EE210: Microelectronics-I

Lecture-33: Operational Amplifiers_1

https://youtu.be/ehekdOHOIZ0

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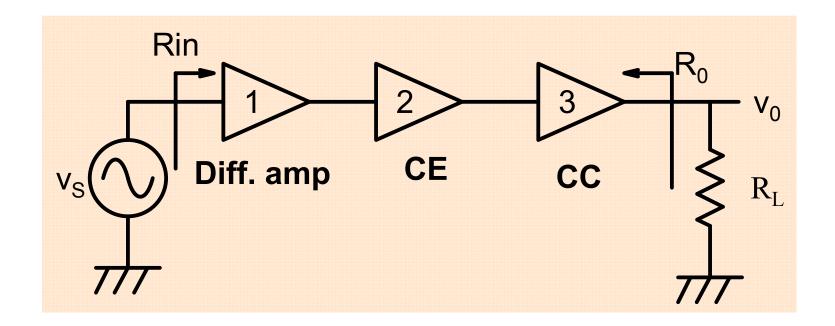
BJT Operational Amplifier

- □ Simple BJT Opamp
- Compensation
- Buffer and Non-inverting amplifier

Specifications:

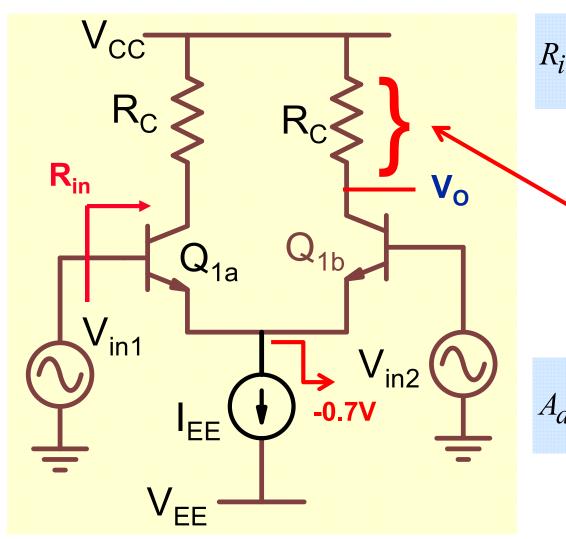
$$A_V \sim 10^3 \; ; \; R_{in} \sim 100 K\Omega \; ; \; R_O = 100 \Omega$$
 Supply: ±12V

In the simple opamp, no active load would be used General architecture:



Input Stage

$$A_V \sim 10^3 \; ; \; R_{in} \sim 100 K\Omega \; ; \; R_O = 100 \Omega$$

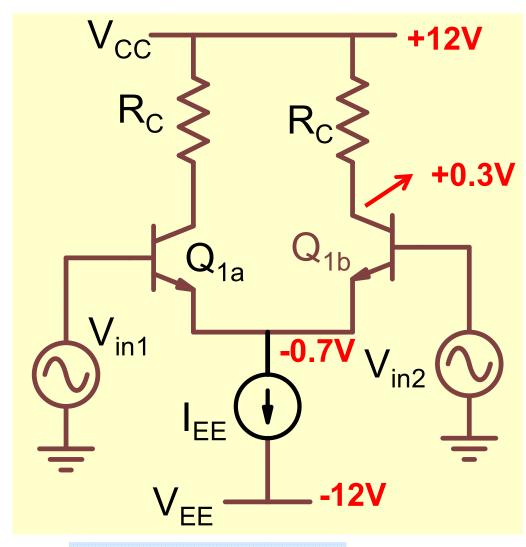


$$R_{in} = 2r_{\pi} = 2\frac{V_T}{I_{CQ1}}\beta = 10^5 \,\Omega$$

$$I_{EE} = 2I_{CQ1} = 0.1 mA$$

$$R_C = ?$$

$$A_{dm} = 0.5g_m R_C = 0.5 \frac{I_{CQ1} R_C}{V_T}$$



$$I_{EE} = 2I_{CQ1} = 0.1 mA$$

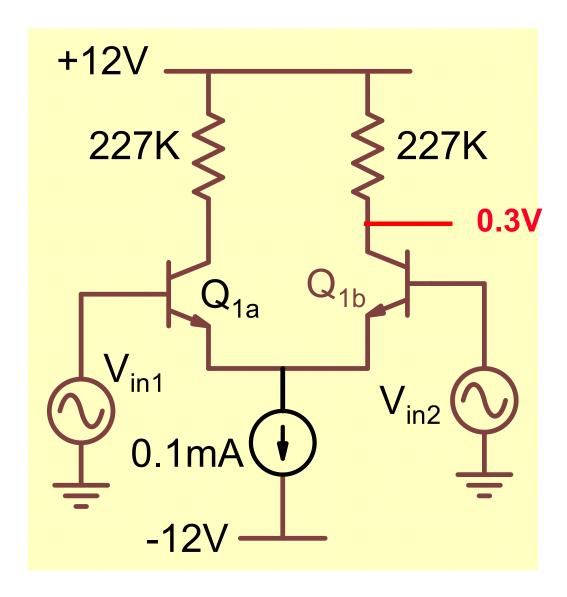
$$A_{V1} = 0.5 \frac{I_{CQ1} R_C}{V_T}$$

