

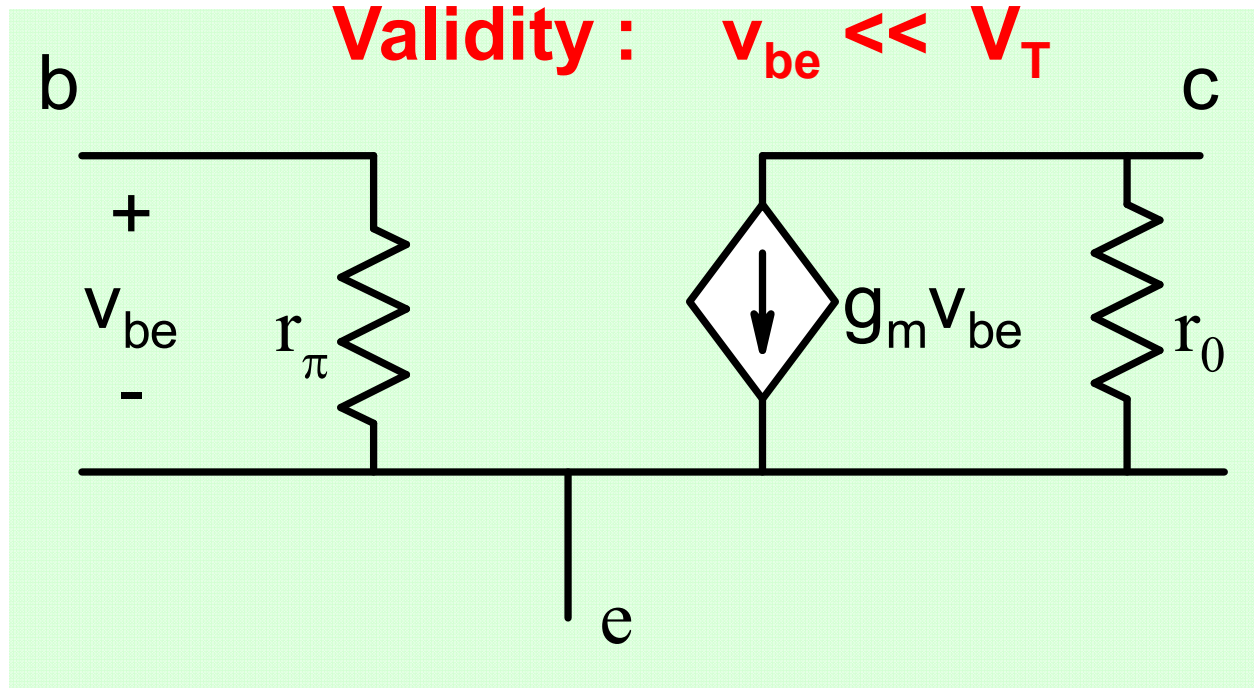
# EE210: Microelectronics-I

## Lecture-11 : Bipolar Junction Transistor-4

Instructor: Y. S. Chauhan

Slides from B. Mazhari  
Dept. of EE, IIT Kanpur

## Hybrid-pi Small Signal Model : low frequency



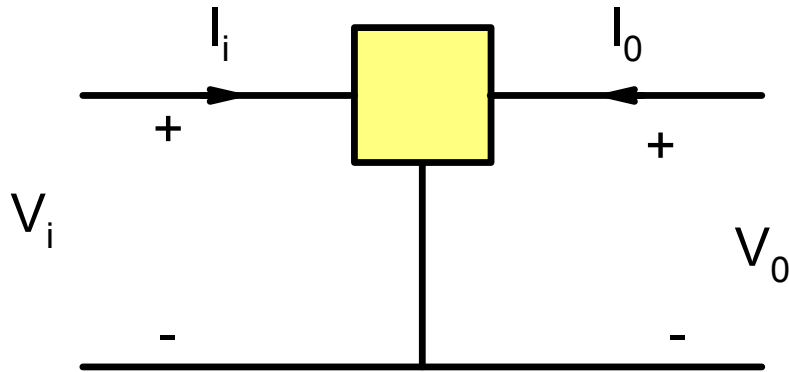
$$r_\pi = \frac{V_T}{I_B} = \frac{V_T}{I_C} \cdot \beta$$

$$g_m = \frac{I_C}{V_T} ; r_o = \frac{V_A}{I_C}$$

$$I_b = \frac{I_S}{\beta_F} \left( \exp\left(\frac{V_{be}}{V_T}\right) - 1 \right)$$

$$I_c = I_S \left( \exp\left(\frac{V_{be}}{V_T}\right) - 1 \right) \times \left( 1 + \frac{V_{ce}}{V_A} \right)$$

## Device is not strictly unilateral



$$I_i = f(V_i, V_o)$$

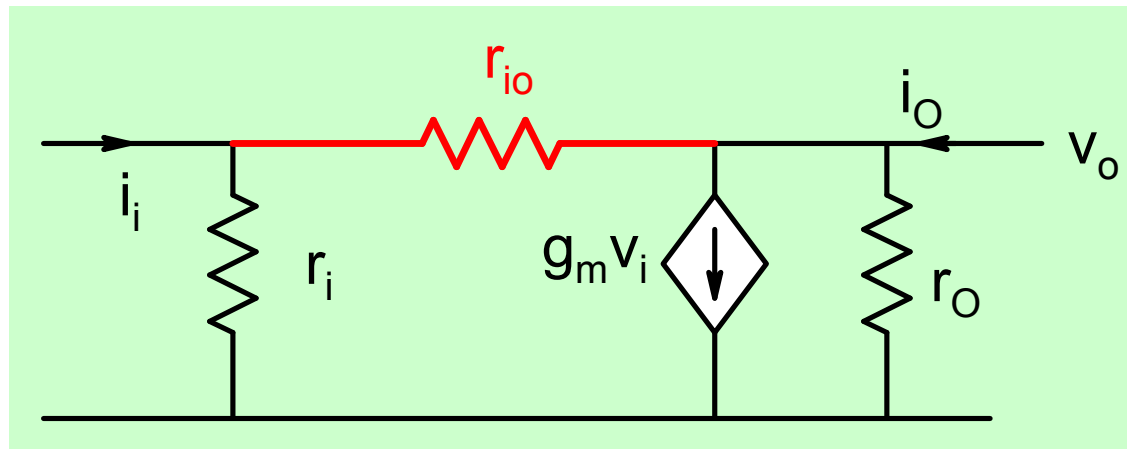
$$\Delta I_i = \left. \frac{\partial f}{\partial V_i} \right| \times \Delta V_i + \left. \frac{\partial f}{\partial V_o} \right| \times \Delta V_o$$

