EE 308: Communication Systems

D Manjunath

Networking Lab Department of Electrical Engineering Indian Institute of Technology Handout 1

August 8, 2016

Hilbert Transforms

Hilbert transform: definition

$$\begin{array}{lll} H(f) & := & -j \operatorname{sgn}(f) \\ h(t) & = & \frac{j}{\pi t} \\ \hat{x}(t) & = & h(t) * x(t) \\ & = & \int \frac{x(\tau)}{\pi (t - \tau)} d\tau \\ \hat{x(t)} & = -x(t) \end{array}$$

- Hilbert transform essentially shifts every frequency by $-\pi/2$.
- Can show that $\cos(2\pi f_0 t) = \sin 2\pi f_0 t$ and $\sin(2\pi f_0 t) = -\cos(2\pi f_0 t)$.
- Properties
 - Preserves energy/power
 - x(t) and $\hat{x}(t)$ are orthogonal
 - $m(t)c(t) = m(t)\hat{c}(t)$ when spectra of m(t) and x(t) are non overlapping.



Hilbert Transforms

• Proof of Property 2:

$$\int x(t)\hat{x}(t)dt = \int X(f)X^*(f)df = (j\operatorname{sgn}(f))|X(f)|^2 df$$

Last integrand is odd and is therefore zero.

• Proof of Property 3: Assume |M(f)| = 0 for |f| < W and |C(f)| = 0 for |f| > W. Using the inverse FT representation, we can write

$$m(t)c(t) = \int \int M(f_1)C(f_2)e^{j2\pi(f_1+f_2)t}df_1df_2$$

Using $e^{j\pi f_0 t} = -j \left[\operatorname{sgn}(2\pi f_0 t) \right] e^{j2\pi f_0 t}$ we can write

$$\widehat{m(t)c(t)} = \int \int M(f_1)C(f_2)[-j \operatorname{sgn}(f_1 + f_2)] e^{j2\pi(f_1 + f_2)t} df_1 df_2$$

Observing that $M(f_1) = 0$ for $|f_1| < W$ and $|f_2| > W$ we can write

$$\widehat{m(t)c(t)} = \int_{f_1 = -W}^{W} \int_{f_2 = -\infty}^{-W} M(f_1) e^{j2\pi f_1 t} df_1 \ C(f_2) [-j \operatorname{sgn}(f_1 + f_2)] \ e^{j2\pi f_2 t} df_2$$

$$+ \int_{f_1 = -W}^{W} \int_{f_2 = W}^{\infty} M(f_1) e^{j2\pi f_1 t} df_1 \ C(f_2) [-j \operatorname{sgn}(f_1 + f_2)] \ e^{j2\pi f_2 t} df_2$$

Properties of Hilbert Transforms

By substituting the values for $sgn(f_1 + f_2)$ in the regions of integration, we can write the following.

$$\widehat{m(t)c(t)} = \int_{f_1 = -W}^{W} \int_{f_2 = -\infty}^{-W} M(f_1) e^{j2\pi f_1 t} df_1 \ C(f_2)[-j(-1)] \ e^{j2\pi f_2 t} df_2$$

$$+ \int_{f_1 = -W}^{W} \int_{f_2 = W}^{\infty} M(f_1) e^{j2\pi f_1 t} df_1 \ C(f_2)[-j(+1)] \ e^{j2\pi f_2 t} df_2$$

$$= \left[\int_{f_1 = -W}^{W} M(f_1) e^{j2\pi f_1 t} df_1 \right] \left[\int_{|f| > W} C(f_1)[-j \operatorname{sgn}(f_2)] \ df_2 \right]$$

The limits of the last equality may be omitted. Observe that

$$\hat{c}(t) = \int \widehat{C(f)} \, e^{j2\pi f t} \, df = \int C(f) \, \widehat{ej2\pi f t} \, df = \int C(f) \, [-j\mathrm{sgn}(f)] \, e^{j2\pi f t} \, df$$

Thus

$$\widehat{m(t)c(t)} = m(t)\widehat{c}(t)$$



Analytic Signals and Bandpass Signals

- Define the analytic signal $x_p(t) = x(t) + j\hat{x}(t)$
- Magnitude of $x_p(t)$ is called the *envelope* of a signal.
- The spectrum of $x_p(t)$ is given by

$$X_p(f) = \begin{cases} 2X(f) & |f| > 0\\ 0 & |f| < 0 \end{cases}$$

- $x_p(t)$ is not real and hence $|X_p(f)|$ is not even.
- Let $x_b(t)$ be a real bandpass signal around frequency f_c . Express $x_p(t)$ as

$$x_p(t) = x_l(t)e^{j2\pi f_0 t}$$

where $x_l(t)$ is a complex low pass signal; can also be obtained as below.

