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# **Declaration**

No portion of the work contained in this project has been submitted in support of an application for another degree or qualification of this or any other university or institute of learning.

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**Dr. Md. Mashiur Rahaman**

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**Noshin Tarannum**

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**Rafid Imam**

# **Forwarding Letter**

To,

Dr. Md. Mashiur Rahaman

Professor

Department of Naval Architecture and Marine  
Engineering Bangladesh University of Engineering and  
Technology.

**Subject:** Regarding completion of our project on designing of 3000 DWT IR class  
general cargo for operation in the inland waterways of Bangladesh.

Sir,

We are pleased to submit our project paper which was done as part of our course NAME 338. This project was aimed towards designing IR class general cargo for operating in inland waterways of Bangladesh. The project was completed over two semesters, and presented to the faculty through four consecutive presentations. This project paper serves as the complete documentation of the entire design process entailed throughout the past two semesters.

All throughout the duration of this project, we have received numerous suggestions as to how to correct, iterate or better our design. This final paper contains the final corrected and completed design-work with all the suggested edits incorporated within it.

This letter has our completed NAME 338 project paper attached and forwarded with it, provided to you for your inspection and approval. Therefore, we hope and pray that you will accept our project paper, and oblige thereby.

Sincerely,

Noshin Tarannum

Student ID- 1712002

Rafid Imam

Student ID- 1712043

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# **Owner's Requirement**

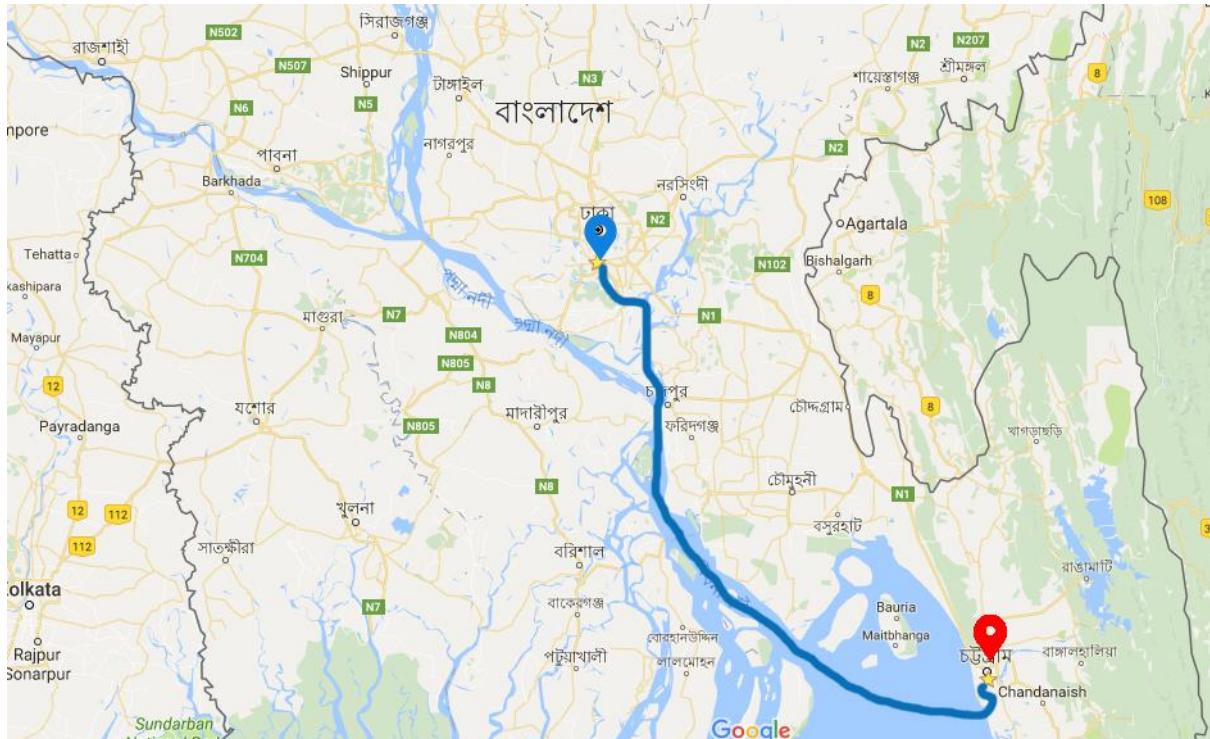
**Vessel Type: General Cargo**

**Route: Dhaka to Chittagong**

**Service Speed: 10 knot**

**Deadweight: 3000 tones**

# Route Specification



**Route:** Dhaka to Chittagong  
(Shadar Ghat to Chittagong Port)

**Route Length:** 304 km  
(164 Nautical Miles)

# Basis Ship Selection



**M.V. ROKNOOR 32**

Length overall, $L_{OA}$	82.56 m
Length between Perpendicular, $L_{BP}$	79.29 m
Breadth, B	16.00 m
Depth, D	5.50 m
Draft, H	4.10m
$C_B$	0.859
Deadweight	3200 tonnes
Speed	10 knot
Displacement	4526.83 tonnes
Class	IRS

Source: <https://www.ome ltd.com/projects/15>

# **Principal Particulars**

# **Principal Particulars of Design Ship**

## **DETERMINATION OF PRINCIPAL PARTICULARS OF DESIGN SHIP**

### **From the Ratio of Basis Ship:**

$$L/B = 4.956$$

$$B/H = 3.902$$

$$B/D = 2.909$$

$$H/B = 0.256$$

Applying Cubic Root Formula Length,  $L = \left[ \frac{DWT \times (L/B)^2 \times (B/H)}{C_D \times C_B \times \rho} \right]^{1/3} = 77.942\text{m}$

Now from the ratio of basis ship we get,

$$\text{Breadth, } B = 15.728 \text{ m}$$

$$\text{Depth, } D = 5.500 \text{ m}$$

$$\text{Draft, } H = 4.100 \text{ m}$$

Displacement 4317.350 tones

### **Using Empirical Method,**

For general cargo ship Length,

$$L = 5.54 \left( \frac{V}{V+2} \right) DWT^{\frac{1}{3}} + 12.041 = 78.620\text{m}$$

$$\text{Breadth, } B = 15.865 \text{ m}$$

$$\text{Depth, } D = 5.453\text{m}$$

$$\text{Draft, } H = 4.065 \text{ m}$$

Displacement= 4355.60 tones

### **Using Munro-Smith,**

For a general Cargo Ship,

$$\frac{DWT}{\Delta} = \frac{.750 \times DWT}{DWT + 300}$$

Displacement = 4400.000 tones

Again,  $\Delta = L/B \times H/B \times B^3 \times C_b$

(page 18, method 3 ,ex-2.3)

Length, L = 78.886 m

Breadth, B = 15.918 m

Depth, D = 5.472 m

Draft, H = 4.079 m

The comparison of the values among different methods for determining preliminary particulars:

	Using Basis Ship Ratio	Using Empirical Formula	Using formula from Munro Smith
Length, L	77.942	78.620	78.886
Breadth, B	15.728	15.865	15.918
Depth, D	5.500	5.453	5.472
Draft, H	4.100	4.065	4.079

## Principal particulars comparison between basis ship and design ship

Parameters	Basis Ship	Design Ship
<b>Length Overall, <math>L_{OA}</math></b>	82.56 m	81.16 m
<b>Length Between Perpendicular, <math>L_{pp}</math></b>	79.29 m	77.94 m
<b>Breadth, B</b>	16.00 m	15.72 m
<b>Depth, D</b>	5.50 m	5.41 m
<b>Draft, H</b>	4.10 m	3.59 m
<b>Deadweight</b>	3200 tonnes	3000 tonnes
<b>Displacement</b>	4526.83 tonnes	3776.00 tonnes
<b><math>C_B</math></b>	0.859	.859
<b><math>C_D</math></b>	0.707	.700

## The Principal Particulars Comparison between Preliminary and Final Design Ship

Parameters	Final Design Ship	Preliminary Design Ship
<b>Length Overall, <math>L_{OA}</math></b>	81.16 m	81.16 m
<b>Length Between Perpendicular, <math>L_{pp}</math></b>	77.94 m	77.94 m
<b>Breadth, B</b>	15.72 m	15.72 m
<b>Depth, D</b>	5.41 m	5.41 m
<b>Draft, H</b>	3.59 m	4.03 m
<b>Deadweight</b>	3000 tonnes	3000 tonnes
<b>Displacement</b>	3776.00 tonnes	4243.90 tones
$C_B$	0.859	0.859
$C_D$	0.70	0.70

**POWER ESTIMATION**  
**&**  
**MANNING**

We know,

$$\text{Admiralty Coefficient, } Ac = \left( \frac{\Delta^{2/3} \times V^3}{P} \right)_D$$

$$\text{For Basis ship and design Ship } \left( \frac{\Delta^{2/3} \times V^3}{P} \right)_B = \left( \frac{\Delta^{2/3} \times V^3}{P} \right)_D$$

Power of Basis Ship 1125 KW

So using the formula we can estimate the power of Design Ship = 1096 KW

1096 KW for two Engines. Thus 548 KW for each of them

Fuel Used : Diesel

## **PRELIMINARY WEIGHT CALCULATION AND POWER ESTIMATION**

Service Speed , V = 10 knot

$$= 18.5 \text{ km/h}$$

Voyage distance , s = 164 nautical miles

Voyage time, t =  $s / v$  = 32.800 Hours

$$= 1.3667 \text{ Days}$$

Endurance time = 4Days

$$= 96 \text{ Hours}$$

Cargo Capacity (tones) = 2950 tones

Power of Basis Ship = 1125 KW

Admiralty Coefficient of Basis Ship : 243.2150866

Crew Member: 16

### **Engine Information**

Model M26

BHP 548 KW each

SFC  $\leq 213 \text{ gKw/h}$

SLOC  $\leq 1.0 \text{ gKw/h}$

Source : Weichai Marine Engines

## Iteration 1

BHP ( Single Engine ) 548 kW

BHP = ( 2 · 1 engine's BHP ) 1096 kW

SFC ( Single Engine ) = 213 g/kW·hr

SLOC ( Single Engine ) = 0.8 g/kW·hr

Constant Addition of Fuel= 1.5 (1.14-1.5)

WHFO = SFC · BHP · Voyage time · Constant Addition = 11485.64 kg

WDO = 20% of WHFO = 2297.128 kg

WLO = SLOC · BHP · Voyage time · Constant Addition = 43.13856 kg

### Fresh water consumption for

Crew = 20 kg per person per day = 1280 kg

Bath & Laundry needs = 200 kg per person per day = 12800 kg

Cooking = 4 kg per person per day = 256 kg

Machinery (Main Engine) ( 10 g/kW·hr ) = 1052.16 kg

Auxiliary needs = 20% of Main Engine = 210.432 kg

Reserve= 5000 kg

Net Crew Weight = 75 kg · Crew Member= 1200 kg

Store & Provision = 10 kg per person per day= 640kg

**Net weight** = 36264.50048 kg= 36.2645 tonnes

Deadweight = Cargo capacity + Net Weight= 2986.2645 tonnes

Displacement ,  $\Delta$  = Deadweight /  $C_D$ = 4340.5007 tonnes

$$PB = \frac{\frac{2}{\Delta^3} \times V^3}{A_c} = 1094.0472 \text{ kW}$$

PB per engine = 547.0236 kW

## Iteration 2

BHP ( Single Engine ) = 547.02 kW

BHP = ( 2 · 1 engine's BHP ) = 1094.047 kW

SFC ( Single Engine ) = 211g/kW·hr

SLOC ( Single Engine )= 0.8 g/kW·hr

Constant Addition of Fuel= 1.5 (1.14-1.5)

WHFO = SFC · BHP · Voyage time · Constant Addition =12557.16kg

WDO = 20% of WHFO= 2511.43 kg

WLO = SLOC · BHP · Voyage time · Constant Addition = 47.61 kg

Fresh water consumption for Crew = 20 kg per person per day = 1280kg

Bath & Laundry needs = 200 kg per person per day =12800 kg

Cooking = 4 kg per person per day = 256 kg

Machinery (Main Engine) ( 10 g/kW·hr )= 1050.28 kg

Auxiliary needs = 20% of Main Engine = 210.05 kg

Reserve = 5000 kg

Net Crew Weight = 75 kg · Crew Member = 1200 kg

Store & Provision = 10 kg per person per day= 640 kg

Net weight = 37552.54 kg

= 37.55 tonnes

Deadweight = Cargo capacity + Net Weight = 2987.55 tonnes

Displacement ,  $\Delta$  = Deadweight /  $C_D$  = 4342.37 tonnes

$$PB = \frac{\frac{2}{3} \times V^3}{A_c} = 1094.384622 \text{ kW}$$

PB per engine 547.1923109 kW

**Following the same path as before we got,**

<b>Iteration 3</b>	<b>546.969 KW</b>
<b>Iteration 4</b>	<b>546.968 KW</b>
<b>Iteration 5</b>	<b>546.968 KW</b>

Source: Ship Design Methodologies of Preliminary Design by Apostolos Papanikolaou

Preliminary Engine Power 547 KW each

Total of 1094 KW

## Determination of Number of Bulkheads

Distance between two bulkheads =  $0.15L + 6.5 = 18.27 \text{ m}$

So the Number of Bulkhead Stands = 4

## Determination of Frame Spacing

Frame spacing =  $450 + 2L \approx 600 \text{ mm}$

Framing System : Transverse Framing

Source: Inland Shipping Ordinance

## MANNING

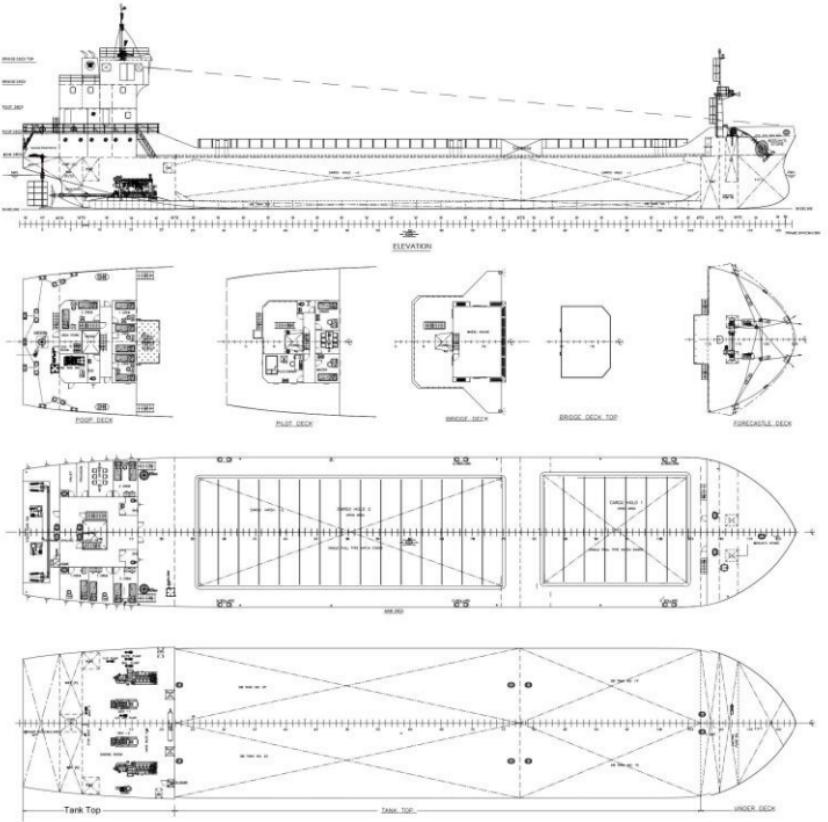
Owner	1
1st Class Master	1
2nd Class Master	1
Sailor	7
Inland Marine Engineer	2
1st Class Driver	1
Greaser	3
Total	16

Source: Inland Shipping Ordinance

# **General Arrangement Plan**

## MAIN PARTICULARS

Length(0A)	81.161 m
Length(WL)	79.038 m
Length(BP)	77.942 m
Breadth(Moulded)	15.728 m
Depth(Moulded)	5.406 m
Draft(Design)	3.588 m
Frame Spacing	650 mm
Service Speed	10 knot
Deadweight	3000 T

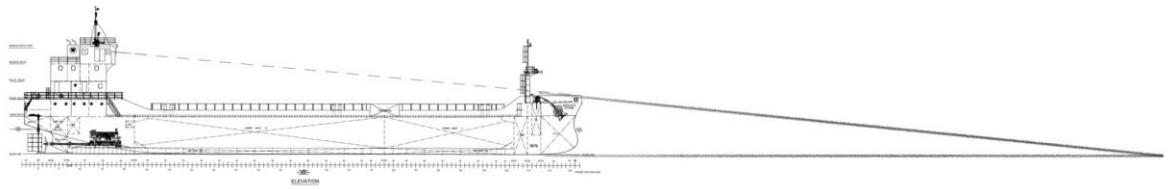


General Arrangement Plan

1712002- Noshin Tarannum

1712043-Rafid Imam

# Visibility Test:



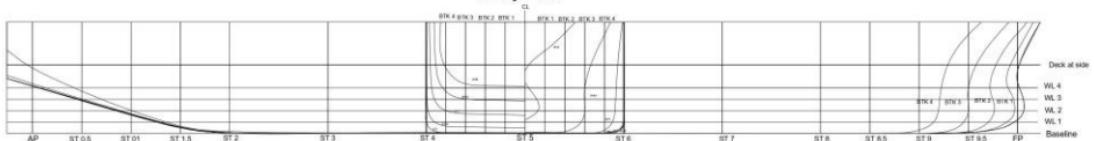
**Note:**  $(2 \times L)$  distance is taken to check if the ship passes the visibility test and it is evident that the ship meets the criteria successfully; where  $L$ = Ship's length.

# **Lines Plan**

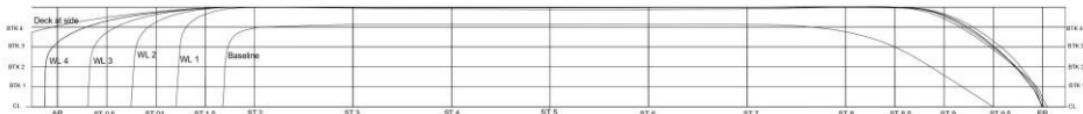
### MAIN PARTICULARS

Length(0A)	81.161 m
Length(WL)	78.955 m
Length(BP)	77.942 m
Breadth(Moulded)	15.728 m
Depth(Moulded)	5.406 m
Draft(Design)	3.588 m
Frame Spacing	650 mm
Service Speed	10 knot
Deadweight	3000 T

Body Plan



Profile Plan



Half Breadth Plan

Lines Plan

1712002- Noshin Tarannum

1712043-Rafid Imam

# **Table of Offset**

**OFFSET TABLE**

Station	Half Breadth						Height Above Base Line						Station
	Baseline	WL - 1	WL - 2	WL - 3	WL - 4	Deck at Side	Keel	BTK - 1	BTK - 2	BTK - 3	Deck	Poop Deck	
<b>0</b>	0	0.0000	0.0000	0.0000	2.5579	6.4200	3.793	3.806	3.826	3.987	5.181	0.000	<b>0</b>
<b>0.5</b>	0	0.0000	0.0000	5.2949	6.6263	7.0855	2.619	2.649	2.680	2.765	3.395	0.000	<b>0.5</b>
<b>1</b>	0	0.0000	6.4510	7.2146	7.4036	7.5062	1.462	1.495	1.529	1.572	1.831	0.000	<b>1</b>
<b>1.5</b>	0	7.2174	7.6930	7.7634	7.7783	7.8011	0.435	0.454	0.473	0.493	0.568	0.000	<b>1.5</b>
<b>2</b>	6.209	7.7965	7.8460	7.8480	7.8480	7.8640	0.03	0.031	0.032	0.032	0.038	0	<b>2</b>
<b>3</b>	6.5	7.8514	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>3</b>
<b>4</b>	6.5	7.8514	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>4</b>
<b>5</b>	6.5	7.8514	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>5</b>
<b>6</b>	6.5	7.8514	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>6</b>
<b>7</b>	6.5	7.8514	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>7</b>
<b>8</b>	5.92	7.8512	7.8640	7.8640	7.8640	7.8640	0	0.000	0.000	0.000	0.001	0	<b>8</b>
<b>8.5</b>	4.72	7.817	7.849	7.851	7.852	7.854	0	0.000	0.000	0.000	0.001	0	<b>8.5</b>
<b>9</b>	2.5	6.9241	7.1250	7.1757	7.2217	7.3322	0	0.000	0.000	0.001	0.251	F Castle	<b>9</b>
<b>9.5</b>	2.48	4.4697	4.7387	4.6910	4.7495	5.2060	0.062	0.065	0.132	2.604	7.913	0.000	<b>9.5</b>
<b>10</b>	0	0.0000	1.0677	0.8461	0.1637	0.5180	4.095	6.534	7.989	0	0.000	0.000	<b>10</b>

# **Hydrostatic Calculation**

Waterplane area, Displacement, LCB VCB calculation for WL - 1												
Water planes		0		1		2		Station Distance	7.7942	WP Distance		1.0075
	SM	5		8		-1		Area products for sectional area	Sectional area below waterline	Volume Function	Levers	Momen ts about amidship
Section	SM	y <sub>0</sub>	y x SM	y <sub>1</sub>	y x SM	y <sub>2</sub>	y x SM					
0	0.5	0	0	0	0	0	0	0	0	0	-5	0
0.5	2	0	0	0	0	0	0	0	0	0	-4.5	0
1	1	0	0	0	0	6.68	6.68	-6.68	-1.12	-1.12	-4	4.49
1.5	2	0	0	7.32	14.63	7.73	15.45	50.81	8.53	17.06	-3.5	-59.72
2	1.5	6.21	9.31	7.84	11.77	7.86	11.79	85.93	14.43	21.64	-3	-64.93
3	4	6.5	26	7.86	31.42	7.86	31.46	87.49	14.69	58.76	-2	-117.52
4	2	6.5	13	7.86	15.71	7.86	15.73	87.49	14.69	29.38	-1	-29.38
5	4	6.5	26	7.86	31.42	7.86	31.46	87.49	14.69	58.76	0	0
6	2	6.5	13	7.86	15.71	7.86	15.73	87.49	14.69	29.38	1	29.38
7	4	6.5	26	7.86	31.42	7.86	31.46	87.49	14.69	58.76	2	117.52
8	1.5	5.92	8.88	7.85	11.78	7.86	11.80	84.55	14.20	21.30	3.00	63.89
8.5	2	4.72	9.44	7.82	15.63	7.85	15.70	78.29	13.15	26.29	3.50	92.02

