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Catch-bot

Tom Queen
School of Computing,
Electronics and Mathematics
Plymouth University
Plymouth, Devon PL4 8AA
Email: xxxx

Daniel Gregory-Turner
School of Computing,
Electronics and Mathematics
Plymouth University
Plymouth, Devon PL4 8AA
Email: xxxx

Demetrius Zaibo
School of Computing,
Electronics and Mathematics
Plymouth University
Plymouth, Devon PL4 8AA
Email: xxxx

Abstract—The abstract goes here.

I. INTRODUCTION

This demo file is intended to serve as a “starter file” for IEEE conference papers produced under L^AT_EX using IEEE-tran.cls version 1.8b and later. I wish you the best of success.

mds

August 26, 2015

A. Subsection Heading Here

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1) Subsubsection Heading Here: Subsubsection text here.

II. DESIGN PROCESS

A. Problem

1) *Inverse Kinematics*: Initially it was thought that the commands to each motor could be generated by looking directly at the returned X and Y coordinates of the tracked objects. To move the gripper upwards, the top two motors should rotate clockwise and the bottom two anticlockwise. To move the gripper to the left, the two left motors should rotate clockwise and the right two anticlockwise. This led to the following kinematic solution:

$$\begin{aligned} M1 &= Y - X \\ M2 &= Y + X \\ M3 &= -Y - X \\ M4 &= -Y + X \end{aligned} \quad (1)$$

For high torque motors, elastic cords and a closed loop between the tracked object and the gripper, this approximation would have been functional. However, it would not have been accurate and it would unnecessarily load the motors. When using stepper motors with low-current drivers, this solution caused the steppers to skip if the gripper was directed more than a few centimeters from the centre of the working area. This led to re-evaluation of the kinematic solution as can be seen in section II-D5.

2) *Force storage*:

3) *Camera speed*: In order to track the target quickly, a low latency high FPS camera was needed.

4) *Motors*: Fast motors were needed to allow the gripper to keep track of the target. The working area of the frame measured XXXX 90cm by 75cm. If the gripper was initialised to the centre of the frame and a ball was thrown from three meters away, then the robot would have 0.7 seconds to move from center to the corner of the working area. PROOF

B. Research

C. Requirements

D. Solutions

To achieve the required speed and torque, several motor solutions were designed.

1) *Micro motors*: The first was to use high torque (300Ncm) encoded DC motors (E192.24.125). The maximum speed of these motors was 33rpm. In order to achieve the required gripper speed of 1.5m/s, a gearbox was needed.

$$\frac{s}{\pi \cdot d \cdot r} = \frac{150}{\pi \cdot 10 \cdot 0.55} = 1 : 8.68 \quad (2)$$

Where d is the spool diameter (10cm), s is required cord speed (150cm/s) and r is motor speed (0.55 RPM). This ratio would result in a gearbox output speed of 149.9cm/s.

2) *Stepper motors*: Another solution was to use stepper motors. Four SST58D3820 stepper motors were acquired. These motors are specified to hold 7.3Kg.cm, which drops to 6.5Kg.cm at a frequency of 1200 pulses per second (PPS). The motors step size was 1.8, giving a max speed of 6RPM.

$$\frac{1.8 \cdot 1200}{360} = 6 \quad (3)$$

3) *Clamps*: To address the problem discussed in II-A2, clamps were designed to lock each cord in place. Each clamp consisted of a high-friction surface suspended above a fixed plate via four springs. The cord to be clamped runs between the two surfaces. A dynamixel ax-12 servo is connected the suspended surface with a pulley. When actuated, the servo pulls the suspended surface towards the fixed plate, closing the gap and clamping the cord in place. A clamp was produced for each of the five cords, one for each corner of the frame and one for the throwing motor.

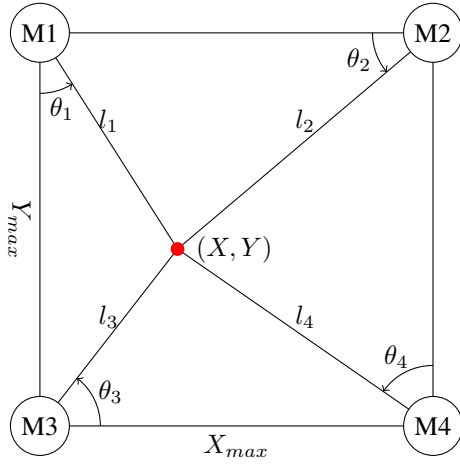


Fig. 1. Kinematic diagram

4) *Camera:* The Sony Playstation3 eye camera can be purchased second-hand for 50p. This camera can output 187 frames per second (FPS) at a resolution of 320x240, or 60 FPS at a resolution of 640x480. In addition, the camera allows for control of exposure, gain, white balance, saturation and hue shift.