$$\begin{array}{rcl} x_p(t) & = & x_l(t)e^{j2\pi f_c t} := x_b(t) + j\hat{x}_b(t) \\ x_b(t) & = & \mathrm{Re}(x_l(t)e^{j2\pi f_c t}) \\ \hat{x}(t) & = & \mathrm{Im}(x_l(t)e^{j2\pi f_c t}) \\ x_b(t) & = & x_R(t)\cos(2\pi f_c t) - jx_I(t)\sin(2\pi f_c t) \\ x_l(t) & := & x_R(t) + j\sin x_I(t) \end{array}$$

 $x_R(t)$ & $x_I(t)$ are, resp., *in-phase* and *quadrature* components of $x_I(t)$.



Analytic Signals and Bandpass Signals

$$\begin{split} \hat{x}_b(t) &= x_R(t)\sin(2\pi f_c t) + jx_I(t)\cos(2\pi f_c t) \\ |x_I(t)| &= a(t) &= \sqrt{x_R^2(t) + x_I^2(t)} \\ \angle x_I(t) &= \theta(t) &= \tan^{-1}\left(\frac{x_I(t)}{x_R(t)}\right) \\ x(t) &= \operatorname{Re}\left(x_I(t)e^{j2\pi f_c t}\right) \\ &= \operatorname{Re}\left(a(t)e^{j(2\pi f_c t + \theta(t))}\right) = a(t)\cos(2\pi f_c t + \theta(t)) \end{split}$$

• Implementations to obtain $x_R(t)$ and $x_I(t)$ from bandpass $x_b(t)$

$$x_R(t) = x_b(t)\cos(2\pi f_c t) + \hat{x}_b(t)\sin 2\pi f_c t$$

- Alternately, write $x_R(t) = x_b(t) \cos(2\pi f_c t)$ and $x_I(t) = x_b(t) \sin 2(\pi f_c t)$ and pass through a LPF of suitable bandwidth.
- Given $x_R(t)$ and $x_I(t)$ we can obtain $x_b(t)$ as $x_R(t) \cos(2\pi f_c t) x_I(t) \sin(2\pi f_c t)$.
- HW: What is the energy in $x_l(t)$ in terms of the energy in $x_l(t)$?



Analytic Signals and Bandpass Signals

• Freq domain relation between $x_b(t)$ and $x_l(t)$

$$x_b(t) = \operatorname{Re} \left(x_l(t) e^{j2\pi f_c t} \right)$$

$$X_b(f) = \mathcal{F} \left(x_l(t) e^{j2\pi f_c t} + x_l^*(t) e^{-j2\pi f_c t} \right)$$

$$= X_l(f + f_c) + X_l^*(-f - f_c)$$

• Alternately, we can derive the above by realising that for f > 0, $X_b(f) = X_l(f - f_c)$ and since $x_b(t)$, is real $X_b(-f) = X^*(f)$

Bandpass Systems

- $H_b(f)$ is the impulse response of a bandpass system
- $H_l(f) = u(f + f_c)H(f + f_c)$. Then $H(f) = H_l(f f_c) + H_l^*(-f f_c)$ and $h_b(t) = \text{Re}\left[h_l(t)e^{j2\pi f_c t}\right]$
- Let $y_b(t) = h_b(t) * x_b(t)$. Since we can write

$$Y_{b}(f) = X_{b}(f)H_{b}(f)$$

$$= [S_{l}(f - f_{c}) + S^{*}(-f - f_{c})][H_{l}(f - f_{c}) + H^{*}(-f - f_{c})]$$

$$\approx X_{l}(f - f_{c})H_{l}(f - f_{c}) + X_{l}^{*}(-f - f_{c})H_{l}^{*}(-f - f_{c})]$$

$$= X_{l}(f)H_{l}(f)$$

- We use $X_l(f f_c)H_l^*(-f f_c) = 0$ for all f since $X_l(f-f_c), H_l(f-f_c) \approx 0$ for all f < 0
- We use $X_t^*(-f f_c)H_t(f f_c) = 0$ for all f since $X_l(f-f_c), H_l(f-f_c) \approx 0$ for all f < 0