9	1	2.5	2.50	6.96	6.96	7.14	7.14	61.03	10.25	10.25	4.00	40.99
9.5	2	2.48	4.96	4.52	9.05	4.75	9.51	43.85	7.36	14.72	4.50	66.26
10	0.5	0	0.00	0.00	0.00	1.38	0.69	-1.38	-0.23	-0.12	5.00	-0.58
<b>Different totals</b>		<b>Sum of the area products of WP 0</b>	139.09	<b>Sum of the area products of WP 1</b>	195.52	<b>Sum of the area products of WP 2</b>	204.59	<b>Summation of volume functions</b>		345.07	<b>Summation of moments</b>	142.42
<b>Waterplane area</b>		722.75		1015.93		1063.05						
<b>SM</b>		5		8		-1		<b>VOLUME</b>		<b>896.5168694</b>	<b>LCB</b>	<b>3.22</b>
<b>Volume products</b>		3613.74		8127.43		-1063.05		<b>Summation of volume products</b>	10678.12	<b>VOLUME</b>		<b>896.52</b>
<b>Levers</b>		0.00		1.00		2.00						
<b>Moment about the keel</b>		0.00		8127.43		-2126.11		<b>Summation of moments</b>	6001.32	<b>VCB</b>		<b>0.57</b>

**Waterplane area, Displacement, LCB VCB calculation for WL - 2**

Water planes		0		1		2		Station Distance	7.7942	WP Distance		1.0075
	SM	1		4		1		Area products for sectional area	Sectional area below waterline	Volume Function	Levers	Moments about amidship
Section	SM	y <sub>0</sub>	y x SM	y <sub>1</sub>	y x SM	y <sub>2</sub>	y x SM					
0	0.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-5.00	0.00
1	2.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-4.50	0.00
1	1.0	0.00	0.00	0.00	0.00	6.68	6.68	6.68	4.49	4.49	-4.00	-17.96
2	2.0	0.00	0.00	7.32	14.63	7.73	15.45	36.99	24.85	49.69	-3.50	-173.93
2	1.5	6.21	9.31	7.84	11.77	7.86	11.79	45.45	30.52	45.79	-3.00	-137.36
3	4.0	6.50	26.00	7.86	31.42	7.86	31.46	45.79	30.75	123.02	-2.00	-246.04
4	2.0	6.50	13.00	7.86	15.71	7.86	15.73	45.79	30.75	61.51	-1.00	-61.51
5	4.0	6.50	26.00	7.86	31.42	7.86	31.46	45.79	30.75	123.02	0.00	0.00
6	2.0	6.50	13.00	7.86	15.71	7.86	15.73	45.79	30.75	61.51	1.00	61.51
7	4.0	6.50	26.00	7.86	31.42	7.86	31.46	45.79	30.75	123.02	2.00	246.04
8	1.5	5.92	8.88	7.85	11.78	7.86	11.80	45.19	30.35	45.53	3.00	136.60
9	2.0	4.72	9.44	7.82	15.63	7.85	15.70	43.84	29.44	58.89	3.50	206.10
9	1.0	2.50	2.50	6.96	6.96	7.14	7.14	37.47	25.17	25.17	4.00	100.68

10	2.0	2.48	4.96	4.52	9.05	4.75	9.51	25.33	17.01	34.03	4.50	153.13
10	0.5	0.00	0.00	0.00	0.00	1.38	0.69	1.38	0.93	0.46	5.00	2.32
<b>Different totals</b>	<b>Sum of the area products of WP 0</b>	139.09	<b>Sum of the area products of WP 1</b>	195.52	<b>Sum of the area products of WP 2</b>	204.59	<b>Summation of volume functions</b>		756.12	<b>Summation of moments</b>		269.59
<b>Waterplane area</b>	722.75		1015.93		1063.05							
<b>SM</b>	1		4		1		<b>VOLUME</b>		<b>1964.46</b>	<b>LCB</b>		<b>2.78</b>
<b>Volume products</b>	722.75		4063.71		1063.05		<b>Summation of volume products</b>	5849.52	<b>VOLUME</b>			<b>1964.46</b>
<b>Levers</b>	0		1		2							
<b>Moment about the keel</b>	0		4063.71		2126.11		<b>Summation of moments</b>	6189.82	<b>VCB</b>			<b>1.07</b>

**Waterplane area, Displacement, LCB VCB calculation for WL - 3**

Water planes		0		1		2		3		ST Distance	7.7942	WP Distance		1.0075
	SM	1		3		3		1		Area products for sectional area	Sectional area below waterline	Volume Function	Levers	Moments about amidship
Section	SM	y <sub>0</sub>	y x SM	y <sub>1</sub>	y x SM	y <sub>2</sub>	y x SM	y <sub>3</sub>	y x SM					
0	0.5	0	0	0	0.000	0	0.00	0.00	0.00	0.00	0.00	0.00	-5	0.00
0.5	2	0	0	0	0.000	0	0.00	5.85	11.71	5.85	4.42	8.85	-4.5	-39.82
1	1	0	0	0	0.000	6.68	6.68	7.29	7.29	27.34	20.66	20.66	-4	-82.64
1.5	2	0	0	7.32	14.63	7.73	15.45	7.77	15.55	52.90	39.97	79.95	-3.5	-279.82
2	1.5	6.21	9.31	7.84	11.77	7.86	11.79	7.86	11.80	61.19	46.24	69.36	-3	-208.07
3	4	6.50	26.00	7.86	31.42	7.86	31.46	7.86	31.46	61.52	46.49	185.96	-2	-371.92
4	2	6.50	13.00	7.86	15.71	7.86	15.73	7.86	15.73	61.52	46.49	92.98	-1	-92.98
5	4	6.50	26.00	7.86	31.42	7.86	31.46	7.86	31.46	61.52	46.49	185.96	0	0.00
6	2	6.50	13.00	7.86	15.71	7.86	15.73	7.86	15.73	61.52	46.49	92.98	1	92.98
7	4	6.50	26.00	7.86	31.42	7.86	31.46	7.86	31.46	61.52	46.49	185.96	2	371.92
8	1.5	5.92	8.88	7.85	11.78	7.86	11.80	7.86	11.80	60.93	46.04	69.06	3	207.19
8.5	2	4.72	9.44	7.82	15.63	7.85	15.70	7.85	15.70	59.57	45.01	90.02	3.5	315.09
9	1	2.50	2.50	6.96	6.96	7.14	7.14	7.19	7.19	51.98	39.27	39.27	4	157.10

9.5	2	2.48	4.96	4.52	9.05	4.75	9.51	4.70	9.39	35.01	26.45	52.91	4.5	238.08
10	0.5	0.00	0.00	0	0.00	1.38	0.69	1.02	0.51	5.17	3.91	1.95	5	9.77
Different totals		<b>Sum of the area products of WP 0</b>	139.09	<b>Sum of the area products of WP 1</b>	195.52	<b>Sum of the area products of WP 2</b>	204.59	<b>Sum of the area products of WP 3</b>	216.75	<b>Summation of volume functions</b>	1175.87	<b>Summation of moments</b>		316.88
Waterplane area		722.75		1015.93		1063.05		1126.26						
SM		1.00		3.00		3.00		1.00		<b>VOLUME</b>	<b>3054.98</b>	<b>LCB</b>		<b>2.10</b>
Volume products		722.75		3047.79		3189.16		1126.26		<b>Summation of volume products</b>	8085.96	<b>VOLUME</b>		<b>3054.98</b>
Levers		0		1		2		3						
Moment about the keel		0.00		3047.79		6378.32		3378.79		<b>Summation of moments</b>	12804.90	<b>VCB</b>		<b>1.60</b>

Waterplane area, Displacement, LCB VCB calculation for WL - 4																
Water planes		0		1		2		3		4		Distance	7.79	WP Distance		1.01
Section	S M	1		4		2		4		1		Area products for sectional area	Sectional area below waterline	Volume Function	Levers	Moments about amidships
		$y_0$	$y \times SM$	$y_1$	$y \times SM$	$y_2$	$y \times SM$	$y_3$	$y \times SM$	$y_4$	$y \times SM$					
0	0.5	0	0	0	0.0	0.0	0.0	0.00	0.00	5.05	2.52	5.05	3.39	1.69	-5	-8.47
0.5	2	0	0	0	0.0	0.0	0.0	5.85	11.71	6.78	13.56	30.20	20.28	40.57	-4.5	-182.56
1	1	0	0	0	0.0	6.68	6.68	7.29	7.29	7.43	7.43	49.95	33.55	33.55	-4	-134.19
1.5	2	0	0	7.32	14.63	7.73	15.45	7.77	15.55	7.79	15.58	83.60	56.15	112.31	-3.5	-393.07
2	1.50	6.21	9.31	7.84	11.77	7.86	11.79	7.86	11.80	7.86	11.80	92.63	62.22	93.32	-3	-279.97
3	4	6.5	26	7.86	31.42	7.86	31.46	7.86	31.46	7.86	31.46	92.97	62.45	249.79	-2	-499.57

4	2	6.5	13	7.86	15.71	7.86	15.73	7.86	15.73	7.86	15.73	92. 97	62. 45	124.89	-1	-124.89
5	4	6.5	26	7.86	31.42	7.86	31.46	7.86	31.46	7.86	31.46	92. 97	62. 45	249.79	0	0.00
6	2	6.5	13	7.86	15.71	7.86	15.73	7.86	15.73	7.86	15.73	92. 97	62. 45	124.89	1	124.89
7	4	6.5	26	7.86	31.42	7.86	31.46	7.86	31.46	7.86	31.46	92. 97	62. 45	249.79	2	499.57
8	1.5	5.92	8.88	7.85	11.78	7.86	11.80	7.86	11.80	7.86	11.80	92. 38	62. 05	93.07	3	279.21
8.5	2	4.72	9.44	7.82	15.63	7.85	15.70	7.85	15.70	7.85	15.70	90. 94	61. 08	122.17	3.5	427.58
9	1	2.5	2.5	6.96	6.96	7.14	7.14	7.19	7.19	7.24	7.24	80. 60	54. 14	54.14	4	216.54
9.5	2	2.48	4.96	4.52	9.05	4.75	9.51	4.70	9.39	4.81	9.62	53. 68	36. 05	72.11	4.5	324.49
10	0.5	0	0	0.00	0.00	1.38	0.69	1.02	0.51	0.00	0.00	6.8 4	4.6 0	2.30	5	11.49
<b>Different totals</b>		<b>Sum of the area products of WP 0</b>	139.0 9	<b>Sum of the area products of WP 1</b>	195.5 2	<b>Sum of the area products of WP 2</b>	204.5 9	<b>Sum of the area products of WP 3</b>	216.7 5	<b>Sum of the area products of WP 4</b>	221.0 8	<b>Summation of volume functions</b>	1624.37	<b>Summation of moments</b>	261.04	

<b>Waterplane area</b>	722.75	1015.93	1063.05	1126.26	1148.76					
<b>SM</b>	1	4	2	4	1	<b>VOLUME</b>	<b>4220.21</b>	<b>LCB</b>	<b>1.25</b>	
<b>Volume products</b>	722.75	4063.71	2126.11	4505.06	1148.76	<b>Summation of volume products</b>	12566.39	<b>VOLUME</b>		<b>4220.21</b>
<b>Levers</b>	0.00	1.00	2.00	3.00	4.00					
<b>Moment about the keel</b>	0.00	4063.71	4252.21	13515.18	4595.04	<b>Summation of moments</b>	26426.14	<b>VCB</b>		<b>2.12</b>

### Transverse Metacentric Height:

<b>BM<sub>T</sub> calculation</b>													
<b>Section</b>	<b>SM</b>	<b>Section Distance</b>			7.7942			<b>Density of fresh water ( t/m<sup>3</sup> )</b>			1		
		<b>1</b>			<b>2</b>			<b>3</b>			<b>4</b>		
		<b>y<sub>1</sub></b>	<b>y<sup>3</sup></b>	<b>y<sup>3</sup> · SM</b>	<b>y<sub>2</sub></b>	<b>y<sup>3</sup></b>	<b>y<sup>3</sup> · SM</b>	<b>y<sub>3</sub></b>	<b>y<sup>3</sup></b>	<b>y<sup>3</sup> · SM</b>	<b>y<sub>4</sub></b>	<b>y<sup>3</sup></b>	<b>y<sup>3</sup> · SM</b>
0	0.5	0	0	0	0	0	0	0	0	0	5.05	128.54	64.27
0.5	2	0	0	0	0	0	0	5.85	200.69	401.38	6.78	311.90	623.81
1	1	0.00	0.00	0.00	6.68	298.67	298.67	7.29	386.94	386.94	7.43	410.42	410.42
1.5	2	7.32	391.66	783.31	7.73	461.24	922.48	7.77	469.74	939.49	7.79	472.78	945.56
2	1.5	7.84	482.51	723.76	7.86	486.15	729.22	7.86	486.33	729.49	7.86	486.33	729.49
3	4	7.86	484.87	1939.49	7.86	486.33	1945.32	7.86	486.33	1945.32	7.86	486.33	1945.32
4	2	7.86	484.87	969.74	7.86	486.33	972.66	7.86	486.33	972.66	7.86	486.33	972.66
5	4	7.86	484.87	1939.49	7.86	486.33	1945.32	7.86	486.33	1945.32	7.86	486.33	1945.32
6	2	7.86	484.87	969.74	7.86	486.33	972.66	7.86	486.33	972.66	7.86	486.33	972.66
7	4	7.86	484.87	1939.49	7.86	486.33	1945.32	7.86	486.33	1945.32	7.86	486.33	1945.32
8	1.5	7.85	484.14	726.22	7.86	486.33	729.49	7.86	486.33	729.49	7.86	486.33	729.49
8.5	2	7.82	477.63	955.26	7.85	483.60	967.20	7.85	483.96	967.92	7.85	484.14	968.29

9	1	6.96	336.96	336.96	7.14	363.62	363.62	7.19	371.34	371.34	7.24	379.32	379.32
9.5	2	4.52	92.64	185.27	4.75	107.36	214.72	4.70	103.54	207.09	4.81	111.34	222.68
10	0.5	0.00	0.00	0.00	1.38	2.65	1.33	1.02	1.06	0.53	0.00	0.00	0.00
<b>TOTALS</b>				11468.73			12008.00			12514.94			12854.59
<b>Waterplane</b>		<b>1</b>			<b>2</b>			<b>3</b>			<b>4</b>		
<b>Volume</b>		896.52			1964.46			3054.98			4220.21		
<b><math>\Delta</math></b>		896.52			1964.46			3054.98			4220.21		
<b>Moment of Inertia, I</b>		19864.35			<b>20798.40</b>			21676.44			22264.73		
<b>Transverse metacentric height, <math>BM_T</math></b>		22.16			10.59			7.10			5.28		

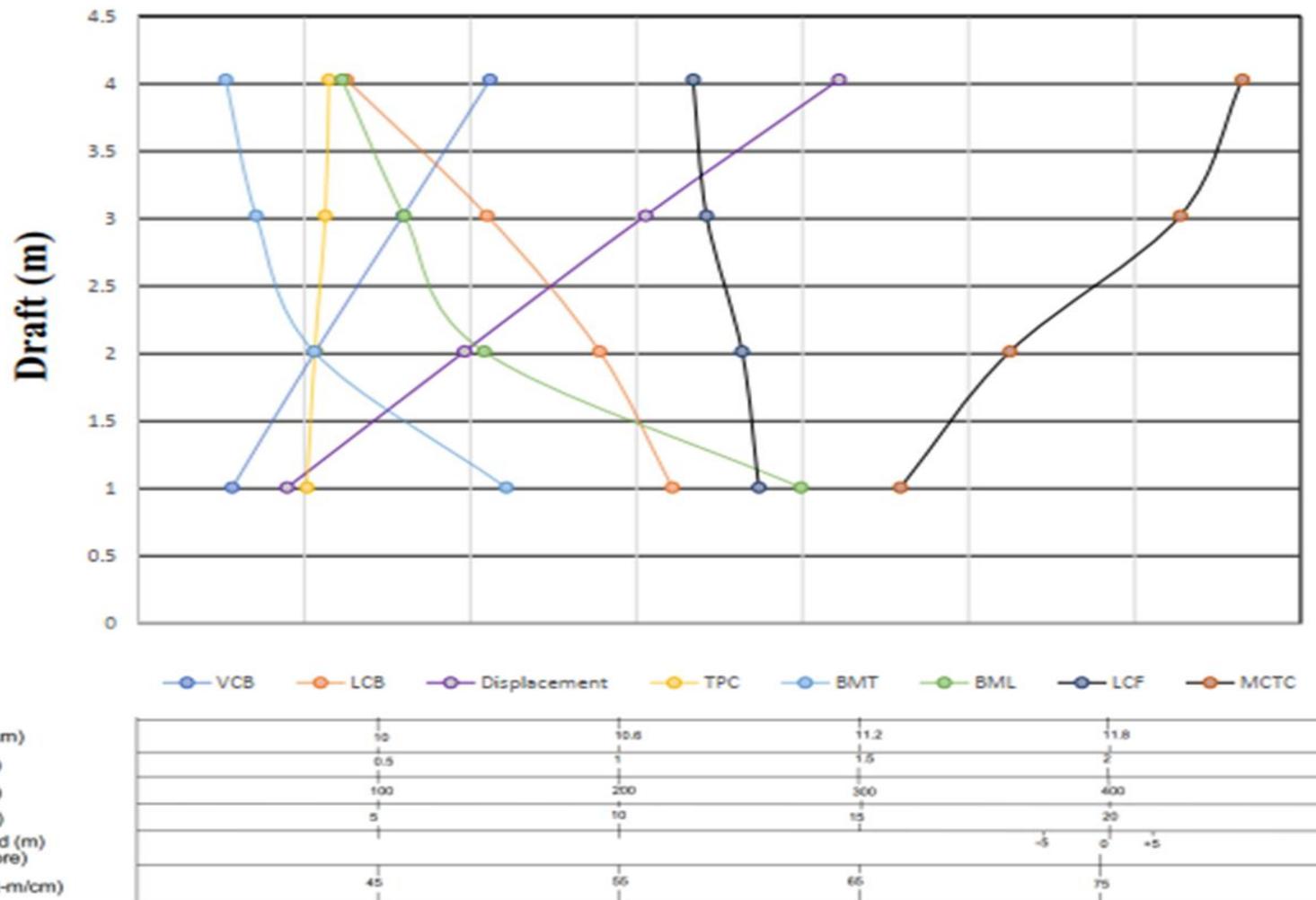
## Longitudinal Metacentric Height:

LCF and $B_{ML}$ calculation																			
Section	S M	Section Distance				7.7942		Length				77.942		Density of fresh water (t/m <sup>3</sup> )				1	
		Lever s from	1			2			3			4							
		amids ips (x)	y <sub>1</sub>	y · SM	(y · SM) x	(y · SM) x <sup>2</sup>	y <sub>2</sub>	y · SM	(y · SM) x	(y · SM) x <sup>2</sup>	y <sub>3</sub>	y · SM	(y · SM) x	(y · SM) x <sup>2</sup>	y <sub>4</sub>	y · SM	(y · SM) x	(y · SM) x <sup>2</sup>	
0	0. 5	-5	0	0	0	0	0	0	0	0	0	0	0	0	5.05	2.52	- 12.62	63.08	
0.5	2	-4.5	0	0	0	0	0	0	0	0	5.85	11.7 1	- 52.69	237.12	6.78	13.56	- 61.04	274.66	
1	1	-4	0.00	0.00	0.00	0.00	6.68	6.68	- 26.74	106.9 5	7.29	7.29	- 29.15	116.59	7.43	7.43	- 29.73	118.90	
1.5	2	-3.5	7.32	14.63	-51.22	179.25	7.73	15.45	- 54.08	189.3 0	7.77	15.5 5	- 54.41	190.45	7.79	15.58	- 54.53	190.86	
2	1. 5	-3	7.84	11.77	-35.30	105.89	7.86	11.79	- 35.38	106.1 5	7.86	11.8 0	- 35.39	106.16	7.86	11.80	- 35.39	106.16	
3	4	-2	7.86	31.42	-62.85	125.70	7.86	31.46	- 62.91	125.8 2	7.86	31.4 6	- 62.91	125.82	7.86	31.46	- 62.91	125.82	
4	2	-1	7.86	15.71	-15.71	15.71	7.86	15.73	- 15.73	15.73	7.86	15.7 3	- 15.73	15.73	7.86	15.73	- 15.73	15.73	

5	4	0	7.86	31.42	0.00	0.00	7.86	31.46	0.00	0.00	7.86	31.4 6	0.00	0.00	7.86	31.46	0.00	0.00
6	2	1	7.86	15.71	15.71	15.71	7.86	15.73	15.73	15.73	7.86	15.7 3	15.73	15.73	7.86	15.73	15.73	15.73
7	4	2	7.86	31.42	62.85	125.70	7.86	31.46	62.91	125.8 2	7.86	31.4 6	62.91	125.82	7.86	31.46	62.91	125.82
8	1. 5	3	7.85	11.78	35.33	106.00	7.86	11.80	35.39	106.1 6	7.86	11.8 0	35.39	106.16	7.86	11.80	35.39	106.16
8.5	2	3.5	7.82	15.63	54.72	191.51	7.85	15.70	54.94	192.3 1	7.85	15.7 0	54.96	192.35	7.85	15.70	54.97	192.38
9	1	4	6.96	6.96	27.83	111.34	7.14	7.14	28.55	114.2 0	7.19	7.19	28.75	115.00	7.24	7.24	28.96	115.82
9.5	2	4.5	4.52	9.05	40.72	183.25	4.75	9.51	42.78	192.4 9	4.70	9.39	42.26	190.18	4.81	9.62	43.30	194.84
10	0. 5	5	0	0	0	0	1.38	0.69	3.46	17.30	1.02	0.51	2.55	12.73	0	0	0	0
<b>TOTALS</b>				195.5 2	72.10	1160.0 7		204.5 9	48.91	1307. 96		216. 75	-7.74	1549.8 6		221.0 8	- 30.69	1645.98
				<b>1</b>			<b>2</b>			<b>3</b>			<b>4</b>					
<b>Volume</b>			<b>896.52</b>			<b>1964.46</b>			<b>3054.98</b>			<b>4220.21</b>						
<b>Water plane Area</b>			<b>1015.93</b>			<b>1063.05</b>			<b>1126.26</b>			<b>1148.76</b>						
<b>TPC</b>			<b>10.16</b>			<b>10.63</b>			<b>11.26</b>			<b>11.49</b>						

