

MEOE12 ASSIGNMENT – 3

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Problem 1)

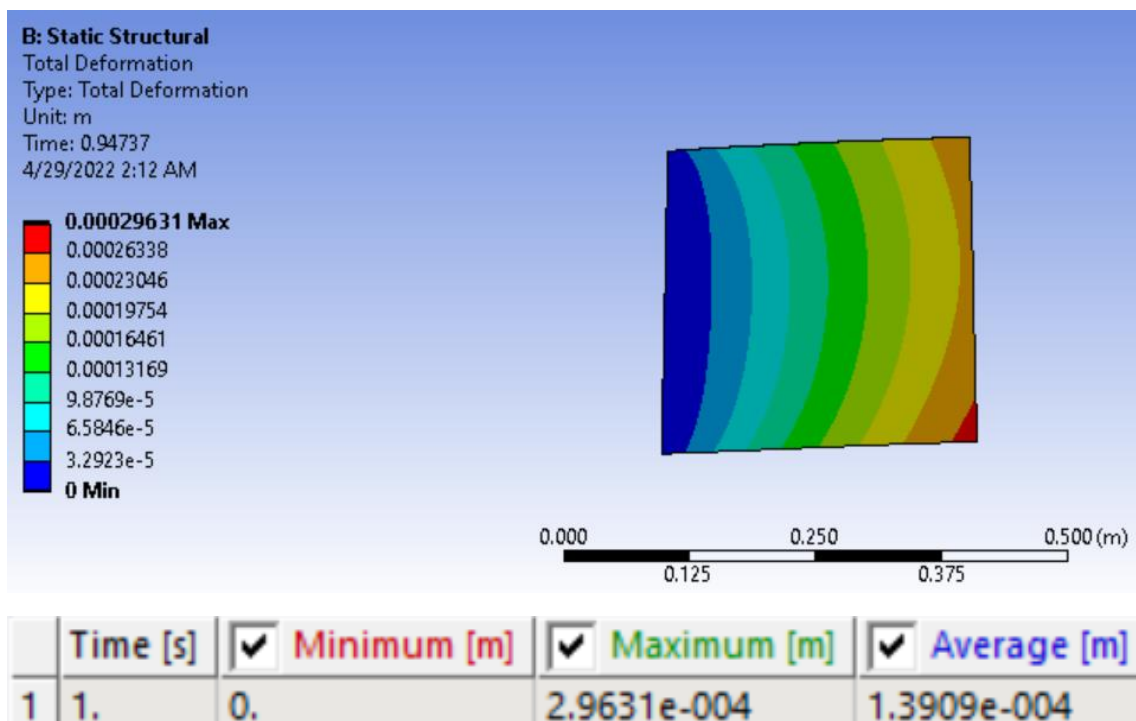
Consider the laminate stacking sequence $[0^\circ/90^\circ]$ is made up of Glass/epoxy material which is subjected to $N_x = 20 \text{ N/mm}$ and $N_y = 20 \text{ N/mm}$. The geometry of laminate is $300 \text{ mm} \times 300 \text{ mm} \times 2 \text{ mm}$ and thickness of each ply is 1 mm . Determine (i) total deformation of laminate (ii) maximum principal stress at each ply (iii) maximum shear stress at each ply (iv) Equivalent Von-mises stress at each ply. Check that whether the lamina fails if (i) Tsai-Hill theory (ii) Hoffman and (iii) Tsai-Wu theory is used.

Ansys Workbench:

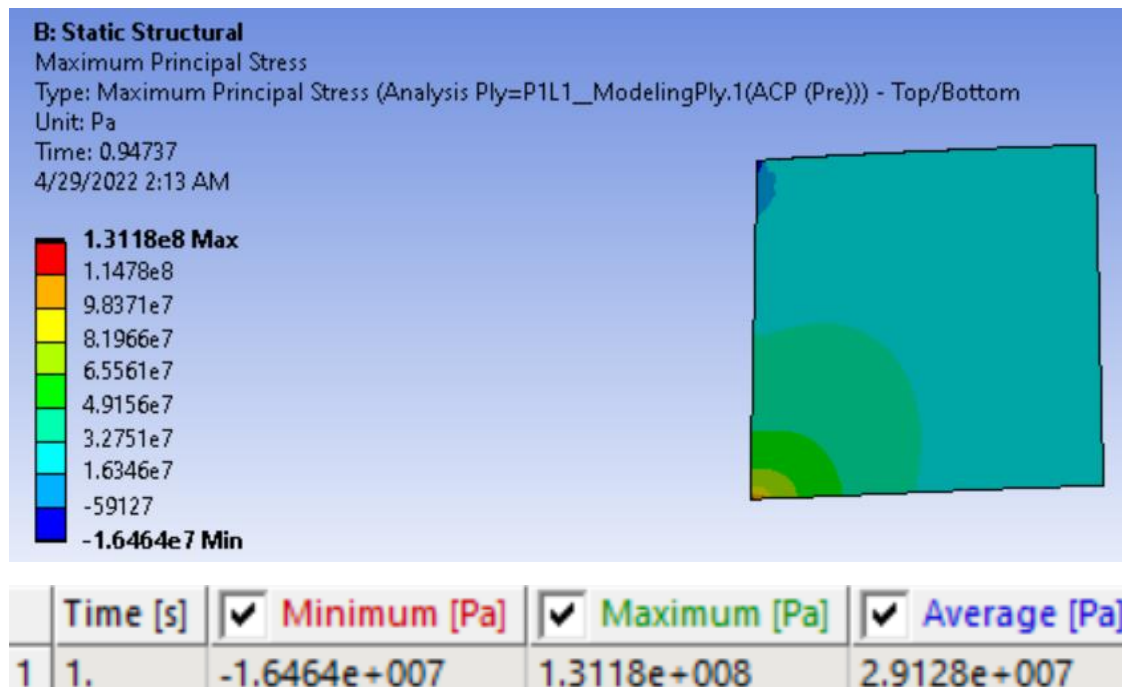
Considering the laminate containing 2 ply's made of Glass/epoxy material with stacking sequence of $[0^\circ \text{ and } 90^\circ]$ with each ply thickness = 1 mm , making it to total geometry of laminate as $300 \text{ mm} \times 300 \text{ mm} \times 2 \text{ mm}$.