Say
$$V_{CE1} = 1V$$

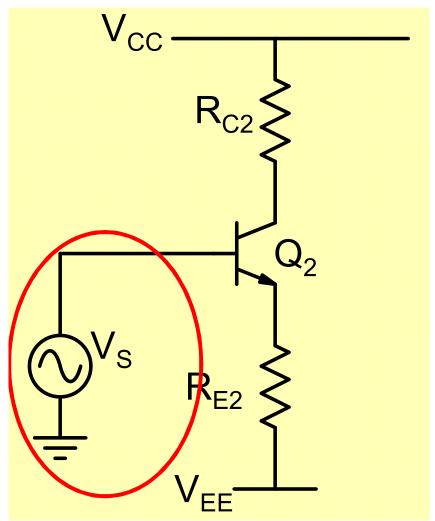
$$A_{V1} = 227$$

$$R_C = \frac{V_{CC} - V_{C1b}}{I_{CQ1}} = 227K$$

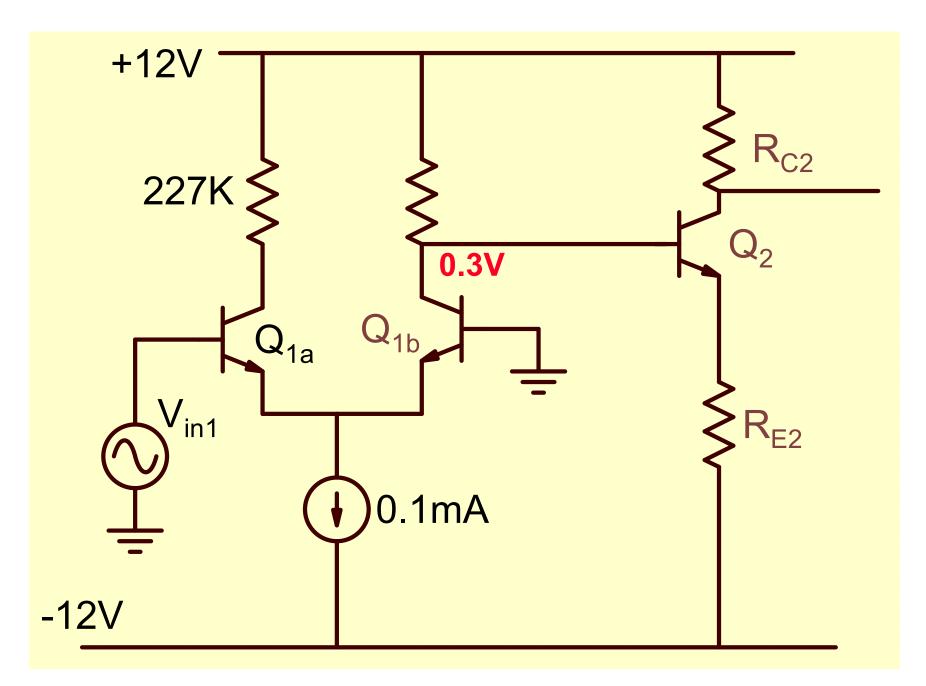
Differential Amplifier

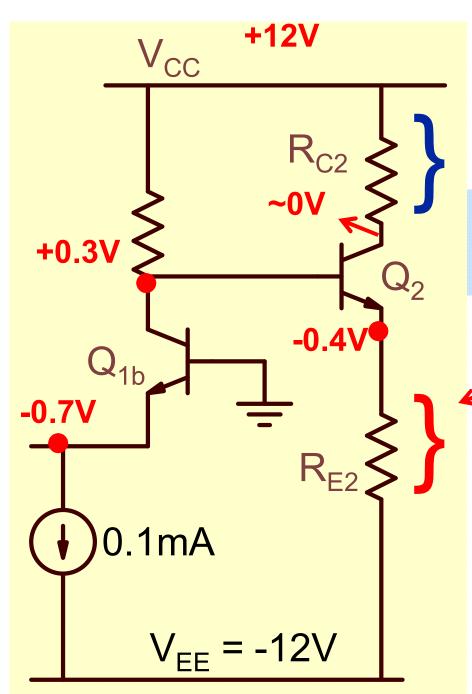


CE Gain Stage



We have to see how to interface it to previous stage





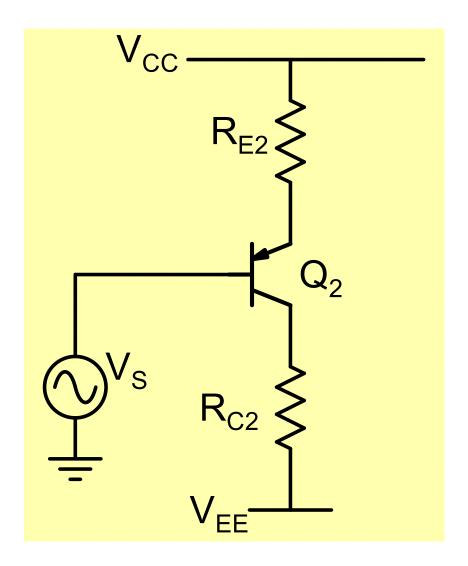
$$A_{V2} = \frac{g_{m2} \times R_{C2}}{1 + g_{m2} \times R_{E2}} \cong \frac{R_{C2}}{R_{E2}}$$

