ V}$  (assumed).

$$I_{C,\text{sat}} = \frac{5 - 0.2}{17.2 \text{ k}\Omega} = 279 \mu\text{A}$$

(Note the reduction in  $I_C$ ).

$V_{BE}$  will adjust itself to  $0.8 \text{ V}$  in hard saturation (Why? – Because of increase in base current as discussed in the class.).

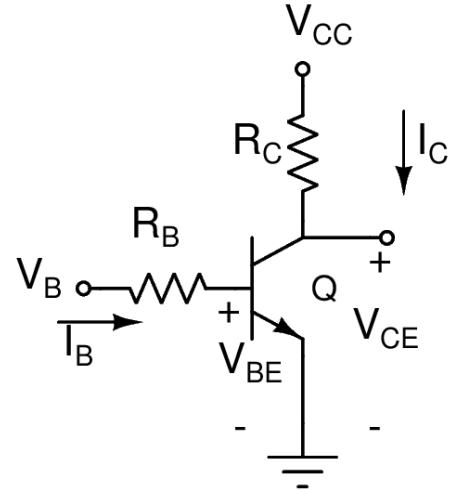
Therefore,

$$I_{B,\text{sat}} = \frac{5 - 0.8}{860 \text{ k}\Omega} = 4.88 \mu\text{A}$$

$$\beta_{\text{sat}} = \frac{I_{C,\text{sat}}}{I_{B,\text{sat}}} = \frac{279}{4.88} = 57$$

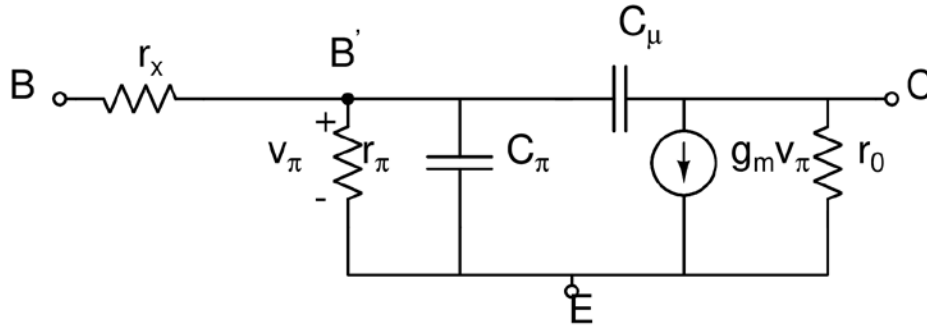
Degree of saturation (DoS),

$$DoS = \frac{\beta}{\beta_{\text{sat}}} = \frac{100}{57} = 1.75$$



**Q2.** The total emitter-base capacitance  $C_\pi$  for an npn transistor under forward active mode of operation is measured to be 6 pF and 8 pF at dc bias current  $I_C$  of 1 mA and 2mA respectively. Determine the zero-bias emitter-base junction capacitance  $C_{je0}$  (using the thumb rule given in class for forward biased junctions), and the base transit time  $\tau_F$ , assuming that both of these are constants.

**Solution:**



$$C_\pi = C_{je} + g_m \tau_F$$

$\therefore (C_{je1} = C_{je2})$ , we have

$$C_{\pi 2} - C_{\pi 1} = \tau_F (g_{m2} - g_{m1})$$

$$8pF - 6pF = \tau_F \left( \frac{2mA}{26mV} - \frac{1mA}{26mV} \right)$$

We get,

$$\tau_F = 52 pSec$$

$$C_{je} = 6 pF - 52 pSec \times \frac{1}{26} = 4 pF$$

$\therefore$  EB junction is forward biased, apply thumb rule (empirical),

$$C_{je} = 2C_{je0}$$

Which, gives  $C_{je0}=2$  pf.

**Q3.** An integrated-circuit npn transistor has  $\beta_0 = 100$ , and  $r_o = 50$  k $\Omega$  at  $I_C = 1$  mA. With  $V_{CB}$  held constant at 10 V,  $C_\mu = 0.15$  pF, and  $f_T = 600$  MHz and 1 GHz for  $I_C = 1$  mA and 10 mA respectively. Assume  $V_{bi} = 0.55$  V for all junctions, and  $C_{je}$  is constant in the forward-bias region. Use  $r_\mu = 5 \beta_0 r_o$ . Form the complete small-signal equivalent circuits for this transistor at  $I_C = 0.1$  mA, 1 mA and 5 mA, all with  $V_{CB}$  held constant at 2 V.