Ansys Results:

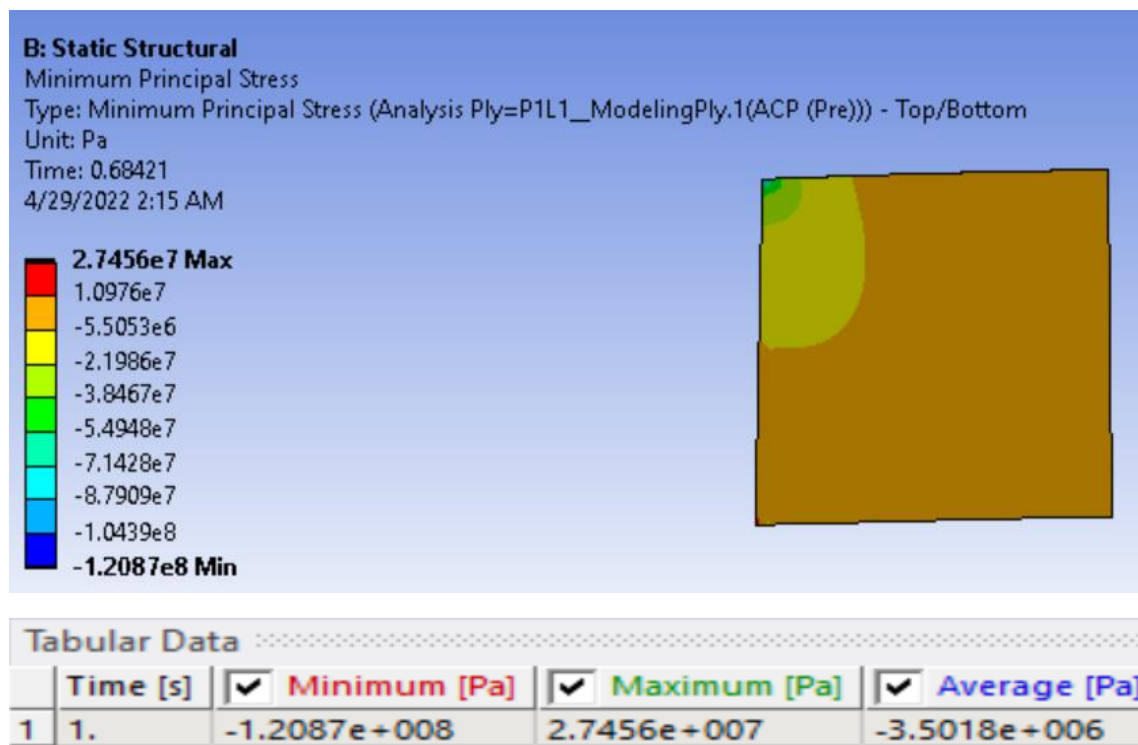
Total Deformation



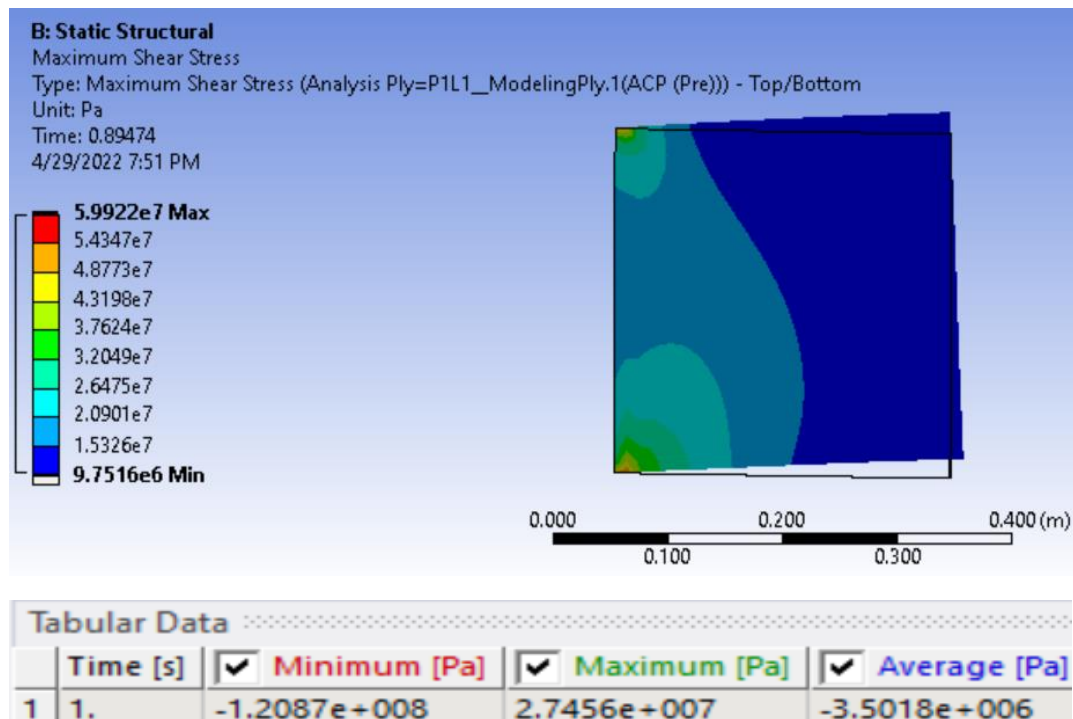
Maximum Principal Stress for both 0 degree and 90-degree ply,



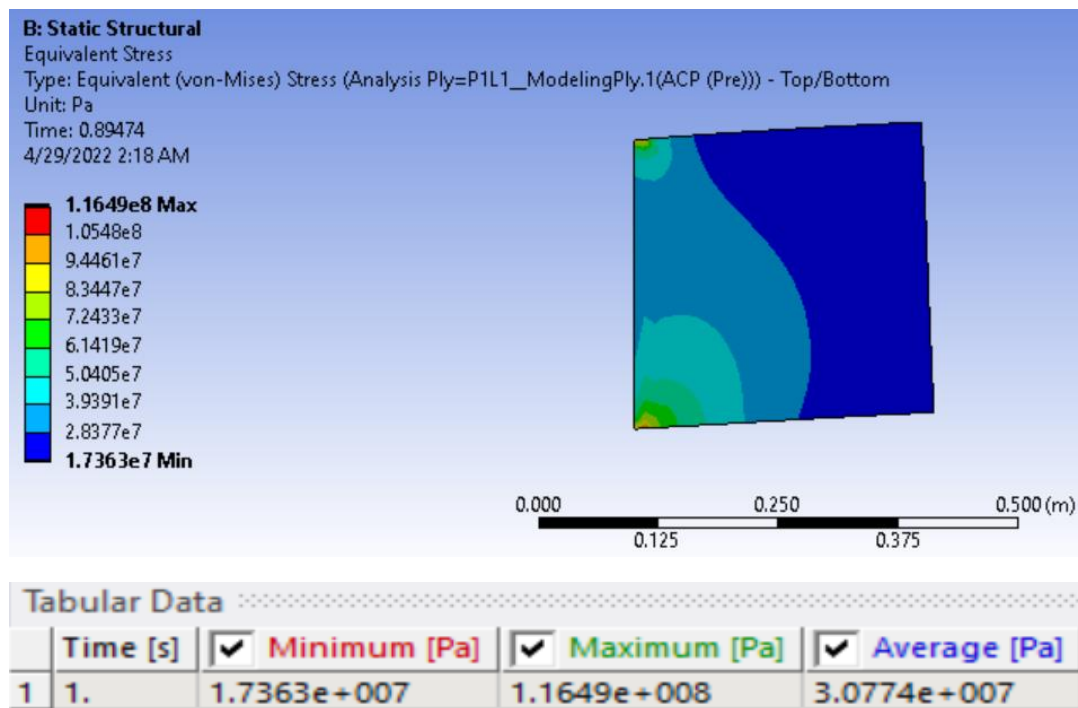
Minimum Principal Stress for 0 degree and 90-degree ply,