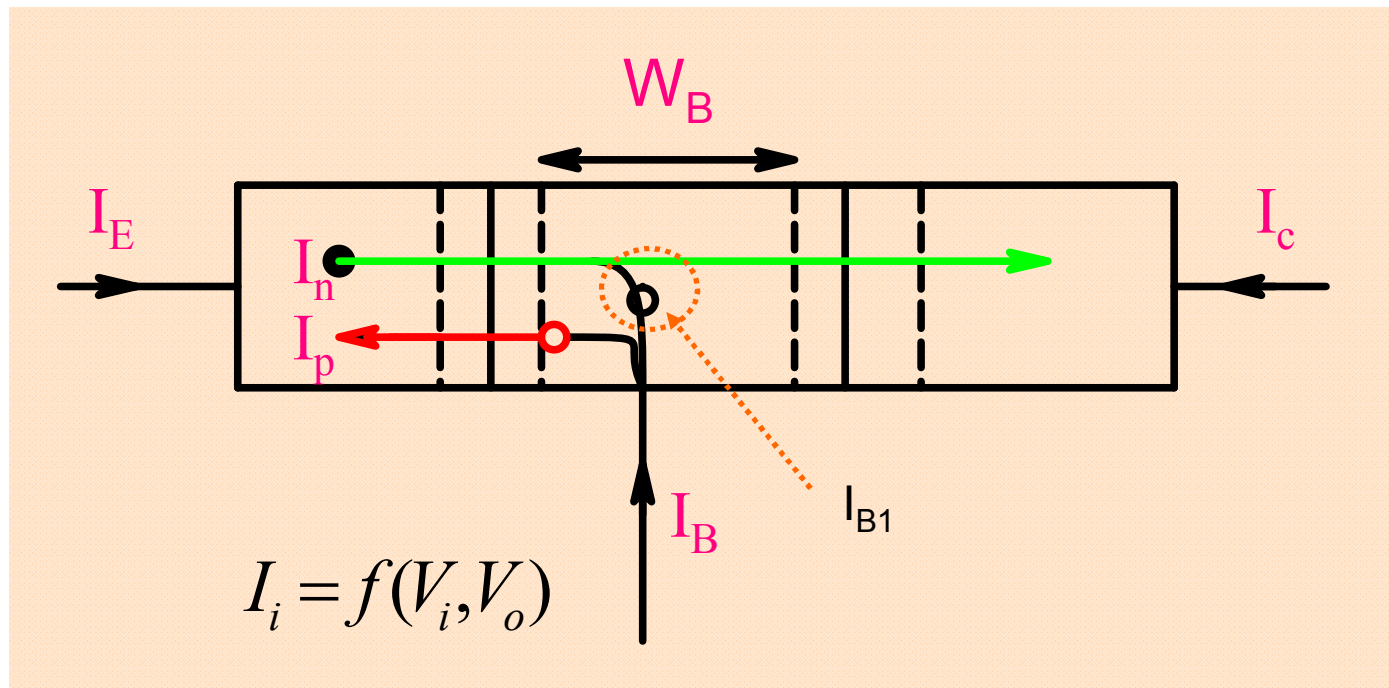
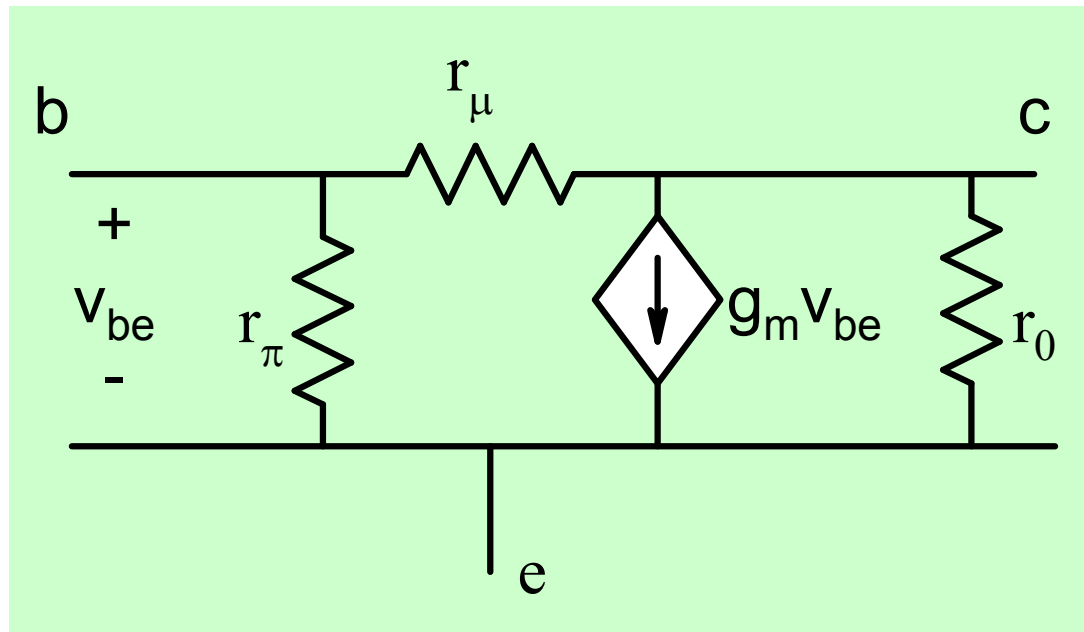
$$i_i = \frac{v_i}{r_i} - \frac{v_o}{r_{io}} \quad \text{---ve}$$

$$i_i = \left( \frac{v_i}{r_i} - \frac{v_i}{r_{io}} \right) + \frac{v_i - v_o}{r_{io}}$$

$$r_{io} \gg r_i$$

100+1~100  
100-99+1 =2





$$I_B = I_P + I_{B1}$$

$$I_{B1} \propto W_B$$

$$I_{B1} = f_1(V_{CB})$$

# **Capacitances and High Frequency Model**

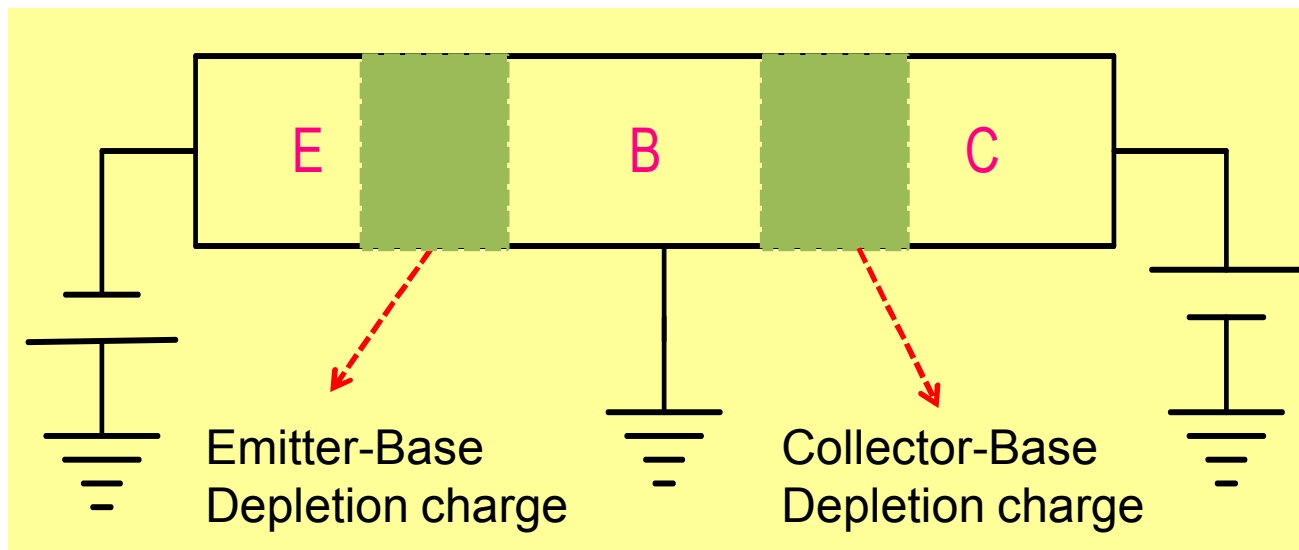
## Capacitances in a BJT

Anytime we have a charge which changes with voltage, we have a capacitance

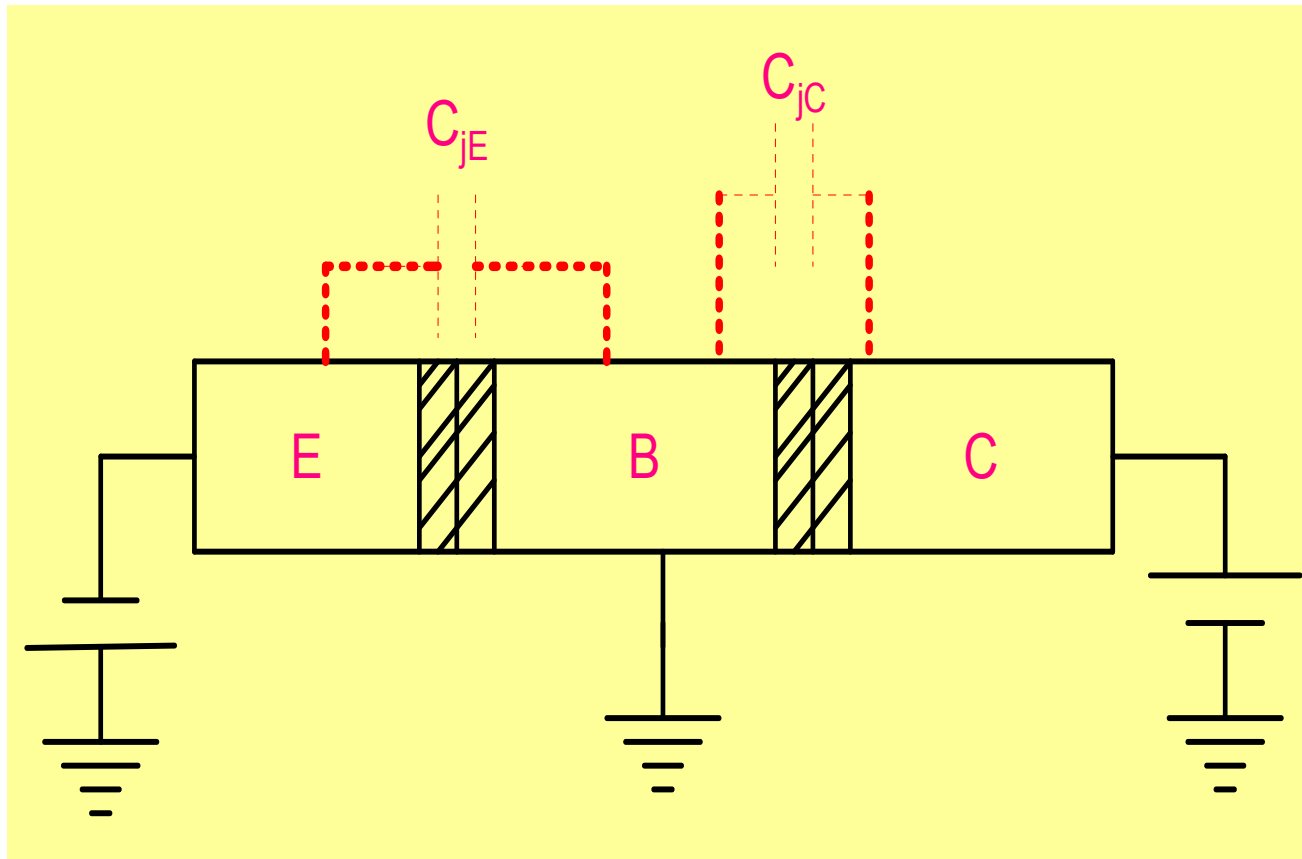
$$C = \frac{\partial Q}{\partial V}$$

There are two kinds of charges:

1. Depletion charge
2. Diffusion charge



Change in emitter-base depletion charge with base-emitter voltage gives rise to base-emitter junction capacitance. Similarly, change in collector-base depletion charge with base-collector voltage gives rise to base-collector junction capacitance

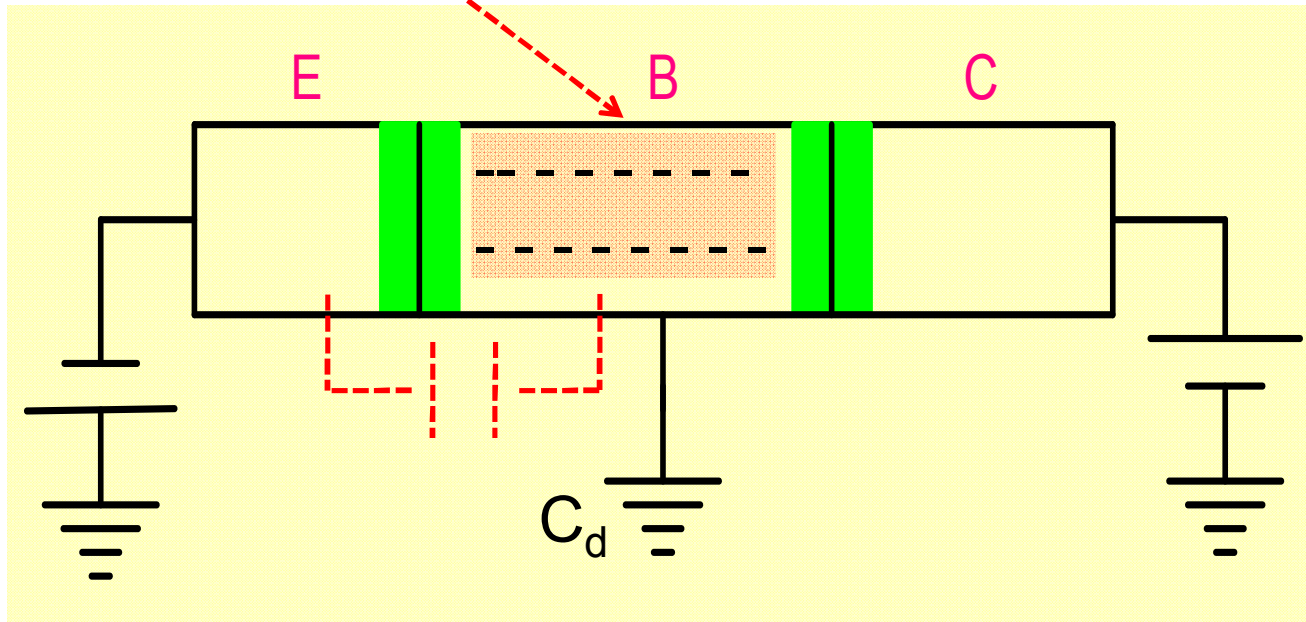


$$C_{je} = \frac{C_{jeo}}{\left(1 - \frac{V_{BE}}{V_{bi}}\right)^m}$$

$$C_{jc} = \frac{C_{jco}}{\left(1 - \frac{V_{BC}}{V_{bi}}\right)^m}$$

## Diffusion Charge and Capacitance

When base-emitter junction is forward biased, electrons are injected into base. These excess electrons constitute diffusion charge  $Q_D$



$$C_d = \frac{\partial Q_d}{\partial V_{be}}$$

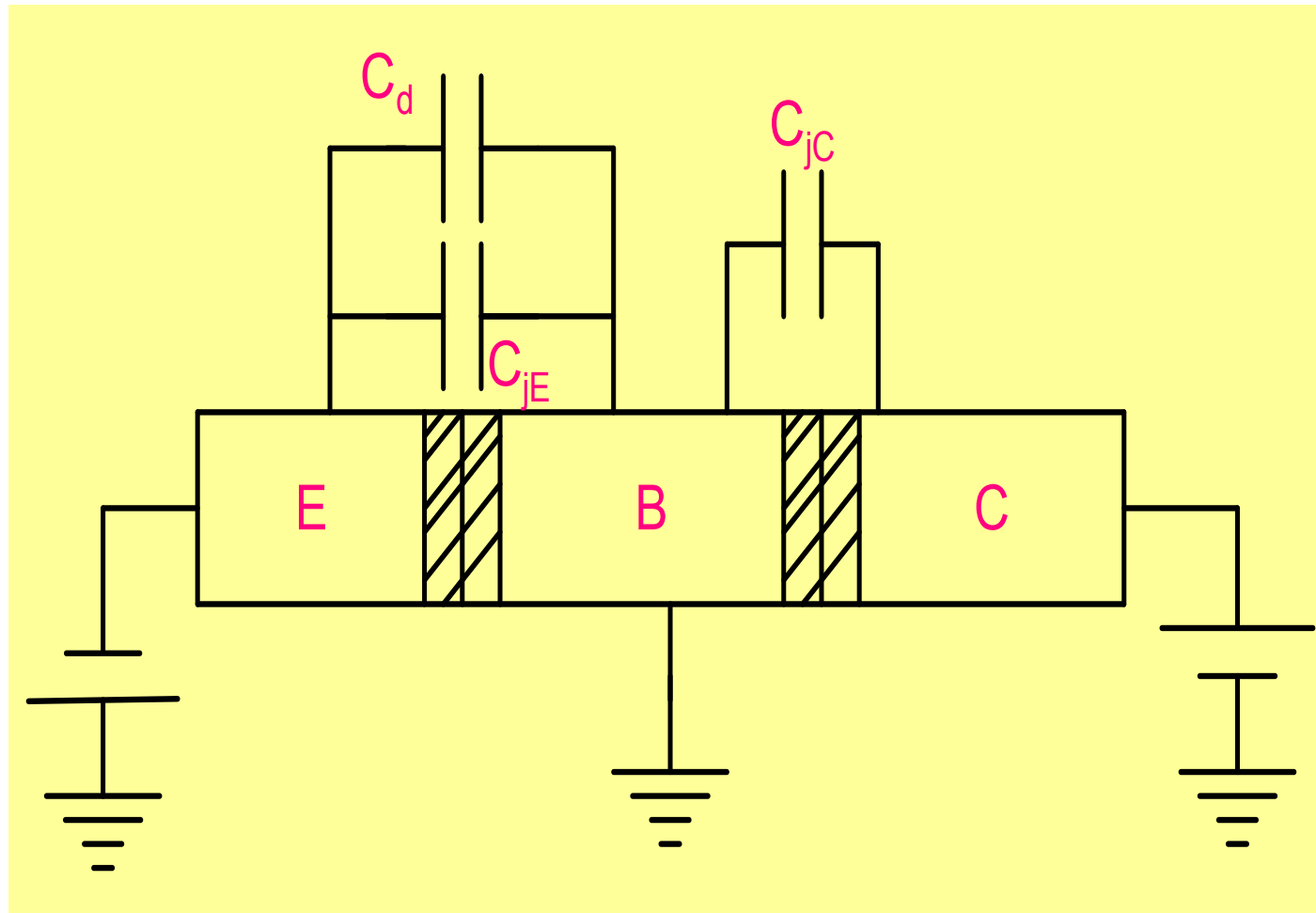
$$C_{diff} = \frac{I_C}{V_T} \times \tau_F$$
$$= g_m \times \tau_F$$

$$\tau_F = K \times \frac{W_B^2}{\mu} + \dots$$

In Forward active mode, collector-base junction is reverse biased so no carriers are injected and hence there is no collector-base diffusion capacitance .