5) *Kinematic solution 1: Inverse Kinematics:*

$$\cos(\theta_3) = \frac{X_{max}^2 + l_3^2 - l_4^2}{2 * X_{max} * l_3} \quad (4)$$

$$X = l_3 \sin(\theta_3) \quad (5)$$

$$Y = l_3 \cos(\theta_3) \quad (6)$$

Or, without trigonometry:

$$X = \left(\frac{X_{max}^2 + l_3^2 - l_4^2}{2 * X_{max} * l_3} \right) = \frac{X_{max}}{2} + \frac{l_3^2 - l_4^2}{2 * X_{max}} \quad (7)$$

$$Y = \left(\frac{Y_{max}^2 + l_4^2 - l_3^2}{2 * Y_{max} * l_3} \right) = \frac{Y_{max}}{2} + \frac{l_4^2 - l_3^2}{2 * Y_{max}}$$

Forward Kinematics:

$$\begin{aligned} l_1 &= \sqrt{(X)^2 + (Y_{max} - Y)^2} \\ l_2 &= \sqrt{(X_{max} - X)^2 + (Y_{max} - Y)^2} \\ l_3 &= \sqrt{(X)^2 + (Y)^2} \\ l_4 &= \sqrt{(X_{max} - X)^2 + (Y)^2} \end{aligned} \quad (8)$$

E. Prototype

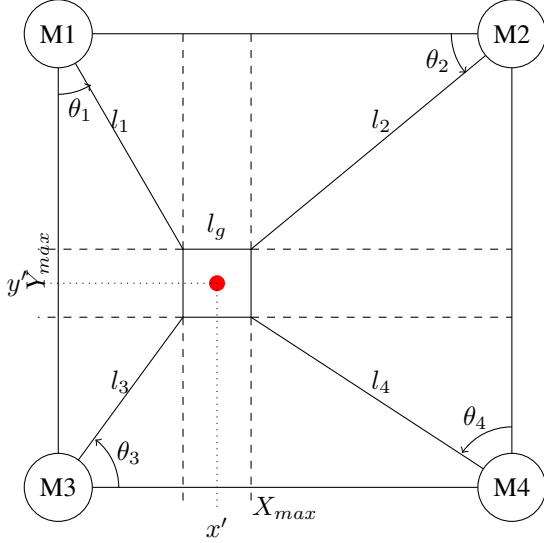
1) *Hardware:* These solutions led to the development of the initial prototype. This robot used four stepper motors to drive the gripper. Each motor was driven by a HST-8325B stepper driver with control signals generated on an teensy3.2 running the arduino firmware.

2) *Software:* The teensy was using the rosserial library to receive the targets CofM from the computer. The teensy then offset the coordinate system so that pixel 0,0 was in the centre of the image. The teensy kept track of all motor positions, and when a new CofM arrived the current gripper position was calculated from the motor positions using the forward kinematics described by equation 8 in II-D5. The program generates motor commands designed to move the gripper so that the centre of the camera image contains the CofM of the target. This is known as visual servoing. The x and y error between the centre of the camera image and the target is calculated, generating a vector that points towards the target. This vector is translated into the change in length of each cord required to center the gripper over the tracked target using the inverse kinematics described by equation 7 in II-D5. The desired gripper location is then checked to see if it has left the bounds of the working area, if it has then movement in the direction of the axis which has been breached is set to zero. Finally, motor speeds are calculated from the desired changes in lengths as is described in equation 11 in section II-G1.