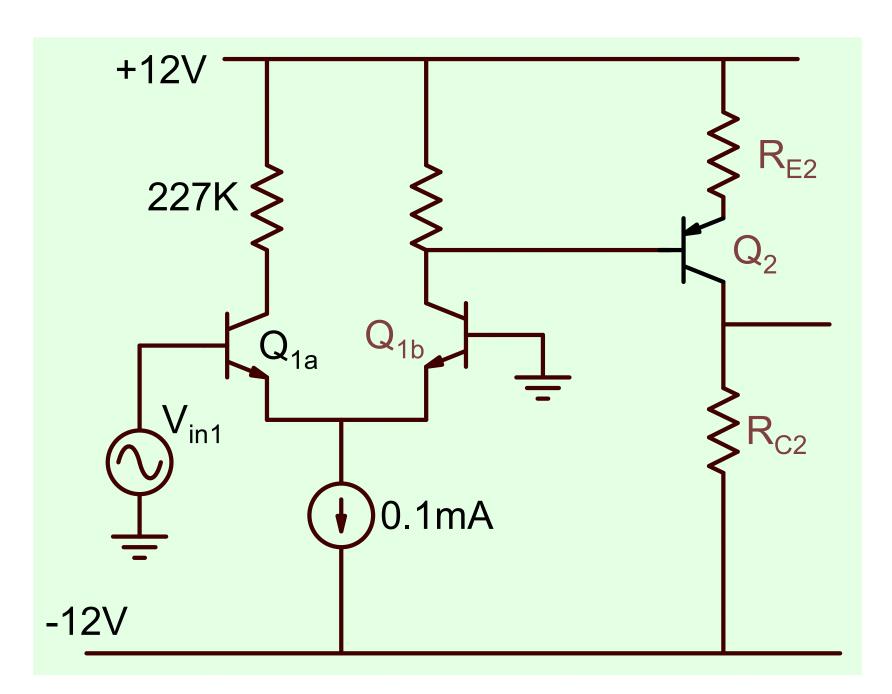
$$A_{V2} \cong \frac{I_{CQ2} \times R_{C2}}{I_{CQ2} \times R_{E2}} = \frac{\Delta V_C}{\Delta V_E}$$

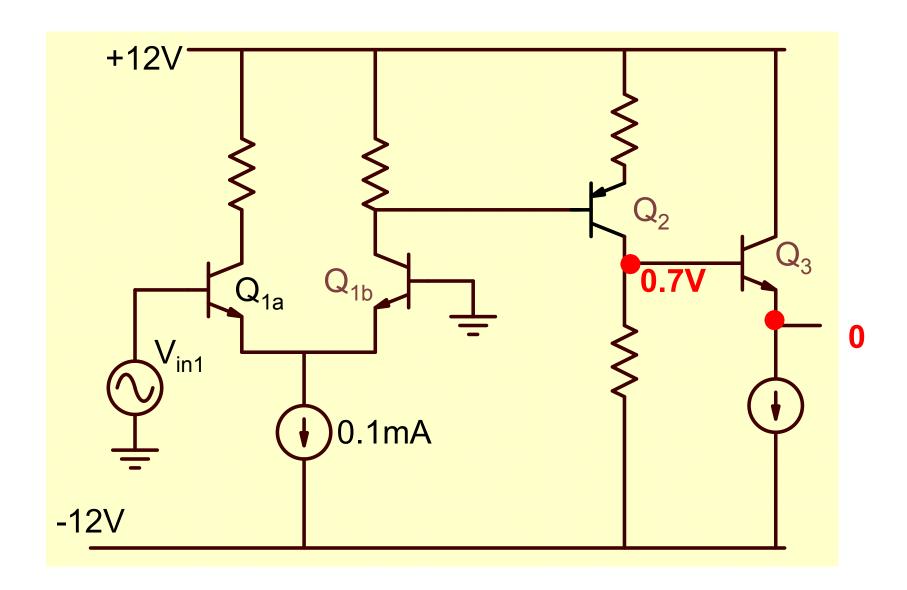
$$A_{V2} \sim \frac{12}{11.6}$$

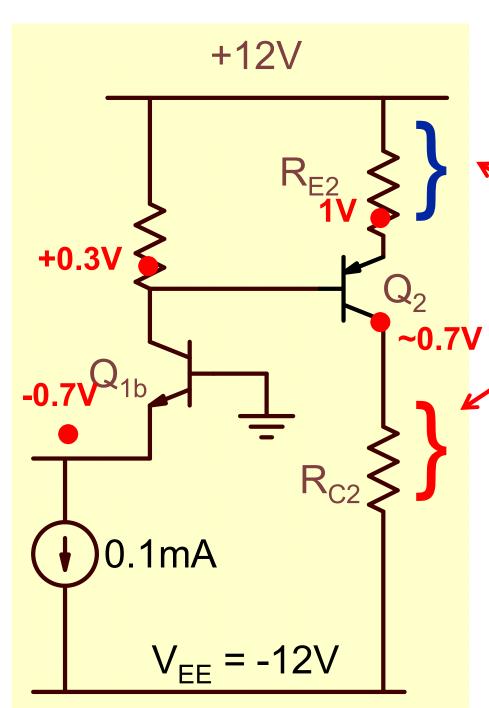
Negligible Gain!

PNP Gain Stage:

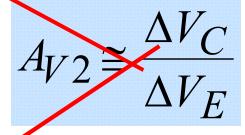








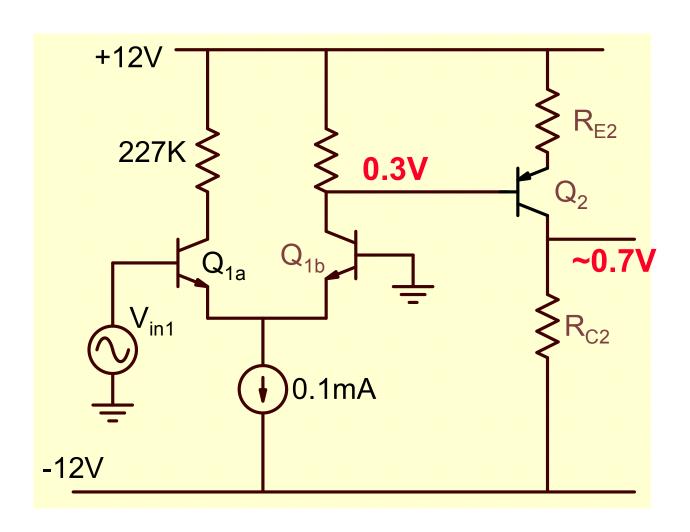
$$A_{V2} \cong \frac{R_{C2}}{R_{E2}} = \frac{I_{CQ2} \times R_{C2}}{I_{CQ2} \times R_{E2}}$$



