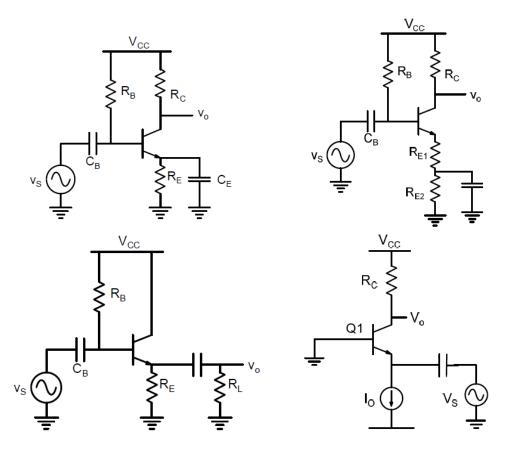
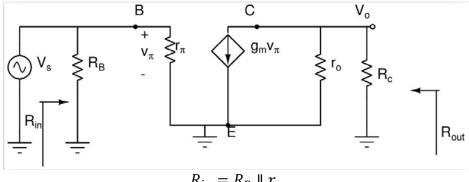
EE210: HW-8 Solution

Date: 28-02-2019

Q1. Analyze the following circuits from first principles to determine voltage gain and input resistance.



Sol. (a)



$$R_{in} = R_B \parallel r_{\pi}$$

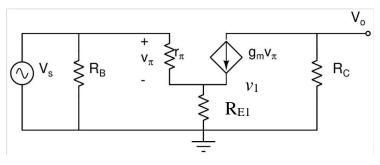
$$v_{\pi} = v_S$$

$$R_{out} = R_C \parallel r_0$$

$$v_0 = -g_m(R_C \parallel r_0)v_{\pi}$$

$$A_V = \frac{v_0}{v_S} = -g_m(R_C \parallel r_0) \cong -g_mR_C$$

(b)



$$v_{s} = v_{\pi} + v_{1}$$

$$\frac{v_{1} - v_{s}}{r_{\pi}} + \frac{v_{1}}{R_{E1}} = g_{m}v_{\pi}$$

$$\frac{v_{s} - v_{\pi} - v_{s}}{r_{\pi}} + \frac{v_{s} - v_{\pi}}{R_{E1}} = g_{m}v_{\pi}$$

$$\frac{v_{s}}{R_{E1}} - v_{\pi} \left(\frac{1}{r_{\pi}} + \frac{1}{R_{E1}}\right) = g_{m}v_{\pi}$$

$$\frac{v_{s}}{R_{E1}} = v_{\pi} \left(\frac{1}{r_{\pi}} + \frac{1}{R_{E1}} + g_{m}\right)$$

$$v_{\pi} = \frac{r_{\pi}}{R_{E1} + r_{\pi} + g_{m}R_{E1}r_{\pi}} v_{s}$$

$$v_{\pi} = \frac{r_{\pi}}{r_{\pi} + R_{E1}(1 + \beta)} v_{s}$$

$$v_{O} = -g_{m}v_{\pi}R_{C}$$

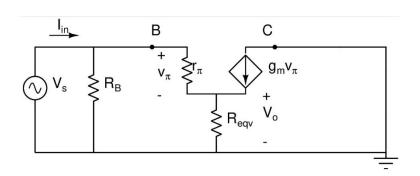
Gain

$$A_{v} = \frac{v_{O}}{v_{S}} = \frac{-g_{m}r_{\pi}R_{c}}{r_{\pi} + R_{E1}(1+\beta)}$$

Input resistance

$$R_{in} = R_B \parallel (r_{\pi} + R_{E1}(1 + \beta))$$

(c)



 C_B , C_E = short circuit

$$R_{eq} = R_E \parallel R_L$$

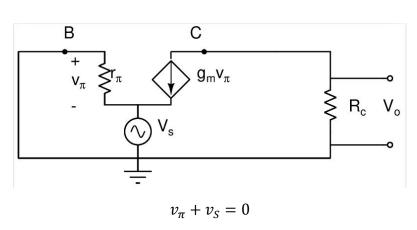
Assuming $r_0 \rightarrow \infty$,

$$\begin{aligned} v_{\rm S} &= v_{\rm m} + {\rm v}_0 \\ \frac{{\rm v}_0}{R_{eq}} &= g_m v_{\rm m} + \frac{{\rm v}_{\rm m}}{r_{\rm m}} \\ v_0 &= R_{eq} v_{\rm m} \left(g_m + \frac{1}{r_{\rm m}} \right) \\ v_0 &= R_{eq} (v_{\rm S} - {\rm v}_0) \left(g_m + \frac{1}{r_{\rm m}} \right) \\ A_v &= \frac{v_0}{v_{\rm S}} = \frac{R_{eq} \left({\rm gm} + \frac{1}{r_{\rm m}} \right)}{1 + R_{eq} \left({\rm gm} + \frac{1}{r_{\rm m}} \right)} \end{aligned}$$