F. Further problems

1) *Gearbox:* A gearbox ratio of 1:8.68 was chosen as can be seen in II-D1. If a 500g gripper were to be raised along either vertical wall of the workspace, the output of the gearbox raising it would experience 5Kg.cm of force. Transferring this force through the gearbox, a 1cm input gear would experience 43.4Kg.cm of force. By making the length of each gear inversely proportional to its accumulated speed multiplier, the stress felt by the input gear could be spread out over the rest of the gears. However, as this would have more than doubled the size of our original gearbox (SIZESXXXXXXXXXXXX), the decision was made to use stepper motors instead.

2) *Kinematics:* Initially the kinematic solution considered the gripper as a point. This worked for preliminary testing, but soon proved to be a problem when the limited torque of the stepper motors required equal tension on all cords at all times. This led to the development of the following kinematic model, which considered the gripper as a square.



Inverse Kinematics:

$$X = \frac{X_{max}}{2} + \frac{l_3^2 - l_4^2}{2(X_{max} - l_g)}$$

$$Y = \frac{Y_{max}}{2} + \frac{l_3^2 - l_4^2}{2(Y_{max} - l_g)}$$

Forward Kinematics:

$$\begin{aligned} l_1 &= \sqrt{\left(X - \frac{l_g}{2}\right)^2 + \left(Y_{max} - Y + \frac{l_g}{2}\right)^2} \\ l_2 &= \sqrt{\left(X_{max} - X + \frac{l_g}{2}\right)^2 + \left(Y_{max} - Y + \frac{l_g}{2}\right)^2} \\ l_3 &= \sqrt{\left(X - \frac{l_g}{2}\right)^2 + \left(Y - \frac{l_g}{2}\right)^2} \\ l_4 &= \sqrt{\left(X_{max} - X + \frac{l_g}{2}\right)^2 + \left(Y - \frac{l_g}{2}\right)^2} \end{aligned} \quad (10)$$

3) *Motor velocities*: For the tension to remain equal on all cords during motion of the gripper, the motors must turn at different rates. For example: if the gripper starts in the centre of the frame and moves upwards, the top two lengths will shorten and the bottom two cords will get longer. To maintain a uniform velocity of the gripper, the top two motors must slow down and the bottom two must speed up.

4) *Motors*:

5) *Arduino*:

G. Redesign

1) *Motor velocities*: To address the issue raised in II-F3 a simple speed scaling system was devised. This algorithm was called once per main loop after the required changes in lengths are calculated. The algorithm takes in the requested changes in length of each cord and divides each change in length by

the largest. The algorithm then scales the relative speeds of each motor by the global speed scalar.

$$\vec{l} = \begin{bmatrix} l_1 \\ l_2 \\ l_3 \\ l_4 \end{bmatrix} \quad x = \max\{l\} \quad (11)$$

$$\vec{s} = \frac{g}{x} \cdot \vec{l}$$

Where g is the global speed scalar and s is the speed of each motor.

H. Final solution

III. IMPLEMENTATION

(9) A. Software

Frames enter the object tracking node at a rate of 60FPS. The object tracker performs a series of filters in different colour spaces on the image before calculating its centre of mass. This coordinate is published to the kinematic controller xxxx milliseconds after the frame enters the object tracker. Upon entering the kinematic controller, the coordinate frame is offset so that the center of the camera image is now at pixel 0,0. The required change in length of each cord is then calculated and set (via the method described in II-F2). From this the required speed of each motor is calculated and set. The kinematic controller node then calculates the current gripper position in order to calculate the changes in length for the next loop. Figure 2 shows the high-level software flow diagram of the robot.

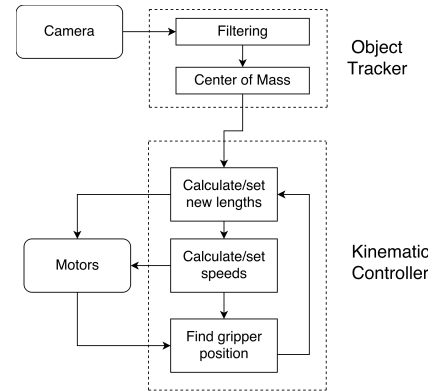


Fig. 2. High-level software flow diagram.

- B. *Frame*
- C. *Kinematics*
- D. *Grippers*
- E. *Clamps*

IV. EXPERIMENTS

- A. *Method*
- B. *Results*
- C. *Discussion*

V. OVERALL DISCUSSION

VI. CONCLUSION

The conclusion goes here.

ACKNOWLEDGMENT

The authors would like to thank...

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