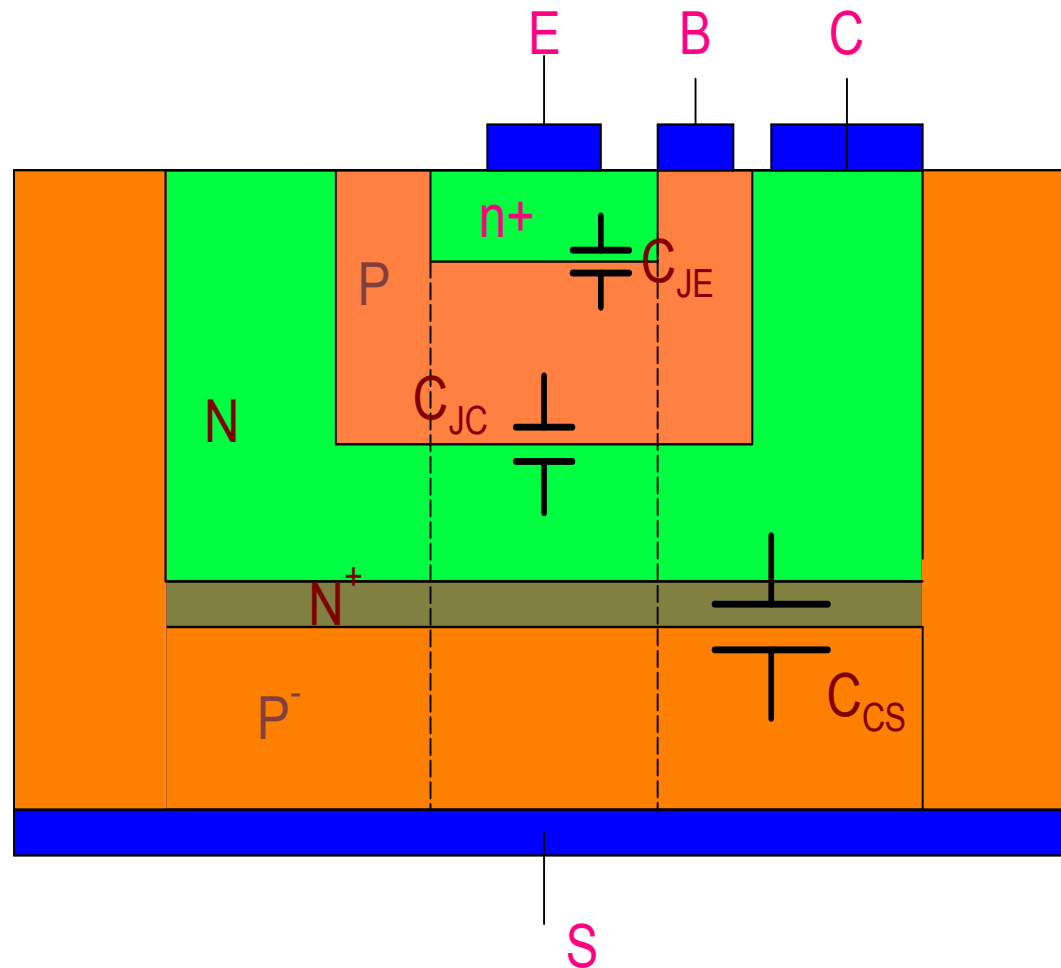


## Capacitances in a BJT



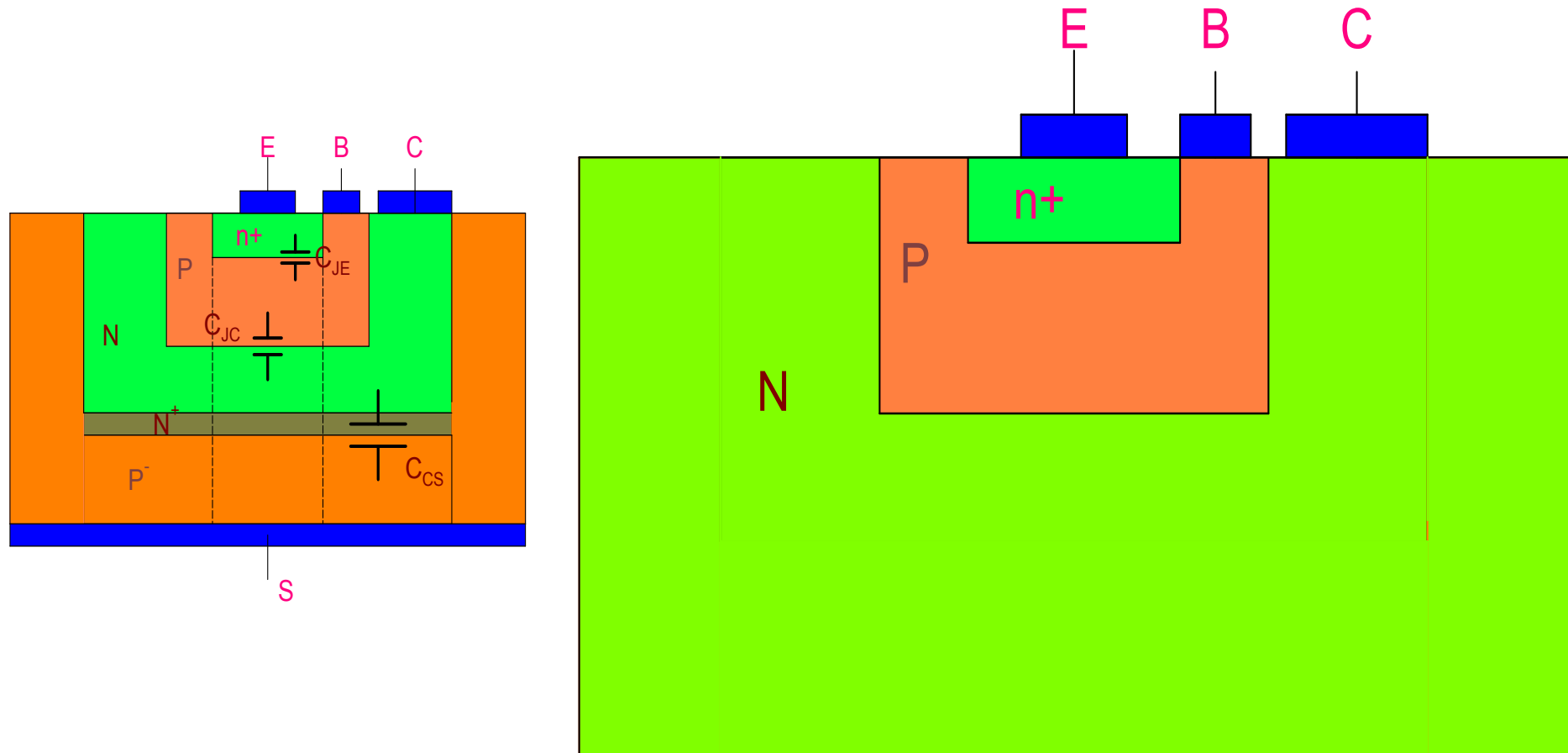
There is one more capacitance which is not observable in this one dimensional view of the transistor