Maximum Shear Stress at 0 degree and 90-degree ply,



Equivalent stress:



Failure theory:

(iii) Tsai-Wu failure Criteria:

$$F_1 \sigma_1 + F_2 \sigma_2 + F_3 \sigma_6 + F_{11} \sigma_1^2 + F_{22} \sigma_2^2 + F_{66} \sigma_6^2 + 2F_{12} \sigma_1 \sigma_2 = 1.$$

→ using same simplifications:

$$\Rightarrow F_1 \sigma_1 + F_2 \sigma_2 + F_{11} \sigma_1^2 + F_{22} \sigma_2^2 + F_{66} \sigma_6^2 = 1.$$

$$F_1 = \frac{1}{X_t} + \frac{1}{X_c}, \quad F_{11} = \frac{-1}{X_t X_c}, \quad F_3 = 0,$$

$$F_{66} = \frac{1}{S^2}, \quad F_2 = \frac{1}{Y_t} + \frac{1}{Y_c}, \quad F_{22} = \frac{-1}{Y_t Y_c}$$

$$\rightarrow \text{By solving } \Rightarrow 3.8431 > 1.$$

(ii) Hoffman - failure criteria:

$$\frac{-\sigma_1^2}{X_c X_t} + \frac{\sigma_1 \sigma_2}{X_c X_t} + \frac{-\sigma_2^2}{Y_c Y_t} + \frac{X_c + X_t}{X_c X_t} \sigma_1 + \frac{Y_c + Y_t}{Y_c Y_t} \sigma_2 + \frac{\sigma_1^2}{S^2} = 1.$$

$$\rightarrow X_T = 1062 \text{ mpa}, \quad X_c = 610 \text{ mpa},$$

$$Y_T = 31 \text{ mpa}, \quad Y_c = 118 \text{ mpa},$$

$$S = 72 \text{ mpa}.$$

$$\Rightarrow \rightarrow \text{result} \rightarrow \text{equal to } = 3.8375.$$

$$\rightarrow 3.8375 > 1$$

⇒ The lamina fails in 2 direction.

(i) Tsai-Hill Criteria: [for both 0° & 90° ply].

from Ansys; $\sigma_1 = 131.8 \text{ MPa}$, $\sigma_2 = 27.45 \text{ MPa}$,

$$\tau_{12} = 116.49 \text{ MPa}.$$

[Glass/Epoxy].

from material properties; $X = 1062 \text{ MPa}$,

$$Y = 31 \text{ MPa} \quad \& \quad S = 72 \text{ MPa}$$

$$\Rightarrow \frac{\sigma_1^2}{X^2} - \frac{\sigma_1 \sigma_2}{X^2} + \frac{\sigma_2^2}{Y^2} + \frac{\tau_{12}^2}{S^2}$$

$$\Rightarrow 3.413 > 1$$

→ The lamina failure occurred due to loading in z -dirⁿ.

Problem 2)

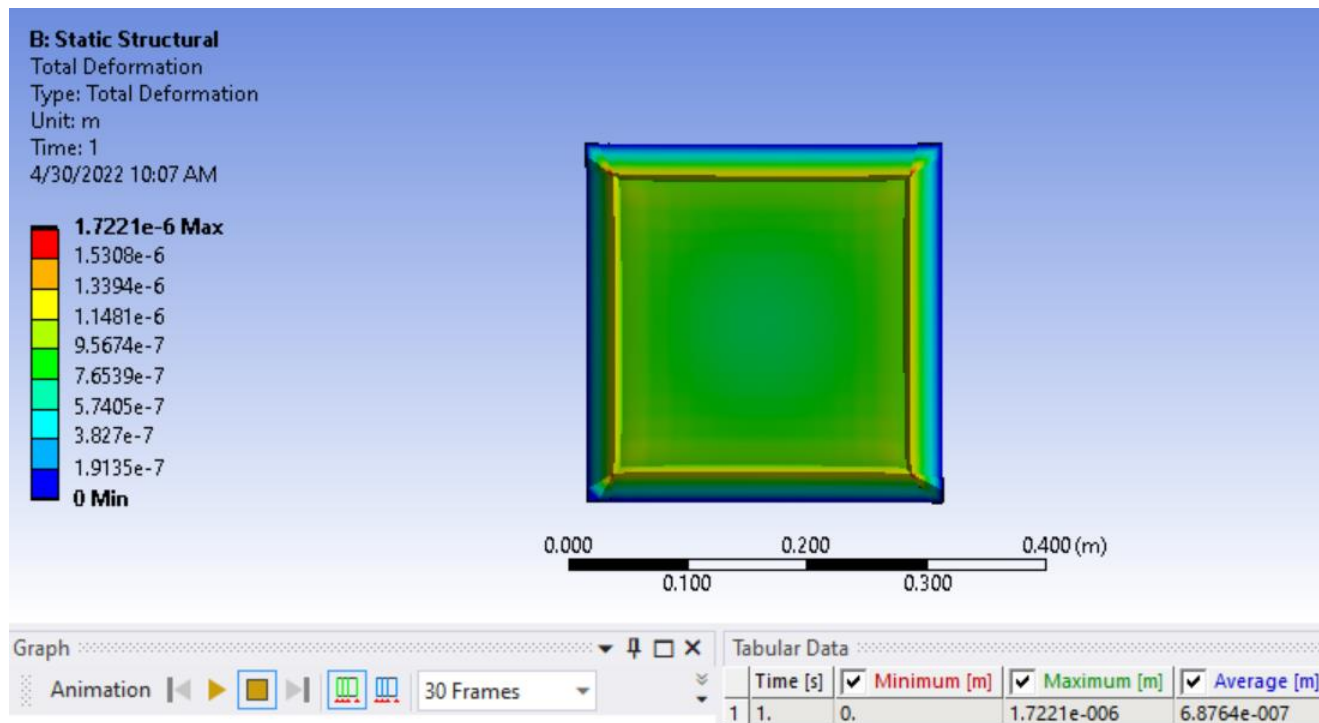
Consider the laminate stacking sequence $[0^\circ/60^\circ/-60^\circ]$ is made up of Glass/epoxy material which is subjected to temperature change of 150°C . The geometry of laminate is $300 \text{ mm} \times 300 \text{ mm} \times 1.5 \text{ mm}$ and thickness of each ply is 0.5 mm . The boundary conditions of the plate are fixed at all edges. Determine (i) total deformation of laminate (ii) maximum principal stress at each ply (iii) maximum shear stress at each ply (iv) Equivalent Von-mises stress at each ply. Check that whether the lamina fails if (i) Tsai-Hill theory (ii) Hoffman and (iii) Tsai-Wu theory is used.

