



AVIATION FORUM

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Skewness effects on the turbulence structure in a high-speed compressible and multi-component inert mixing layers

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- 2 Numerical setup
- 3 Numerical results
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PROBLEM DESCRIPTION

- Scramjet engines are exciting candidates for the next generation air-breathing propulsion.
- Mixing layer is a classical paradigm case for free-shear turbulent flows.
- Emergence and evolution of turbulent features exhibit high sensitivity to the parametric set-up of the test case.
 - ✓ Compressibility effects quantified with convective Mach number

$$\text{Ma}_c = (\mathbb{U}^h - \mathbb{U}^l) / (\mathfrak{c}^h + \mathfrak{c}^l)$$

- ✓ Pressure influence quantified with the gradient Mach number

$$\text{Ma}_g = S\ell / \langle \mathfrak{c} \rangle$$

- ✓ Inlet density ratio $\mathfrak{s} = \varrho^h / \varrho^l$
- Most classical analysis assume that \mathbb{U}^h and \mathbb{U}^l are perfectly aligned.

PROBLEM DESCRIPTION

- Few studies dedicated to the analysis of skewing effect
 - ✓ Skewing effects on incompressible shear layer (Meldi *et al.* 2020)¹
 - ✓ Sweeping effects in a backward-facing step (Kaltenbach 2004)²
- Numerous features of the inlet flow can affect the features of the turbulent mixing region.

Assessment of the present study

- Investigation of the skewing effects on shear layer development
- Inert configuration
- Direct numerical simulations: no turbulence models
- High-speed combustion regimes: Scramjet engines
- Multicomponent transport
- Gas mixtures: hydrogen, air ...

¹Meldi, M., Mariotti, A., Salvetti, M. V., & Sagaut, P. (JFM-2020). Numerical investigation of skewed spatially evolving mixing layers.

²Kaltenbach, H. J. (EJMB/F-2004). Turbulent flow over a swept backward-facing step.

COMPUTATIONAL METHODOLOGY

- Cartesian Navier-Stokes solver, three-dimensional, compressible, unsteady, viscous, multi-species, massively parallel in-house solver

$$\begin{cases} \partial_t \varrho + \partial_j (\varrho u_j) = 0, \\ \partial_t (\varrho u_i) + \partial_j (\varrho u_i u_j) + \partial_i p = \partial_j \tau_{ij}, \\ \partial_t (\varrho e_t) + \partial_j (\varrho e_t + p) u_i = \partial_j (u_i \tau_{ij}) - \partial_j q_j, \\ \partial_t (\varrho Y_\alpha) + \partial_j (\varrho u_j Y_\alpha) = -\partial_j (\varrho Y_\alpha u_{\alpha j}), \quad \alpha \in \mathcal{S} \\ p = \varrho R T / W, \quad W = 1 / (\sum_{\alpha \in \mathcal{S}} Y_\alpha / W_\alpha), \quad h_\alpha(T) = \varphi_\alpha R T / W_\alpha \end{cases} \quad (1)$$

with the polynomial φ_α being determined from JANAF tables

- Convective fluxes are discretized hybrid energy-conservative shock-capturing scheme in locally conservative form with *Ducros* sensor^a.
- Molecular fluxes: Laplacian form with fourth-order formulas.
- Temporal integration: RK3 scheme
- Multicomponent transport (Soret and Dufour): EGLIB library^b.

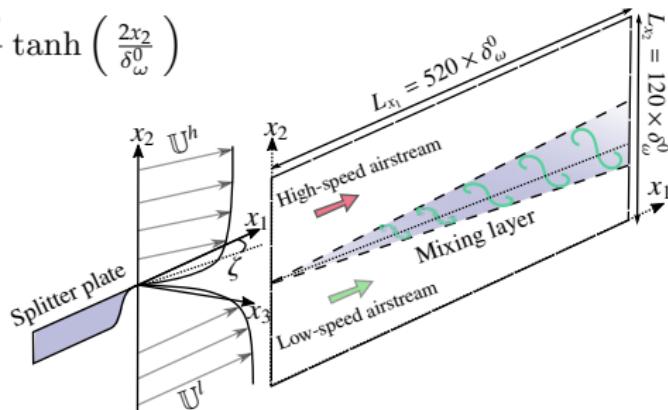
^a Pirozzoli, S. (JCP-2010). Generalized conservative approximations of split convective derivative operators.