## Collector Substrate Capacitance

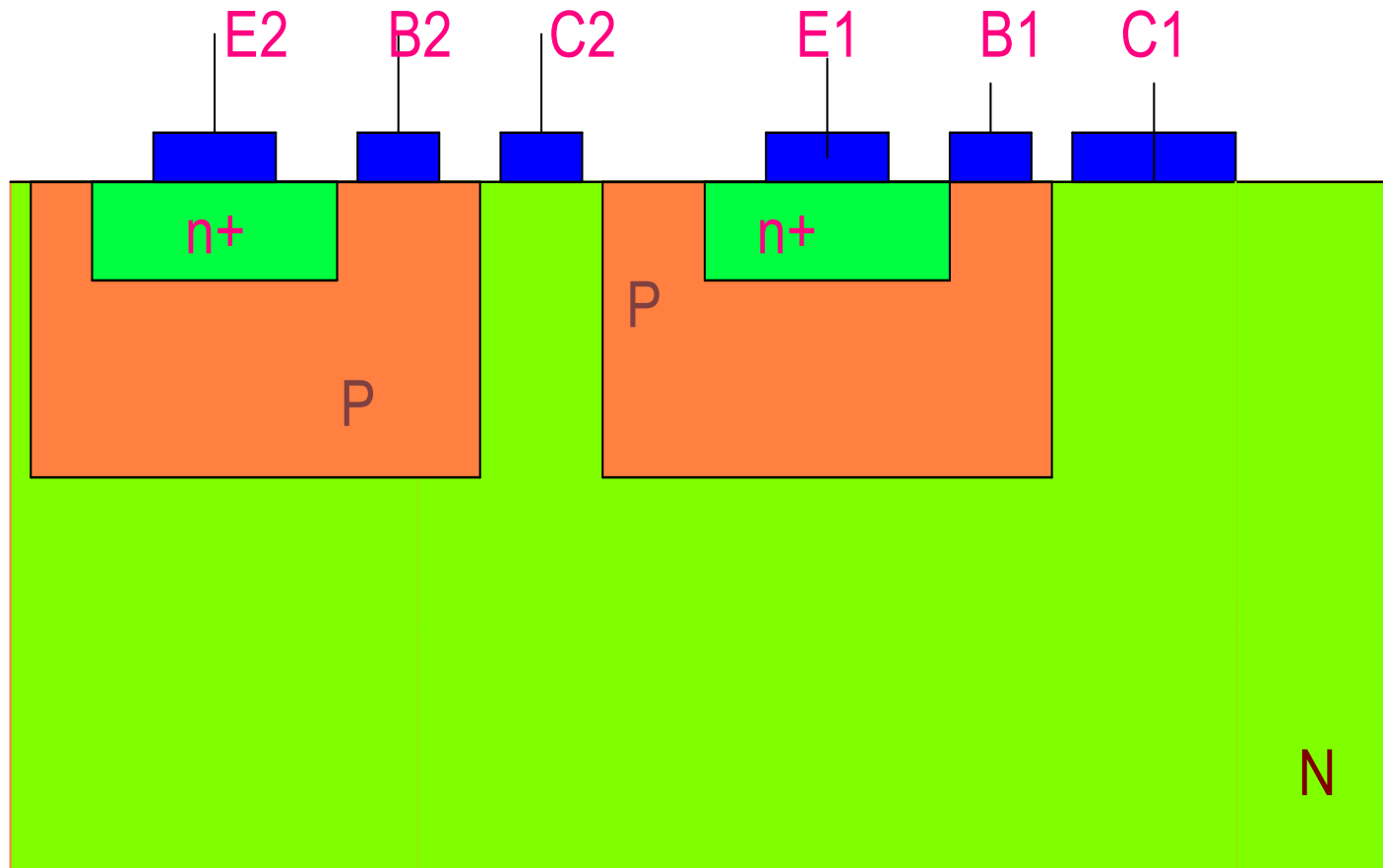


Why do we use a P substrate and not make a transistor on N-Silicon ?

## Transistor on an N-substrate that serves as a Collector

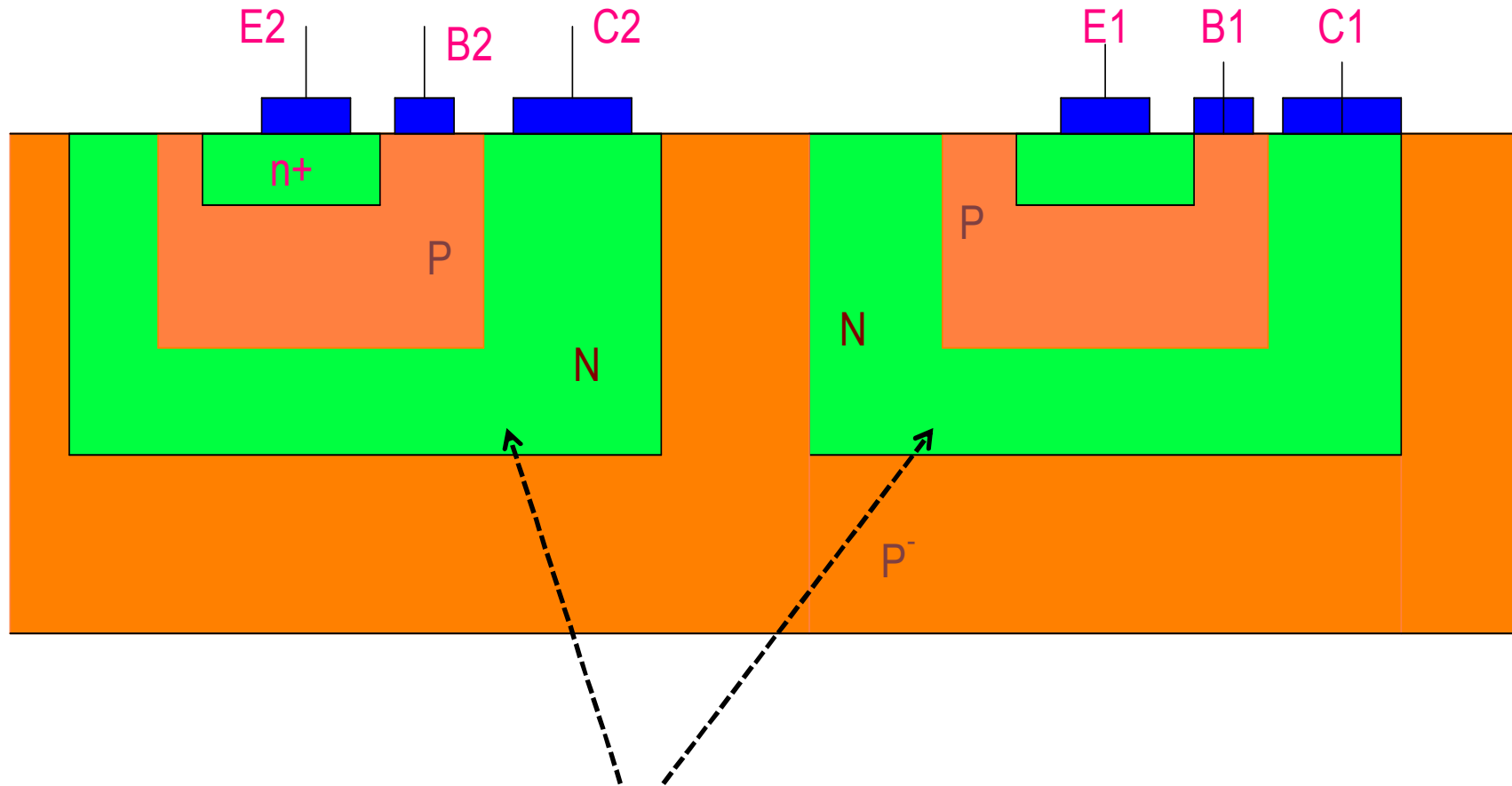


The problem is that we have to make not just one but several transistors on the same silicon substrate



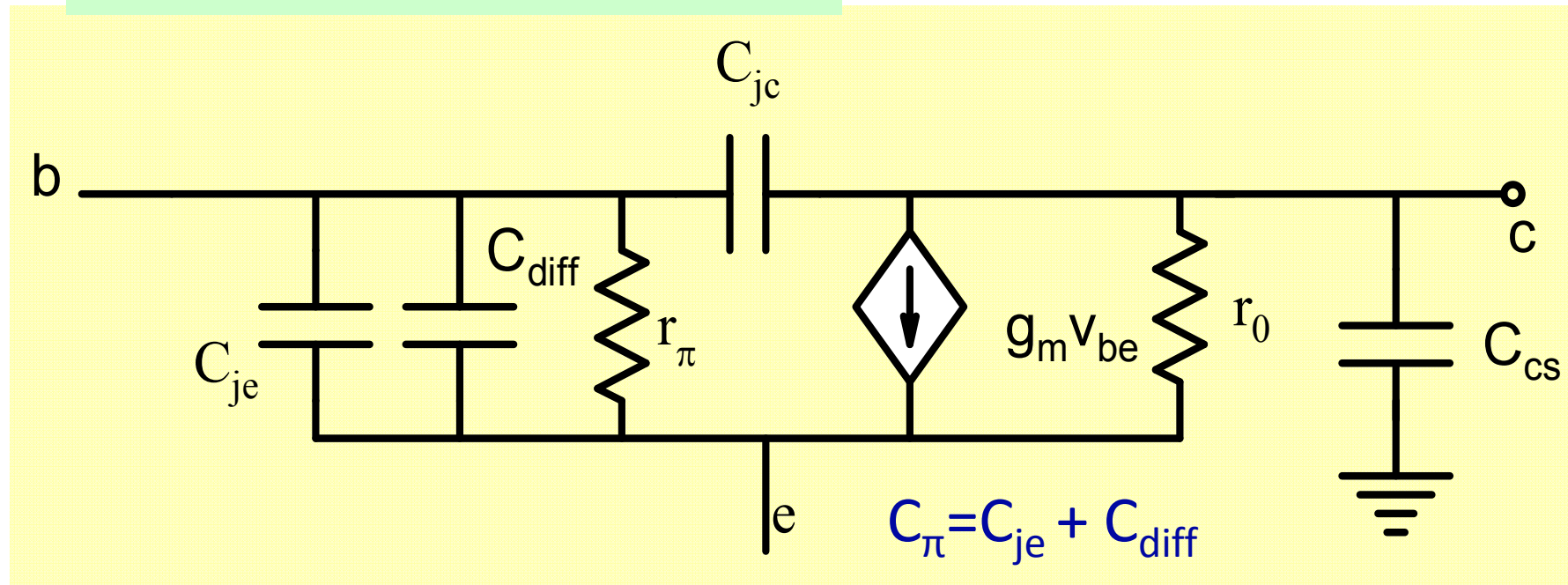
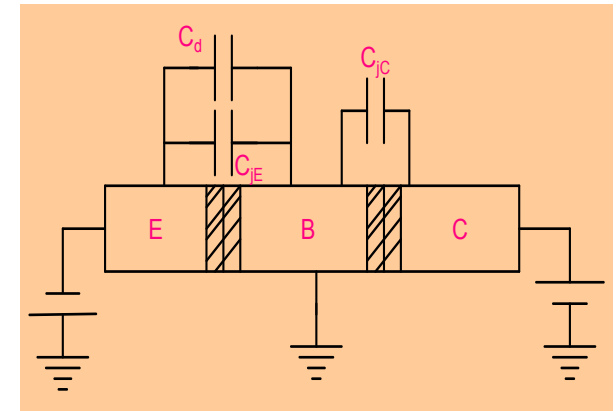
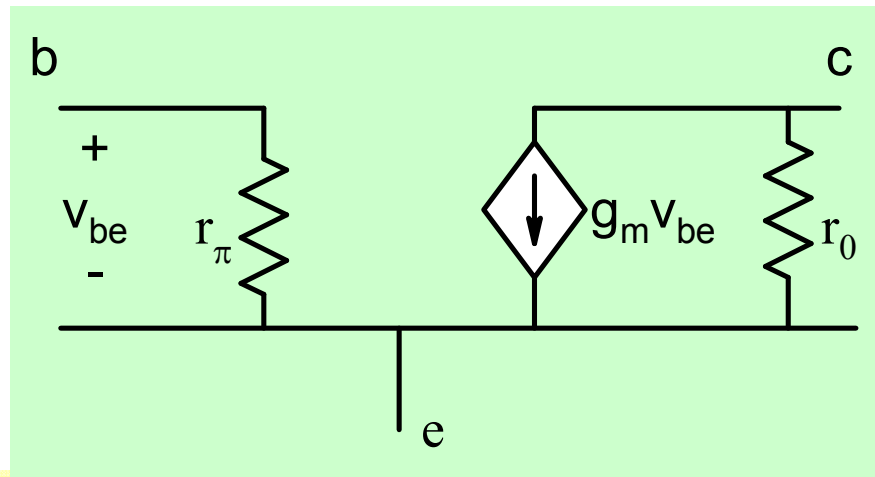
The two collectors are shorted together !