Ansys Workbench:

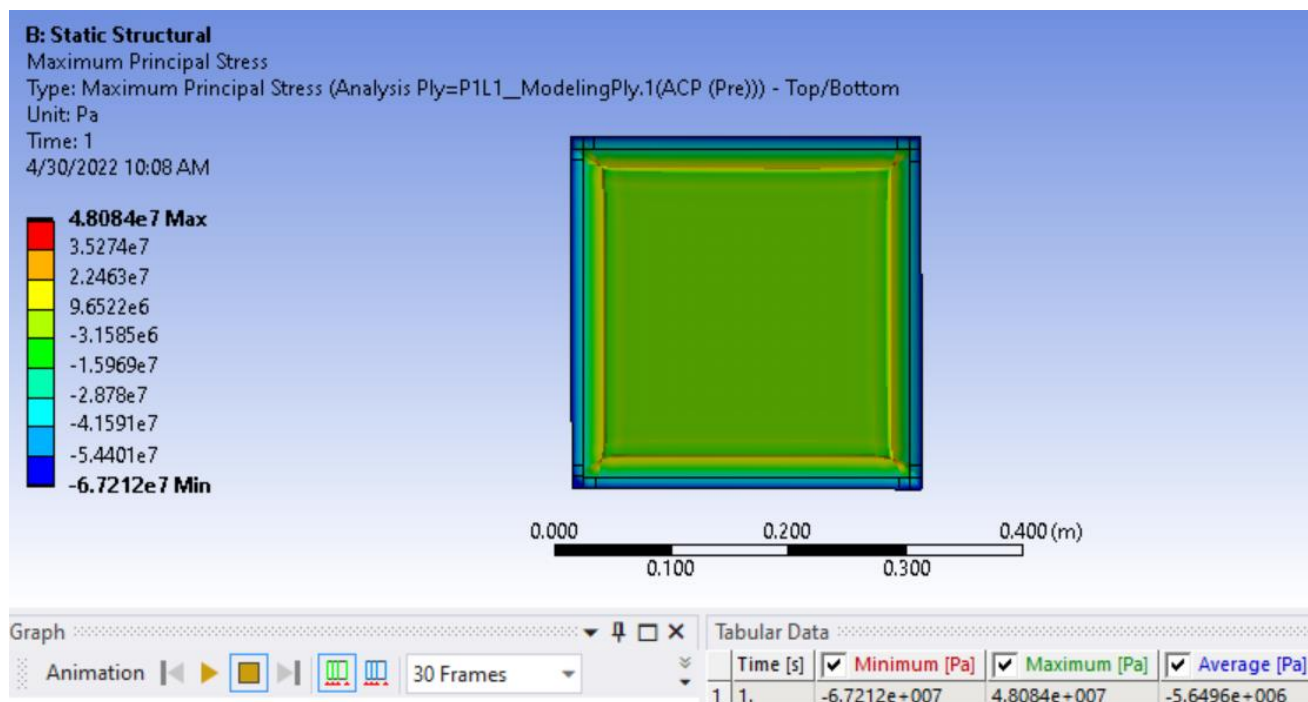
Considering the laminate containing 3 ply's made of Glass/epoxy material with stacking sequence of $[00^\circ, 60^\circ, -60^\circ]$ with each ply thickness = 0.5 mm , making it to total geometry of laminate as $300 \text{ mm} \times 300 \text{ mm} \times 1.5 \text{ mm}$.

Ansys Results:

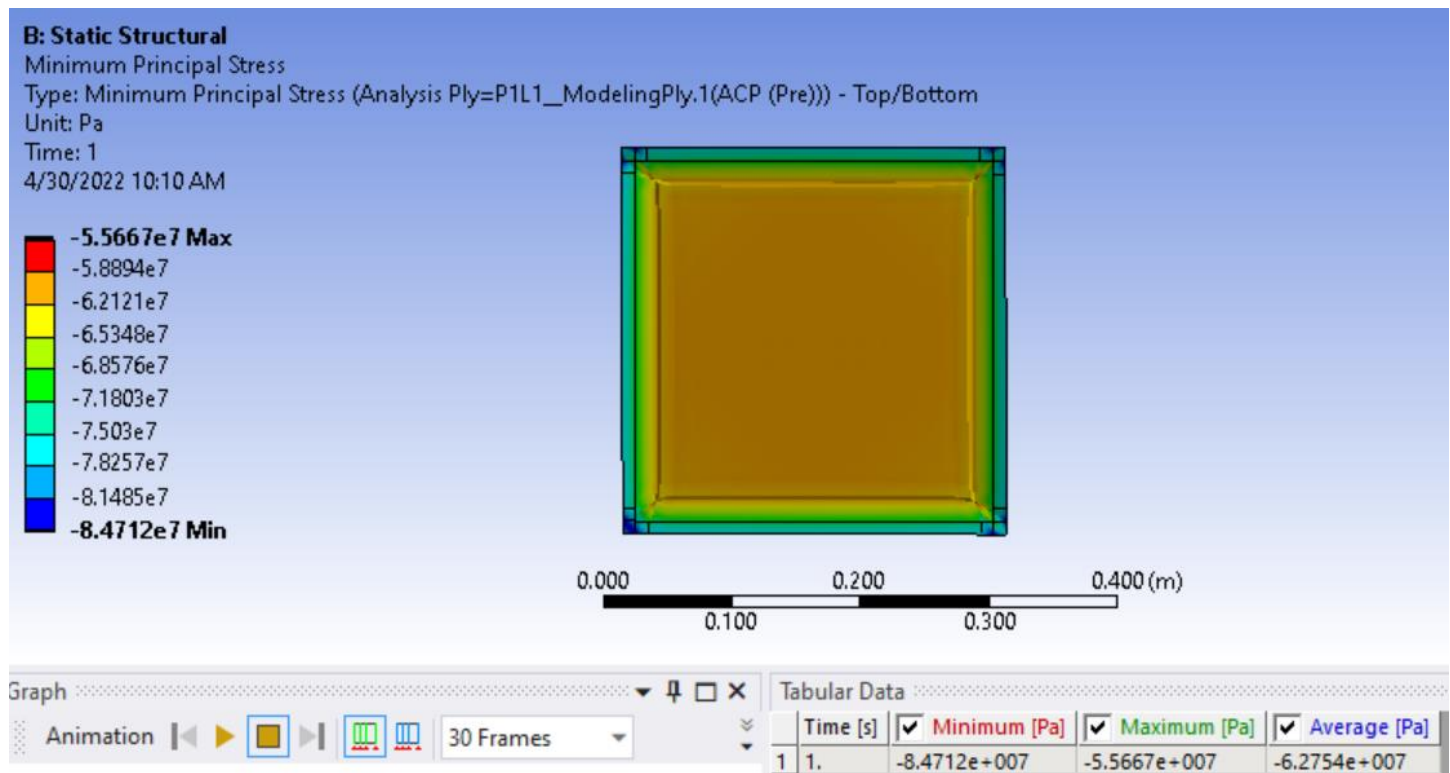
Total Deformation



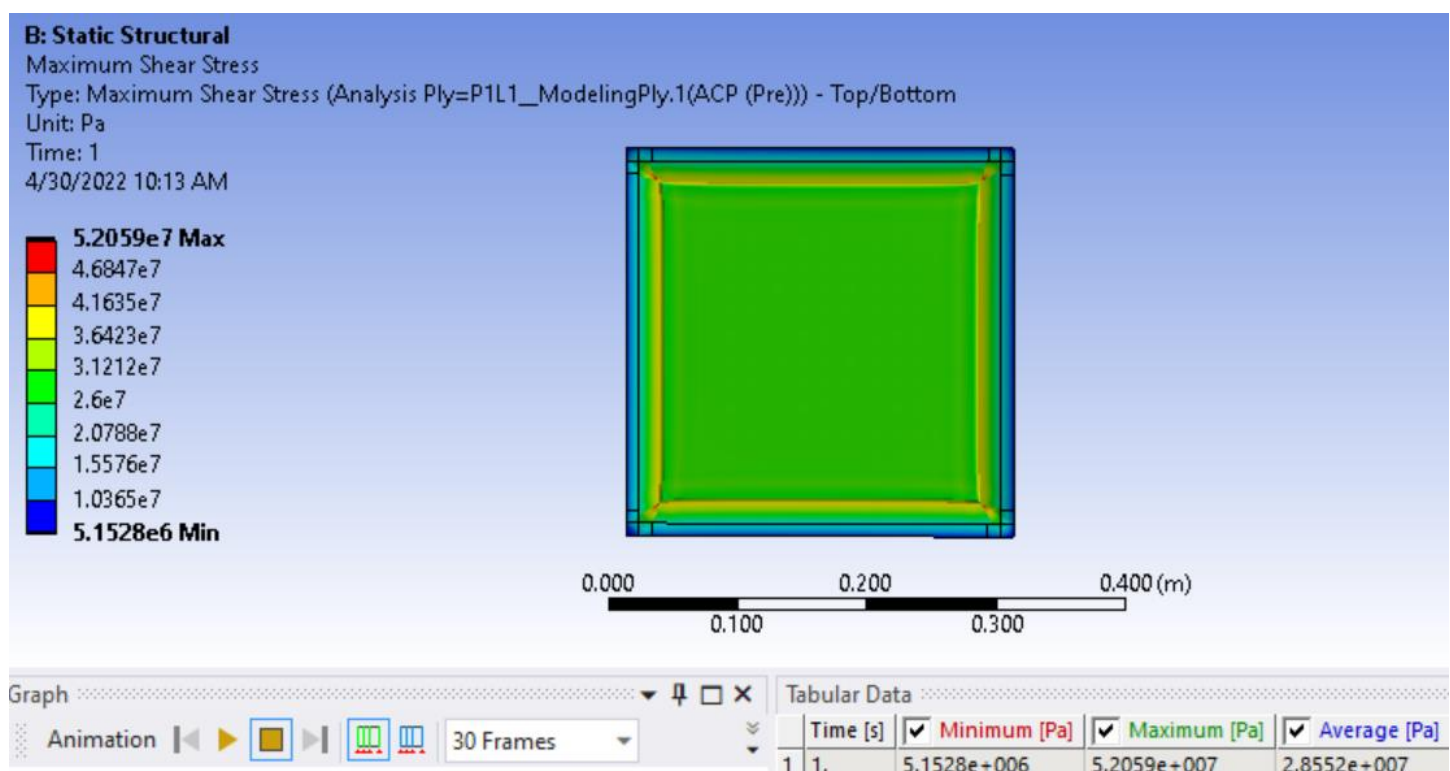
Maximum Principal stress for 0 degree and -60 degree ply,