<b>LCF from Amidship</b>	<b>2.87</b>	<b>1.86</b>	<b>-0.28</b>	<b>-1.08</b>
<b>LCF from Aft</b>	<b>37.37</b>	<b>36.36</b>	<b>34.22</b>	<b>33.42</b>
<b>Moment of inertia about the amidship</b>	<b>366190.07</b>	<b>412875.11</b>	<b>489233.34</b>	<b>519574.14</b>
<b>Moment of inertia about the LCF</b>	<b>357797.28</b>	<b>409183.72</b>	<b>489146.14</b>	<b>518229.11</b>
<b>Longitudinal Metacenter BM<sub>L</sub></b>	<b>399.10</b>	<b>208.29</b>	<b>160.11</b>	<b>122.80</b>
<b>Δ</b>	<b>896.52</b>	<b>1964.46</b>	<b>3054.98</b>	<b>4220.21</b>
<b>MCT 1 cm</b>	<b>45.91</b>	<b>52.50</b>	<b>62.76</b>	<b>66.49</b>

# Hydrostatic Curve



# **Scantling Calculation**

## **(IRS Inland Rules 2021)**

# Scantling Calculation: Thickness of Plates

Deadweight	3000	tonnes
Speed	10	knots
L	77.942	m
B	15.728	m
D	5.406	m
T	4.030	m
Displacement	4243.9031	tonnes
C <sub>b</sub>	0.859	

## IRS inland rules: Section 1.2; Chapter 2

Material Factor, K = 1

Minimum Yield stress = 235 N/mm<sup>2</sup>

Range for Tensile Strength = 400-490 N/mm<sup>2</sup>

Taken, Tensile Strength = 450 N/mm<sup>2</sup>

## IRS inland rules: Section 1.4; Chapter 2

Plate thickness, ts = 20 mm

Frame Spacing = 650 mm

## IRS inland rules: Section 2.1; Chapter 3

### Corrosion Addition

T<sub>c</sub> = 2 mm

## **IRS inland rules: Section 3.1 ; Chapter 6**

### **Design Load**

At Bottom Shell

$$\begin{aligned} T_1 &= T+1 \quad [ L > 60m ] \\ &= 4.030+1 \\ &= 5.030 \text{ m} \end{aligned}$$

Load,  $P = 10 T_1$

$$\begin{aligned} &= 10 * 5.030 \\ &= 50.303 \text{ KN/m}^2 \end{aligned}$$

At inner bottom

$H$  = height [m], to deck or top of hatchway coaming

$$= 5.406 \text{ m}$$

Load,  $P = 12.5 * \rho * H$

$$\begin{aligned} &= 12.5 * 0.7 * 5.406 \\ &= 47.306 \text{ t/m}^2 \end{aligned}$$

## **IRS inland rules: Section 2.1; Chapter 5**

### **Bar Keel**

Depth =  $75 + 0.75 L$

$$\begin{aligned} &= 75 + (0.75 * 77.942) \\ &= 133.46 \text{ mm} \end{aligned}$$

Thickness =  $10 + 0.4 L$

$$= 10 + (0.4 * 77.942) \\ = 41.18 \text{ mm}$$

### **IRS inland rules: Section 3.1; Chapter 5**

#### **Stem**

Cross Sectional Area =  $0.6L$

$$= 0.6 * 77.942 \\ = 46.77 \text{ cm}^2$$

Thickness =  $(0.08 L + 5.0)$

$$= (0.08 * 77.942) + 5.0 \\ = 11.24 \text{ mm}$$

### **IRS inland rules: Section 4.1; Chapter 6**

#### **Bottom Structure**

##### **Double Bottom calculations**

$$\text{Bottom Plate Thickness} = (4 + 0.04L) + tc \\ = (4 + 0.04 * 77.942) + 2 \\ = 9.118 \text{ mm}$$

Width of Keel Plate =  $400 + 10 * L$

$$= 400 + (10 * 77.942) \\ = 1179.421 \text{ mm}$$

$$\text{Keel Plate Thickness} = \text{Bottom Plate Thickness} + 1 \\ = 9.118 + 1 \\ = 10.118 \text{ mm}$$

Inner Bottom Thickness =  $(4 + 0.03 * L) + 2$

$$\begin{aligned}
 &= (4+0.03*77.942)+2 \\
 &= 8.338 \text{ mm}
 \end{aligned}$$

### **IRS inland rules: Section 6.1 ; Chapter 6**

Depth of the center Girder,  $d = 250 + 20B + 50T$

$$\begin{aligned}
 &= 250 + (20*15.728) + (50*4.030) \\
 &= 766.069 \text{ mm}
 \end{aligned}$$

Minimum thickness of bottom girder,  $t = (0.007d + 3)$

$$\begin{aligned}
 &= (0.007*766.069) + 3 \\
 &= 8.362 \text{ mm}
 \end{aligned}$$

Minimum thickness of floors  $t = (0.007d + 3)$

$$\begin{aligned}
 &= (0.007*766.069) + 3 \\
 &= 8.362 \text{ mm}
 \end{aligned}$$

### **IRS inland rules: Section 4.1; Chapter 7**

#### **Side Shell Plating and Stiffeners**

$$\begin{aligned}
 \text{Minimum Side shell plating, } t &= (4 + 0.04L) + tc \\
 &= (4+0.04*77.942) + 2 \\
 &= 9.118 \text{ mm}
 \end{aligned}$$

Minimum Breadth of sheer strake = 100 D

$$\begin{aligned}
 &= 100 * 5.406 \\
 &= 540.643 \text{ mm}
 \end{aligned}$$

**IRS inland rules: Section 3.1; Chapter 8**  
**Deck Structure**

$$\begin{aligned} h_o &= D - T \\ &= 5.406 - 4.030 \\ &= 1.376 \end{aligned}$$

$$H_1 = 15$$

Pressure on exposed decks,  $= H_1 - 10 h_o$

$$\begin{aligned} &= 15 - (10 * 1.376) \\ &= 1.238 \text{ kN/mm}^2 \end{aligned}$$

For strength and forecastle deck,

$$t_o = 5$$

$$\begin{aligned} \text{Minimum Thickness of Deck Plating } t &= (t_o + 0.02L) \sqrt{k} + t_c \\ &= (5 + 0.02 * 77.942) + 2 \\ &= 8.559 \text{ mm} \end{aligned}$$

For other decks,

$$t_o = 4$$

$$\begin{aligned} \text{Minimum Thickness of Deck Plating } t &= (t_o + 0.02L) \sqrt{k} + t_c \\ &= (4 + 0.02 * 77.942) + 2 \\ &= 7.559 \text{ mm} \end{aligned}$$

## **IRS inland rules: Section 5.1.2; Chapter 9**

### **Bulkheads**

$$\text{Minimum bulkhead thickness} = t = (4.0 + 0.01L) + tc$$

$$= (4+0.01*77.942)+2$$

$$= 6.779 \text{ mm}$$

$$\text{Design Pressure , } p = 10 \text{ h}$$

$$= 10*(D/2)$$

$$= 10*(5.406/2)$$

$$= 27.032 \text{ KN/m}^2$$

$$\begin{aligned}\text{Bulkhead Thickness (watertight bulkhead) , } t &= 15.8s \sqrt{p/\sigma} \times 0.001 + tc \\ &= 15.8*650*((27.032 /220)^{0.5})*0.001 + 2 \\ &= 5.600 \text{ mm or 7 mm} \\ &= 7\text{mm, is taken}\end{aligned}$$

$$\begin{aligned}\text{Bulkhead thickness ( tank and collision bulkhead) , } t &= 15.8s \sqrt{p/\sigma} \times 0.001 + tc \\ &= 15.8*650*(27.032 \\ /160)^{(1/2)}*0.001 + 2 \\ &= 6.221 \text{ mm or 7 mm} \\ &= 7\text{mm, is taken}\end{aligned}$$

## **IRS inland rules: Section 4.3.1 & 2.1.1; Chapter 10**

### **Superstructures, Deckhouses and Bulwarks**

$$\text{Bulwark Thickness} = 6 \text{ mm}$$

$$\text{Lower tier Thickness , } t = (0.004 s + 2.5) \sqrt{k}$$

$$=(0.004*650)+2.5$$

$$=5.1 \text{ mm}$$

$$\begin{aligned}
 \text{Upper tier thickness } t &= (0.004 s + 1.5) \sqrt{k} \\
 &= (0.004 * 650) + 1.5 \\
 &= 4.1 \text{ mm}
 \end{aligned}$$

IRS inland rules: Section 2.3.1& 3.3.1; Chapter 11  
Hatch

### **Hatch coaming thickness**

At strength and forecastle deck = Minimum Thickness of Deck Plating at strength and forecastle deck

$$\begin{aligned}
 &= (t_o + 0.02L) \sqrt{k} + t_c \\
 &= (5 + 0.02 * 77.942) + 2 \\
 &= 8.559 \text{ mm}
 \end{aligned}$$

Others = Minimum Thickness of Deck Plating at other decks t

$$\begin{aligned}
 &= (t_o + 0.02L) \sqrt{k} + t_c \\
 &= (4 + 0.02 * 77.942) + 2 \\
 &= 7.559 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{Hatch Cover thickness} &= 15.8s \sqrt{p/\sigma} \times 0.001 + t_c \\
 &= 15.8 * M17 * ((D99/G5)^{(1/2)}) * 0.001 + D12 \\
 &= 8.124 \text{ mm}
 \end{aligned}$$

Design pressure = 160/k

$$\begin{aligned}
 &= 160/1 \\
 &= 160 \text{ N/mm}^2
 \end{aligned}$$

## **IRS inland rules: Section 2.2 ; Chapter 10**

### **Machinery Thickness**

Minimum Machinery casing thickness =  $(0.003 s + 1.5) \sqrt{k}$

$$= (0.003 * 650) + 1.5$$

$$= 3.45 \text{ mm}$$

Minimum Exposed Machinery casing = 20% of Minimum Machinery casing thickness

$$= 3.45 + 3.45 * 20\%$$

$$= 4.14 \text{ mm}$$

IRS rules for bulk cargo carriers

Part 1 Chapter 6 Section 3.1.1

### **Machinery Thickness**

Double bottom centreline girder = Machinery space

$$= 1.55(L_2)^{1/3} + 3.5$$

$$= 1.55 * (77.946^{(1/3)}) + 3.5$$

$$= 10.121 \text{ mm}$$

Other bottom Girder = Machinery space =  $1.7 (L_2)^{1/3} + 1.0$

$$= 1.7 * (77.946^{(1/3)}) + 1$$

$$= 8.262 \text{ mm}$$

Bottom Floor = Machinery space =  $1.7 (L_2)^{1/3} + 1.0$

$$= 1.7 * (77.946^{(1/3)}) + 1$$

$$= 8.262 \text{ mm}$$

# Scantling Calculation: Section Modulus Of Structural Members

Deadweight	3000	tonnes
Speed	10	knots
L	77.94209643	m
B	15.72780697	m
D	5.406433647	m
T	4.030250537	m
Displacement	4243.903125	tonnes
C <sub>b</sub>	0.859	

## Bottom Structures

**Bottom Frames and Reverse  
Frames**

[Pt -3, CH -6,Sec-6.3.4]

$$Z = \frac{sp lk^2}{1.6} \times 10^{-3} + Z_c \text{ cm}^3$$

Design Pressure      p=10T1=50.30250537 kN/m<sup>2</sup>

T1=T+1=5.030250537 m

Spacing of Stiffeners    s=      650      mm

Span of Stiffeners      l=      1.75      m

Material Factor      k=      1

Section Modulus      Z=      62.58339047 cm<sup>3</sup>

**T-300×150×10**

## **Side Structures:**

$$\text{Design Pressure , } \pi=10 \text{ (hs +1) [kN/m}^2\text{]} \quad 10h_0 + \left(15 - 5 \frac{h_0}{T}\right) \text{ for } L \geq 60$$

vertical distance [m], from the maximum load waterline to the loadpoint.  $h_0=1.6 \text{ m}$

External Pressure ,  $p= 29.01501174 \text{ kN/m}^2$

### **Internal Tank Pressure**

The vertical distance [m] from the load point to the top of tank , $h_s = 0.4 \text{ m}$

Internal Tank Pressure, $P= 14 \text{ kN/m}^2$

### **Main Frames [Pt 3, CH 7, Sec-4 ,4.3.1]**

Spacing of Stiffeners  $s= 650 \text{ mm}$

Span Of stiffeners  $l= 2.6 \text{ m}$

Material factor $k= 1$

$$Z = \frac{sp lk^2}{2400} \times 10^{-3} + Z_c \text{ cm}^3$$

Section Modulus,  $Z= 48.55665162 \text{ cm}^3$

**L-130×130×12**

<b>Main Frame Brackets</b>	<b>Upper Bracket</b>	<b>70 l</b>	<b>182</b>	<b>mm</b>
	<b>Lower Bracket</b>	<b>120 l</b>	<b>312</b>	<b>mm</b>

**Side Stringers [Pt 3, CH 7, Sec-5 ,5.1.5]**

h0=1.6

Design Pressure p= 29.01501174 kN/m<sup>2</sup>

Spacing of Girders b= 2.6 m

Span of Girders S= 2.6 m

Material Factor k= 1

Allowable stress σ= 160 N/mm<sup>2</sup>

Constant m= 12

$$Z = \frac{bps^2}{m\sigma} \times 10^3 + Z_c \text{ cm}^3$$

Section Modulus ,Z= 265.6082533 cm<sup>3</sup>

**T-350×175×13**

**Side Web Frames [Pt 3, CH 7, Sec-5 ,5.1.5]**

h0 =1.6 m

Design Pressure p= 29.01501174 kN/m<sup>2</sup>

Spacing of Girders b= 2.6 m

Span of Girders S= 2.6 m

Material Factor k= 1

Allowable stress σ= 160 N/mm<sup>2</sup>

Constant m= 12

$$Z = \frac{bpS^2}{m\sigma} \times 10^3 + Z_c \text{ cm}^3$$

Section Modulus, Z=265.6082533  $\text{cm}^3$

**T-350x175x13**

## Deck Structure

### Design Load

Vertical distance [m], from the maximum load waterline to the deck,  $h_0=1.37618311 \text{ m}$

$H_1=15$

Weather Deck Design Load  $p=H_1-10h_0=5 \text{ kN/m}^2$

Accommodation Decks Design Load  $p=4.5 \text{ kN/m}^2$

### Transverse Deck Beams [Pt 3, CH-8, Sec 4, 4.2.2]

Weather Deck

Spacing Of stiffeners  $s=650 \text{ mm}$

Span of stiffeners  $l=1.75 \text{ m}$

$$Z = \frac{sp l^2}{1600} \times 10^3 + Z_c \text{ cm}^3$$

Section Modulus  $Z=6.220703125 \text{ cm}^3$

## **T-62.5×6.5 and 125×9**

### **Accommodation Deck**

Section Modulus ,Z= 5.598632813 cm<sup>3</sup>

## **T-62.5×6.5 and 125×9**

### **Deck Girders [Pt 3 , CH 8 , Sec 5 , 5.1.3]**

Spacing of Girders b= 2.6 m

Span of Girders S= 2.6 m

Constant m= 12

Material Factor k= 1

Allowable stress σ= 160 N/mm<sup>2</sup>

$$Z = \frac{bps^2}{m\sigma} \times 10^3 + Z_c \text{ cm}^3$$

$$Z = 45.77083333 \text{ cm}^3$$

## **T-150×8 and 200×12**

### **Bulkheads**

The vertical distance [m] from the loadpoint

to the uppermost continuous deck. h= 2.305 m

Ordinary Water Tight Bulkhead Loads p= 23.05 kN/m<sup>2</sup>

Stiffener Spacing s= 650 mm

Span of Stiffeners      l=      1.75      m  
 Constant                  m=      10  
 Allowable Stress        σ=      160      N/mm<sup>2</sup>  
 Material Factor        k=      1

**Bulkhead Stiffener [Pt -3, CH-9, Sec-5, 5.3.1]**

$$Z = \frac{sp l^2}{m\sigma} \times 10^3 + Z_c \text{ cm}^3$$

Section Modulus      Z=      28.67744141      cm<sup>3</sup>

**L-100×100×12**

**Bulkhead Girder [Pt -3, CH-9, Sec-6, 6.1.2]**

Spacing of Girders      b=      2.6      m  
 Span of Girders        S=      2.6      m  
 Constant                  m=      12  
 Material Factor        k=      1  
 Allowable stress       σ=      210      N/mm<sup>2</sup>

$$Z = \frac{bps^2}{m\sigma} \times 10^3 + Z_c \text{ cm}^3$$

Section Modulus      Z=      160.7646032      cm<sup>3</sup>

**L-200×200×14**

**Superstructure [PT-3, CH-10, SEC-2 ,2.1.2]**

The section modulus Z of stiffeners on fronts, sides and aft ends of deck houses and the front and aft ends of superstructures is not to be less than:

$$z = 3.6sl^2 \times 10^{-3} . k \text{ cm}^3$$

Spacing of Stiffeners s= 650 mm

Span of stiffeners l= 2 m

Material Factor k= 1

Section Modulus Z= 9.36 cm<sup>3</sup>

**L-80×80×8**

### **Hatch Cover**

Stiffeners and Girders [Pt 3, Ch-11, Sec 3,3.4.1]

Design Load p= 3 kN/m<sup>2</sup>

Member spacing s= 2.14 m

Member Span l= 2.14 m

Constant m= 12

$$Z = \frac{6.25sp l^2}{m} \text{ cm}^3$$

Section Modulus Z= 15.3130375 cm<sup>3</sup>

**T-150×9 , 100×6**

# Scantling Calculation Summary

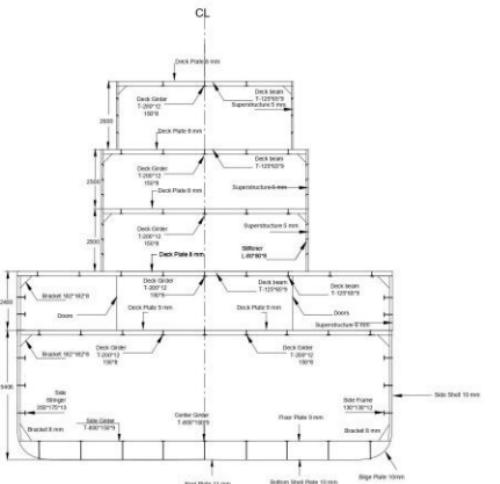
PLATE	THICKNESS
Bottom Plate Thickness	<b>10 mm</b>
Keel Plate Thickness	<b>11 mm</b>
Inner Bottom Thickness	<b>9 mm</b>
Floor Thickness	<b>9 mm</b>
Side Shell Plating	<b>10 mm</b>
Deck Plating ( Strength and Forecastle Deck)	<b>9 mm</b>
Deck plating ( Other Deck)	<b>8 mm</b>
Bulkhead Thickness ( Watertight Bulkhead)	<b>6 mm</b>
Bulkhead Thickness (Tank and Collision Bulkhead)	<b>7 mm</b>
Bulwark Thickness	<b>6 mm</b>
Superstructure Thickness (Upper tier)	<b>5 mm</b>
Superstructure Thickness Lower Tier)	<b>6 mm</b>
Hatch Coaming Thickness ( Strength and Forecastle deck)	<b>9 mm</b>
Hatch Coaming Thickness ( Others )	<b>8 mm</b>
Hatch Cover Thickness	<b>9 mm</b>
Machinery Casing Thickness	<b>4 mm</b>
Machinery Casing ( Bottom floor )	<b>9 mm</b>
Sheerstrake Thickness	<b>11 mm</b>
Bilge Plate Thickness	<b>10 mm</b>

<b>STRUCTURAL MEMBERS</b>	
Center Girder	<b>T-800×150×9</b>
Side Girder	<b>T-800×150×9</b>
Floor	<b>T-800×150×9</b>
Side Web Frame	<b>T-350×175×13</b>
Side Frame	<b>L-130×130×12</b>
Side Stringers	<b>T-350×175×13</b>
Deck Girders	<b>T-200×12, 150×8</b>
Deck Web beam	<b>T-125×65×9</b>
Bulkhead Stiffeners	<b>L-100×100×12</b>
Bulkhead Girders	<b>L-200×200×14</b>
Superstructure Stiffeners	<b>L-80×80×8</b>
Girder(Machinery Space)	<b>T-800×150×9</b>
Web Frame(Machinery Space)	<b>T-350×175×13</b>
Hatch Cover Stiffeners and Girders	<b>T-150×9, 100×6</b>

# **Midship Section**

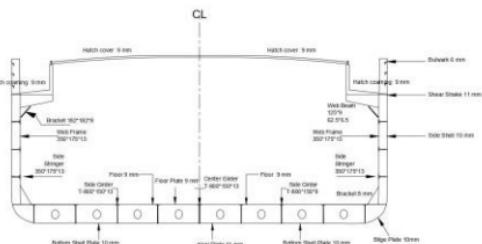
## MAIN PARTICULARS

Length(0A)	81,161 m
Length(WL)	78,955 m
Length(BP)	77,942 m
Breadth(Moulded)	15,728 m
Depth(Moulded)	5,406 m
Draft(Design)	3,588 m
Frame Spacing	650 mm
Service Speed	10 knot
Deadweight	3000 T



FRAME NO- 16

## MIDSHIP SECTION



FRAME NO- 45 (Web)

## MIDSHIP SECTION

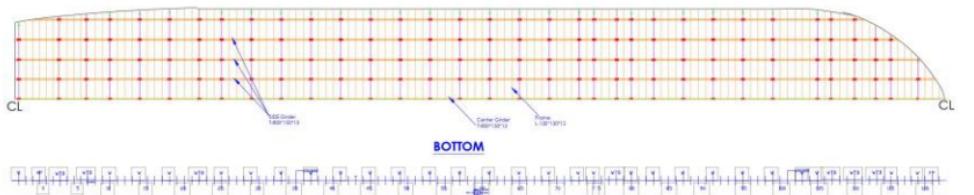
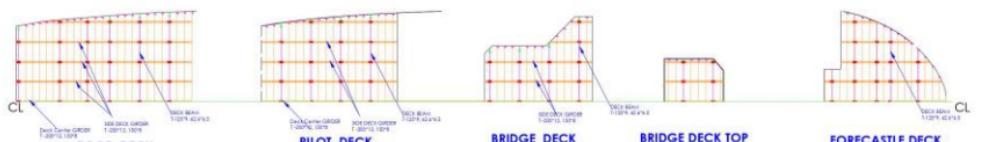
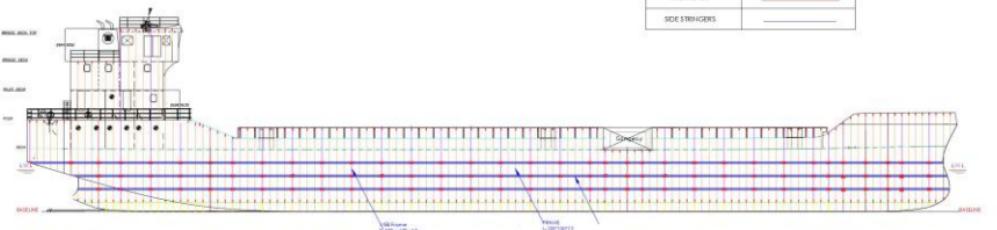
MIDSHIP SECTION	
Student ID	Name
<u>1712002</u>	Noshin Tarannum
<u>1712043</u>	Rafid Imam

# **Longitudinal Construction**

## MAIN PARTICULARS

Length(0A)	81.161 m
Length(WL)	78.955 m
Length(BP)	77.942 m
Breadth(Moulded)	15.728 m
Depth(Moulded)	5.406 m
Draft(Design)	4.030 m
Frame Spacing	650 mm
Service Speed	10 knot
Deadweight	3000 T

GIRDERS	.....
FRAME	.....
WEB FRAME	.....
BULKEADS	.....
SIDE STRINGERS	.....