$$A_{V2} \sim \frac{12.7}{11}$$

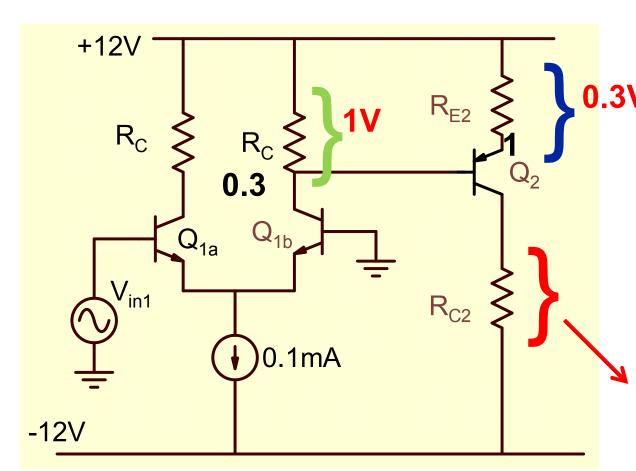
Gain negligible again

With present first stage design, gain of second stage is still negligible



$$A_{V2} = \frac{R_{C2}}{R_{E2}} = \sim 1$$

Re-look at design of first stage



$$A_{V1} = 0.5 \frac{\Delta V_{C1}}{V_T}$$

$$A_{V2} = \frac{R_{C2}}{R_{E2}} = \frac{\Delta V_{C2}}{\Delta V_{E2}}$$

Assuming no loading:

Total gain: $A_{V1} \times A_{V2}$

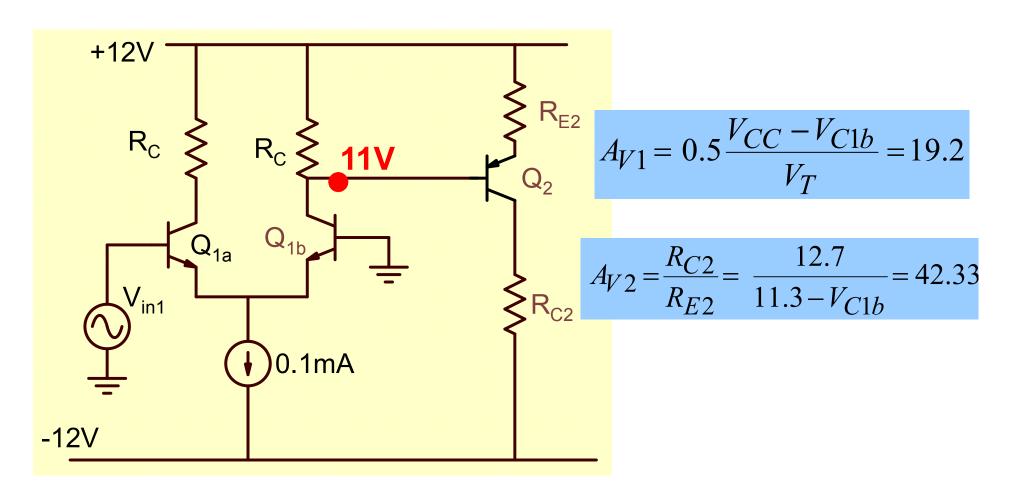
Constant ~12.7V

Earlier
$$A_V = \left(0.5 \frac{11.7}{V_T}\right) \times \left(\frac{12.7}{11}\right)$$

Now
$$A_V = \left(0.5 \frac{1}{V_T}\right) \times \left(\frac{12.7}{0.3}\right)$$

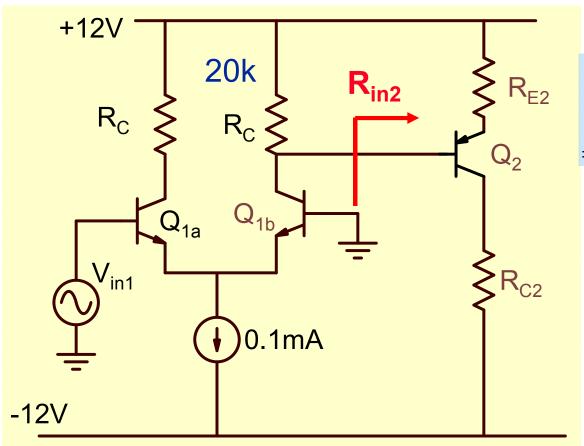
$$\sim$$
19.2 x 42.3 = 814

For $V_{C1b} = 11V$ choice:



$$R_C = \frac{V_{CC} - V_{C1b}}{I_{CQ1}} = 20K\Omega$$

R_{E2} and R_{C2} ?