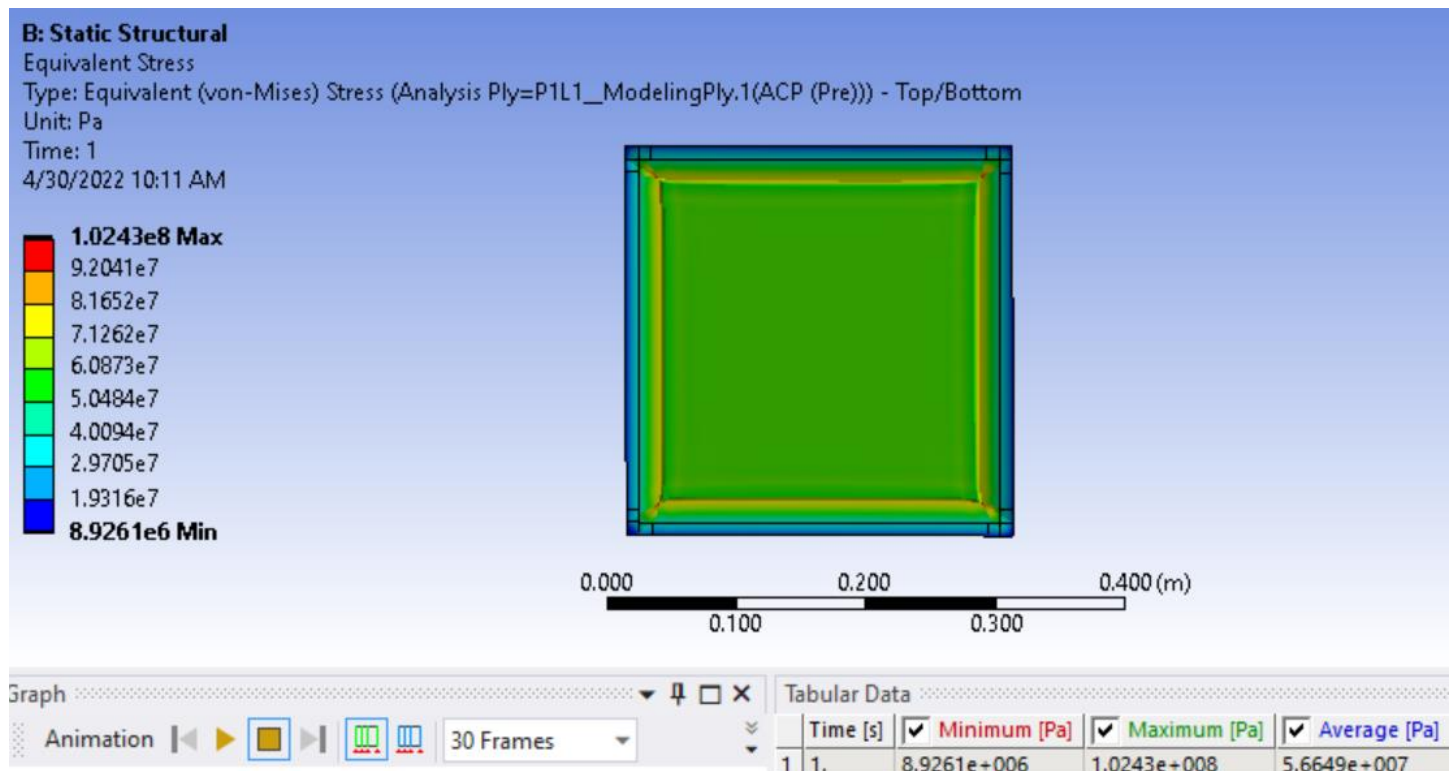
Minimum Principal Stress for 0-degree and -60 degree ply,