^b Ern, A., & Giovangigli, V. (JCP-1995). Fast and accurate multicomponent transport property evaluation.

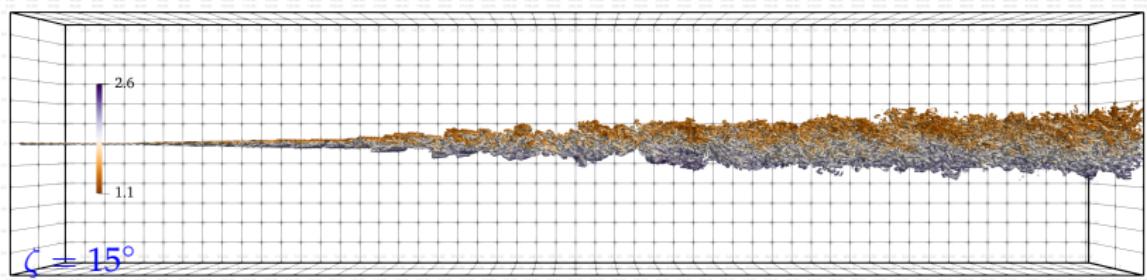
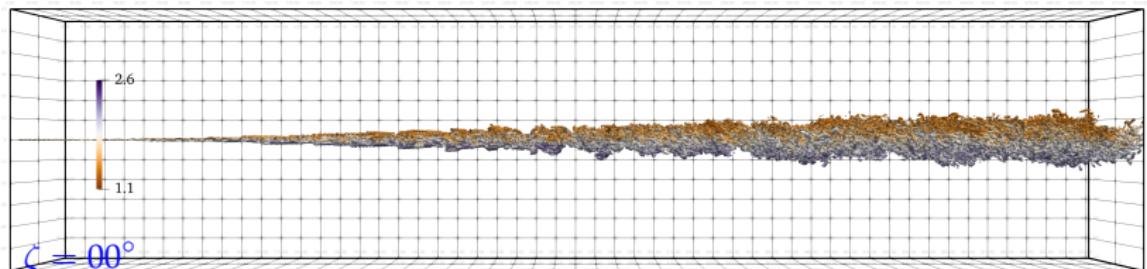
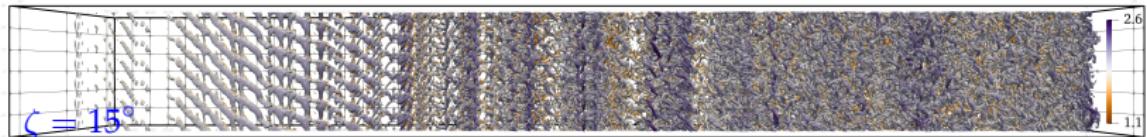
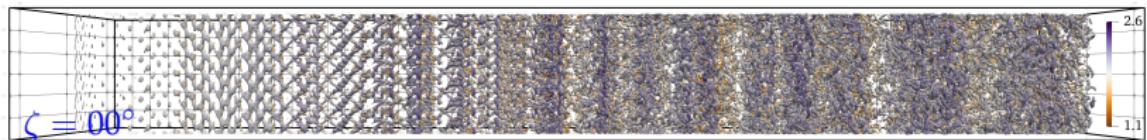
NUMERICAL CONFIGURATION

- $L_1 \times L_2 \times L_3 = 520\delta_{\omega,0} \times 120\delta_{\omega,0} \times 60\delta_{\omega,0}$, $N_1 \times N_2 \times N_3 = 2500 \times 380 \times 180$.
- Dirichlet BC at the inlet, perfectly non-reflecting BCs at the the outflow and the x_2 -directions, and periodic BCs along x_3 -directions.
- Air-fuel (OConaire) : H₂, H, H₂O, HO₂, HO₂, O₂, O, OH, N₂
- $\text{Re}_{\omega} = \bar{\rho}\Delta U\delta_{\omega,0}/\bar{\mu} = 640$, $\text{Ma}_c = 0.48$, $\xi = 0^\circ, 5^\circ, 10^\circ$ and 15° .