## LONGITUDINAL CONSTRUCTION

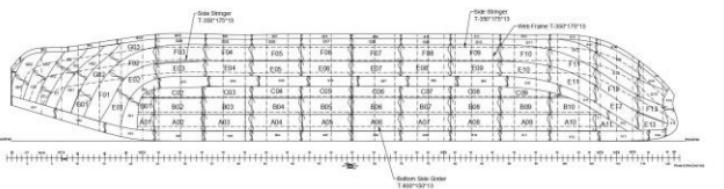
Student ID	Name
1712002	Noshin Tarannum
1712043	Rafid Imam

# **Shell Expansion**

# MAIN PARTICULARS

Length(0A)	81.161 m
Length(WL)	78.955 m
Length(BP)	77.942 m
Breadth(Moulded)	15.728 m
Depth(Moulded)	5.406 m
Draft(Design)	3.588 m
Frame Spacing	650 mm
Service Speed	10 knot
Deadweight	3000 T

## SYMBOLS



## PLATE SIZE TABLE

K STRAKE	A STRAKE	B STRAKE	C STRAKE	D STRAKE	E STRAKE	F STRAKE	G STRAKE	H STRAKE	I STRAKE	J STRAKE	I STRAKE	M STRAKE	N STRAKE	S STRAKE			
PLT. NO	SIZE																
K1	6000X1200X15mm	A1	2000X2000X15mm	B1	3000X2000X15mm	C1	1000X1000X15mm	E1	3000X2000X15mm	F1	3000X2000X15mm	H1	6000X2000X15mm	I1	2000X2000X15mm	M1	3000X2000X15mm
K2	6000X1200X15mm	A2	6000X2000X15mm	B2	6000X2000X15mm	C2	6000X2000X15mm	E2	6000X2000X15mm	F2	6000X2000X15mm	G2	6000X2000X15mm	I2	3000X2000X15mm	M2	4000X2000X15mm
K3	6000X1200X15mm	A3	6000X2000X15mm	B3	6000X2000X15mm	C3	6000X2000X15mm	E3	6000X2000X15mm	F3	6000X2000X15mm	G3	6000X2000X15mm	H3	6000X2000X15mm	I3	6000X2000X15mm
K4	6000X1200X15mm	A4	6000X2000X15mm	B4	6000X2000X15mm	C4	6000X2000X15mm	E4	6000X2000X15mm	F4	6000X2000X15mm	G4	6000X2000X15mm	H4	6000X2000X15mm	I4	6000X2000X15mm
K5	6000X1200X15mm	A5	6000X2000X15mm	B5	6000X2000X15mm	C5	6000X2000X15mm	E5	6000X2000X15mm	F5	6000X2000X15mm	G5	6000X2000X15mm	H5	6000X2000X15mm	I5	6000X2000X15mm
K6	6000X1200X15mm	A6	6000X2000X15mm	B6	6000X2000X15mm	C6	6000X2000X15mm	E6	6000X2000X15mm	F6	6000X2000X15mm	G6	6000X2000X15mm	H6	6000X2000X15mm	I6	6000X2000X15mm
K7	6000X1200X15mm	A7	6000X2000X15mm	B7	6000X2000X15mm	C7	6000X2000X15mm	E7	6000X2000X15mm	F7	6000X2000X15mm	G7	6000X2000X15mm	H7	6000X2000X15mm	I7	6000X2000X15mm
K8	6000X1200X15mm	A8	6000X2000X15mm	B8	6000X2000X15mm	C8	6000X2000X15mm	E8	6000X2000X15mm	F8	6000X2000X15mm	G8	6000X2000X15mm	H8	6000X2000X15mm	I8	6000X2000X15mm
K9	6000X1200X15mm	A9	6000X2000X15mm	B9	6000X2000X15mm	C9	6000X2000X15mm	E9	6000X2000X15mm	F9	6000X2000X15mm	G9	6000X2000X15mm	H9	6000X2000X15mm	I9	6000X2000X15mm
K10	6000X1200X15mm	A10	6000X2000X15mm	B10	6000X2000X15mm	C10	6000X2000X15mm	E10	6000X2000X15mm	F10	6000X2000X15mm	G10	6000X2000X15mm	H10	6000X2000X15mm	I10	6000X2000X15mm
K11	6000X1200X15mm	A11	6000X2000X15mm	B11	6000X2000X15mm	C11	6000X2000X15mm	E11	6000X2000X15mm	F11	6000X2000X15mm	G11	6000X2000X15mm	H11	6000X2000X15mm	I11	6000X2000X15mm
K12	6000X1200X15mm																
K13	6000X1200X15mm																
K14	6000X1200X15mm																
K15	6000X1200X15mm																
K16	6000X1200X15mm																

## SHELL EXPANSION

Student ID	Name
1712002	Noshin Tarannum
1712043	Rafid Imam

# **Preliminary**

# **Weight Calculation**

## Preliminary

### Lightweight and Deadweight Calculation

Total Weight of plates	417.98
Total weight of structural and stiffening members	185.72
<b>Total Steel weight (considering 10% scrap)</b>	<b>664.07</b>

Machinery weight	44.28
------------------	-------

Wood and Outfit Weight	12.60
------------------------	-------

<b><u>Lightweight</u></b>	<b><u>720.97</u></b>
---------------------------	----------------------

Capacity of the Cargo Holds	2886.86
Capacity of Fresh Water Tank	11.25
Capacity of Fuel Oil Reserve Tank	26.4
Capacity of Lubricating Oil Reserve Tank	0.66
Capacity of Forward Ballast Water Tank	160.19
Crew weight	1.12
Provision	0.80
<b>Deadweight</b>	<b>3089.21</b>

Lightweight	720.97
Deadweight	3089.21
<b>Displacement</b>	<b>3810.18</b>

Preliminary calculated deadweight was **3000** tones.

Preliminary calculated displacement was **4243.90** tones

# **Resistance and Power Calculation**

## Resistance Calculation by Holtrop and Mennen's Method

Frictional Resistance, $R_F$	35.6 kN
Wave-Making Resistance, $R_W$	10.5 kN
Appendage Resistance , $R_{APP}$	1.64 kN
Model Ship Correlation Resistance , $R_A$	11.7 kN
Air Resistance , $R_{AA}$	12.1 kN
<b>Total Resistance, <math>R_T</math></b>	<b>90 kN</b>
Total Resistance Co-efficient, $C_T$	$4.32 \times 10^{-3}$

# Power Calculation

## Efficiencies and QPC Calculation

Taylor Wake Fraction ,  $w_T = 0.26$

Thrust Deduction Factor ,  $t = 0.22$

Hull Efficiency ,  $n_H = 1.057$

Relative Rotative Efficiency,  $n_R = 1.028$

## QPC, Open Water Efficiency and Propeller RPM

	Method 1 ( $B_p$ - Delta Chart)	Method 2 ( $K_T$ and $K_Q$ )
QPC	0.475	0.478
Propeller Open Water Efficiency, $n_o$	0.44	0.446
Propeller RPM	325	329

**Note:** Detailed Calculation is provided in Appendix 1

## Power Calculation Summary

Total resistance	$R_T$	$R_F + R_{APP} + R_w + R_A + R_{AA}$	90	kN
Effective Power	$P_E$	$R_T * V$	460.52	kW
QPC			0.47	
Delivered Power	$P_D$		969.66	kW
Shaft Efficiency	$n_s$		0.95	
Shaft Power	$P_S$		1020.69	kW
		Transmission line loss 5% for transmission via gear box		
Engine power			1074.41	kW
Brake Power	$P_b$	(85% MCR), Considering 15% sea margin	1200.81	kW
Total installed power	$P_I$	(100% MCR)	1412.72	kW
			710*2	kW

**Note:** Detailed Calculation is provided in Appendix 1

## Engine Selection

We finally considered **Two Engines** of 710 kW or 950 HP

## Engine Specifications

**Model No: XCW6200ZC-1** (Ref. Marine Propulsion Engine, Weichai Catalogue)

Engine Power: 720 kW or 969 HP

Engine RPM: 1000

Net Weight: 6300 kg

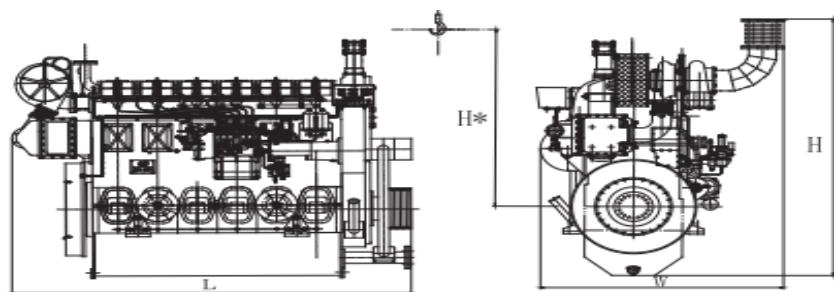
Mechanical Pump Bore and stroke: 200×270 mm

Displacement: 50.89 L

Min Fuel Consumption: 200 g /kW-h

Dimension: L-2828 mm, W-1726 mm, H-2412mm, H\*-2000 mm

**Note:** Detailed Calculation is provided in Appendix 1



## Gear Box Selection

## **Marine Gear Box Specifications**

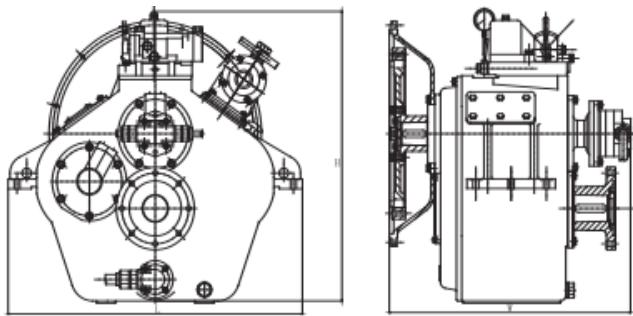
**Model: WHG120** (Ref. Marine Propulsion Engine, Weichai Catalogue)

Input Speed: 750-2000 RPM

Gear Rati: 3.03

Net Weight: 120 kg

Dimension: 792 mm



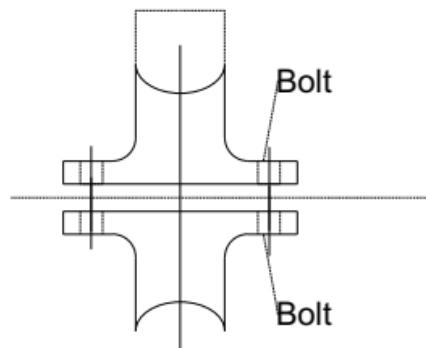
**Note:** Detailed Calculation is provided in Appendix 1

## Rudder Calculation Summary

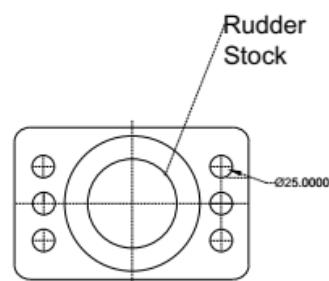
ITEM	VALUES
Area of a Single Rudder	2.98 m <sup>2</sup>
Rudder Force	60.40 kN
Rudder Torque	21.20 kN-m
Rudder Stock Diameter	100 mm
Rudder Coupling Bolt Diameter	25 mm
Rudder Coupling Flange Thickness	25 mm
Rudder Pintle Thickness	8 mm
Rudder Pintle Diameter	55 mm
Rudder Plate Thickness	8 mm
Rudder Web Plate Thickness	7 mm
Rudder Horizontal Frame Spacing	560 mm
Rudder Vertical Frame Spacing	830 mm
Rudder Profile	NACA -0020

**Note:** Detailed Calculation is provided in Appendix 2

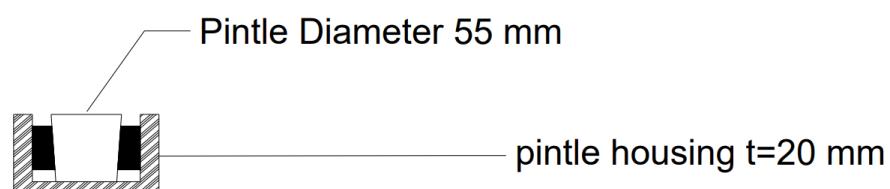
## Details of Rudder Drawing:



Coupling Details

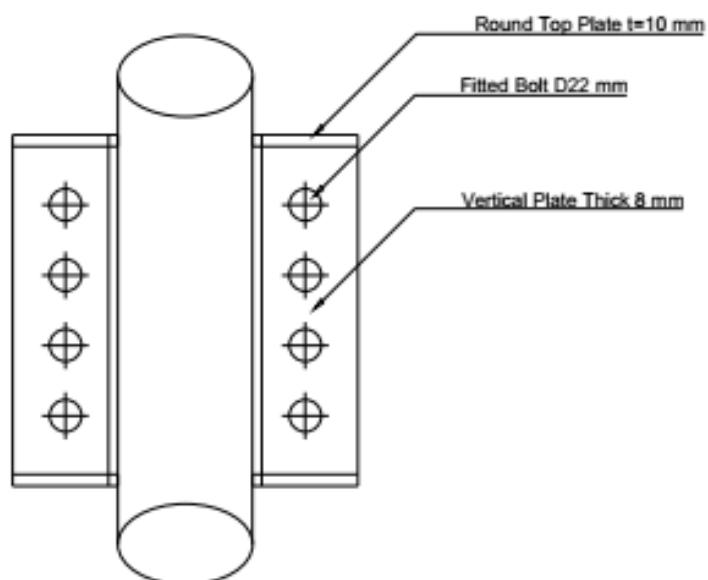
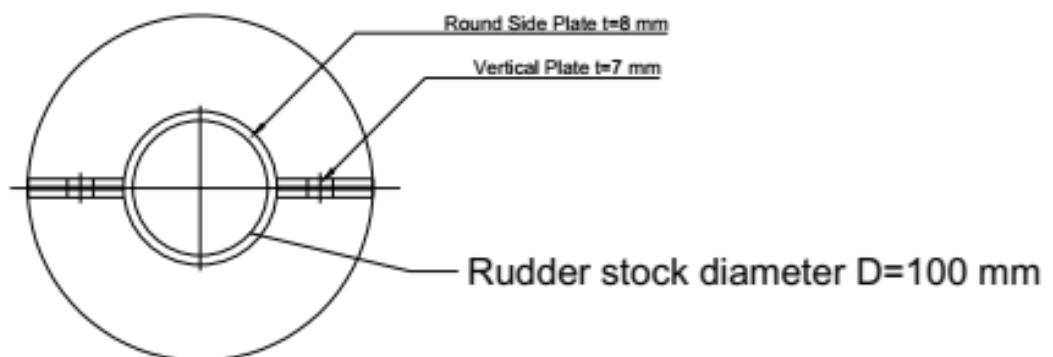


Coupling Flange

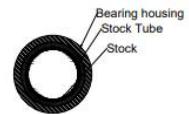
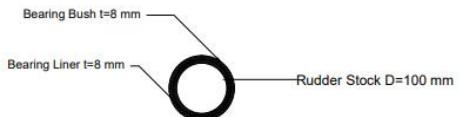


Pindle

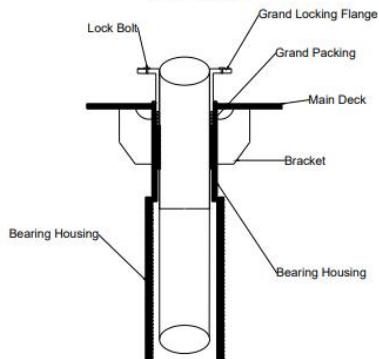
## Details of Rudder Drawing (Contd....)