With a P-substrate, it is easy to isolate the transistors

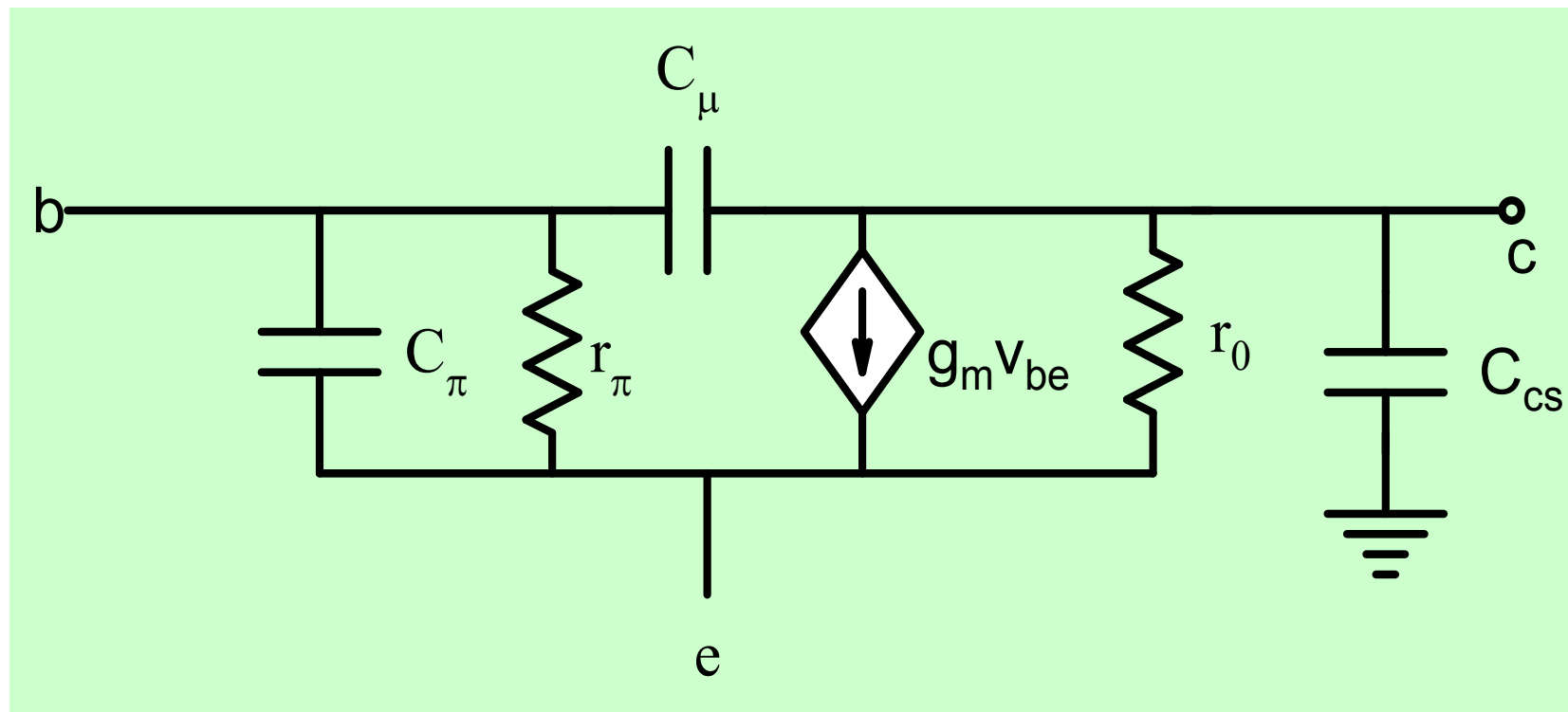


Reverse biased PN junction maintains isolation

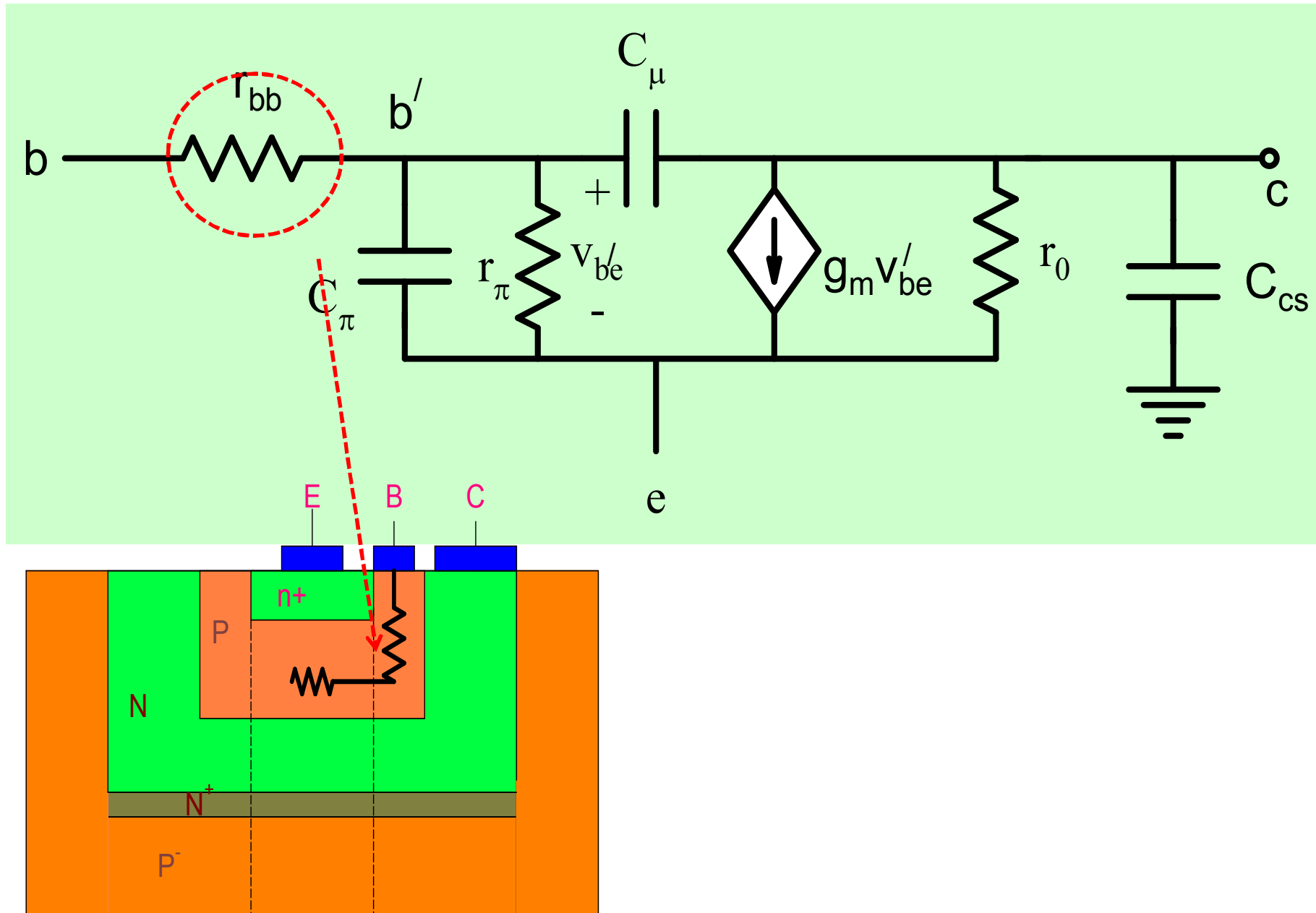
# High Frequency Hybrid-pi Model



$$C_\mu = C_{jc}$$



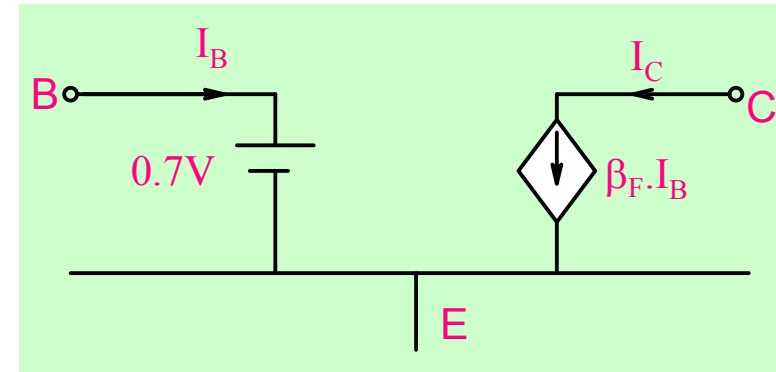
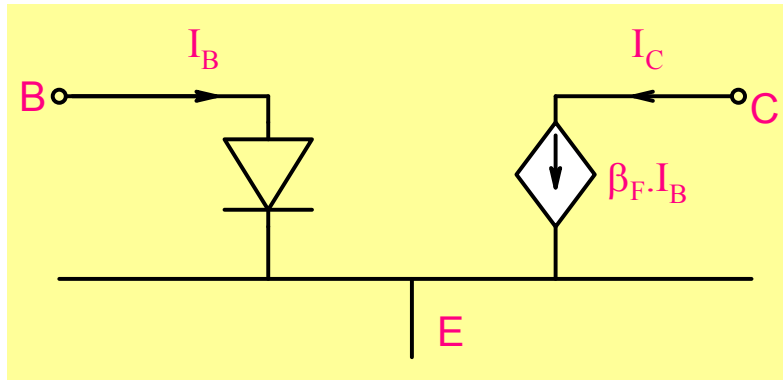
## High Frequency Hybrid-pi Model





# Summary

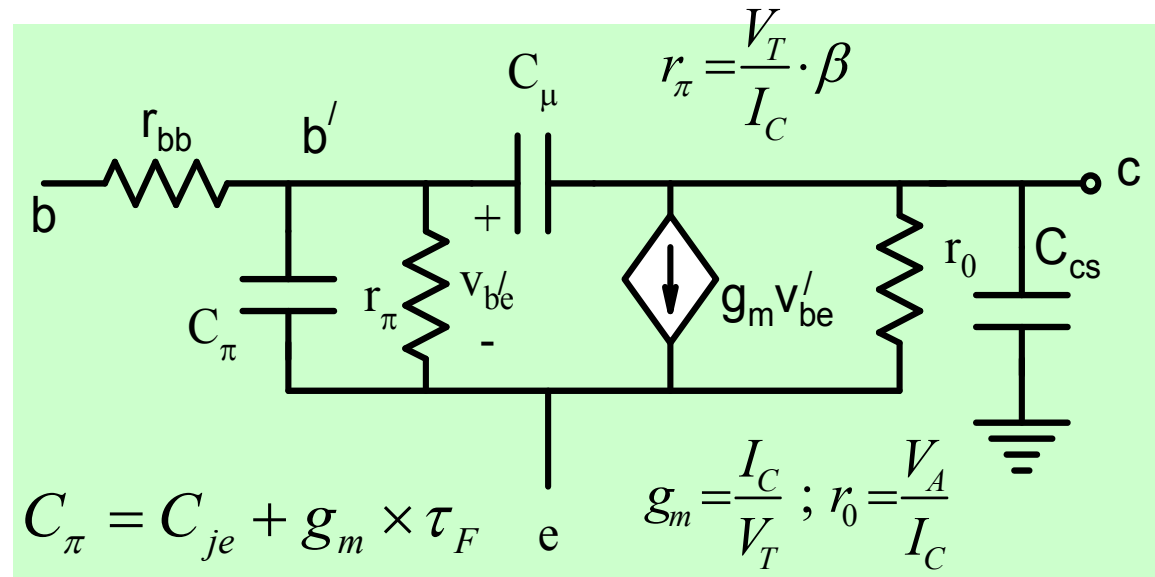
Model of an NPN BJT in forward active mode