$$\begin{cases} \varphi(x_1 = 0, x_2, x_3) = \frac{\varphi^h + \varphi^l}{2} + \frac{\varphi^h - \varphi^l}{2} \tanh \left(\frac{2x_2}{\delta_{\omega}^0} \right) \\ \mathbf{u}^h = (\mathbb{U}^h \cos \zeta, 0, \mathbb{U}^h \sin \zeta) \\ \mathbf{u}^l = (\mathbb{U}^l, 0, 0) \\ \delta_{\omega}^0 = (\mathbb{U}^h - \mathbb{U}^l) / \max |\partial_2 \langle u_1 \rangle_F| \end{cases}$$

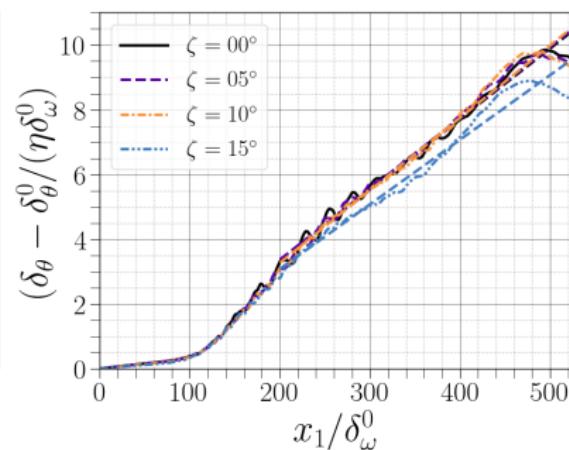
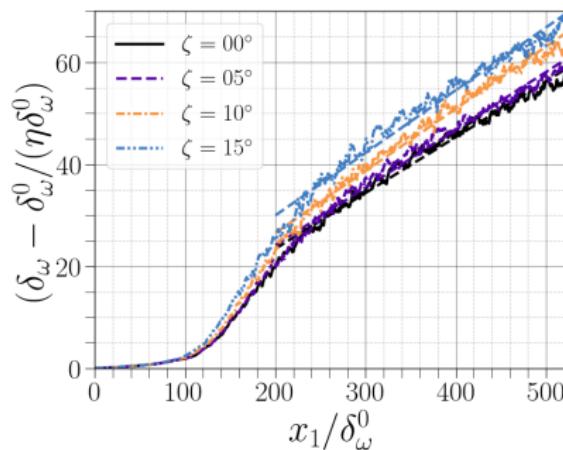