## Jumping Clamp



Top View

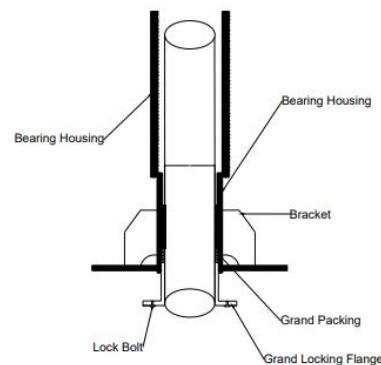


Upper Bearing

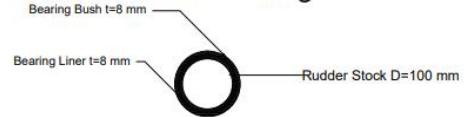


Bottom View

Top View

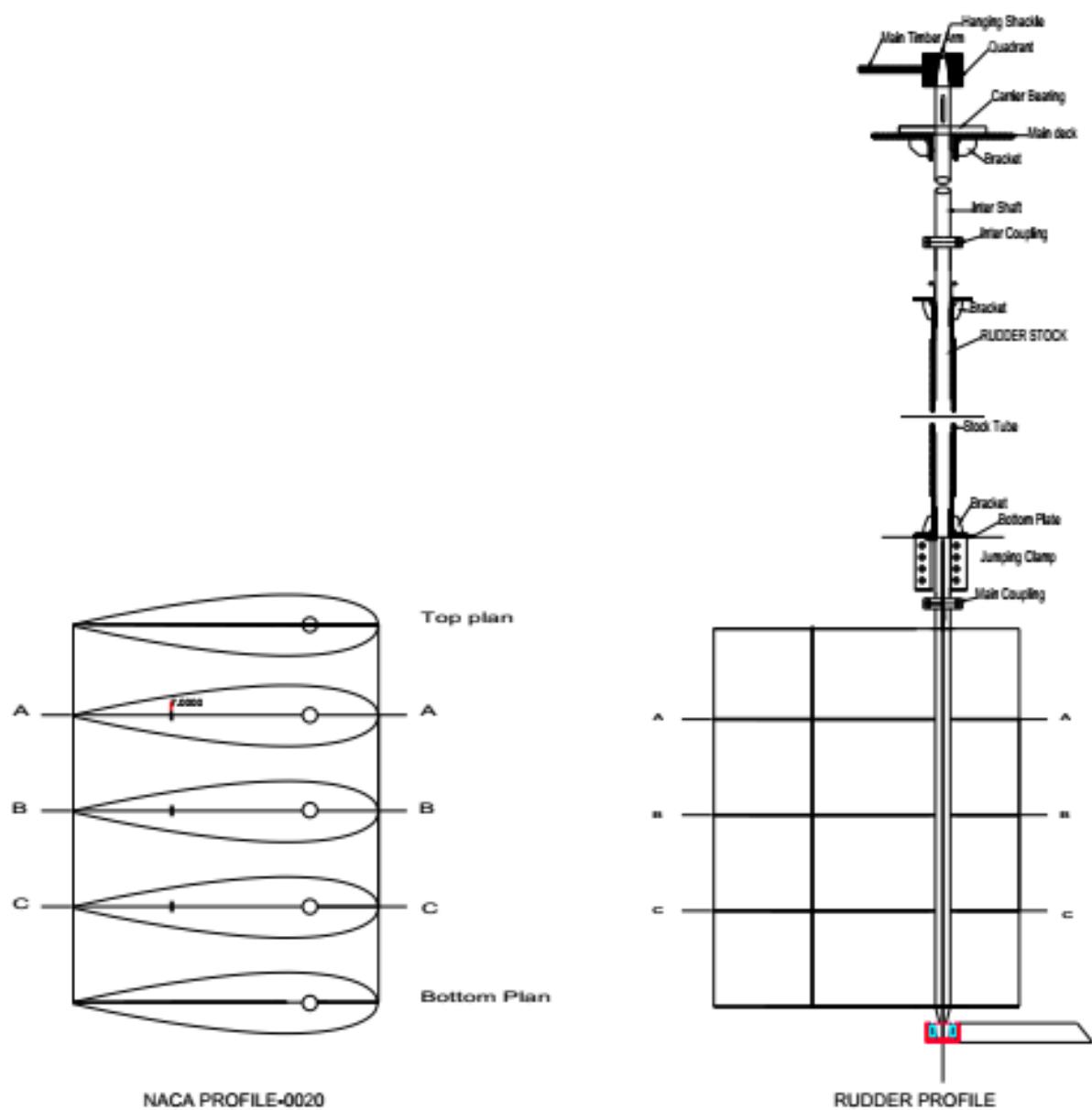


Lower Bearing

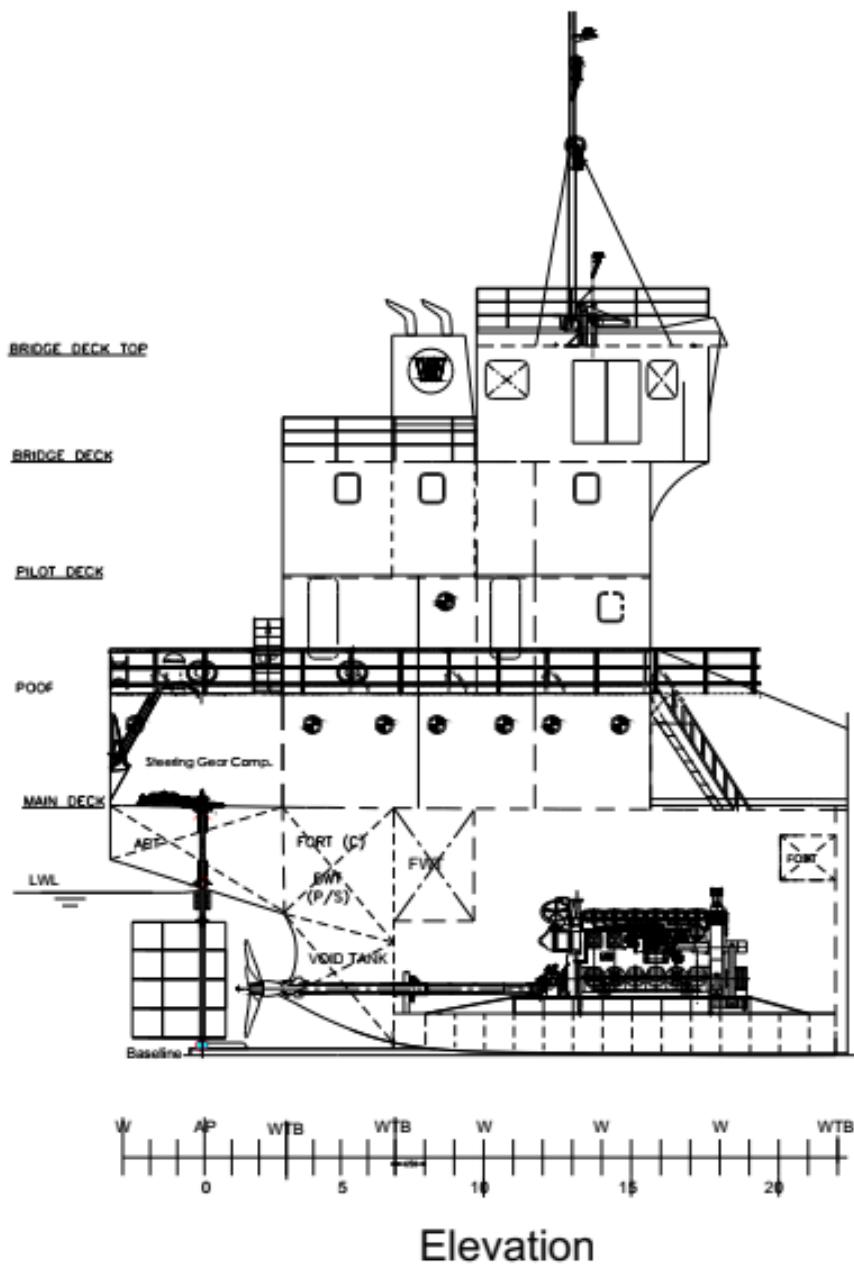


Bottom View

## Details of Rudder Drawing (Contd....)



# Rudder Arrangement in Ship Profile

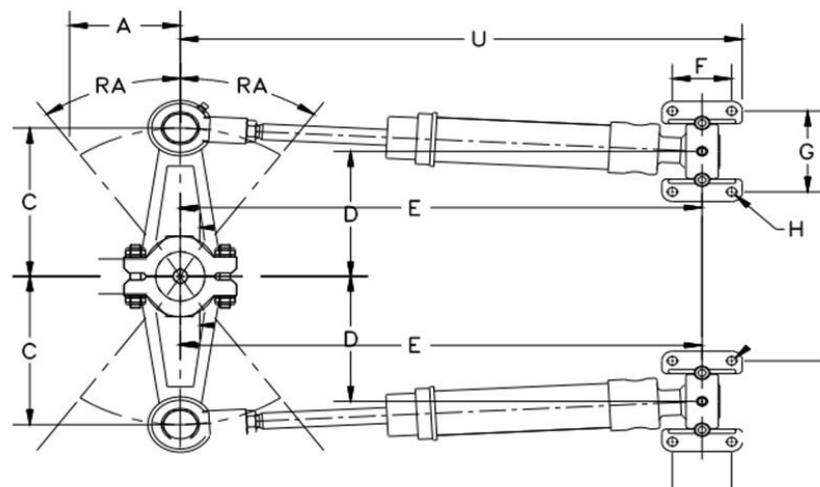


# STEERING GEAR ARRANGEMENT

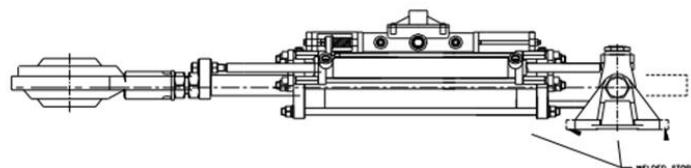
Working Torque for Steering Gear 25.5 kN-m

Steering Gear Model -7093- B20 ( Ref. Kobelt Electro-Hydraulic Steering Gear Catalogue)

**Note:** Detailed Calculation is provided in Appendix 3



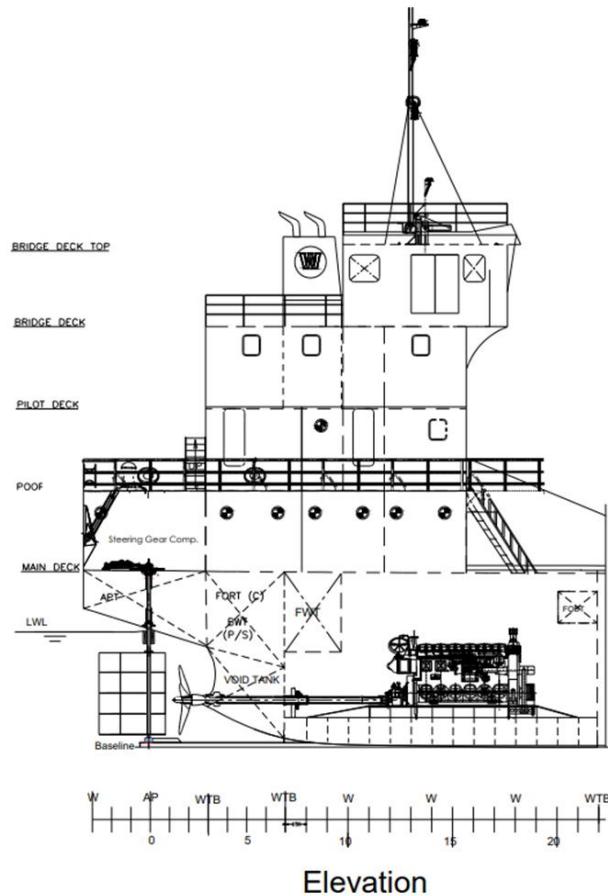
**STEERING GEAR (TOP VIEW)**



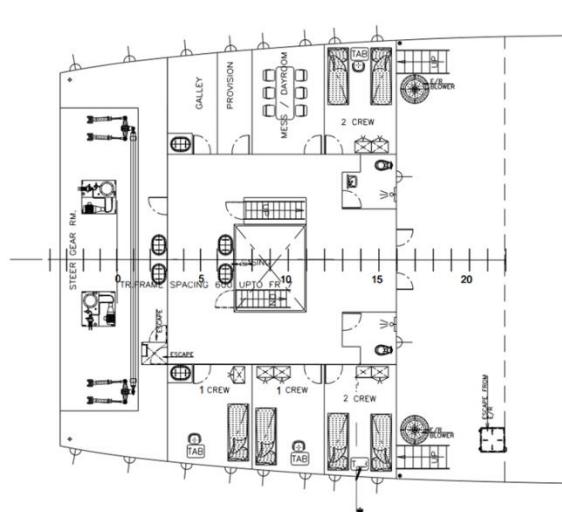
**STEERING GEAR (SIDE VIEW)**

**Model No-7093-B20**

# Steering Gear Arrangement Drawing:



## Profile View



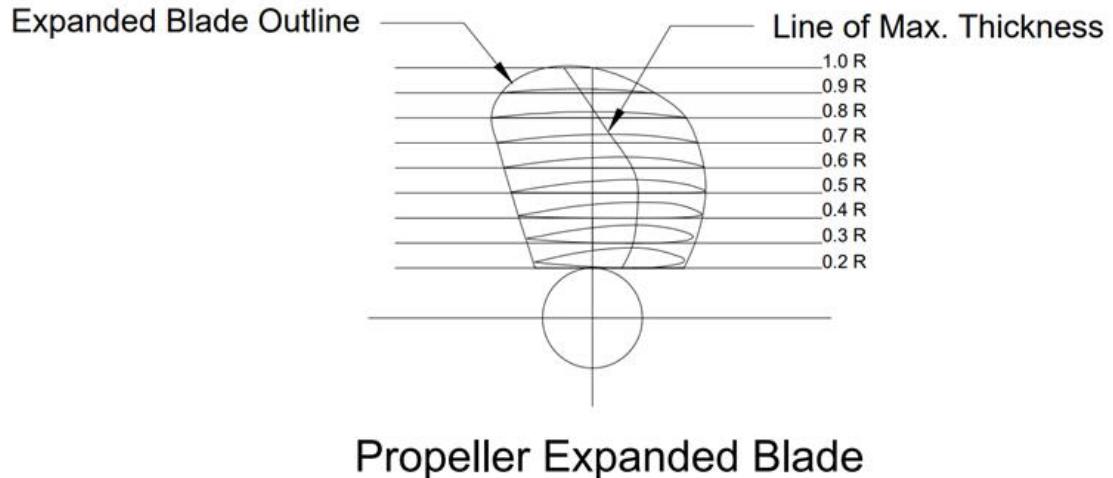
## Plan View

## Summary of Propeller Calculation

Particulars	Value	Unit
Propeller diameter	2.15	meter
Taylor wake fraction	0.26	--
Thrust deduction co-efficient	0.22	--
Expanded blade area ratio, $\frac{A_E}{A_0}$	0.46	--
Pitch-dia Ratio	0.64	--
Projected blade area, $A_P$	3.63	$m^2$
Burrill co-efficient, $\tau_c$	0.16	--
Shaft efficiency, $\eta_S$	0.95	--

**Note:** Detailed Calculation is provided in Appendix 2

# Propeller Expanded Blade Section Drawing:



Propeller Expanded Blade

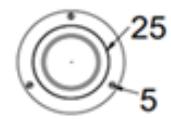
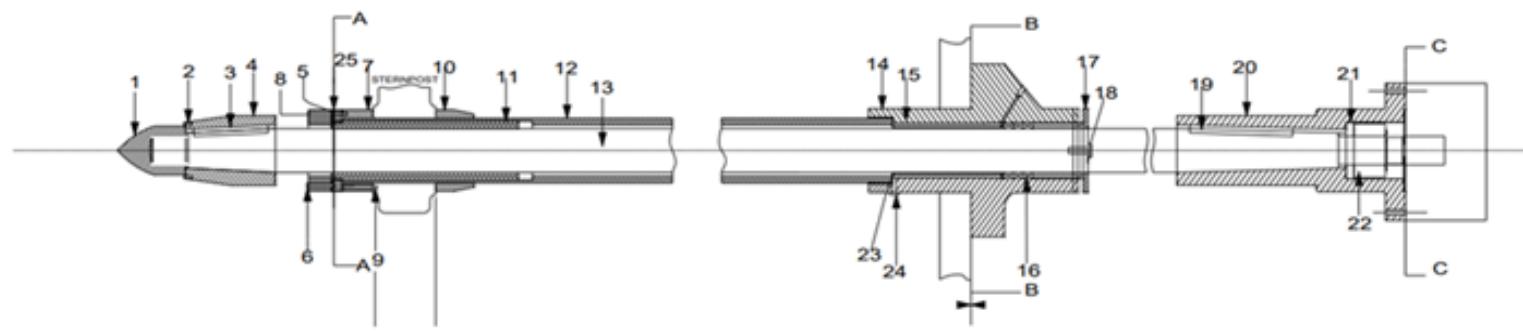
**Note:** 1) The vessel is twin-screw vessel and the propeller is of 3 blades.

2) The geometry of the propeller is drawn from Wageningen B-screw propeller.

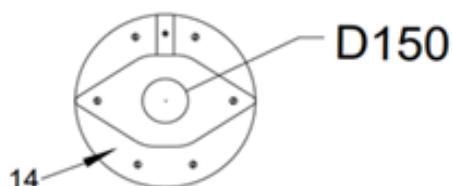
**Note:** Detailed Calculation is provided in Appendix 2

# Propeller Shaft Arrangement

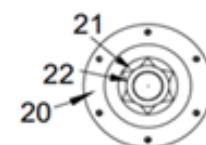
Diameter of Propeller Shaft 150 mm



Section : A-A



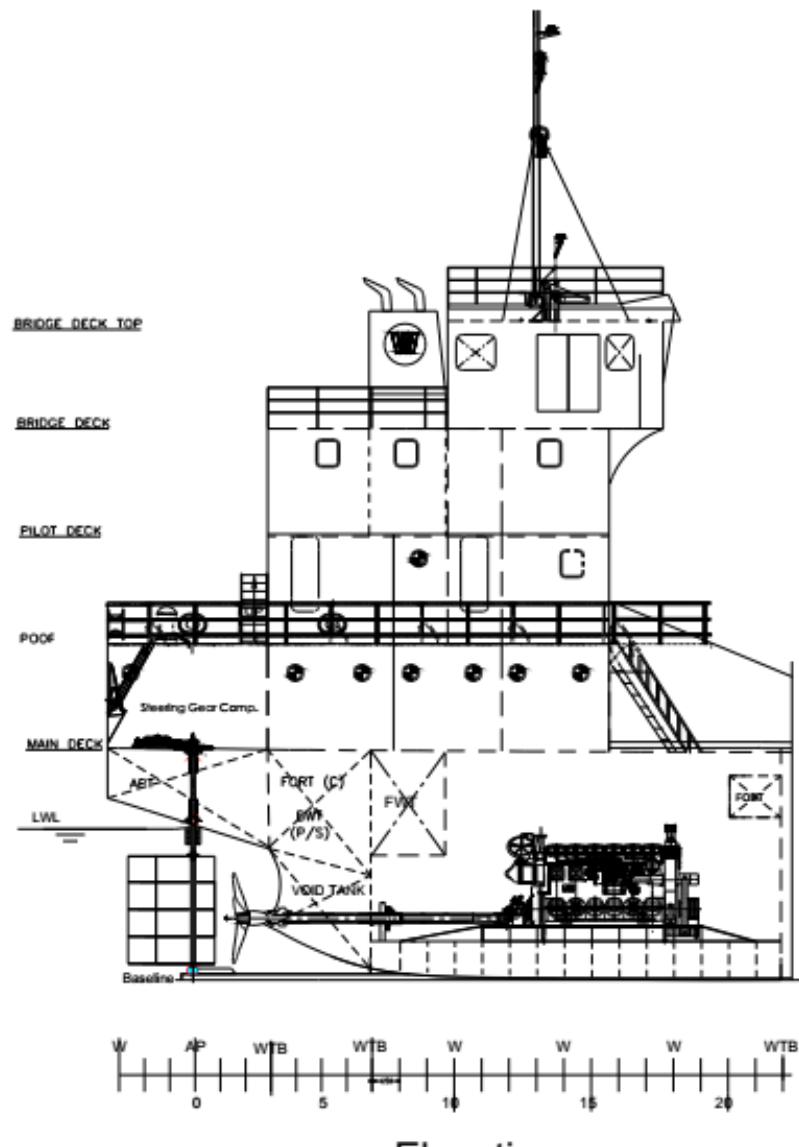
Section : B-B



Section :  
C-C

Propeller shaft arrangement

## **Propeller Shaft Arrangement on Ship Profile:**



# Engine Foundation And Engine Room Arrangement

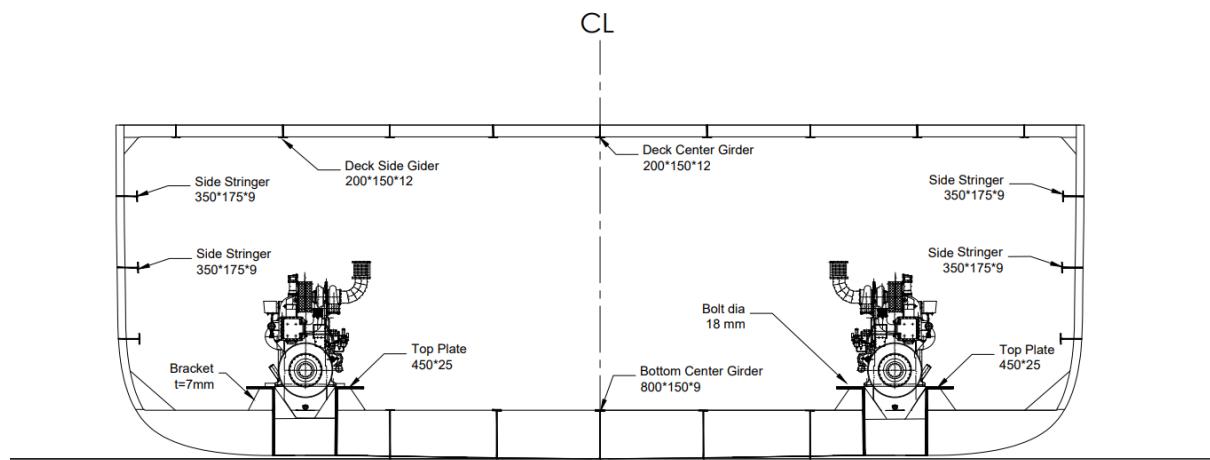
## Summary of Engine Foundation Scantling:

Item	Dimension
Top Plate Area	10520 mm <sup>2</sup>
Top Plate Width	450 mm
Top Plate Thickness	25 mm
Girder Web Thickness	12 mm
Floor Web Thickness	9 mm
Floor Depth	800 mm
Bracket Thickness	7 mm
Foundation Bolt Diameter	30 mm

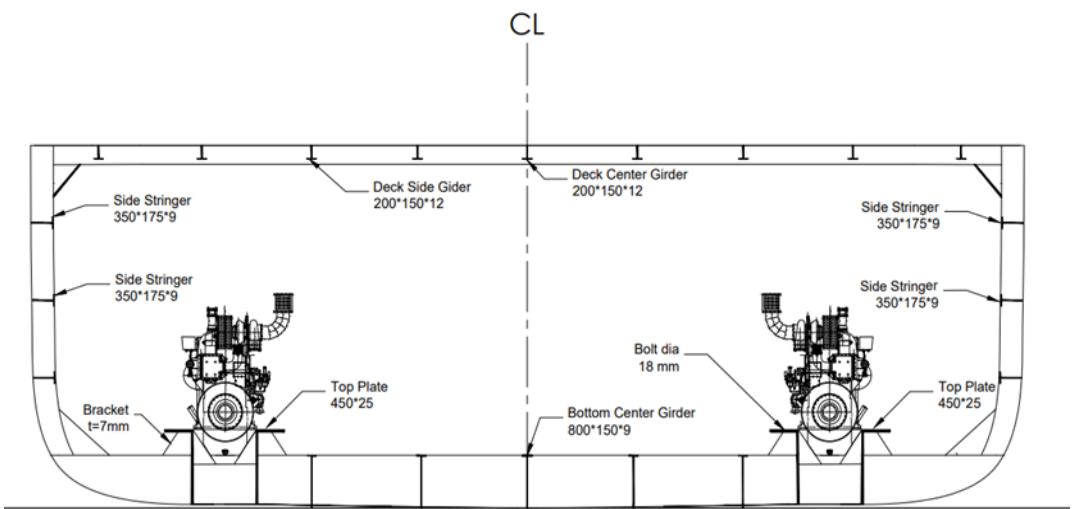
**Note:** Detailed Calculation is provided in Appendix 4

