

Complex impedance of L , C and R

As a start we derive the formulas for the complex impedance for a capacitor, an inductor and a resistor. Subsequently, this is applied in simple passive analogue filters using these devices.

We consider an (harmonic) electric current $I(t) = I_0 \cos(\omega t)$ with I_0 the current amplitude and $\omega = 2\pi f$ the radial frequency (and f the frequency in Hz). In complex notation the current reads

$$I(t) = I_0 e^{j\omega t} \quad (1)$$

For an inductor, see figure 1, the relation between the voltage V across the inductor and the current through it is given by

$$V(t) = L \frac{dI(t)}{dt} \quad (2)$$

with L the coefficient of self-induction of the inductor.



Figure 1: Inductor symbol.

Substitution of the equation for the current, equation (1), into equation (2) yields

$$V(t) = L j \omega I_0 e^{j\omega t} \quad .$$

Using $j = e^{\frac{1}{2}\pi j}$ this can be written as

$$V(t) = \omega L I_0 e^{j\left(\omega t + \frac{1}{2}\pi\right)} = V_0 e^{j\left(\omega t + \frac{1}{2}\pi\right)} \quad (3)$$

where we have introduced the voltage amplitude $V_0 = \omega L I_0$.

Going back to non-complex notation, this would read $V(t) = V_0 \cos\left(\omega t + \frac{1}{2}\pi\right)$, i.e. there is a phase shift of 90° between the current and the voltage across an inductor.

Now, the complex impedance of an inductor is defined as $Z_L = \frac{V}{I} = \frac{j\omega L I_0 e^{j\omega t}}{I_0 e^{j\omega t}}$, i.e.

$$Z_L = j\omega L \quad (4)$$

The inductive reactance is given as $X_L = |Z_L| = \omega L$ and has units Ohm.

Note: The same result can be obtained by going to the frequency domain using the Fourier transform, which is defined for signal $x(t)$ as

$$X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt \quad (5a)$$

The inverse Fourier transform reads

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega) e^{j\omega t} d\omega \quad (5b)$$

We rewrite equation (2) as

$$v(t) = L \frac{di(t)}{dt} \quad (6)$$

now using lowercase symbols to indicate that we are in the time domain. We use the property that if X is the Fourier transform of x then $j\omega X$ is the Fourier transform of the derivative $x' = \frac{dx}{dt}$. Hence, Fourier transforming equation (6) yields $V(\omega) = j\omega L I(\omega)$ with V and I the Fourier transform of v and i , respectively. Hence

$$Z_L = \frac{V(\omega)}{I(\omega)} = j\omega L \quad (7)$$

For a capacitor, see figure 2, the relation between the voltage V across the capacitor and the accumulated charge Q is given by

$$V = \frac{Q}{C} \quad (8)$$

with C the capacitance of the capacitor. We have $I(t) = \frac{dQ(t)}{dt} = I_0 \cos(\omega t)$ or in complex notation $I(t) = I_0 e^{j\omega t}$.



Figure 2: Capacitor symbols (left: fixed, right: variable).

Now

$$V = \frac{Q}{C} = \frac{1}{C} \int I(t) dt = \frac{1}{C} \int I_0 e^{j\omega t} dt = \frac{I_0}{j\omega C} e^{j\omega t} = \frac{I}{j\omega C}.$$

Hence, the complex impedance of a capacitor, being the ratio of V and I , becomes

$$Z_C = \frac{1}{j\omega C} \quad (9)$$

The capacitive reactance is given as $X_C = |Z_C| = \frac{1}{\omega C}$ and has units Ohm.

Using $\frac{1}{j} = e^{-\frac{1}{2}\pi j}$ we see that $V(t) = V_0 \cos\left(\omega t - \frac{1}{2}\pi\right)$ with voltage amplitude $V_0 = \frac{I_0}{\omega C}$.

Finally, as for a resistor $V = IR$ (Ohm's law), the complex impedance of a resistor is simply

$$Z_R = R \quad (10)$$

with R the resistance of the resistor (which is of course real-valued).