$$R_{E2}$$
 $A_{V2} = \frac{R_{C2}}{R_{E2}} = \frac{12.7}{11.3 - V_{C1b}}$ = 42.33

$$R_{F2} = ?$$

$$R_{in2} >> R_C$$

$$R_{in2} \cong \beta R_{E2} >> R_C = 20K$$

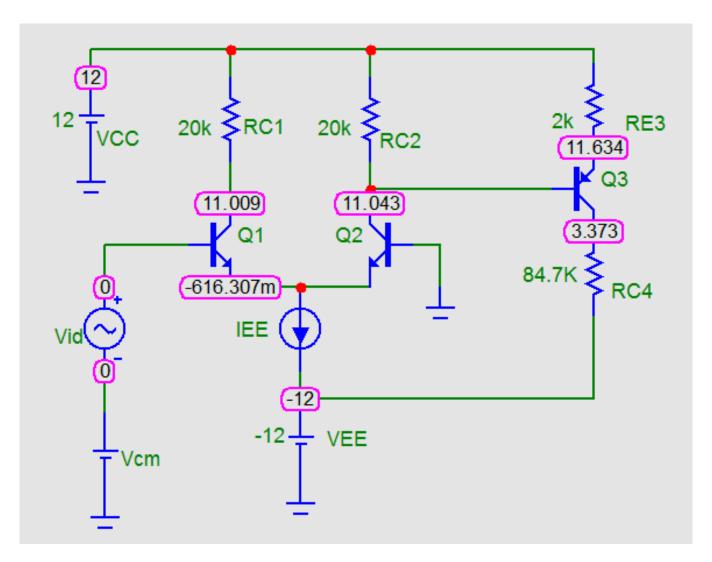
 $R_{E2} >> 200\Omega$

Choose
$$R_{E2} = 2K$$

$$\Rightarrow R_{C2} = 84.7K$$

Simulation Results

$$A_V \sim 10^3 \; ; \; R_{in} \sim 100 K\Omega \; ; \; R_O = 100 \Omega$$



$$A_V = 671$$

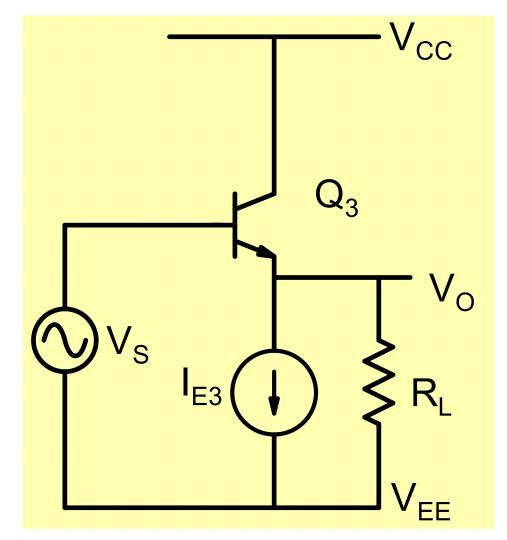
= 17.3 × 38.8

$$R_{in1} = 116K\Omega$$

$$R_O = 82.9K\Omega$$

Expected Gain~19.2 x 42.3 = 814

Output Stage: CC Amplifier



$$V_O$$
 is directly coupled so V_O (dc) = 0V

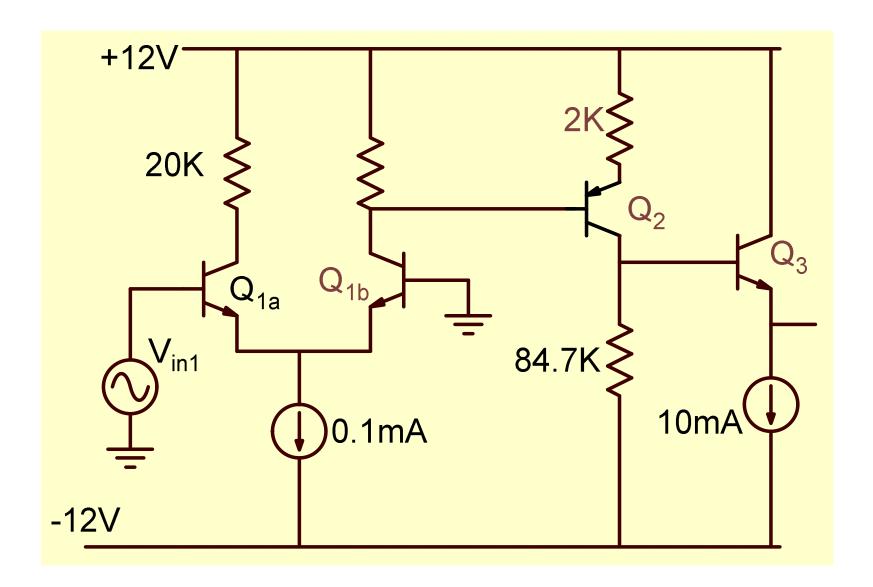
Current source bias gives better swing for a given bias current