**Ref.IRS, Ch-6, Sec-7,7.2**

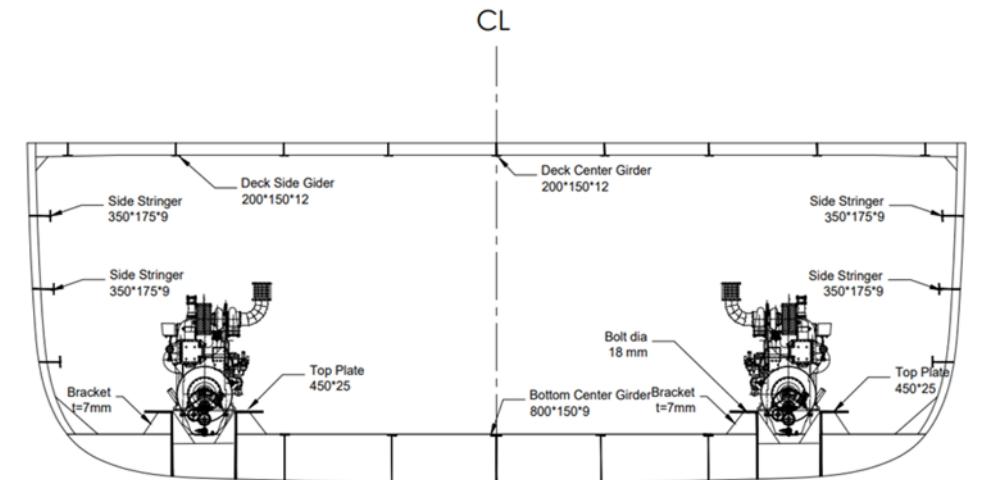
## Engine Foundation Drawing



Frame no 17

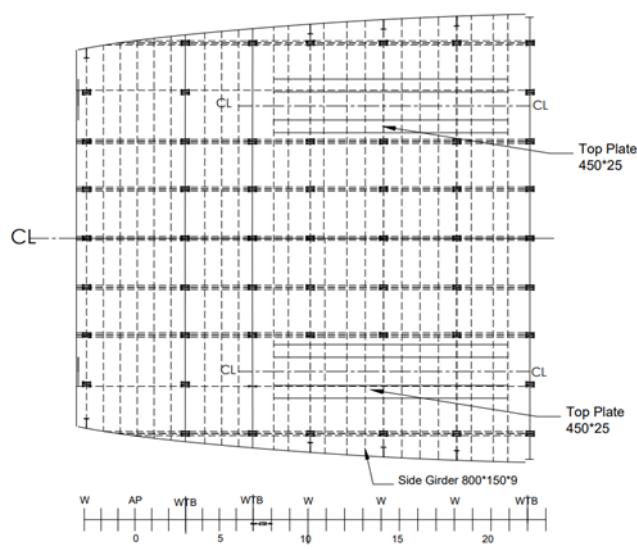
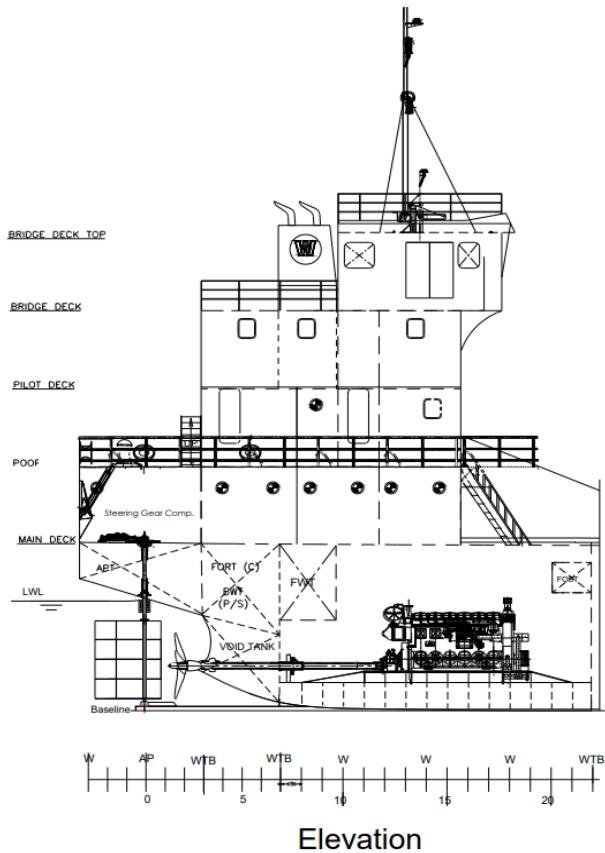


Frame no 14(Web)



Frame no 12 (Engine with Gear Box)

# Engine Foundation And Engine Room Arrangement In Ship:



Engine Room

# **Detailed Weight Calculation**

## Detailed Lightweight and Deadweight Calculation

Total Weight of plates	418.98 tonnes
Total weight of structural and stiffening members	154.04 tonnes
<b>Total Steel weight (considering 10% scrap)</b>	<b>630.20 tonnes</b>

Machinery weight	45.61 tonnes
------------------	--------------

Wood and Outfit Weight	12.60 tonnes
------------------------	--------------

<b>Lightweight</b>	<b>688.41 tonnes</b>
--------------------	----------------------

Capacity of the Cargo Holds	2898.86
Capacity of Fresh Water Tank	15.00
Capacity of Fuel Oil Reserve Tank	9.77
Capacity of Lubricating Oil Reserve Tank	0.06
Capacity of Forward Ballast Water Tank	160.19
Crew weight	1.12
Provision	0.80
<b>Deadweight</b>	<b>3087.21</b>

Lightweight	688.41 tonnes
Deadweight	3087.21 tonnes
<b>Displacement</b>	<b>3776.00 tonnes</b>

Preliminary calculated deadweight was **3000** tones.

Preliminary calculated displacement was **4243.90** tones.

# **Trim Calculation**

<b>T</b>	3.59	m
<b>LBP</b>	77.94	m
<b>half length</b>	38.97	m
<b>LCG</b>	0.40	fwd from mid
<b>LCB</b>	1.46	fwd of mid
<b>WF</b>	38.42	m
<b>FL</b>	39.52	m
<b>LCF</b>	-0.55	fwd(+)
<b>MCTC</b>	63.53	
<b>Displacement</b>	3775.00	tonnes

$$\text{Change in trim} = x = \frac{(LCG - LCB)\Delta}{MCT \text{ 1 cm}} = \frac{(0.40 - 1.46)3775}{63.53}$$

**= -62.75 cm**

$$\begin{aligned}\text{Change in draught at aft perpendicular } WW' &= \frac{WF}{L} \times \text{Change of trim} \\ &= \frac{38.42}{77.94} \times (-62.75) \\ &= -30.93 \text{ cm} \\ &= -0.31 \text{ m}\end{aligned}$$

$$\begin{aligned}\text{Change in draught at fore perpendicular } LL' &= \frac{FL}{L} \times \text{Change of trim} \\ &= \frac{39.52}{77.94} \times (-62.75) \\ &= -31.82 \text{ cm} \\ &= -0.32 \text{ m}\end{aligned}$$

<b>Final draft fwd.</b>	<b>3.27 m</b>
<b>Final draft aft</b>	<b>3.89 m</b>

## Trim by Stern

## Principal Particulars Comparison between Preliminary and Final Design Ship

Parameters	Final Design Ship	Preliminary Design Ship
Length Overall, $L_{OA}$	<b>81.16 m</b>	<b>81.16 m</b>
Length Between Perpendicular, $L_{pp}$	<b>77.94 m</b>	<b>77.94 m</b>
Breadth, B	<b>15.72 m</b>	<b>15.72 m</b>
Depth, D	<b>5.41 m</b>	<b>5.41 m</b>
Draft, H	<b>3.59 m</b>	<b>4.03 m</b>

<b>Deadweight</b>	<b>3000 tonnes</b>	<b>3000 tonnes</b>
<b>Displacement</b>	<b>3776.00 tonnes</b>	<b>4243.90 tones</b>
$C_B$	<b>0.859</b>	<b>0.859</b>
$C_D$	<b>0.70</b>	<b>0.70</b>

# **Capacity Calculation**

Cargo Hold Name	Volume	Capacity	LCG (from stern)	VCG(from keel)	LCG moment	VCG moment
Cargo hold 1	768	937.6	62.2	3.09	58318.72	2897.184
Cargo Hold 2	1637.72	1965.264	33.63	3.09	66091.82832	6072.66576

**Total capacity 2902.864 tonnes**

	Length	Breadth	Depth	Volume	Weight	LCG	VCG	moment LCG	moment VCG
FWT(both)	1.50	1.50	2.50	11.25	11.25	11.17	4.10	125.66	46.13
FORT	2.39	7.37	1.50	26.40	9.77	5.01	3.90	48.97	38.12
LORT	0.65	1.02	0.99	0.66	0.07	14.43	3.90	0.95	0.26
FOST*2	0.99	0.98	0.99	1.93	1.93	15.44	3.90	29.76	7.52
B.BWT	1.93	14.82	5.60	160.19	160.19	2.69	2.80	430.92	448.54
crew					1.12				
provision					0.80				540.55

**Total Weight 185.13**

Dhaka Chittagong route distance	212.43 KM
Engine fuel consuption rate	0.079 KG/s
Speed of vessel	5.144 m/s
Time required in voyage	41296.66 s
Fuel amount needed	3257.85 KG 9.77 tonne

<b>Lightship Condition</b>			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	0.00	3.09	0.00
Cargo Hold2	0.00	3.09	0.00
Lightweight	688.97	3.66	2518.75
FWT(both)	0.00	4.10	0.00
FORT	0.00	3.90	0.00
LORT	0.00	3.90	0.00
FOST*2	0.00	3.90	0.00
B.BWT	0.00	2.80	0.00
Total Capacity	688.97	VCG	3.66 m

<b>Fully Loaded Departure Condition</b>			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	937.60	3.09	2897.18
Cargo Hold2	1965.26	3.09	6072.67
Lightweight	688.55	3.72	2562.93
FWT(both)	11.25	4.10	46.13
FORT	9.77	3.90	38.12
LORT	0.07	3.90	2.56
FOST*2	1.93	3.90	7.52
B.BWT	160.19	2.80	448.54
Total Capacity	3774.62	VCG	3.20 m

<b>In Ballast in Departure Condition</b>			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	0.00	3.09	0.00
Cargo Hold2	0.00	3.09	0.00
Lightweight	688.97	3.66	2518.75
FWT(both)	15.00	4.10	46.13
FORT	9.77	3.90	38.12
LORT	0.07	3.90	2.56
FOST*2	1.93	3.90	7.52
B.BWT	135.19	2.80	448.54
FPT	191.44	3.28	627.91
FBWT	190.74	2.75	524.54
BBWT	81.35	4.23	344.11
DBT1	285.62	0.44	125.67
DBT2	563.36	0.44	247.88
APT	130.06	4.76	619.09
Total Capacity	2293.50	VCG	2.42 m

# **Stability**

## **Calculation**

## STABILITY IN LIGHTSHIP CONDITION

<b>Lightship Condition</b>			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	0.00	3.09	0.00
Cargo Hold2	0.00	3.09	0.00
Lightweight	688.97	3.66	2518.75
FWT(both)	0.00	4.10	0.00
FORT	0.00	3.90	0.00
LORT	0.00	3.90	0.00
FOST*2	0.00	3.90	0.00
B.BWT	0.00	2.80	0.00
Total Capacity	688.97	VCG	3.66 m

Properties	IMO value	Lightship Condition	
Area up to 30 degree (m-rad)	$\geq 0.055$	1.41	PASS
Area up to 40° (m-rad)	$\geq 0.09$	2.16	PASS
Area up to 30° - 40° (m-rad)	$\geq 0.03$	0.75	PASS
GZ at 30 degree (m)	$\geq 0.2$	4.901	PASS
Max. GZ at (degree)	$\geq 30$ (preferable) but not $\leq 25$	47.00	PASS
Initial Metacentric Height (m)	Should not be $\leq 0.15$	10.80	PASS

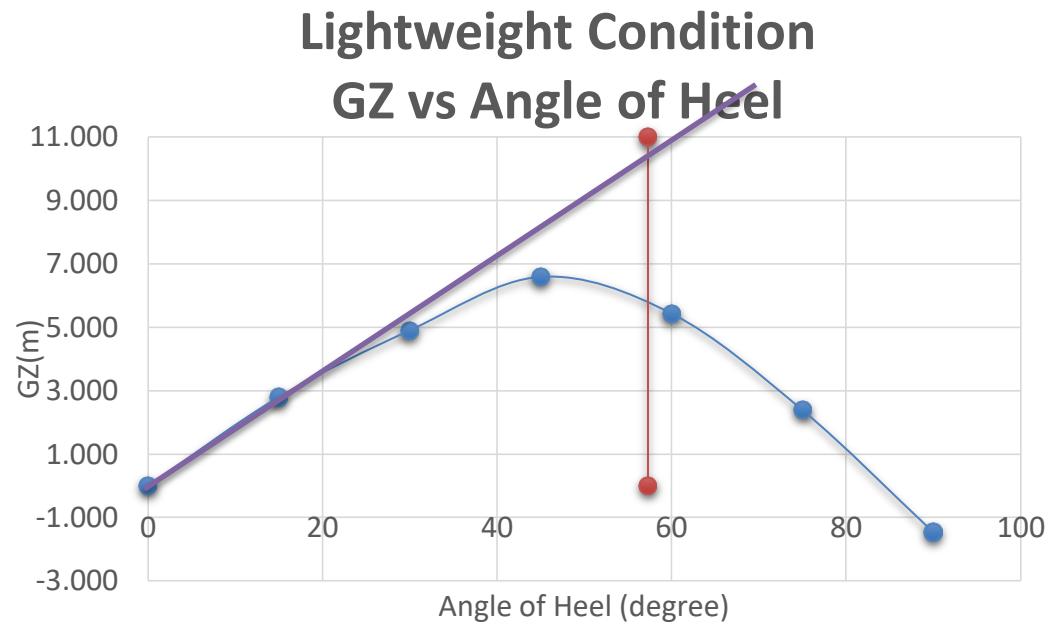


Fig :GZ vs Angle of Heel

## STABILITY IN FULLY LOADED DEPARTURE CONDITION

Fully Loaded Departure Condition			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	937.60	3.09	2897.18
Cargo Hold2	1965.26	3.09	6072.67
Lightweight	688.55	3.72	2562.93
FWT(both)	11.25	4.10	46.13
FORT	9.77	3.90	38.12
LORT	0.07	3.90	2.56
FOST*2	1.93	3.90	7.52
B.BWT	160.19	2.80	448.54
Total Capacity	3774.62	VCG	3.20 m

Properties	IMO value	Loaded Condition	
Area up to 30 degree (m-rad)	$\geq 0.055$	0.609	PASS
Area up to $40^\circ$ (m-rad)	$\geq 0.09$	0.925	PASS
Area up to $30^\circ - 40^\circ$ (m-rad)	$\geq 0.03$	0.316	PASS
GZ at 30 degree (m)	$\geq 0.2$	2.179	PASS
Max. GZ at (degree)	$\geq 30$ (preferable) but not $\leq 25$	42.000	PASS
Initial Metacentric Height (m)	Should not be $\leq 0.15$	4.500	PASS

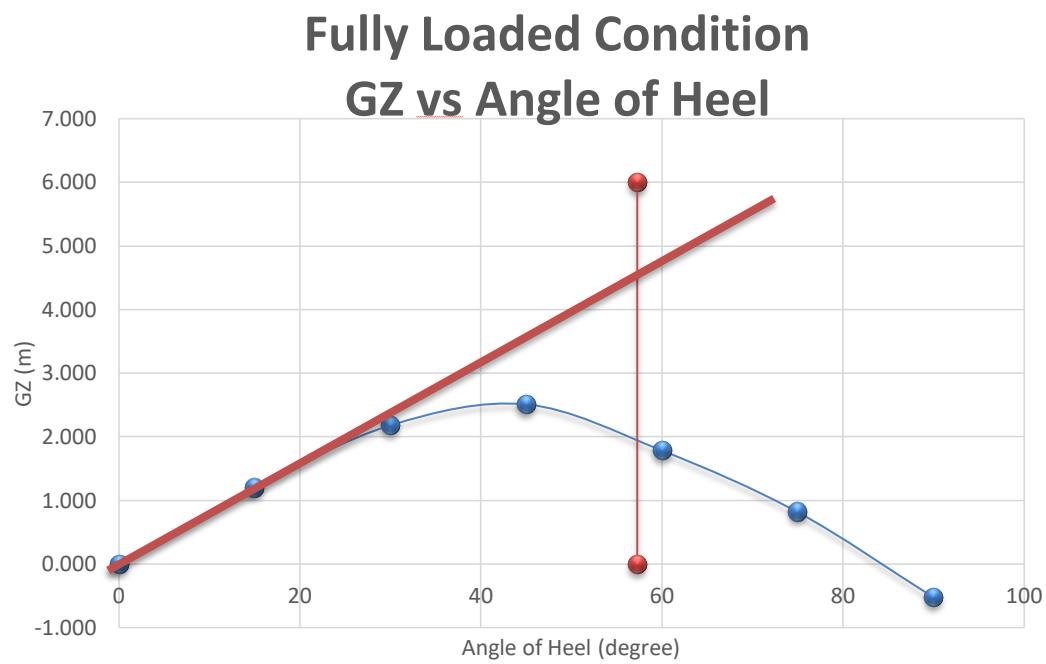


Fig :GZ vs Angle of Heel

## STABILITY IN BALLAST IN DEPARTURE CONDITION

In Ballast in Departure Condition			
	Capacity (tonnes)	vcg(from keel) (m)	Vcg moment (tonnes-m)
Cargo Hold1	0.00	3.09	0.00
Cargo Hold2	0.00	3.09	0.00
Lightweight	688.97	3.66	2518.75
FWT(both)	15.00	4.10	46.13
FORT	9.77	3.90	38.12
LORT	0.07	3.90	2.56
FOST*2	1.93	3.90	7.52
B.BWT	135.19	2.80	448.54
FPT	191.44	3.28	627.91

FBWT	190.74	2.75	524.54
BBWT	81.35	4.23	344.11
DBT1	285.62	0.44	125.67
DBT2	563.36	0.44	247.88
APT	130.06	4.76	619.09
Total Capacity	2293.50	VCG	2.42 m

Properties	IMO value	Ballast in Departure Condition	
Area up to 30 degree (m-rad)	$\geq 0.055$	1.1958	PASS
Area up to $40^\circ$ (m-rad)	$\geq 0.09$	5.3890	PASS
Area up to $30^\circ - 40^\circ$ (m-rad)	$\geq 0.03$	4.1932	PASS
GZ at 30 degree (m)	$\geq 0.2$	3.9968	PASS
Max. GZ at (degree)	$\geq 30$ (preferable) but not $\leq 25$	44	PASS
Initial Metacentric Height (m)	Should not be $\leq 0.15$	9.2	PASS

## GZ vs Angle of Heel

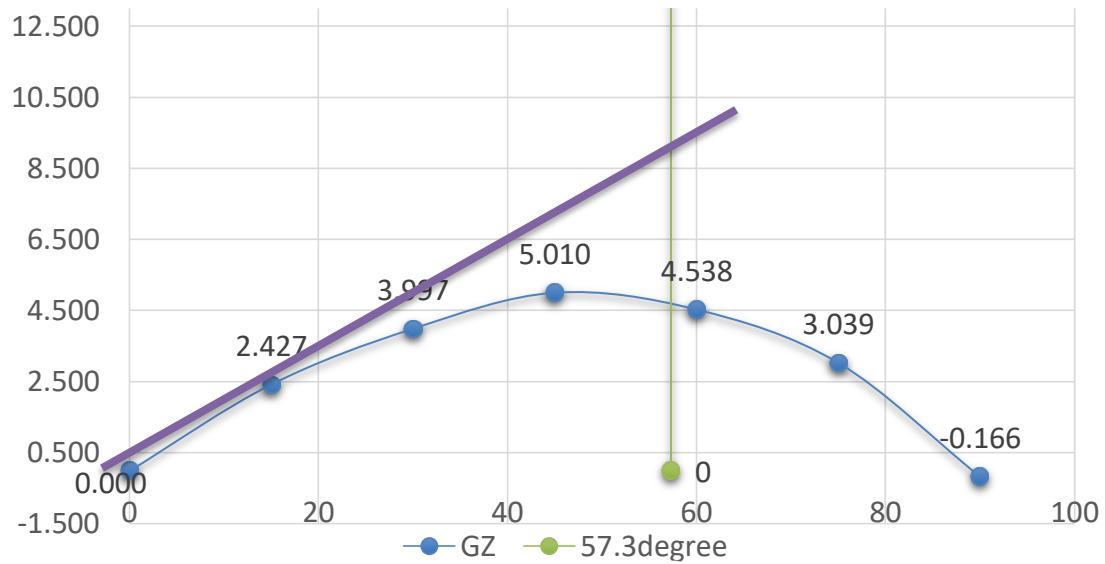


Fig : GZ vs Angle of Heel

# **Appendix 1**

## **Power and Engine Selection:**

Total resistance,  $R = 90 \text{ kN}$

Effective power,  $P_E = 90 \times 10 \times 5.144 = 460.52 \text{ kW}$

Ship Length,  $L_{Bp} = 77.942 \text{ m}$

Breadth,  $B = 15.728 \text{ m}$

Draft,  $T = 3.585 \text{ m}$

Speed,  $V = 10 \text{ knots}$

Volume displacement,  $= 3775.123 \text{ m}^3$

Propeller diameter,  $D = 0.6T = 2.151 \text{ m}$

Taylor wake fraction,

$$\omega_t = 0.26$$

Thrust Deduction factor,  $t = 0.22$

We know,

$$T(1-t) = R$$

$$T = 115.059 \text{ kN}$$

$$\eta_H = \frac{(1-t)}{1-\omega_t} = 1.049$$

$$\eta_R = 1.028$$

$$V_A = V(1-\omega_t) = 7.416 \text{ knot}$$

$$\text{Shaft immersion, } h = D/2 + 0.2 = 1.276 \text{ m}$$

$$H = T(\text{Draft}) - h$$

$$= 2.309 \text{ m}$$

$$P_0 = P_{atm} + \rho g H$$

$$= 123956.195 \text{ N/m}^2$$

$$P_V = 1646 \text{ N/m}^2$$

$$K = 0.1 \text{ (for twin screw)}$$

$$Z = 3$$

Do= 2.26 m

$$\text{Here, } \frac{A_E}{A_0} = \frac{(1.3+0.3Z)T}{(P_0-P_v)D^2} + K \\ = 0.547$$

$$\text{We know, } K_T/j^2 = \frac{T}{\rho D^2 V_a^2} \\ = 1.3$$

From chart,

$$\text{here, } j = \frac{V_a}{nD}$$

so, n = 330 rpm

assume,  $\eta_D = 0.46$

$$P_D = \frac{P_E}{\eta_D} = 460.52/0.46 = 1001.13 \text{ kW}$$

Va = 7.416 knots

$$B_p = 1.158 \left( \frac{n \times P_D}{V_a^{2.5}} \right)^5 \\ = 81.294$$

$$\delta = 3.28 \frac{nD}{V_a} \\ = 332.474$$

And, P/D = .0.64

So , From Bp - $\delta$  chart we get,

$$\eta_o = .44$$

$$P/D = .64$$

Here,

$$\eta_D \text{ Calculated} = \eta_H \times \eta_R \times \eta_o \\ = 0.47$$

$$\epsilon = \eta_{D \text{ Calculated}} - \eta_D \text{ assumed} \\ = -0.0149 < 0.005$$

So,  $\eta_D = 0.47$

Now,  $P_D = 460.52 / 0.47 = 969.66 \text{ kW}$

And  $P_s = P_D/\eta_s = 1020.692 \text{ kW}$

So, Break Power(85% MCR) = 1200.815 kW

And Installed Power (100% MCR) = 1412.724 kW

As ours a twin screw power of each engine=  $1412.724/2 = 706.362 \text{ kW}$

$$= 946.865 \text{ HP}$$

We finally selected **two engines** of 950 HP .