Input Resistance,

$$R_{in} = R_B \parallel (r_\pi + R_{eq}(\beta + 1))$$

(d)

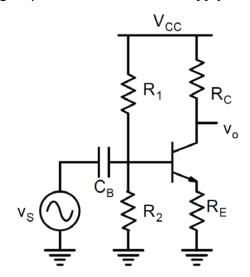


$$v_0 = g_m R_C v_\pi$$

$$\frac{v}{v_S} = -g_m R_C$$

$$R_{in} = \frac{r_\pi}{1+\beta}$$

Q2. Check the claim that "it is not possible to design the single stage BJT amplifier shown below such that magnitude of open circuit voltage gain is ≥ 100 , input resistance is $\geq 1 k\Omega$ and the design is such that voltage gain stability against variation in current gain β is better than 5% and supply voltage is less than 12V".



Sol:

Let's assume

$$V_{CC} = 12V$$

$$A_V = 100$$

$$R_{in} = 1K\Omega$$

Stability

$$S = \frac{\Delta I_{CQ}/I_{CQ}}{\Delta \beta/\beta} = \frac{1}{1 + \frac{\beta R_E}{R_B}} \le 0.05$$

Thus

$$\frac{\beta R_E}{R_B} \ge 19$$

$$\beta R_E \ge 19 * R_B$$

$$R_{in} = R_B \parallel (r_\pi + \beta R_E) \geq 1k$$

Thus

$$R_R \ge 1k$$

For $R_B = 1k$, let's assume $R_2=1k$ and $R_1=11k$. This gives,

$$V_B = \frac{1k}{1k + 11k} * V_{CC} \cong 1V$$

$$V_E = V_B - 0.7V = 0.3V = I_{CQ}R_E$$

Also,

$$|A_V| \ge \frac{g_m R_C}{1 + g_m R_E} \ge 100$$

$$R_C \ge 100 * R_E$$

Thus

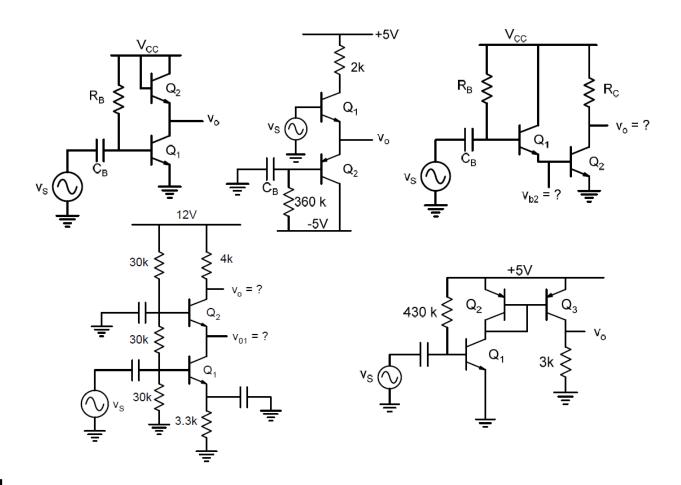
$$I_{CQ}R_C \geq 100*I_{CQ}*R_E = 30V$$

This gives us

$$V_{CC} \ge I_{CQ}R_C + v_{om} + I_{CQ}R_E \ge 30V + v_{om} + 0.3V$$

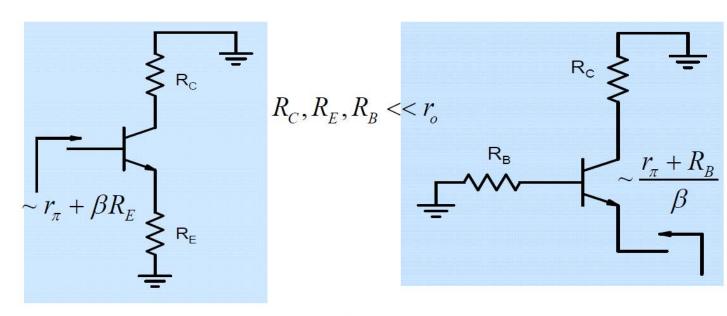
Thus $V_{CC} = 12V$ cannot satisfy the input resistance and gain conditions.

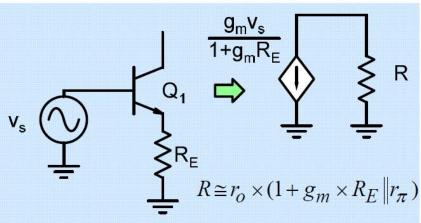
Q3. Analyze the following circuit through use of "divide & reuse "methodology.