Suppose
$$R_L \ge 1K\Omega$$

For a $\pm 10V$ Swing $I_{E3} \ge 10mA$

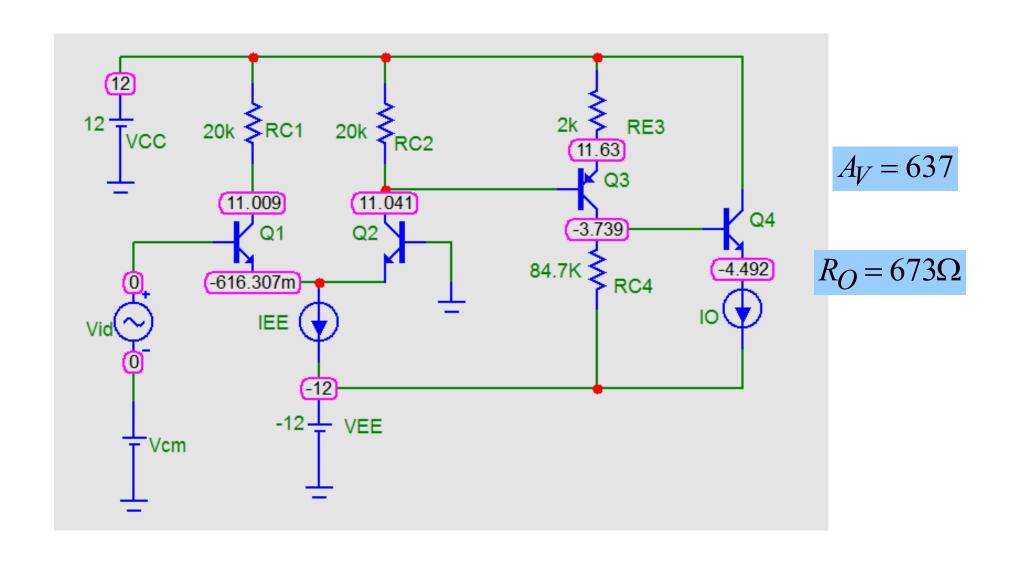
Choose 10mA

Complete Amplifier

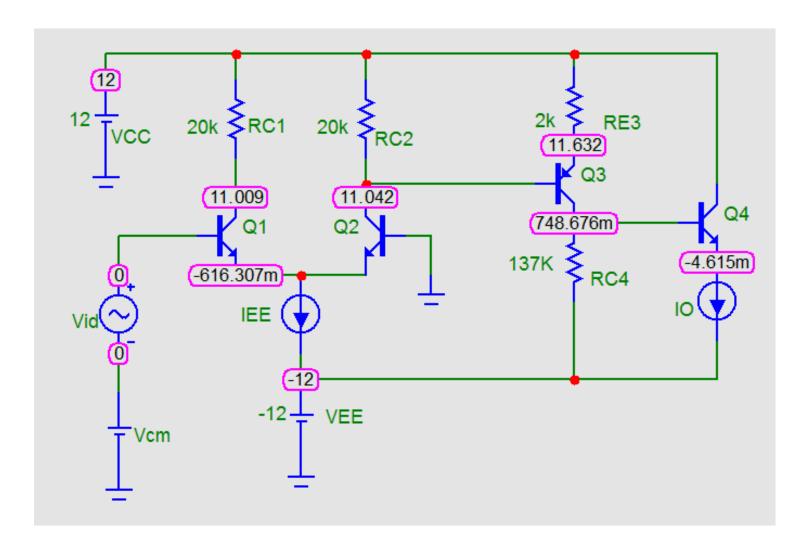


Simulation Results

$$A_V \sim 10^3 \; ; \; R_{in} \sim 100 K\Omega \; ; \; R_O = 100 \Omega$$



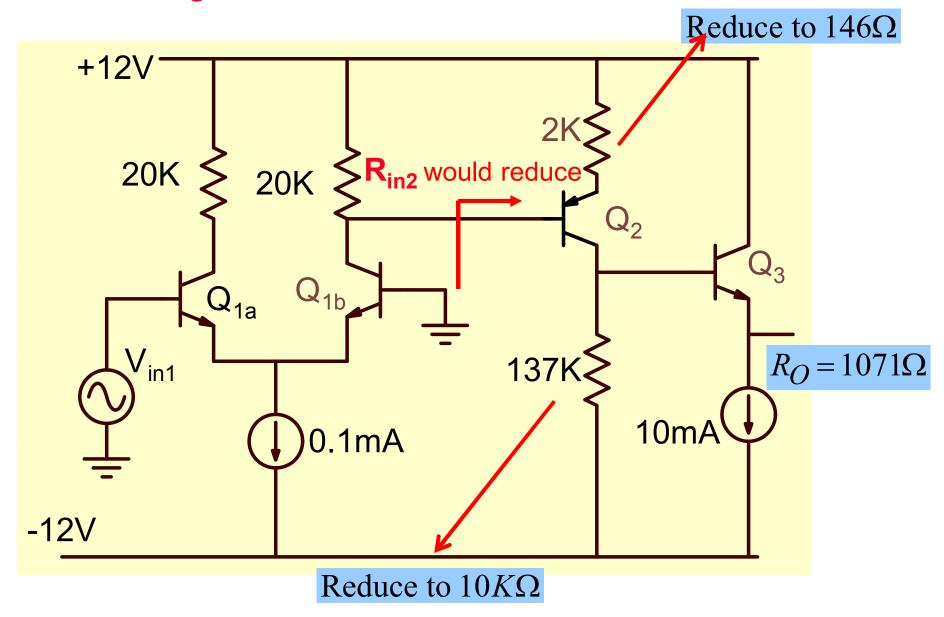
After tuning to obtain ~zero dc output voltage