We will now consider the *LRC* series circuit depicted in figure 3. The current at all points in the circuit is the same and assumed to be given as $I(t) = I_0 \cos(\omega t)$ (or $I(t) = I_0 e^{j\omega t}$ in complex notation). With the expressions for the complex impedances derived above, the expression for the (AC) voltage V is easily found. The total impedance of the circuit is given by

$$Z = R + j\omega L + \frac{1}{j\omega C} = R + j\left(\omega L - \frac{1}{\omega C}\right) \quad (11)$$

Hence, the voltage reads

$$V = ZI = \left[R + j\left(\omega L - \frac{1}{\omega C}\right) \right] I_0 e^{j\omega t}$$

which can be written as

$$V = \sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2} e^{j\phi} I_0 e^{j\omega t} = V_0 e^{j(\omega t + \phi)}$$

with voltage amplitude $V_0 = I_0 \sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}$ and phase angle $\phi = \tan^{-1} \left(\frac{\omega L - \frac{1}{\omega C}}{R} \right)$.

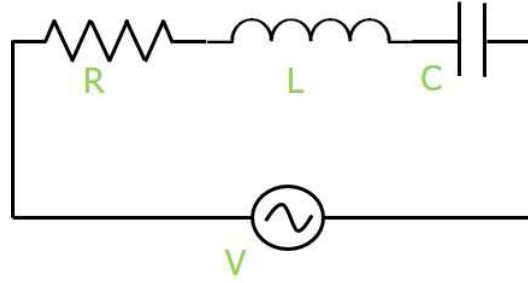


Figure 3: *RLC* series circuit.

The peak current in the *LRC* series circuit is given by

$$I_0 = \frac{V_0}{\sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}} \quad (12)$$

which is maximum when $\omega L - \frac{1}{\omega C} = 0$ or $\omega_0 = \frac{1}{\sqrt{LC}}$ at which frequency the circuit is in resonance,

see figure 4 where we plotted $\frac{I_0}{V_0}$ versus frequency for two values of R .

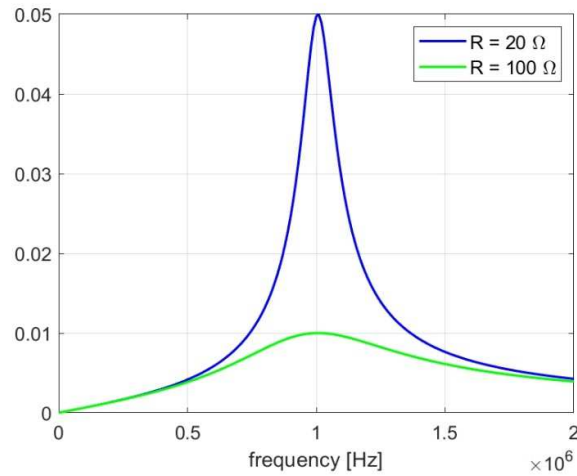


Figure 4: Resonance in an *LRC* series circuit for $L = 25 \mu\text{H}$ and $C = 1 \text{ nF}$ ($f_0 = 1 \text{ MHz}$)

As a second example we consider the *LRC* parallel circuit of figure 5. Given the voltage $V(t) = V_0 \cos(\omega t)$ (or $V(t) = V_0 e^{j\omega t}$ in complex notation), what is the expression for total current leaving the source?

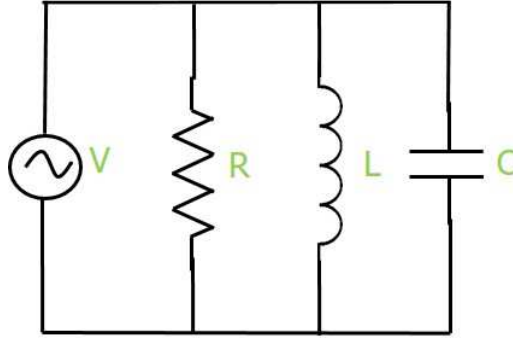


Figure 5: *RLC* parallel circuit.

Now, the total impedance Z of the circuit is determined by

$$\frac{1}{Z} = \frac{1}{Z_R} + \frac{1}{Z_L} + \frac{1}{Z_C} = \frac{1}{R} + \frac{1}{j\omega L} + j\omega C \quad (13)$$

Hence, the current is

$$I = \frac{V}{Z} = V \left(\frac{1}{R} + \frac{1}{j\omega L} + j\omega C \right) = V \left[\frac{1}{R} + j \left(\omega C - \frac{1}{\omega L} \right) \right]$$

which can be written as

$$I = V_0 e^{j\omega t} \sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L} \right)^2} e^{j\phi} = I_0 e^{j(\omega t + \phi)}$$

with current amplitude $I_0 = V_0 \sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L} \right)^2}$ and phase angle $\phi = \tan^{-1} \left[R \left(\omega C - \frac{1}{\omega L} \right) \right]$.