INSTANTANEOUS FLOW

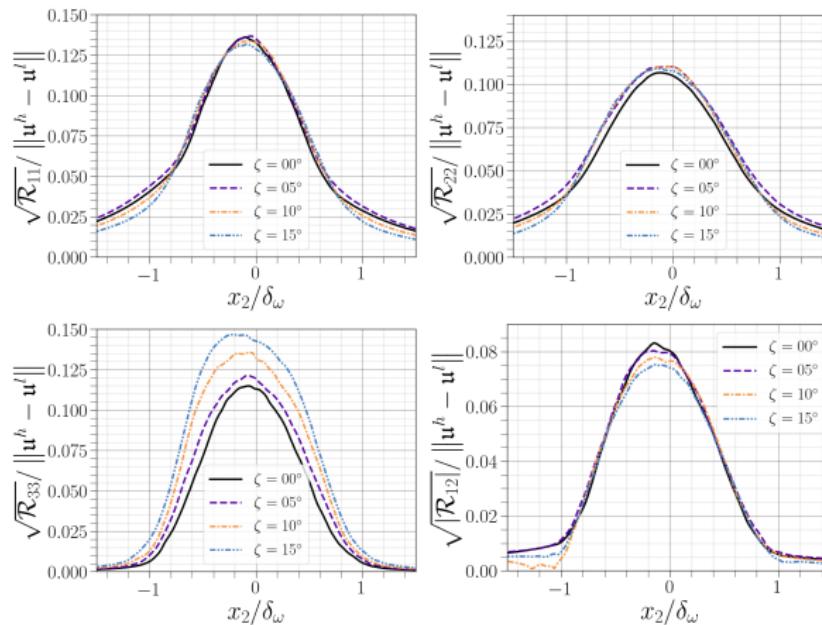


QUANTITATIVE ANALYSIS

- Growth rates of δ_ω and $\delta_\theta = \frac{1}{\varrho_0} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \langle \varrho \rangle \frac{\langle u_1 \rangle_f - \mathbb{U}^h}{\|u^h - u^l\|} \left(1 - \frac{\langle u_1 \rangle_f - \mathbb{U}^h}{\|u^h - u^l\|} \right) dx_2 dx_3$



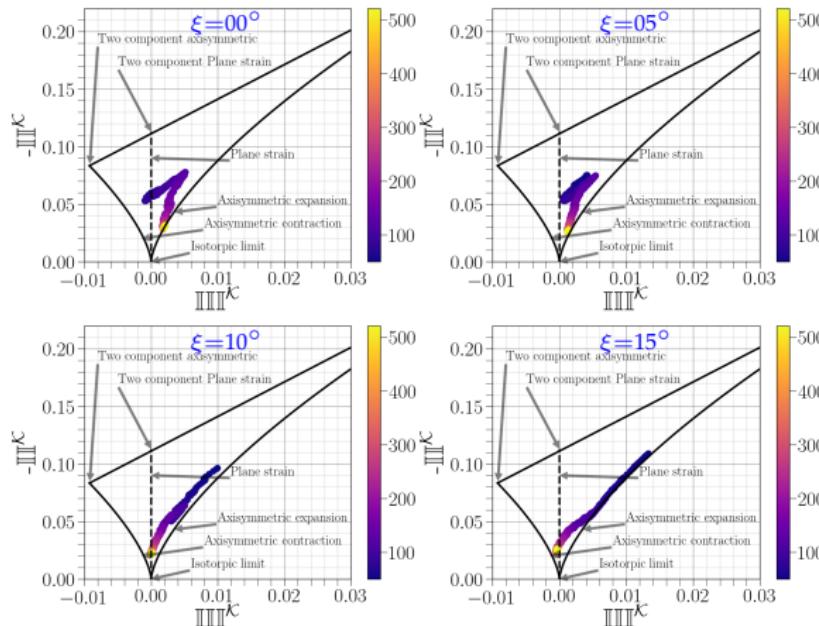
REYNOLDS STRESSES



- As ξ get higher $\mathcal{R}_{33} > \mathcal{R}_{11} > \mathcal{R}_{22} > \mathcal{R}_{12} \equiv \mathcal{R}_{23} > \mathcal{R}_{13}$.
- Skewing SLs induce more intense turbulence and enlarge the momentum exchange between the turbulent structures and the inflow mainstream.

ANISOTROPY EFFECT

- Reynolds stress anisotropy $b_{ij}^K = \frac{\mathcal{R}_{ij} - \frac{2}{3}\delta_{ij}\mathcal{K}}{2\mathcal{K}}$.
- Invariants of \mathbf{b}^K : $\mathbb{II}^K = -\frac{1}{2}(\Lambda_1^2 + \Lambda_2^2 + \Lambda_3^2)$, $\mathbb{III}^K = \frac{1}{3}(\Lambda_1^3 + \Lambda_2^3 + \Lambda_3^3)$.



CONCLUSIONS & PERSPECTIVES

Perspectives

- Inlet skewing tends to amplify the inlet disturbances resulting in a faster increase of the mixing process
 - ✓ An increase of the cross-wise velocity fluctuation energy.
- Longitudinal evolution of vorticity thickness exhibit remarkable modification with inlet skewing

Perspectives

- application towards flow control, and reliable comparison.
- Investigation of the skewing effects in combination with inlet perturbations.
- Heat release effects.
- Variations of the Reynolds number.

Thanks for tuning in!
Please leave comments & questions

Acknowledgments