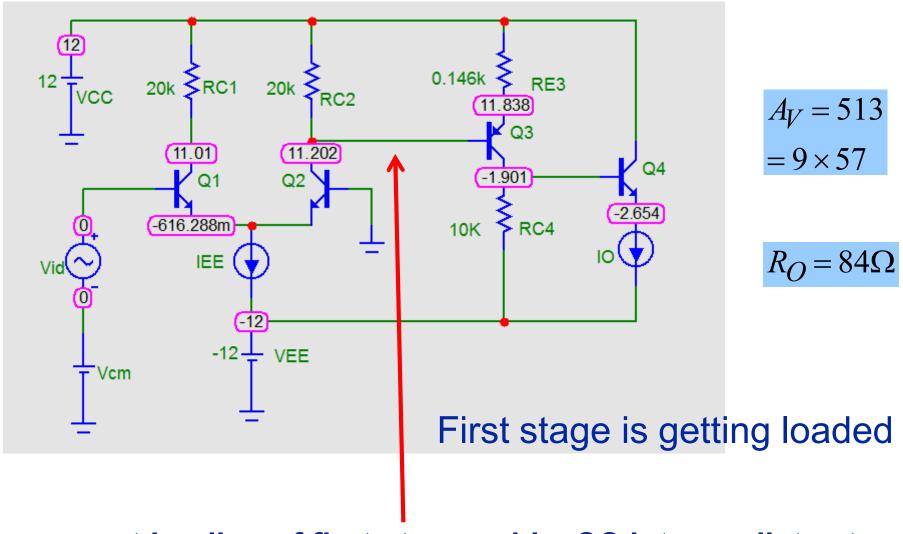
$$A_V = 972.6$$

$$R_O = 1071\Omega$$

Present design

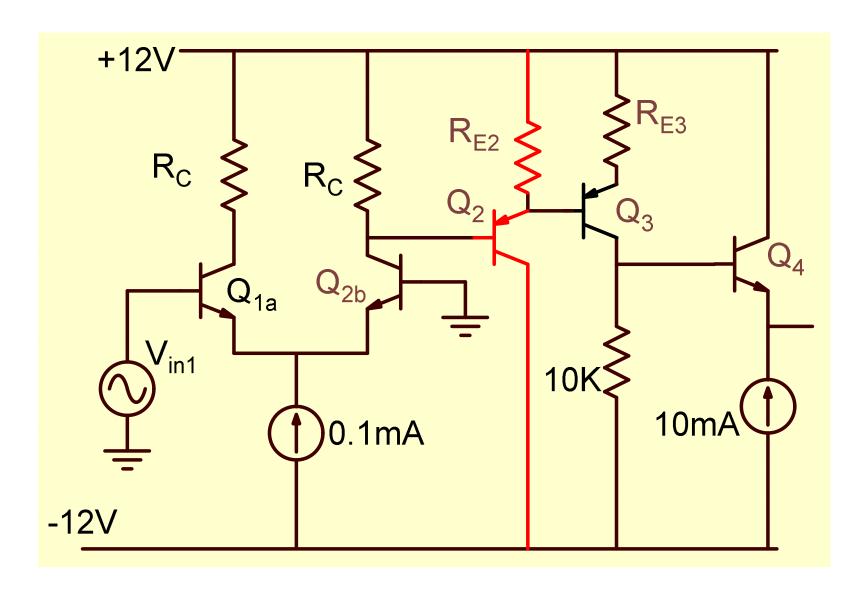


Simulation Results

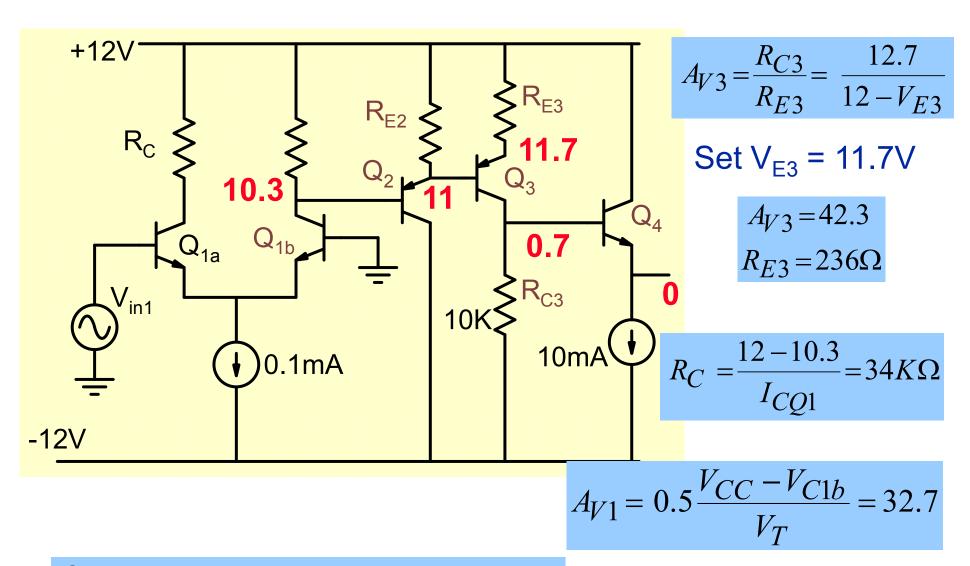


To prevent loading of first stage, add a CC intermediate stage

New Opamp Schematic



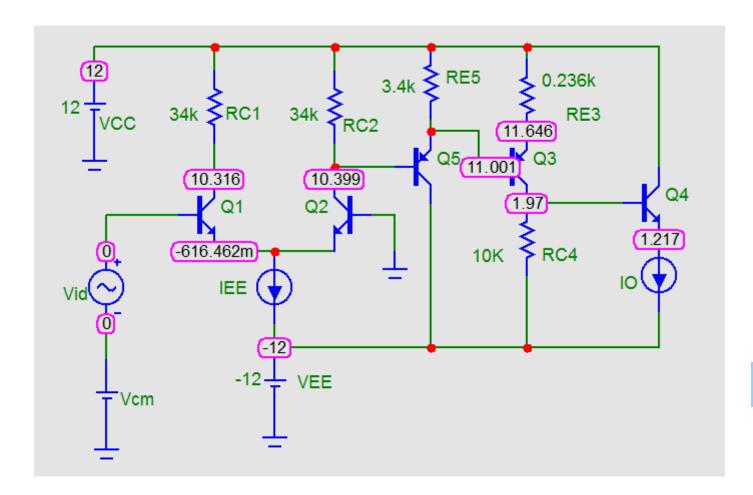
Design



 $\beta R_{E2} >> R_C = 34K; R_{E2} >> 340\Omega$

Let $R_{F_2} = 3.4K$

Simulation Results



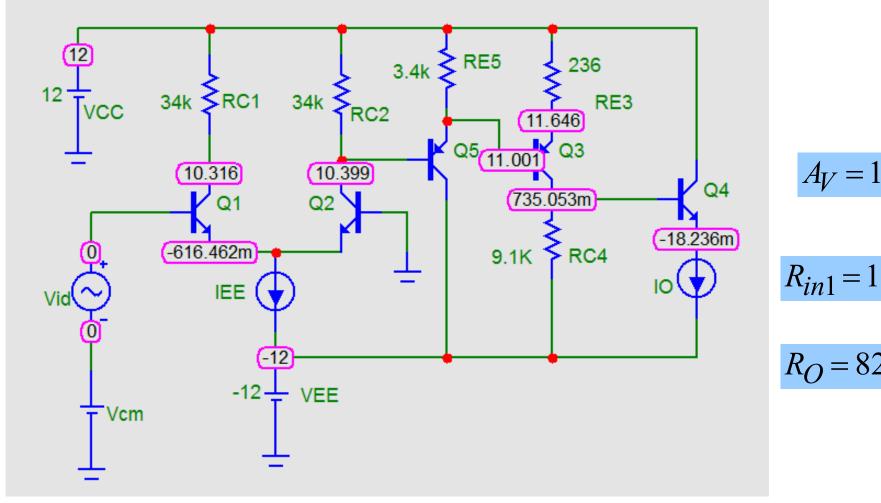
$$A_V = 1099$$