Passive analog filters

Passive low-pass, high-pass, band-pass and band-stop filters consisting of combinations of resistors, capacitors and inductors can be assessed by the complex impedance method developed in the previous section. In addition, the formula for a voltage divider using two resistors, see figure 6, is needed and given by

$$\frac{v_{out}}{v_{in}} = \frac{R_2}{R_1 + R_2}. \quad (14a)$$

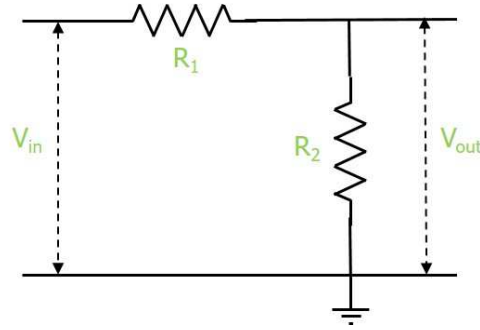


Figure 6: A simple voltage divider using two resistors R_1 and R_2 (which may be replaced by complex impedances Z_1 and Z_2 , respectively).

When the resistors R_1 and R_2 are replaced by the complex impedances Z_1 and Z_2 , respectively, then the relation between output voltage v_{out} and input voltage v_{in} is still given by

$$\frac{v_{out}}{v_{in}} = \frac{Z_2}{Z_1 + Z_2}. \quad (14b)$$

The ratio $\frac{v_{out}}{v_{in}}$ is called the transmission function $H(j\omega)$ of the filter.

As a first example we consider the filter depicted in figure 7. The transmission function or voltage amplification of this simple low-pass filter is given as

$$H(j\omega) = \frac{v_{out}}{v_{in}} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{1 + j\omega RC}. \quad (15)$$

A so-called Bode diagram of $H(j\omega)$ is given in figure 8 for $R = 850 \, \Omega$ and $C = 1 \, \mu\text{F}$. A Bode diagram shows plots of the absolute value (in dB) and phase (in degrees) of $H(j\omega)$ as a function of frequency (using a logarithmic frequency axis). The roll-off in the stop band of the filter is 6 dB/octave (1 octave being a factor 2 in frequency) or 20 dB/decade. In this case the cut-off frequency is $f_c = \frac{1}{2\pi RC} = 187$

Hz at which $|H(j\omega)| = \frac{1}{\sqrt{2}}$ (= -3 dB).

Note: A filter is fully characterized by its transmission function, which gives its behavior in the frequency domain. A filter is also fully determined by its impulse response $h(t)$ being the response of the filter to a Dirac delta function, i.e. $v_{in}(t) = \delta(t)$. $h(t)$ is the inverse Fourier transform of $H(j\omega)$.

In this case $h(t) = \frac{1}{RC} e^{-\frac{t}{RC}}$, $t \geq 0$.

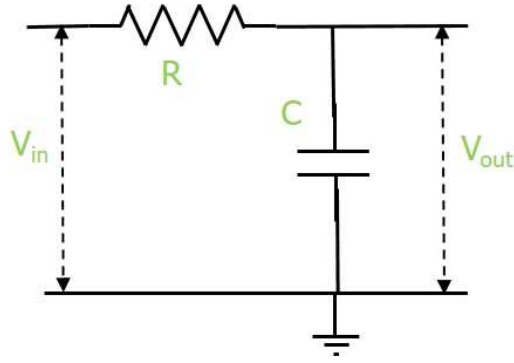


Figure 7: The simplest low-pass filter.