Maximum Shear Stress for 0 degree and -60 degree ply,

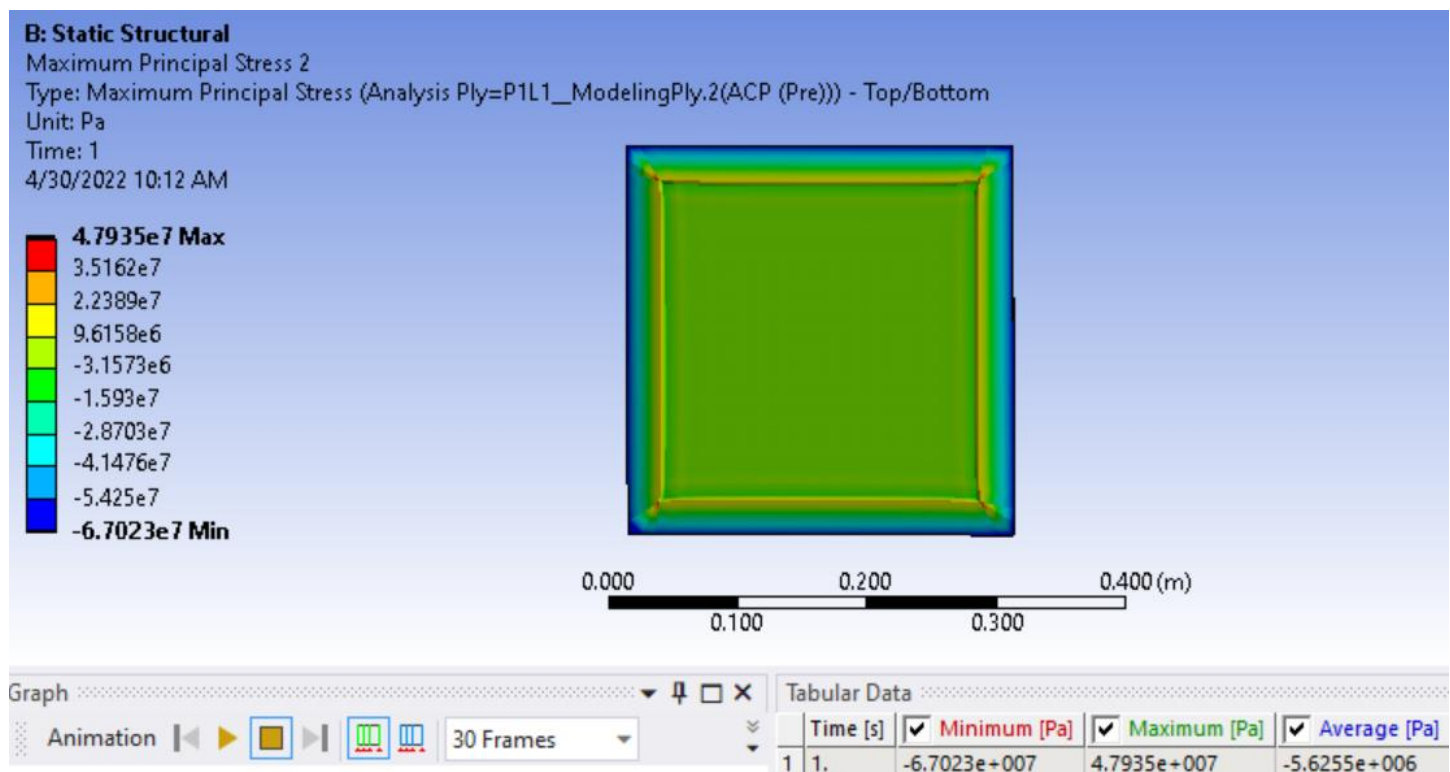


Equivalent Von-Mises Stress for 0-degree and -60 degree ply,

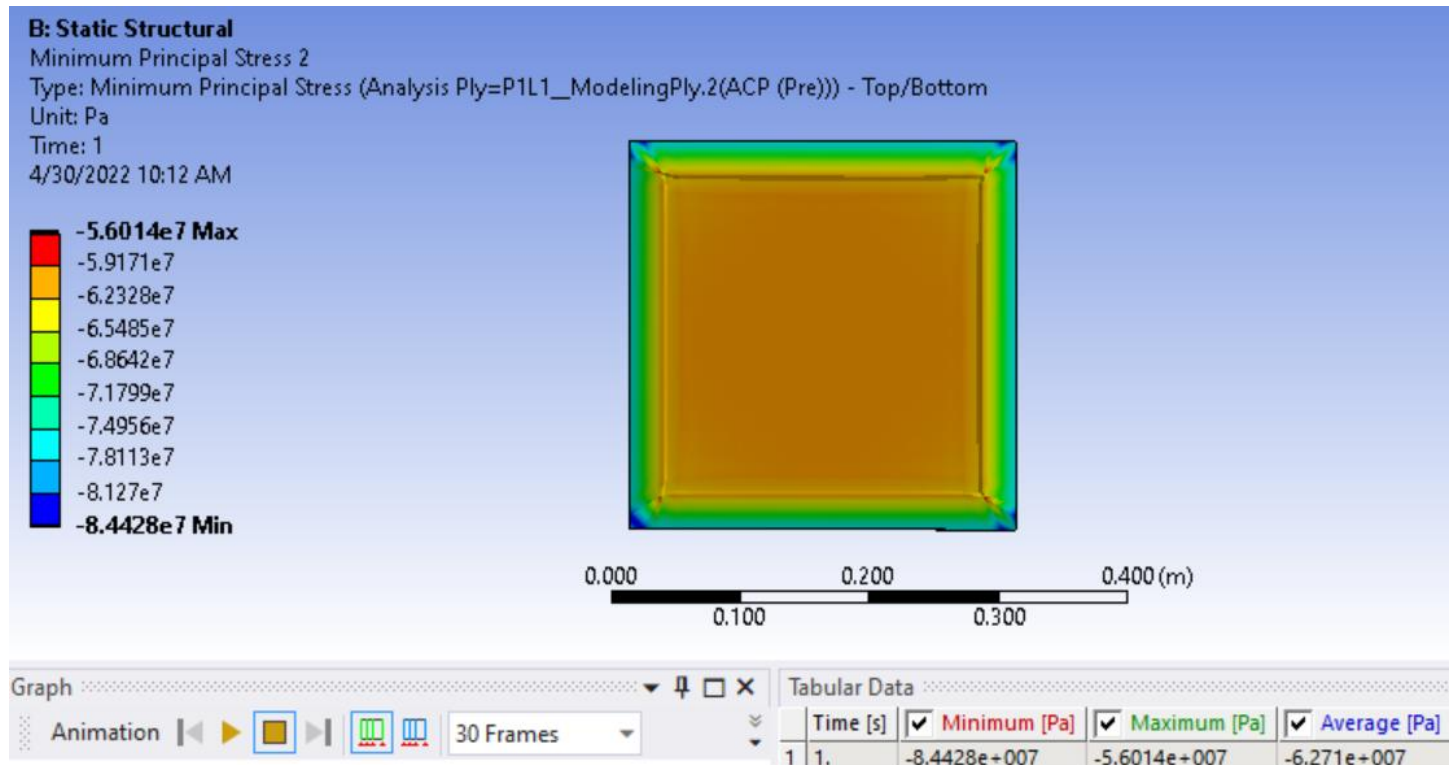


For 60-degree ply,

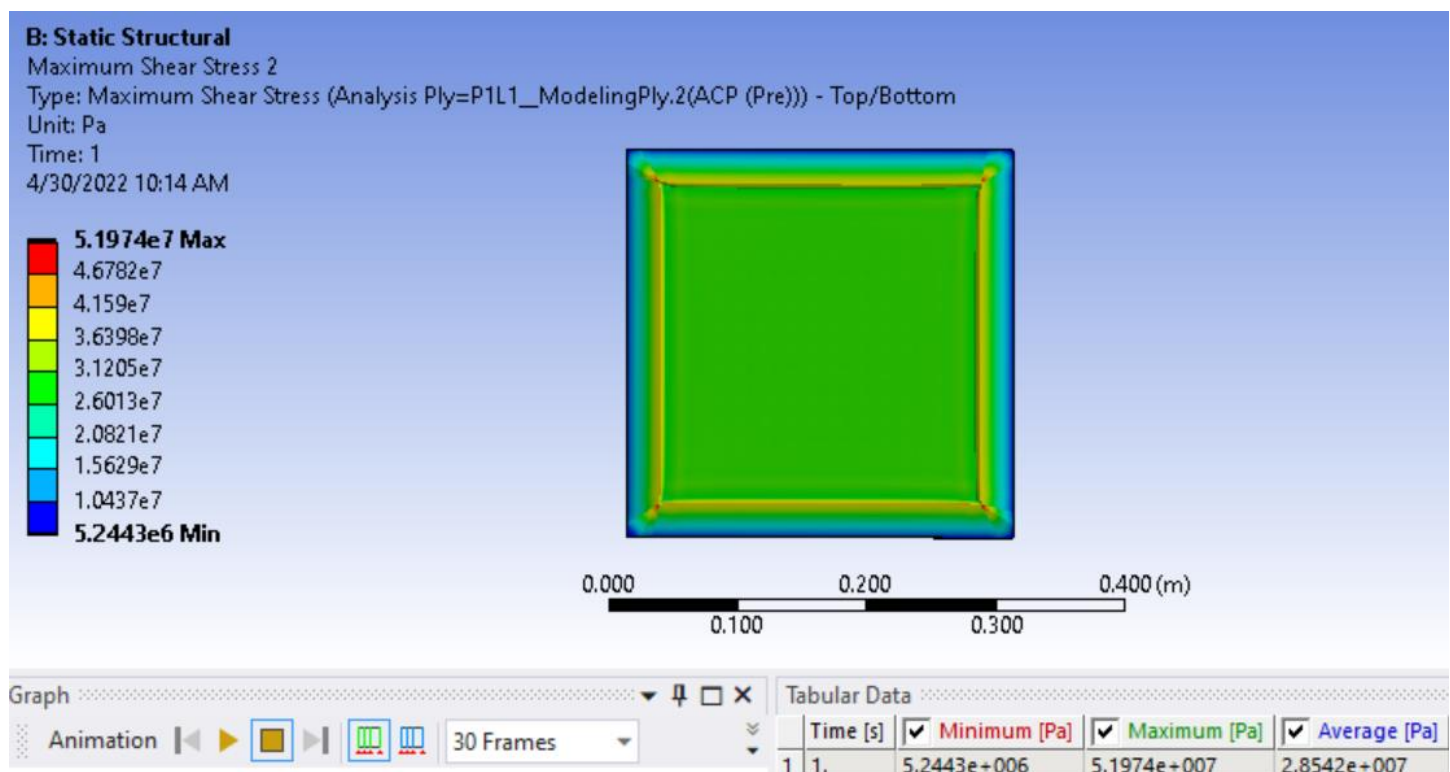
Maximum Principal Stress,



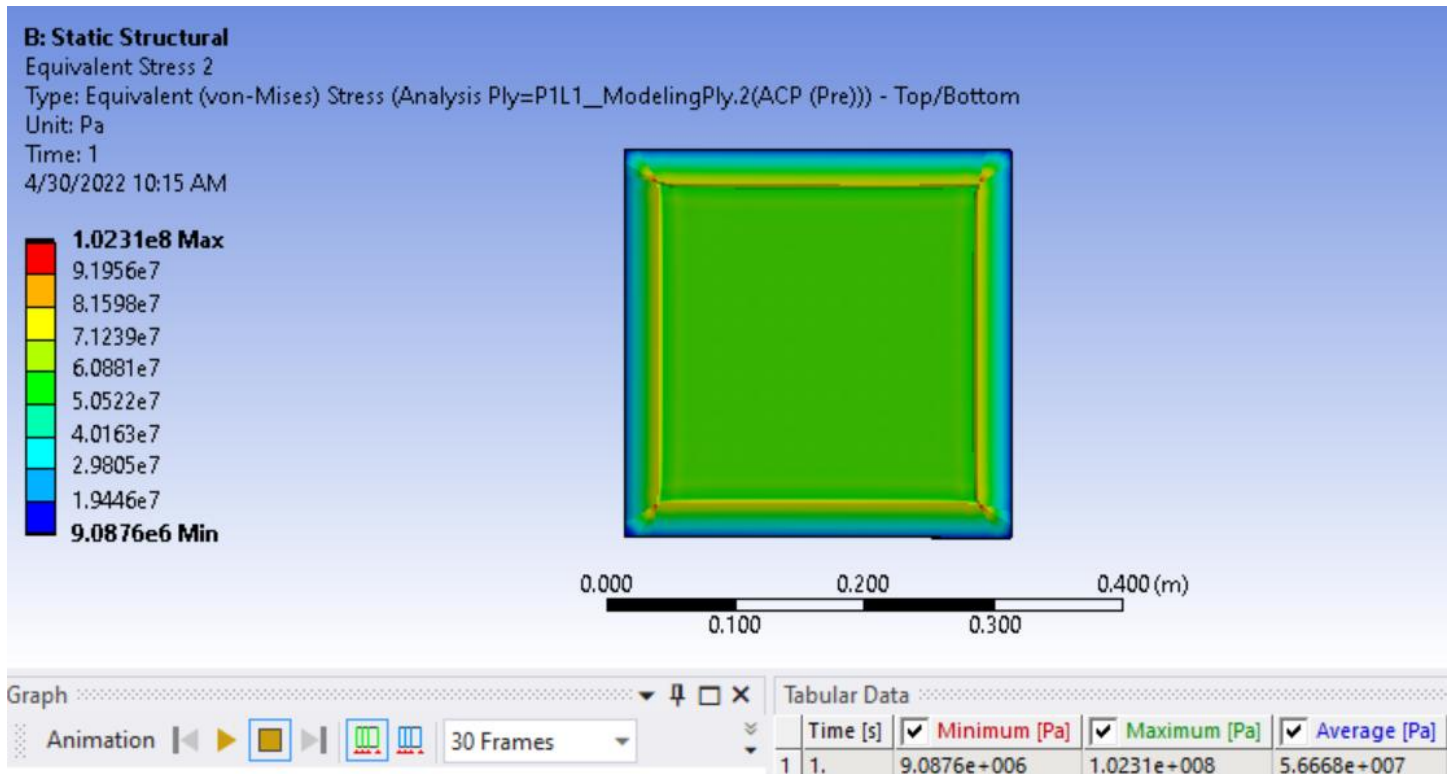
Minimum Principal Stress,



Maximum Shear Stress,



Equivalent Von-Mises Stress,



Failure Theory,

1) Tsai -hill, hoffman, and tsai-wu failure criteria for 0 degree and -60 degree ply,

```
sigma_1=48.084;
sigma_2=-55.667;
tau_12= 52.059;
```

```
Xt=1062;
Xc=610;
Yt=31;
Yc=118;
S=72;
```

```
f1= (1/Xc)+(1/Xt);
f11= -(1/(Xc*Xt));
f6=0;
f66=1/S^2;
f2= (1/Yc)+(1/Yt);
f22= -(1/(Yt*Yc));
```

```
tsai_hill = (sigma_1^2/Xt^2)-((sigma_1*sigma_2)/Xt^2) + (sigma_2^2/Yt^2) + tau_12^2/S^2
```

```
hoffman_failure = -(sigma_1^2/(Xt*Xc))-((sigma_1*sigma_2)/(Xt*Xc))...
```

```
- (sigma_2^2/(Yt*Yc)) + ((Xc+Xt)/(Xc*Xt))*sigma_1 + ((Yc+Yt)/(Yc*Yt))*sigma_2 + (tau_12^2/S^2)
```

```