**Solution:**

For both  $I_C = 1$  mA & 10 mA,  $V_{CB}$  is held constant at 10 V.  $\Rightarrow C_\mu$  remains constant,

$$f_T = \frac{g_m}{2\pi(C_\pi + C_\mu)} = \frac{1}{2\pi\tau}$$

Where,  $\tau$  is an effective time constant  $= \frac{C_\pi + C_\mu}{g_m}$ .

For  $I_C = 1 \text{ mA}$ ,

$$\tau_1 = \frac{1}{2\pi f_{\tau 1}} = \frac{1}{2\pi * 600 \text{ MHz}} = 0.265 \text{ nSec}$$

For  $I_C = 10 \text{ mA}$ ,

$$\tau_2 = \frac{1}{2\pi f_{\tau 2}} = 0.159 \text{ nSec.}$$

Thus,

$$0.265 \text{ nsec} = \frac{C_\pi + C_\mu}{g_{m1}} = \tau_f + \frac{C_{je} + C_\mu}{g_{m1}}$$

$\because \tau_f, C_{je} \text{ \& } C_\mu$  are constants, with  $g_{m1} = \frac{1}{26} \text{ U}$ .

$$0.159 \text{ nsec} = \tau_f + \frac{C_{je} + C_\mu}{g_{m2}}$$

With  $g_{m2} = \frac{1}{2.6} \text{ U}$ ,  $C_\mu = 0.15 \text{ pf}$  is given. Solving, we get

$$C_{je} = 4.38 \text{ pf}$$

$$\tau_f = 147.22 \text{ pSec}$$

Assuming that the junction is abrupt,  $C_\mu = \frac{C_{\mu 0}}{\left(1 - \frac{V_{BC}}{V_{bi}}\right)^{0.5}}$

With  $V_{BC} = -10 \text{ V}$ ,  $C_\mu = 0.15 \text{ pf}$ , &  $V_{bi} = 0.55 \text{ V}$  (given), we get  $C_{\mu 0} = 0.657 \text{ pf}$

So, with  $V_{BC} = -2 \text{ V}$ ,

$$C_\mu = \frac{0.657 \text{ pf}}{\left(1 - \frac{2}{0.55}\right)^{0.5}} = 0.305 \text{ pF}, r_0 = 50 \text{ K}\Omega \text{ at } I_C = 1 \text{ mA then } V_A = I_C r_0 = 50 \text{ V.}$$

Now, we have all the required parameters to obtain the small-signal model.

**$I_C = 0.1 \text{ mA}$ :**  $g_m = 3.846 \text{ mU}$ ,  $r_\pi = 26 \text{ K}\Omega$ ,  $r_0 = 500 \text{ K}\Omega$ ,  $r_\mu = 250 \text{ M}\Omega$ ,

$C_b = \tau_f \cdot g_m = 0.566 \text{ pf}$ ,  $C_\pi = C_{je} + C_b = 4.946 \text{ pf}$ ,  $C_\mu = 0.305 \text{ pf}$ .

**$I_C = 1 \text{ mA}$ :**  $g_m = 38.46 \text{ mU}$ ,  $r_\pi = 2.6 \text{ K}\Omega$ ,  $r_0 = 50 \text{ K}\Omega$ ,  $r_\mu = 25 \text{ M}\Omega$ ,

$C_b = \tau_f \cdot g_m = 5.66 \text{ pf}$ ,  $C_\pi = C_{je} + C_b = 10.04 \text{ pf}$ ,  $C_\mu = 0.305 \text{ pf}$ .

**$I_C = 5 \text{ mA}$ :**  $g_m = 192.3 \text{ mU}$ ,  $r_\pi = 520 \text{ }\Omega$ ,  $r_0 = 10 \text{ K}\Omega$ ,  $r_\mu = 5 \text{ M}\Omega$ ,

$C_b = \tau_f \cdot g_m = 28.31 \text{ pf}$ ,  $C_\pi = C_{je} + C_b = 32.69 \text{ pf}$ ,  $C_\mu = 0.305 \text{ pf}$ .