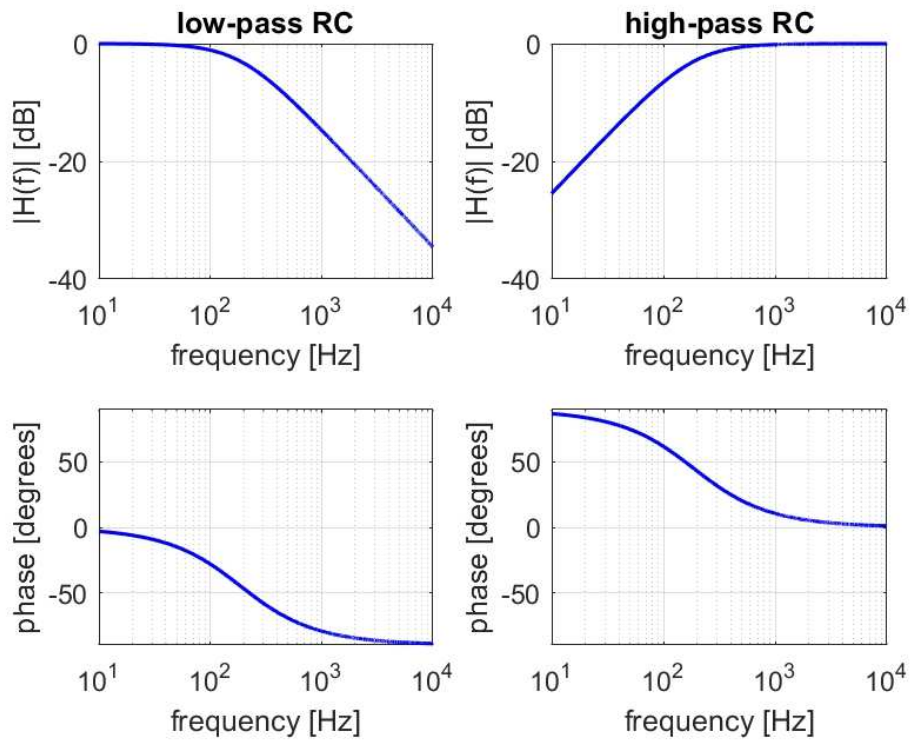


Figure 8: Bode plots of the low-pass RC filter (left) and high-pass RC filter (right).

Figure 9 shows the simplest high-pass filter, the transmission function of which is

$$H(j\omega) = \frac{v_{out}}{v_{in}} = \frac{R}{\frac{1}{j\omega C} + R} = \frac{j\omega RC}{1 + j\omega RC}. \quad (16)$$

The corresponding Bode plot is shown in figure 8, again for $R = 850 \, \Omega$ and $C = 1 \, \mu\text{F}$.

Note: The transmission function of this filter can be rewritten as $H(j\omega) = \frac{1}{1 + j\omega RC}$. The inverse

Fourier transform of this, i.e. the impulse response, is $h(t) = \delta(t) - \frac{1}{RC} e^{-\frac{t}{RC}}, t \geq 0$.

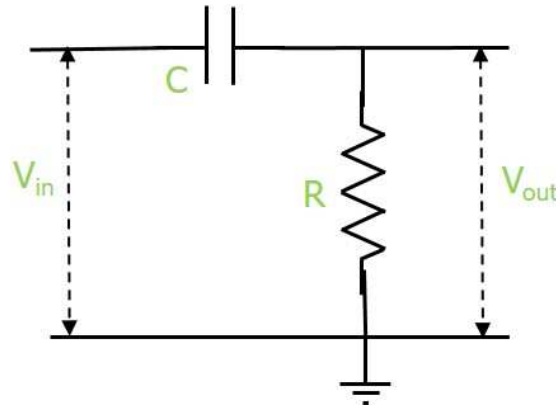


Figure 9: the simplest high-pass filter.

A simple band-pass filter can be made by adding an inductor parallel to the capacitor in the low-pass filter of figure 7, see figure 10. The transmission function of this filter is derived as follows. The impedances Z_1 and Z_2 (of equation 14b) are given by $Z_1 = R$ and

$\frac{1}{Z_2} = \frac{1}{j\omega L} + j\omega C = j\left(\omega C - \frac{1}{\omega L}\right)$, i.e. the transmission function $H(j\omega)$ is thus

$$\frac{Z_2}{Z_1 + Z_2} = \frac{\frac{1}{j\left(\omega C - \frac{1}{\omega L}\right)}}{R + j\left(\omega C - \frac{1}{\omega L}\right)}. \text{ Hence,}$$

$$H(j\omega) = \frac{1}{1 + jR\left(\omega C - \frac{1}{\omega L}\right)}. \quad (17)$$

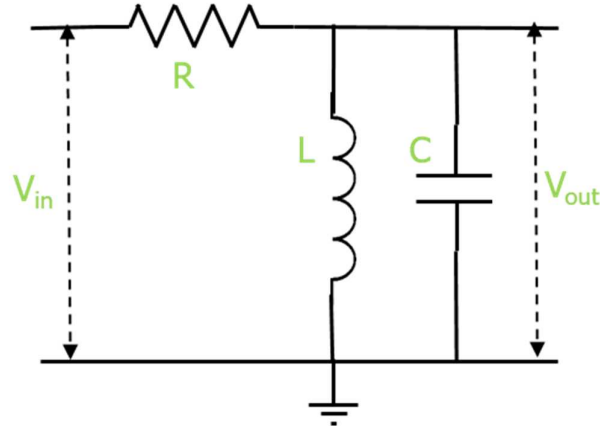


Figure 10: The simplest band-pass LRC filter.