tsai_wu = f1*sigma_1 + f2*sigma_2 + f11*(sigma_1)^2 + f22*(sigma_2)^2 + f66*(tau_12)^2
```

Results:

```
>> untitled
```

```
tsai_hill =
```

```
3.7518
```

```
hoffman_failure =
```

```
-2.4671
```

```
tsai_wu =
```

```
-2.4713
```

2) Tsai -hill, Hoffman, and tsai-wu failure criteria for 60-degree ply,

```
sigma_1=47.935;  
sigma_2=-56.014;  
tau_12= 51.974;
```

```
Xt=1062;  
Xc=610;  
Yt=31;  
Yc=118;  
S=72;
```

```
f1= (1/Xc)+(1/Xt);  
f11= -(1/(Xc*Xt));  
f6=0;  
f66=1/S^2;  
f2= (1/Yc)+(1/Yt);  
f22= -(1/(Yt*Yc));
```

```
tsai_hill = (sigma_1^2/Xt^2)-((sigma_1*sigma_2)/Xt^2) + (sigma_2^2/Yt^2) + tau_12^2/S^2  
hoffman_failure = -(sigma_1^2/(Xt*Xc))-((sigma_1*sigma_2)/(Xt*Xc))...  
                -(sigma_2^2/(Yt*Yc)) + ((Xc+Xt)/(Xc*Xt))*sigma_1 + ((Yc+Yt)/(Yc*Yt))*sigma_2 + (tau_12^2/S^2)  
tsai_wu = f1*sigma_1 + f2*sigma_2 + f11*(sigma_1)^2 + f22*(sigma_2)^2 + f66*(tau_12)^2
```

Results:

```
>> untitled
```

```
tsai_hill =
```

```
3.7904
```

```
hoffman_failure =
```

```
-2.4939
```

```
tsai_wu =
```

```
-2.4981
```