## Appendix 2

### Propeller Cavitation Check:

$$p_0 - p_v = 122310.195 \text{ kPa}$$

$$q_{0.7R} = \frac{1}{2} \times \rho \times V_R^2$$

$$= \frac{1}{2} \times 1.000 \times (V_A^2 + (0.7 \times \pi \times n \times D)^2)$$

$$= \frac{1}{2} \times 1.000 \times (3.815^2 + (0.7 \times \pi \times 3.00 \times 2.15)^2)$$

$$= 33.552 \text{ kPa}$$

$$\sigma_{0.7R} = \frac{p_0 - p_v}{q_{0.7R}} = \frac{83.85}{250.33} = 0.406$$

$$\frac{A_E}{A_{0\text{necessary}}} = \frac{T}{\frac{\pi}{4} \times D^2 \left( 1.067 - 0.229 \frac{P}{D} \right) (0.3\sigma_{0.7R}^{0.5} - 0.03) q_{0.7R}}$$

$$= \frac{115.059}{\frac{\pi}{4} \times 2.151^2 (1.067 - 0.229 \times 0.67) (0.3 \times 0.406^{0.5} - 0.03) 0.406}$$

$$= 1.989$$

$$A_D = \frac{\pi}{4} \times D^2 = 3.634 \text{ m}^2$$

$$\text{Therefore, } A_E = 7.229 \text{ m}^2$$

Assuming  $A_E = A_D$ ,

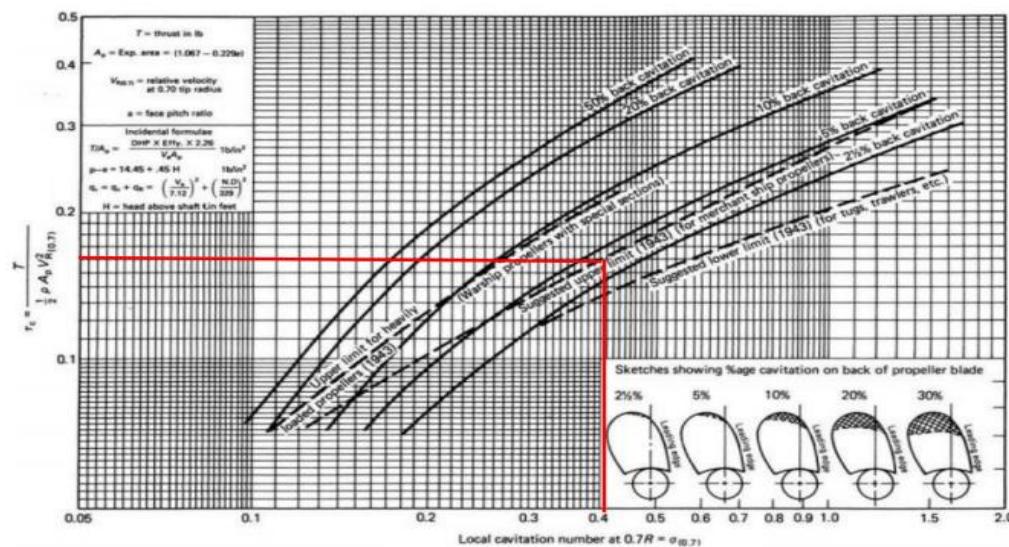
$$A_E \approx \frac{A_P}{1.067 - 0.229 \times \frac{P}{D}}$$

$$A_P = 1.831 \text{ m}^2$$

$$\tau_c = \frac{\frac{T}{A_P}}{q_{0.7R}} = 0.187$$

From Burrill Cavitation Diagram ( $\tau_c$  vs  $\sigma_{0.7R}$ ), the value obtained is just below the upper limit for merchant ship propeller.

Figure 1. Burril Diagram



## Propeller profile generation:

BAR=  $A_E/A_O = 0.550$       D=2.151 m

r/R	(c/D)*(Z/BAR)	a/c	b/c	Ar	Br	c	a	b	T (max)	c-a
0.200	1.633	0.616	0.350	0.053	0.004	0.644	0.397	0.225	0.087	0.247
0.300	1.832	0.611	0.350	0.046	0.004	0.722	0.441	0.253	0.077	0.281
0.400	2.000	0.599	0.351	0.040	0.003	0.789	0.472	0.277	0.067	0.316
0.500	2.120	0.583	0.355	0.034	0.003	0.836	0.487	0.297	0.057	0.349
0.600	2.186	0.558	0.389	0.028	0.002	0.862	0.481	0.335	0.047	0.381
0.700	2.168	0.526	0.442	0.022	0.002	0.855	0.450	0.378	0.037	0.405
0.800	2.127	0.481	0.478	0.015	0.001	0.839	0.403	0.401	0.027	0.435
0.850	1.892	0.441	0.489	0.012	0.001	0.746	0.329	0.365	0.022	0.417
0.900	1.657	0.400	0.500	0.009	0.001	0.653	0.261	0.327	0.017	0.392
1.000	0.000	0.000	0.000	0.003	0.000	0.000	0.000	0.000	0.006	0.000

**Table of V1**

r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.2	0.0873	0.0009	0.0017	-1.00	0.2826	1.00	0.3560
	0.0873	0.0009	0.0017	-0.95	0.2630	0.95	0.2821
	0.0873	0.0009	0.0017	-0.90	0.2400	0.90	0.2353
	0.0873	0.0009	0.0017	-0.80	0.1967	0.80	0.1685
	0.0873	0.0009	0.0017	-0.70	0.1570	0.70	0.1180
	0.0873	0.0009	0.0017	-0.60	0.1207	0.60	0.0804
	0.0873	0.0009	0.0017	-0.50	0.0880	0.50	0.0520
	0.0873	0.0009	0.0017	-0.40	0.0592	0.40	0.0304
	0.0873	0.0009	0.0017	-0.20	0.0172	0.20	0.0049
	0.0873	0.0009	0.0017	0.00	0.0000	0.00	0.0000

**Table of V2**

<b>Table of V2</b>				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0242	0.0259	0.0308	0.0322
-0.95	0.0640	0.95	0.1560	0.0225	0.0297	0.0244	0.0392
-0.90	0.1455	0.90	0.2840	0.0205	0.0347	0.0203	0.0462
-0.80	0.3060	0.80	0.4777	0.0168	0.0448	0.0146	0.0571
-0.70	0.4535	0.70	0.6190	0.0134	0.0540	0.0102	0.0648
-0.60	0.5842	0.60	0.7277	0.0103	0.0621	0.0070	0.0709
-0.50	0.6995	0.50	0.8170	0.0075	0.0691	0.0045	0.0761
-0.40	0.7984	0.40	0.8875	0.0051	0.0751	0.0026	0.0803
-0.20	0.9446	0.20	0.9750	0.0015	0.0841	0.0004	0.0856
0.00	1.0000	0.00	1.0000	0.0000	0.0873	0.0000	0.0873

**Table of V1**

r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.3	0.0772	0.0008	0.0015	-1.00	0.2306	1.00	0.2923
	0.0772	0.0008	0.0015	-0.95	0.2040	0.95	0.2186
	0.0772	0.0008	0.0015	-0.90	0.1790	0.90	0.1760
	0.0772	0.0008	0.0015	-0.80	0.1333	0.80	0.1191
	0.0772	0.0008	0.0015	-0.70	0.0943	0.70	0.0790
	0.0772	0.0008	0.0015	-0.60	0.0623	0.60	0.0503
	0.0772	0.0008	0.0015	-0.50	0.0376	0.50	0.0300
	0.0772	0.0008	0.0015	-0.40	0.0202	0.40	0.0148
	0.0772	0.0008	0.0015	-0.20	0.0033	0.20	0.0027
	0.0772	0.0008	0.0015	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0175	0.0190	0.0223	0.0237
-0.95	0.0800	0.95	0.1890	0.0154	0.0230	0.0167	0.0324
-0.90	0.1670	0.90	0.3197	0.0135	0.0277	0.0135	0.0391
-0.80	0.3360	0.80	0.5130	0.0101	0.0371	0.0091	0.0494
-0.70	0.4885	0.70	0.6505	0.0071	0.0456	0.0060	0.0568
-0.60	0.6195	0.60	0.7520	0.0047	0.0531	0.0038	0.0623
-0.50	0.7335	0.50	0.8315	0.0028	0.0599	0.0023	0.0667
-0.40	0.8265	0.40	0.8020	0.0015	0.0656	0.0011	0.0634
-0.20	0.9583	0.20	0.9750	0.0002	0.0743	0.0002	0.0755
0.00	1.0000	0.00	1.0000	0.0000	0.0772	0.0000	0.0772

Table of V1							
r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.4	0.0671	0.0007	0.0013	-1.00	0.1467	1.00	0.2181
	0.0671	0.0007	0.0013	-0.95	0.1200	0.95	0.1467
	0.0671	0.0007	0.0013	-0.90	0.0972	0.90	0.1088
	0.0671	0.0007	0.0013	-0.80	0.0630	0.80	0.0637
	0.0671	0.0007	0.0013	-0.70	0.0395	0.70	0.0357
	0.0671	0.0007	0.0013	-0.60	0.0214	0.60	0.0189
	0.0671	0.0007	0.0013	-0.50	0.0116	0.50	0.0090
	0.0671	0.0007	0.0013	-0.40	0.0044	0.40	0.0033
	0.0671	0.0007	0.0013	-0.20	0.0000	0.20	0.0000
	0.0671	0.0007	0.0013	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0096	0.0110	0.0145	0.0157
-0.95	0.0905	0.95	0.1935	0.0079	0.0152	0.0097	0.0237
-0.90	0.1810	0.90	0.3235	0.0064	0.0196	0.0072	0.0298
-0.80	0.3500	0.80	0.5220	0.0041	0.0285	0.0042	0.0399
-0.70	0.0504	0.70	0.6590	0.0026	0.0073	0.0024	0.0470
-0.60	0.6353	0.60	0.7593	0.0014	0.0445	0.0013	0.0525
-0.50	0.7525	0.50	0.8345	0.0008	0.0516	0.0006	0.0568
-0.40	0.8415	0.40	0.8933	0.0003	0.0570	0.0002	0.0603
-0.20	0.9645	0.20	0.9725	0.0000	0.0648	0.0000	0.0653
0.00	1.0000	0.00	1.0000	0.0000	0.0671	0.0000	0.0671

**Table of V1**

r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.5	0.0570	0.0006	0.0011	-1.00	0.0522	1.00	0.1278
	0.0570	0.0006	0.0011	-0.95	0.0420	0.95	0.0778
	0.0570	0.0006	0.0011	-0.90	0.0330	0.90	0.0500
	0.0570	0.0006	0.0011	-0.80	0.0190	0.80	0.0211
	0.0570	0.0006	0.0011	-0.70	0.0100	0.70	0.0085
	0.0570	0.0006	0.0011	-0.60	0.0040	0.60	0.0034
	0.0570	0.0006	0.0011	-0.50	0.0012	0.50	0.0008
	0.0570	0.0006	0.0011	-0.40	0.0000	0.40	0.0000
	0.0570	0.0006	0.0011	-0.20	0.0000	0.20	0.0000
	0.0570	0.0006	0.0011	0.00	0.0000	0.00	0.0000

**Table of V2**

<b>Table of V2</b>				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0029	0.0041	0.0072	0.0083
-0.95	0.0950	0.95	0.1750	0.0023	0.0088	0.0044	0.0153
-0.90	0.1865	0.90	0.3056	0.0018	0.0134	0.0028	0.0210
-0.80	0.3569	0.80	0.5039	0.0011	0.0221	0.0012	0.0305
-0.70	0.5140	0.70	0.6430	0.0006	0.0304	0.0005	0.0375
-0.60	0.6439	0.60	0.7478	0.0002	0.0373	0.0002	0.0431
-0.50	0.7580	0.50	0.8275	0.0001	0.0436	0.0000	0.0474
-0.40	0.8456	0.40	0.8880	0.0000	0.0484	0.0000	0.0507
-0.20	0.9639	0.20	0.9710	0.0000	0.0550	0.0000	0.0554
0.00	1.0000	0.00	1.0000	0.0000	0.0570	0.0000	0.0570

**Table of V1**

r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.6	0.0469	0.0005	0.0009	-1.00	0.0000	1.00	0.0382
	0.0469	0.0005	0.0009	-0.95	0.0000	0.95	0.0169
	0.0469	0.0005	0.0009	-0.90	0.0000	0.90	0.0067
	0.0469	0.0005	0.0009	-0.80	0.0000	0.80	0.0006
	0.0469	0.0005	0.0009	-0.70	0.0000	0.70	0.0000
	0.0469	0.0005	0.0009	-0.60	0.0000	0.60	0.0000
	0.0469	0.0005	0.0009	-0.50	0.0000	0.50	0.0000
	0.0469	0.0005	0.0009	-0.40	0.0000	0.40	0.0000
	0.0469	0.0005	0.0009	-0.20	0.0000	0.20	0.0000
	0.0469	0.0005	0.0009	0.00	0.0000	0.00	0.0000

**Table of V2**

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0000	0.0009	0.0018	0.0027
-0.95	0.0965	0.95	0.1485	0.0000	0.0054	0.0008	0.0085
-0.90	0.1885	0.90	0.2720	0.0000	0.0096	0.0003	0.0137
-0.80	0.3585	0.80	0.4620	0.0000	0.0174	0.0000	0.0222
-0.70	0.5110	0.70	0.6060	0.0000	0.0244	0.0000	0.0288
-0.60	0.6415	0.60	0.7200	0.0000	0.0304	0.0000	0.0340
-0.50	0.7530	0.50	0.8090	0.0000	0.0355	0.0000	0.0381
-0.40	0.8426	0.40	0.8790	0.0000	0.0397	0.0000	0.0413
-0.20	0.9613	0.20	0.9690	0.0000	0.0451	0.0000	0.0455
0.00	1.0000	0.00	1.0000	0.0000	0.0469	0.0000	0.0469

**Table of V1**

r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.7	0.0368	0.0004	0.0007	-1.00	0.0000	1.00	0.0000
	0.0368	0.0004	0.0007	-0.95	0.0000	0.95	0.0000
	0.0368	0.0004	0.0007	-0.90	0.0000	0.90	0.0000
	0.0368	0.0004	0.0007	-0.80	0.0000	0.80	0.0000
	0.0368	0.0004	0.0007	-0.70	0.0000	0.70	0.0000
	0.0368	0.0004	0.0007	-0.60	0.0000	0.60	0.0000
	0.0368	0.0004	0.0007	-0.50	0.0000	0.50	0.0000
	0.0368	0.0004	0.0007	-0.40	0.0000	0.40	0.0000
	0.0368	0.0004	0.0007	-0.20	0.0000	0.20	0.0000
	0.0368	0.0004	0.0007	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0000	0.0007	0.0000	0.0007
-0.95	0.0975	0.95	0.1240	0.0000	0.0043	0.0000	0.0052
-0.90	0.1900	0.90	0.2337	0.0000	0.0076	0.0000	0.0092
-0.80	0.3600	0.80	0.4140	0.0000	0.0137	0.0000	0.0157
-0.70	0.5100	0.70	0.5615	0.0000	0.0191	0.0000	0.0210
-0.60	0.6400	0.60	0.6840	0.0000	0.0238	0.0000	0.0254
-0.50	0.7500	0.50	0.7850	0.0000	0.0278	0.0000	0.0290
-0.40	0.8400	0.40	0.8660	0.0000	0.0310	0.0000	0.0320
-0.20	0.9600	0.20	0.9675	0.0000	0.0353	0.0000	0.0356
0.00	1.0000	0.00	1.0000	0.0000	0.0368	0.0000	0.0368

Table of V1							
r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.8	0.0267	0.0003	0.0005	-1.00	0.0000	1.00	0.0000
	0.0267	0.0003	0.0005	-0.95	0.0000	0.95	0.0000
	0.0267	0.0003	0.0005	-0.90	0.0000	0.90	0.0000
	0.0267	0.0003	0.0005	-0.80	0.0000	0.80	0.0000
	0.0267	0.0003	0.0005	-0.70	0.0000	0.70	0.0000
	0.0267	0.0003	0.0005	-0.60	0.0000	0.60	0.0000
	0.0267	0.0003	0.0005	-0.50	0.0000	0.50	0.0000
	0.0267	0.0003	0.0005	-0.40	0.0000	0.40	0.0000
	0.0267	0.0003	0.0005	-0.20	0.0000	0.20	0.0000
	0.0267	0.0003	0.0005	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0000	0.0005	0.0000	0.0005
-0.95	0.0975	0.95	0.1050	0.0000	0.0031	0.0000	0.0033
-0.90	0.1900	0.90	0.2028	0.0000	0.0055	0.0000	0.0058
-0.80	0.3600	0.80	0.3765	0.0000	0.0099	0.0000	0.0104
-0.70	0.5100	0.70	0.5265	0.0000	0.0139	0.0000	0.0143
-0.60	0.6400	0.60	0.6545	0.0000	0.0173	0.0000	0.0176
-0.50	0.7500	0.50	0.7635	0.0000	0.0201	0.0000	0.0205
-0.40	0.8400	0.40	0.8520	0.0000	0.0225	0.0000	0.0228
-0.20	0.9600	0.20	0.9635	0.0000	0.0256	0.0000	0.0257
0.00	1.0000	0.00	1.0000	0.0000	0.0267	0.0000	0.0267

Table of V1							
r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
0.9	0.0166	0.0002	0.0003	-1.00	0.0000	1.00	0.0000
	0.0166	0.0002	0.0003	-0.95	0.0000	0.95	0.0000
	0.0166	0.0002	0.0003	-0.90	0.0000	0.90	0.0000
	0.0166	0.0002	0.0003	-0.80	0.0000	0.80	0.0000
	0.0166	0.0002	0.0003	-0.70	0.0000	0.70	0.0000
	0.0166	0.0002	0.0003	-0.60	0.0000	0.60	0.0000
	0.0166	0.0002	0.0003	-0.50	0.0000	0.50	0.0000
	0.0166	0.0002	0.0003	-0.40	0.0000	0.40	0.0000
	0.0166	0.0002	0.0003	-0.20	0.0000	0.20	0.0000
	0.0166	0.0002	0.0003	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0000	0.0003	0.0000	0.0003
-0.95	0.0975	0.95	0.1000	0.0000	0.0019	0.0000	0.0020
-0.90	0.1900	0.90	0.1950	0.0000	0.0034	0.0000	0.0035
-0.80	0.3600	0.80	0.3660	0.0000	0.0062	0.0000	0.0063
-0.70	0.5100	0.70	0.5160	0.0000	0.0086	0.0000	0.0087
-0.60	0.6400	0.60	0.6455	0.0000	0.0107	0.0000	0.0108
-0.50	0.7500	0.50	0.7550	0.0000	0.0125	0.0000	0.0126
-0.40	0.8400	0.40	0.8450	0.0000	0.0140	0.0000	0.0140
-0.20	0.9600	0.20	0.9615	0.0000	0.0159	0.0000	0.0159
0.00	1.0000	0.00	1.0000	0.0000	0.0166	0.0000	0.0166

Table of V1							
r/R	T <sub>max</sub>	T <sub>LE</sub>	T <sub>TE</sub>	P (-)	V1	P (+)	V1
1	0.0065	0.0001	0.0001	-1.00	0.0000	1.00	0.0000
	0.0065	0.0001	0.0001	-0.95	0.0000	0.95	0.0000
	0.0065	0.0001	0.0001	-0.90	0.0000	0.90	0.0000
	0.0065	0.0001	0.0001	-0.80	0.0000	0.80	0.0000
	0.0065	0.0001	0.0001	-0.70	0.0000	0.70	0.0000
	0.0065	0.0001	0.0001	-0.60	0.0000	0.60	0.0000
	0.0065	0.0001	0.0001	-0.50	0.0000	0.50	0.0000
	0.0065	0.0001	0.0001	-0.40	0.0000	0.40	0.0000
	0.0065	0.0001	0.0001	-0.20	0.0000	0.20	0.0000
	0.0065	0.0001	0.0001	0.00	0.0000	0.00	0.0000

Table of V2				for P<0		for P>0	
P (-)	V2	P (+)	V2	Y <sub>face</sub>	Y <sub>back</sub>	Y <sub>face</sub>	Y <sub>back</sub>
-1.00	0.0000	1.00	0.0000	0.0000	0.0001	0.0000	0.0001
-0.95	0.0975	0.95	0.0975	0.0000	0.0007	0.0000	0.0007
-0.90	0.1900	0.90	0.1900	0.0000	0.0013	0.0000	0.0013
-0.80	0.3600	0.80	0.3600	0.0000	0.0024	0.0000	0.0024
-0.70	0.5100	0.70	0.5100	0.0000	0.0034	0.0000	0.0034
-0.60	0.6400	0.60	0.6400	0.0000	0.0042	0.0000	0.0042
-0.50	0.7500	0.50	0.7500	0.0000	0.0049	0.0000	0.0049
-0.40	0.8400	0.40	0.8400	0.0000	0.0054	0.0000	0.0054
-0.20	0.9600	0.20	0.9600	0.0000	0.0062	0.0000	0.0062
0.00	1.0000	0.00	1.0000	0.0000	0.0065	0.0000	0.0065

## Calculation of Propeller Shaft:

Parameters	Values	Units
Waterline Length, LWL	79.0376	m
Length Between Perpendicular, LBP	77.942	m
Breadth moulded, B	15.728	m
Draft moulded, T	3.588	m
Block Coefficient, C <sub>b</sub>	0.859	
Ship Speed, V	10	knots
Engine Power, P=	710	kW
Shaft Length,L		m
RPM	1000	
Gear Ratio	3.03	
Shaft RPM	330.0330033	rpm
Angular velocity,ω	34.56	rad/sec
Torque,T	20.54	kN-m

### Calculation of shaft diameter using theoretical formula:

We obtain of the tensile strength of steel (AISI 1018) 450 MPa

Allowable stress=450MPa

By taking the Factor of Safety 3we obtain

the Working Stress, $\tau = 150 \text{ MPa}$

So,

$$T = 20543.40174 \text{ N-m}$$

$$\tau = 150000000 \text{ Pa}$$

$$J = \pi d^4/32$$

$$C = d/2$$

$$\text{Shaft Dia, } d = 0.0886 \text{ m}$$

$$= 88.685 \text{ mm}$$

#### **Calculation using GL rule book (Part-1, Chapter-2, Section-4)**

PW (considering 2% gear loss and 3% shaft loss)=532.500KW

Tensile strength of shaft material (Forged Steel)=450N/mm<sup>2</sup>

Material factor,  $C_w = 0.918$

k (for propeller shafts with flange mounted and propeller is keyed to the tapered propeller shaft) = 1.26