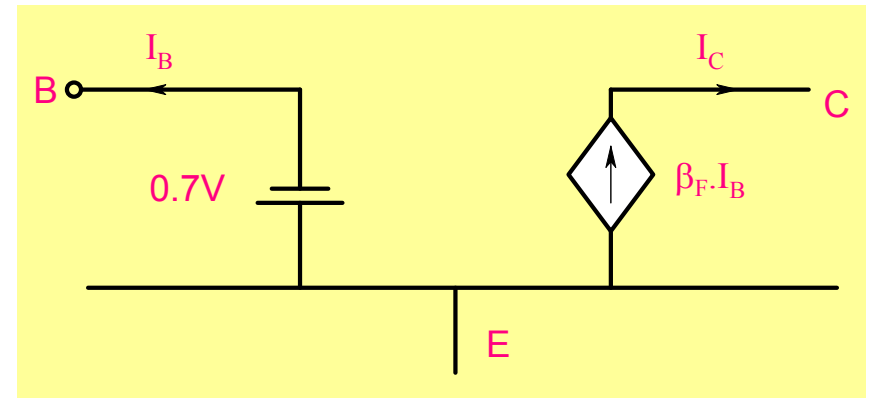
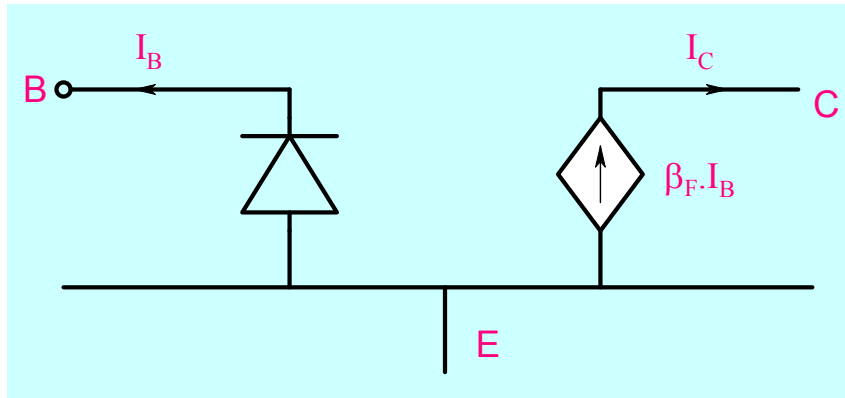
$$I_C = I_S \left( \exp\left(\frac{V_{BE}}{V_T}\right) - 1 \right) \left( 1 + \frac{V_{CE}}{V_A} \right)$$

$$I_B = \frac{I_S \left( \exp\left(\frac{V_{BE}}{V_T}\right) - 1 \right)}{\beta_F}$$

$$I_C = \beta_F I_B \left( 1 + \frac{V_{CE}}{V_A} \right)$$



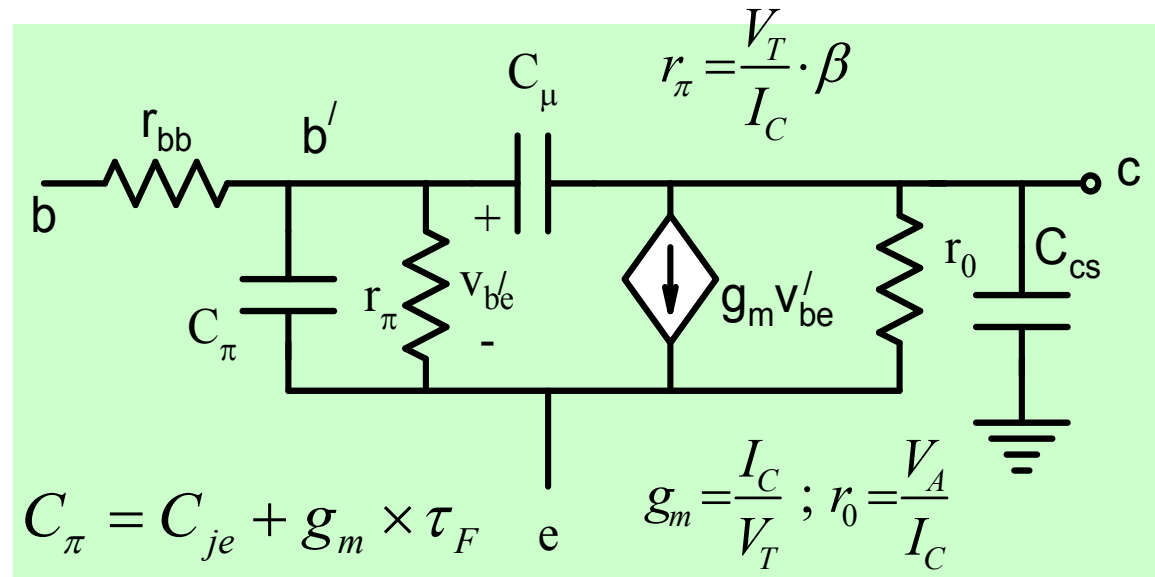
## Model of an PNP BJT in forward active mode