$$R_{in1} = 115K\Omega$$

$$R_O = 90.86K\Omega$$

Some fine tuning is required to bring output closer to zero

After tuning

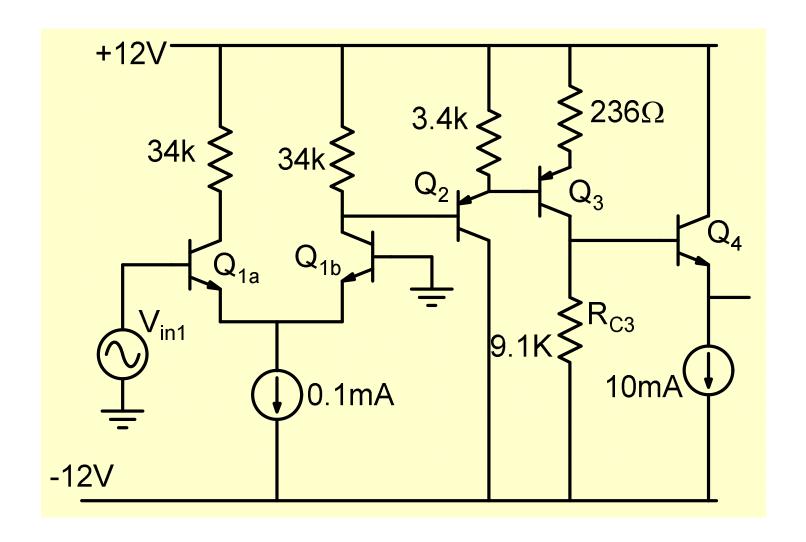


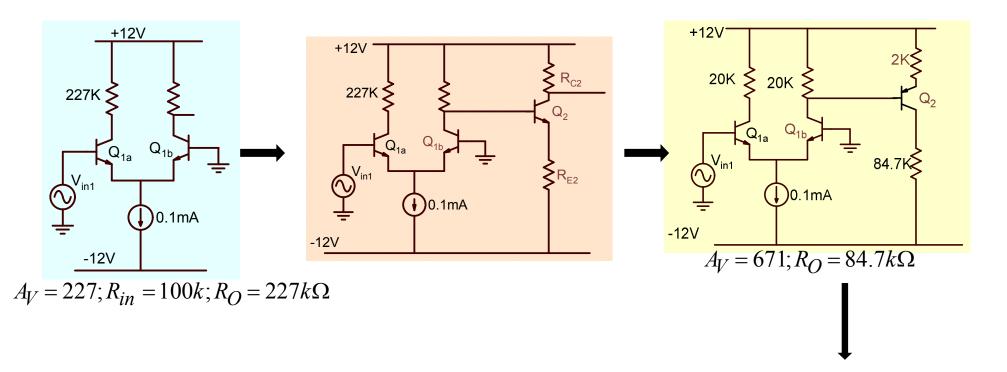
$$A_V = 1002$$

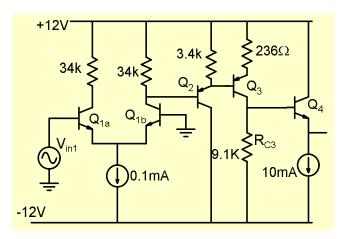
$$R_{in1} = 115K\Omega$$

$$R_O = 82.2K\Omega$$

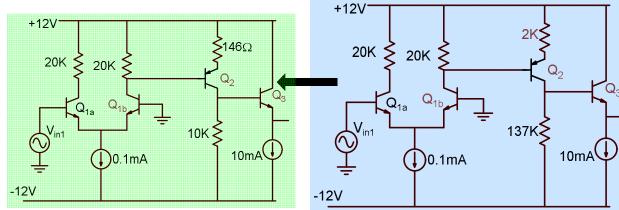
Final Design







$$A_V = 1002; R_{in} = 115k; R_O = 82\Omega$$



$$A_V = 513; R_O = 84\Omega$$

$$A_V = 972; R_O = 1071\Omega$$