The simplest band-stop filter using an inductor is shown in figure 11, the transmission function of which is

$$H(j\omega) = \frac{j\left(\omega L - \frac{1}{\omega C}\right)}{R + j\left(\omega L - \frac{1}{\omega C}\right)} \quad (18)$$

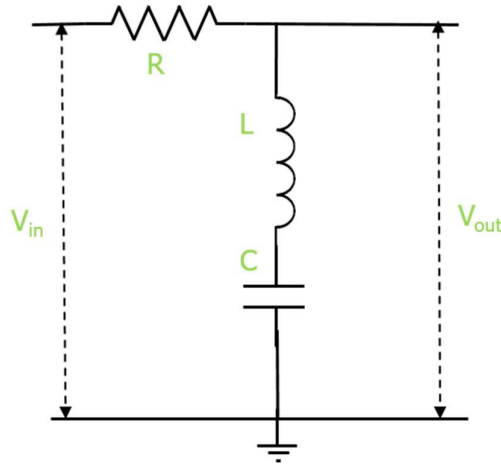


Figure 11: The simplest band-stop LRC filter.

Taking $C = 230 \text{ pF}$ and $L = 110 \text{ }\mu\text{H}$, i.e. resonance frequency $f_0 = \frac{1}{2\pi\sqrt{LC}} = 1 \text{ MHz}$, we have plotted $|H(j\omega)|$ and the phase of $H(j\omega)$ as function of frequency (on a linear frequency axis) in figure 12. The resistance R for the band-pass filter and the band-stop filter is chosen as $10 \text{ k}\Omega$ and $100 \text{ }\Omega$, respectively.

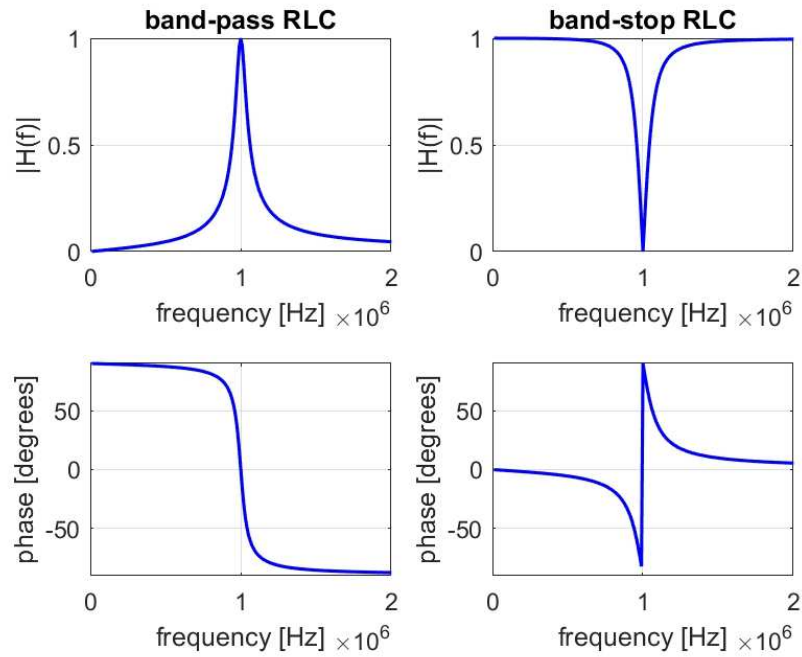


Figure 12: Plots of $H(j\omega)$ (absolute value and phase) for the RLC band-pass (left) and the RLC band-stop filter (right). The same values for L and C are taken (i.e. same resonance frequency being 1 MHz). For the band-pass filter $R = 10 \text{ k}\Omega$ and for the band-stop filter $R = 100 \Omega$.