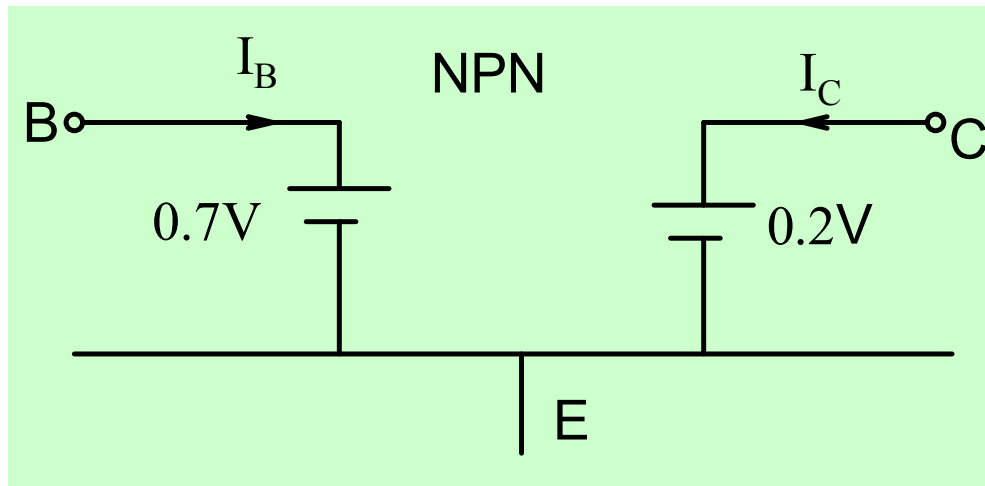
$$I_C = I_S \left( \exp\left(\frac{V_{EB}}{V_T}\right) - 1 \right) \left( 1 + \frac{V_{EC}}{V_A} \right)$$

$$I_B = \frac{I_S \left( \exp\left(\frac{V_{EB}}{V_T}\right) - 1 \right)}{\beta_F}$$

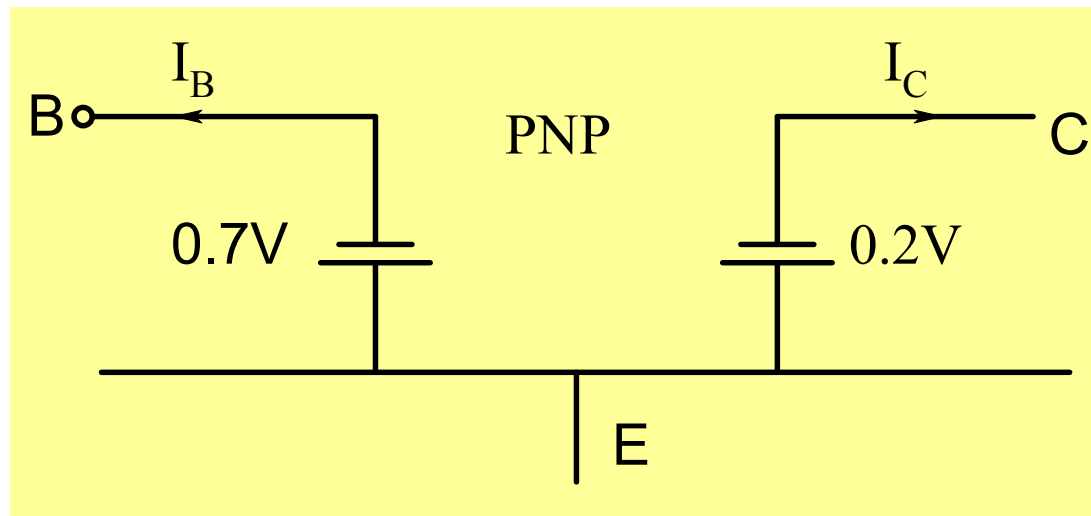
$$I_C = \beta_F I_B \left( 1 + \frac{V_{EC}}{V_A} \right)$$



## Model of a BJT in Saturation mode



$$I_C \neq \beta_F I_B$$



## Example: BJT: NEE210A

$$I_S = 2.03 \times 10^{-15} A; \beta_F = 100; \beta_R = 1; V_A = 100; r_{bb} = 200 \Omega; V_T = 26 mV$$

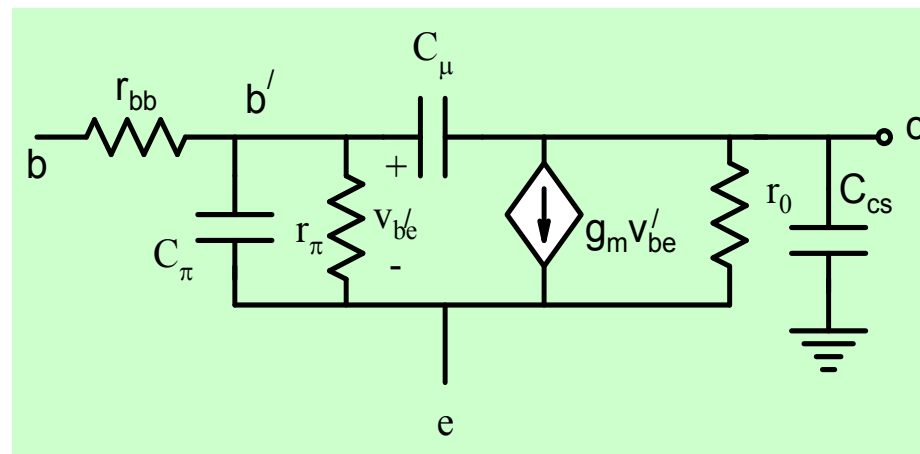
$$C_{jeo} = 1 pF; C_{jco} = 0.5 pF; C_{jso} = 3 pF; m = 0.5; V_{bi} = 0.85; \tau_F = 1 ns$$

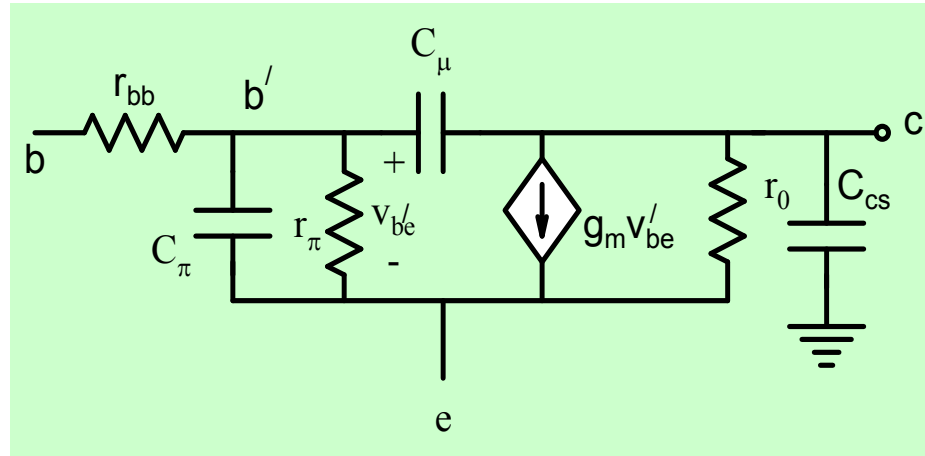
Dc bias condition:

$$V_{BE} = 0.7V; V_{BC} = -3V; V_{CS} = 2V$$

$$I_C = 1mA; I_B = 10\mu A$$

Small Signal Model parameters evaluated at the bias point:





$$g_m = \frac{I_C}{V_T} = 38 \text{ m}\Omega^{-1} ; \quad r_\pi = \frac{V_T}{I_C} \times \beta = 2.6 \text{ k}\Omega ; \quad r_0 = \frac{V_A}{I_C} = 100 \text{ k}\Omega$$

$$C_\pi = g_m \tau_F + C_{je} = g_m \tau_F + \frac{C_{jeo}}{\left(1 - \frac{V_{BE}}{V_{bi}}\right)^m} = 38.5 \text{ pF}$$

$$C_\mu = C_{jc} = \frac{C_{jco}}{\left(1 - \frac{V_{BC}}{V_{bi}}\right)^m} = 0.23 \text{ pF}$$

$$C_{js} = \frac{C_{jso}}{\left(1 + \frac{V_{CS}}{V_{bi}}\right)^m} = 1.6 \text{ pF}$$