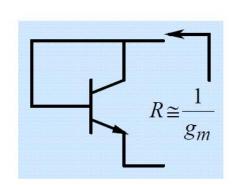


Sol.

Keep in mind following relations.







Input Resistance:

$$R_i = r_{\pi} || R_B$$

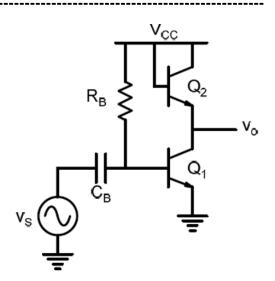
Output Resistance:

$$R_o = R_{01} \| R_{02} = r_{01} \| r_{02} \| (1/g_{m2}) \cong 1/g_{m2}$$

Gain (A_V):

$$\begin{aligned} A_V &= -g_m \times R_{out} = -g_{m1} \times \left(\frac{1}{g_{m2}}\right) \|r_{01}\| r_{02} &\cong -g_{m1} \times \left(\frac{1}{g_{m2}}\right) \\ &= -1 \end{aligned}$$

Note that $g_{m1} = g_{m2}$, as I_{CQ} is same in both transistors.



Input Resistance:

$$R_{in} = r_{\pi 1} + \beta_1 * \frac{1}{g_{m2}}$$

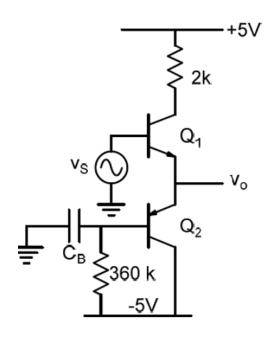
Output Resistance:

$$R_{out} = R_{01} \| R_{02} = \frac{1}{g_{m1}} \| \frac{1}{g_{m2}}$$

Gain:

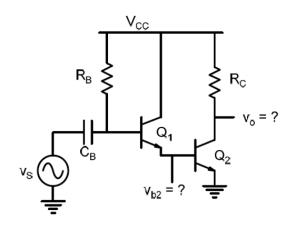
$$v_0 = v_s \frac{\beta_1 * \frac{1}{g_{m2}}}{r_{\pi 1} + \beta_1 * \frac{1}{g_{m2}}}$$
$$\beta_1 * \frac{1}{g_{m2}}$$

$$A_V = \frac{\beta_1 * \frac{1}{g_{m2}}}{r_{\pi 1} + \beta_1 * \frac{1}{g_{m2}}}$$



$$v_{b2} = v_s \frac{\beta_1 * r_{\pi 2}}{r_{\pi 1} + \beta_1 * r_{\pi 2}} \cong v_s$$

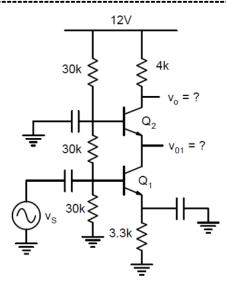
$$v_0 = -g_{m2} \times R_c \times v_{b2} \cong -g_{m2} \times R_c \times v_s$$



$$\begin{split} v_{01} &= -g_{m1} * R_{out} * v_s \\ R_{out} &= \left(\frac{1}{g_{m2}}\right) \| r_{02} \\ v_{01} &= -g_{m1} * \left(\frac{1}{g_{m2}} \| r_{02}\right) * v_s \cong v_s \end{split}$$

Current is same in Q1 and Q2. So, $g_{m1} = g_{m2}$.

$$v_0 = -g_{m1}R_c * v_s$$



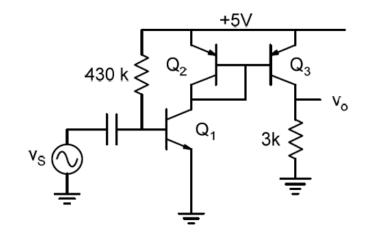
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Resistance seen at the collector of Q1 is parallel combination of r_{01} , $\frac{1}{g_{m2}}$ and $(r_{\pi 3} + \beta R_E)$. Thus,

$$\frac{v_{c1}}{v_s} = -g_{m1} * \left[(r_{01}) \left| \left| \left(\frac{1}{g_{m2}} \right) \right| \right| (r_{\pi 3}) \right]$$

$$\frac{v_{c1}}{v_s} \cong -g_{m1} * \left(\frac{1}{g_{m2}} \right) \cong -1$$

$$v_0 = -g_{m1} R_C * v_{c1}$$



$$\frac{v_0}{v_S} = g_{m1} R_C$$