\*Check all these numbers for their correctness\*

The small signal model will be identical to that given in class.

**Q4.** An integrated-circuit npn transistor has the following parameters:  $\tau_F = 0.25$  nsec, small-signal short-circuit common-emitter current gain is 9 with  $I_C = 1$  mA at frequency  $f = 50$  MHz,  $V_A = 40$  V,  $\beta_0 = 100$ , and  $C_\mu = 0.6$  pF at the bias voltage used. Determine all elements in the small-signal equivalent circuit at  $I_C = 2$  mA, assuming that  $V_{CB}$  is held constant (as that for  $I_C = 1$  mA), and  $\tau_F$  remains constant.

**Solution:**

$$\beta = \frac{\beta_0}{1 + j \frac{f}{f_\beta}}$$

Now, with  $\beta_0 = 100$  &  $\beta$  of only 9 at  $f = 50$  MHz, let's assume that  $f \gg f_\beta$ .

$$|\beta| = \frac{\beta_0 \cdot f_\beta}{f} = \frac{f_T}{f} \Rightarrow f_T = f|\beta| = 50 \text{ MHz} * 9 = 450 \text{ MHz}$$

Now,

$$f_T = \frac{g_m}{2\pi(C_\pi + C_\mu)} \Rightarrow C_{je} + \tau_f g_m + C_\mu = \frac{g_m}{2\pi f_T}$$

It is given that  $I_C = 1$  mA. Thus

$$g_m = \frac{1}{26} \text{ V}, \tau_f = 0.25 \text{ nSec} \text{ \& } C_\mu = 0.6 \text{ pf}$$

$$C_{je} = \frac{1}{26 \times 2\pi \times 450 \times 10^6} - 0.25 \text{ nS} \times \frac{1}{26} - 0.6 \text{ pf} = 3.4 \text{ pf}$$

Small-signal model parameters for  $I_C = 2$  mA:

$$g_m = \frac{I_C}{V_T} = \frac{2 \text{ mA}}{26 \text{ mV}} = 76.923 \text{ mV}$$

$$r_\pi = \frac{\beta_0}{g_m} = 1.3 \text{ K}\Omega$$

$$r_o = \frac{V_A}{I_C} = 20 \text{ K}\Omega$$

$$C_{je} = 3.4 \text{ pf}$$

$$C_b = \tau_f g_m = 19.23 \text{ pf}$$

$$C_\pi = C_{je} + \tau_F g_m = 22.63 \text{ pf}$$

$$C_\mu = 0.6 \text{ pf}$$

\*Check all these numbers for their correctness\*

**Q5.** An npn transistor has the following specifications:  $\beta_0 = 100$ ,  $\tau_F = 26$  psec,  $C_{je} = 5$  pF, and  $C_\mu = 0.5$  pF at a particular bias point with  $I_C = 2$  mA. Determine the three important characteristic frequencies  $f_T$  (unity-gain cutoff frequency),  $f_\beta$  (beta-cutoff frequency), and  $f_\alpha$  (alpha-cutoff frequency) of the transistor at this bias point. Also, estimate  $f_{max}$  (absolute maximum operable frequency) of the transistor.

**Solution:**

$$C_\pi = C_{je} + \tau_F g_m = 5 \text{ pf} + 26 \text{ ps} \times \frac{2}{26} = 7 \text{ pf}$$

$$C_\mu = 0.5 \text{ pf (given)}$$

$$f_T = \frac{g_m}{2\pi(C_\pi + C_\mu)} = \frac{2}{26} \times \frac{1}{2\pi(7 \text{ pf} + 0.5 \text{ pf})} = 1.63 \text{ GHz}$$

$$f_\beta = \frac{f_T}{\beta_0} = 16.32 \text{ MHz}$$

(Note: how small  $f_\beta$  is as compared to  $f_T$ , of course, the difference depends on  $\beta_0$ )

$$f_\alpha = (\beta_0 + 1)f_\beta = 1.65 \text{ GHz}$$

(Note: that  $f_\alpha$  is so very slightly larger than  $f_T$ )

$$f_{max} = \frac{1}{2\pi\tau_f} = 6.12 \text{ GHz}$$

(way higher than  $f_\beta$ , and almost 4 times that of  $f_T$  and  $f_\alpha$ )

The transistor cannot be operated for any frequency higher than  $f_{max}$ .