F=100

$$1 - (d_i/d_a)^4 = 1$$

Diameter of the shaft,  $d = 143.630 \text{ mm}$

Diameter taken=150 mm

#### **Twisting Angle Calculation:**

Here, length of the shaft is,  $L = 3.5 \text{ m}$

Polar moment of inertia,  $J = \pi d^4/32 = 4.9701 \times 10^{-5} \text{ m}^4$

Shearing modulus of elasticity,  $G = 83 \text{ GPa}$

$$= 83000000000 \text{ Pa}$$

Torque,  $T = 20543.40174 \text{ N-m}$

Twisting angle,  $\theta = TL/GJ = 0.01743 \text{ radian}$

$$= 0.998 \text{ degree}$$

The twisting angle is  $.998^\circ$  which is less than  $1^\circ$

**Minimum wall thickness:**

Minimum wall thickness=0.03d+7.5mm= 11.809 mm

Thickness taken= 12 mm

**Coupling:**

Thickness of the coupling =0.2d= 28.726 mm

Thickness taken 30 mm

**Distance between bearings:**

K2=8400

The maximum bearing spacing= $k2 * \sqrt{\frac{d}{n}} = 5541.44$  mm

Spacing taken 5550 mm

**Stern tube bearing:**

Length of after stern tube bearing=2d=287 mm

Length of forward stern tube bearing =0.8\*d=115 mm

### List Of Materials For Propeller Shaft:

Sl. No	Description	Materials	Number of component	Dimensions (mm)
1	Cone nut	M.B. BS	1	208 (Length)
2	Cone nut securing screw	M.B. BS	2	12.5 (dia), 23 (Length)
3	Propeller key	M.B. BS	1	25(depth), 22.5(Length)
4	Propeller dia	M.B. BS	1	1960(dia) X 1570(pitch)
5	Aft. BRG . securing screw	M.B. BS	3	16 (dia), 46.5(Length)
6	Cover plate securing screw	STEEL BS	3	15.5(dia), 84.5 (Length)
7	Aft locking ring	STEEL BS	1	260 (o/d), 206 (i/d)
8	Cover plate	STEEL BS	1	260 (o/d), 165 (i/d), 70.5 (Length)
9	Lock ring securing screw	STEEL BS	3	15.5 (dia), 108 (Length)
10	Forward locking ring	STEEL BS	1	260 (o/d), 206 (i/d), 117.5 (Length)
11	Rubber bearing	RUBBER		187 (o/d), 140 (i/d)
12	Stern tube	STEEL BS	1	206 (o/d), 166 (i/d)
13	Tail shaft	FORGED STEEL	1	140 (dia)
14	Forward gland housing	G.M. BS	1	270 (o/d), 206 (i/d)
15	Forward bearing	G.M. BS	1	176 (o/d), 146.5 (i/d)
16	Greasy packing	GRAPHITED ASBESTOS	3 turns	29.4X19.4
17	Gland ring	G.M. BS	1	268 (o/d), 140 (i/d)
18	Gland studs and nuts	M.B. BS	2	44.5 (dia), 70 (Length)
19	Coupling key	STEEL BS	1	28 (depth), 315.5 (Length)
20	Half coupling	STEEL BS	1	222.5 (o/d), 140 (i/d)
21	Backing washer	STEEL BS	1	180 (o/d), 91 (i/d), 24 (thickness)
22	Locking nut	STEEL En7 BS	1	171.5 (o/d), 91 (i/d)
23	Sealing ring	BS	1	175 (o/d), 2.5 (thickness)
24	Fwd.BRG. securing screw	M.B. BS	1	53.5 (length), 28 (dia)
25	Bearing lock ring	STEEL BS	1	260 (o/d), 32.5 (Length)

## Appendix 3

### Rudder Calculation:

Lbp=77.942 m

B=15.728 m

T=3.583 m

B/Lbp =0.201

H/Lbp=0.051

LWL =79.0376 m

Block Coefficient, CB=0.847

Prismatic Coefficient, CPR=0.852

CX=0.994

CS=0.923

L/Lbp=1.014

Speed=10 knots

#### Calculation of Rudder Area: (GL-13, rules I part -1 chapter-1 Section 14 A.3)

$$\begin{aligned} A &= c_1 \times c_2 \times c_3 \times \frac{c_4}{\underline{c_4}} \frac{1.75 \times L_{WL} \times T}{100} \\ &= 1 \times 1 \times 1 \times \frac{1.75 \times 79.0376 \times 3.585}{100} \\ &= 5.26 \text{ m}^2 \end{aligned}$$

From 'Applied Naval Architecture' Munro & Smith

$$A = L \times T / 60 = 5.006 \text{ m}^2$$

From DNV rulebook,

$$\begin{aligned} A &= (T/L) / 100 * (1 + 25(B/L)^2) \\ &= 5.977 \text{ m}^2 \end{aligned}$$

Maximum Area = 5.977 m<sup>2</sup>

Area of a single rudder =2.988 m<sup>2</sup>  
Yield Str Material used -High strength steel "GL F-36" (**DNV GL Pt. 3 Chapter 14, 1.6**)

Yield strength =355 MPa

Material Factor,kr =(235/Reh)0.75 =0.734

Assuming clearance for rudder =1.000m ( Ref.**GL-13, rules I part -1 chapter-1 Section 14 A.4**)

Allowable height =3.550m

Mean height of rudder,b=2.550m

Mean Breadth,c=A/b=2.061m

#### **Calculation of Rudder Force: (GL-13, Rules-I, Part-1, Chapter-1 Section 14 D.1.1)**

**Rudder Force, CR =  $132 \times A \times V2 \times k1 \times k2 \times k3 \times kt$**

$$k1=(Aspect\ ratio+2)/3 = 1.392$$

k2 = 1.1 (Naca-00 series ahead and astern)

k3= 1

kt= 1

$$CR = 132*2.988*10*1.392*1.1*1*1*1$$

$$=60400\text{N(Ahead)}$$

$$CR=15800\text{ N(Astern)}$$

Total Ahead Force=1.21E+05 N

Total Astern Force=3.16E+04 N

#### **Calculation of Rudder Torque: (GL-13, Rules-I, Part-1, Chapter-1 Section 14 D.1.2)**

$$Q_r=C_R r$$

$$r=c(\alpha-k_b),$$

$$K_b = A_f / A,$$

$$A_f = 25\% \text{ of } A$$

Balance Factor,  $K_b = 0.25$

$\alpha = 0.33$  ( ahead)

= 0.9 (astern)

Lever,  $r = 0.16$  (ahead)

= 1.34 (astern)

$Q_r = 1.24E+04$  Nm, Ahead

= 2.12E+04 Nm, Astern

### **Calculation of Rudder Stock Diameter: GL-13, Rules-I, Part-1, Chapter-1 Section 14 E.1.1**

Material Factor  $K_r = 0.734$

Rudder Torque ,  $Q_r = 2.12E+04$  Nm, Astern

$$\begin{aligned} D_t &= 4.2(Q_r * K_r)^{1/3} \\ &= 4.2 \times (2.12E+04 \times 0.734)^{1/3} \\ &= 100 \text{ mm} \end{aligned}$$

### **Calculation Of Rudder Coupling: (GL-13, Rules-I, Part-1, Chapter-1 Section 14 F.1)**

Rudder stock diameter,  $D = 100.000$  mm

Material Factor,  $K_b = 0.734$

$K_r = 0.733887739$

No of Bolts,  $n = 6$

Mean distances of bolts,  $e = 115$  mm

$$\begin{aligned} \text{Bolt dia, } db &= 0.62 * (D^3 * K_b / K_r * n * e)^{0.5} \\ &= 25 \text{ mm} \end{aligned}$$

Flange thickness ,  $T_f = 25$  mm

Filler radius minimum 45 mm & angle 30 degree .

The minimum thickness After the bolt holes =  $0.65 * T_f = 16.466$  mm

The minimum width of the materials outside of the bolt holes =  $0.67 * db = 16.973$  mm

### **Calculation Of Pintle :GL-13, Rules-I, Part-1, Chapter-1 Section 14 G.5.1**

$$b_1 = C_r * 0.5 = 30199.703$$

$$\text{Diameter} = 0.35 * (B_1 * K_r)^{0.5}$$

$$= 52.106 \text{ mm}$$

$$T = 0.01 * (B_1)^{0.5} = 1.738 \text{ mm}$$

Or,  $T = 8 \text{ mm}$ , Whichever Is Maximum  
So,  $T = 8.000 \text{ mm}$

$$\text{Bearing Clearance} = (D_b / 1000) + 1$$

$$= 1.052 \text{ mm}$$

### **Calculation of Rudder Plates and Web: (GL-2008, Section 14, Article-2.1)**

The thickness of the Rudder Plating,  $t = 1.74 \times a \times \sqrt{(P_r \times K_r)} + 2.5 \text{ mm}$

Smaller supported width of plate panel,  $a = 0.5 \text{ m}$

$$P_r = 10T + \frac{C_R}{1000 \times a} = 58.212 \text{ kN/m}^2$$

Rudder Plate thickness  $t_p = 1.74 \times 0.5 \times \sqrt{(58.212 \times 0.734)} + 2.5 = 8.186 \text{ mm}$

Thickness considered,  $t_p = 8 \text{ mm}$

Thickness of Web  $= 0.7 \times t_p = 5.6 \text{ mm}$

Minimum thickness  $= 8\sqrt{k} = 6.853 \text{ mm}$

Thickness of the web considered  $= 7 \text{ mm}$

### **Calculation of Rudder bearing: GL-13, Rules-I, Part-1, Chapter-1 Section 14 G.5.1**

$$T_{min} = 8.000 \text{ mm}$$

$$B_1 = C_R * 0.5 = 30199.703$$

$$A_b = C_R / q = 10981.710 \quad (5.5 \text{ For Synthetic Material})$$

### **Calculation of Rudder Framing:**

Spacing of Horizontal rudder frame  $a_h = (0.2 * L / 100) + 0.40 = 558.075 \text{ mm}$

Spacing of Vertical rudder frame  $a_v = 1.5 \times a_h = 0.837 \text{ m} = 837.113 \text{ mm}$

Approximate vertical frame spacing 840 mm and horizontal frame spacing 560 mm

**Airfoil Generator:**

Chord Length,c= 2.15 m

x/c	x	x (mm)	y/c	y	y(mm)
0.000	0.000	0.000	0.044	0.095	95.030
0.013	0.027	26.875	0.032	0.068	67.854
0.025	0.054	53.750	0.044	0.094	93.654
0.050	0.108	107.500	0.059	0.127	127.366
0.100	0.215	215.000	0.078	0.168	167.786
0.150	0.323	322.500	0.089	0.192	191.565
0.200	0.430	430.000	0.096	0.206	205.583
0.250	0.538	537.500	0.099	0.213	212.893
0.300	0.645	645.000	0.100	0.215	215.000
0.400	0.860	860.000	0.097	0.208	207.948
0.450	0.968	967.500	N/A	N/A	N/A
0.500	1.075	1075.000	0.088	0.190	189.716
0.600	1.290	1290.000	0.076	0.164	163.529
0.700	1.505	1505.000	0.061	0.131	131.279
0.800	1.720	1720.000	0.044	0.094	93.998
0.900	1.935	1935.000	0.024	0.052	51.901
1.000	2.150	2150.000	0.002	0.005	4.515

## **Appendix 4**

### **Calculation of Steering Gear Arrangement :**

Rudder Torque=12,449 kN-m,ahead  
=21.186 kN-m,astern

Working Torque= $1.2 \times 21.186 = 25.423$  kN-m  
=18751.707 lbs-ft

**Steering Gear MODEL:7093-B20 (REF.Kobelt Catalogue hydraulic Steering Gear)**

Net Weight=51.4 kg  
Total Weight=120 kg

## **Appendix 5**

### **Engine Foundation Scantling (IRS, CH-6, Sec-7, 7.2)**

Maximum Power of a Engine P=710 kW  
Maximum RPM ,R=1000

Top Plate Area = $A = 20 + 120 \times \frac{P}{R} = 105.2$  cm<sup>2</sup>

Top Plate Width= $\frac{A}{tp} \times 10 = 42.903$  cm  
Width taken= 45 cm

Thickness of Top Plate=tp= 0.1A+14 mm = 24.52 mm

Thickness taken= 25 mm

Girder Web Thickness=tg=0.043A+7 mm= 11.5236 mm

Thickness taken= 12 mm

Floor Web Thickness tf= 0.02A+6 mm = 8.104 mm

Thickness taken =9 mm

Floor Depth =800 mm

Thickness of Bracket =7 mm

Bracket arm a=340 mm , b=340 mm



## Appendix 6

### Detailed Weight Calculation

#### WEIGHT OF SHELL PLATES

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u><math>m^2</math></u>	<u>mm</u>	<u>m</u>	<u><math>m^3</math></u>	<u>tonnes</u>				
			k01	6	1.2	7.2	11	0.011	0.0792	0.622	4.07	2.53	2.8	1.74
			k02	6	1.2	7.2	11	0.011	0.0792	0.622	2.46	1.53	8.28	5.15
			k03	6	1.2	7.2	11	0.011	0.0792	0.622	0.91	0.57	14.28	8.88
			k04	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	20.28	12.61
			k05	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	26.28	16.34
			k06	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	32.28	20.07
<b><u>KEEL Strake</u></b>			k07	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	38.28	23.80
			k08	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	44.28	27.53

		k09	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	50.28	31.26
		k10	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	56.28	34.99
		k11	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	62.28	38.72
		k12	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	68.28	42.45
		k13	6	1.2	7.2	11	0.011	0.0792	0.622	0.6	0.37	74.28	46.18
		k14	6	1.2	7.2	11	0.011	0.0792	0.622	0.75	0.47	78	48.49
		k15	4	1.2	4.8	11	0.011	0.0528	0.414	2.2	0.91	79.75	33.05
		k16	6	1.2	7.2	11	0.011	0.0792	0.622	4.83	3.00	79.38	49.35

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>	
				<u>m</u>	<u>m</u>	<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>					
<b><u>Garboard Strake</u></b>				A01	2	2	4	10	0.01	0.04	0.314	2.22	0.70	16.25	5.10
				A02	6	2	12	10	0.01	0.12	0.942	2.2	2.07	20.18	19.01
				A03	6	2	12	10	0.01	0.12	0.942	2.2	2.07	26.18	24.66
				A04	6	2	12	10	0.01	0.12	0.942	2.2	2.07	32.18	30.31
				A05	6	2	12	10	0.01	0.12	0.942	2.2	2.07	38.18	35.97
				A06	6	2	12	10	0.01	0.12	0.942	2.2	2.07	44.18	41.62
				A07	6	2	12	10	0.01	0.12	0.942	2.2	2.07	50.18	47.27
				A08	6	2	12	10	0.01	0.12	0.942	2.2	2.07	56.18	52.92
				A09	6	2	12	10	0.01	0.12	0.942	2.2	2.07	62.18	58.57
<b>A Strake</b>				A10	6	2	12	10	0.01	0.12	0.942	2.2	2.07	68.18	64.23
				A11	1	4	4.57	10	0.01	0.0457	0.3587	2.07	0.74	71.4	25.61

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG from keel</u>	<u>Moment from Base</u>	<u>LCG from aft</u>	<u>Moment from aft</u>	
				<u>m</u>	<u>m</u>	<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>					
<b><u>Garboard Strake</u></b>				B01	2	2	4	10	0.01	0.04	0.314	4.18	1.313	16.34	5.13
				B02	6	2	12	10	0.01	0.12	0.942	4.2	3.956	20.22	19.05
				B03	6	2	12	10	0.01	0.12	0.942	4.2	3.956	26.22	24.70
				B04	6	2	12	10	0.01	0.12	0.942	4.2	3.956	32.22	30.35
				B05	6	2	12	10	0.01	0.12	0.942	4.2	3.956	38.22	36.00
				B06	6	2	12	10	0.01	0.12	0.942	4.2	3.956	44.22	41.66
<b><u>B Strake</u></b>				B07	6	2	12	10	0.01	0.12	0.942	4.2	3.956	50.22	47.31
				B08	6	2	12	10	0.01	0.12	0.942	4.2	3.956	56.22	52.96
				B09	6	2	12	10	0.01	0.12	0.942	4.2	3.956	62.22	58.61
			B10	6	2.3	8.34	10	0.01	0.083	0.655	4.05	2.651	67	43.86	
				<u>Dimensions</u>			<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG from</u>	<u>Moment from Base</u>	<u>LCG from</u>	<u>Moment from aft</u>

									<u>keel</u>		<u>aft</u>			
				<u>m</u>	<u>m</u>	<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>				
<b><i>Garboard Strake</i></b>			C01	1.55	1	1.55	10	0.01	0.016	0.122	5.5	0.669	16.7	2.032
<b><i>C Strake</i></b>			C02	6	1.4	8.4	10	0.01	0.084	0.659	5.75	3.792	20.52	13.531
<b><i>C Strake</i></b>			C03	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	26.52	17.487
<b><i>C Strake</i></b>			C04	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	32.52	21.444
<b><i>C Strake</i></b>			C05	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	38.52	25.400
<b><i>C Strake</i></b>			C06	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	44.52	29.356
<b><i>C Strake</i></b>			C07	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	50.52	33.313
<b><i>C Strake</i></b>			C08	6	1.4	8.4	10	0.01	0.084	0.659	5.76	3.798	56.52	37.269
<b><i>C Strake</i></b>			C09	6	1.4	8.1	10	0.01	0.081	0.636	5.74	3.650	62.52	39.753
			C10	2.5	0.7	0.8225	10	0.01	0.008	0.065	5.4	0.349	65.52	4.230

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>	
				<u>m</u>	<u>m</u>	<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>					
<b><u>Bilge Strake</u></b>				D01	3	1.5	4.5	10	0.01	0.045	0.353	3	1.060	14.46	5.108
				D02	5	1.25	6.25	10	0.01	0.0625	0.491	6.6	3.238	16.14	7.919
				D03	6	1.25	7.5	10	0.01	0.075	0.589	7.01	4.127	20.86	12.281
				D04	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	26.86	15.814
				D05	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	32.86	19.346
				D06	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	38.86	22.879
<b><u>D Strake</u></b>				D07	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	44.86	26.411
				D08	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	50.86	29.944
				D09	6	1.25	7.5	10	0.01	0.075	0.589	7.2	4.239	56.86	33.476
				D10	6	1.25	7.5	10	0.01	0.075	0.589	6.74	3.968	62.86	37.009
				D11	6	1.25	7.5	10	0.01	0.075	0.589	4.86	2.861	68.86	40.541
			D12	3.5	1.25	4.54	10	0.01	0.0454	0.356	2.3	0.820	73.75	26.284	

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from keel</u>	<u>Moment</u> <u>from Base</u>	<u>LCG</u> <u>from aft</u>	<u>Moment</u> <u>from aft</u>	
				<u>m</u>	<u>m</u>	<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>					
<b><u>Side Shell</u></b>				E01	4	2	7.87	10	0.01	0.079	0.618	3.83	2.366	12.8	7.908
				E02	5	2	9.89	10	0.01	0.099	0.776	7.4	5.745	15.2	11.801
				E03	6	2	12	10	0.01	0.12	0.942	8.6	8.101	20.5	19.311
				E04	6	2	12	10	0.01	0.12	0.942	8.7	8.195	26.5	24.963
				E05	6	2	12	10	0.01	0.12	0.942	8.7	8.195	32.5	30.615
				E06	6	2	12	10	0.01	0.12	0.942	8.7	8.195	38.5	36.267
				E07	6	2	12	10	0.01	0.12	0.942	8.7	8.195	44.5	41.919
				E08	6	2	12	10	0.01	0.12	0.942	8.7	8.195	50.5	47.571
<b><u>E Strake</u></b>				E09	6	2	12	10	0.01	0.12	0.942	8.7	8.195	56.5	53.223
				E10	6	2	12	10	0.01	0.12	0.942	8.5	8.007	62.5	58.875
				E11	6	2	12	10	0.01	0.12	0.942	7.03	6.622	68.2	64.244
				E12	6	2	12	10	0.01	0.12	0.942	3.92	3.693	73.16	68.917

	E13	4	2	4.5	10	0.01	0.045	0.353	2.05	0.724	77	27.200
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				<u>Dimensions</u>	<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG from keel</u>	<u>Moment from Base</u>	<u>LCG from aft</u>	<u>Moment from aft</u>	
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><i>F Strake</i></b>	F01	6	2	12		10		0.01	0.12	0.942	5.5	5.181	11.32	10.663
	F02	6	2	12		10		0.01	0.12	0.942	9.46	8.911	15	14.130
	F03	6	2	12		10		0.01	0.12	0.942	10.61	9.995	20.6	19.405
	F04	6	2	12		10		0.01	0.12	0.942	10.61	9.995	26.6	25.057
	F05	6	2	12		10		0.01	0.12	0.942	10.61	9.995	32.6	30.709
	F06	6	2	12		10		0.01	0.12	0.942	10.61	9.995	38.6	36.361
	F07	6	2	12		10		0.01	0.12	0.942	10.61	9.995	44.6	42.013
	F08	6	2	12		10		0.01	0.12	0.942	10.61	9.995	50.6	47.665
	F09	6	2	12		10		0.01	0.12	0.942	10.61	9.995	56.6	53.317
	F10	6	2	12		10		0.01	0.12	0.942	10.45	9.844	62.6	58.969

F11	6	2	12	10	0.01	0.12	0.942	9	8.478	68	64.056
F12	6	2	12	10	0.01	0.12	0.942	5.86	5.520	73.2	68.954
F13	3.5	2	7.15	10	0.01	0.0715	0.561	3.6	2.021	77.5	43.499

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from keel</u>	<u>Moment</u> <u>from Base</u>	<u>LCG</u> <u>from aft</u>	<u>Moment</u> <u>from aft</u>	
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>					
<b><u>G Strake</u></b>				G01	3	2	6	10	0.01	0.06	0.471	4.45	2.096	8.42	3.966
				G02	6	2	12	10	0.01	0.12	0.942	7.91	7.451	10.6	9.985
				G03	6	1.5	11	10	0.01	0.11	0.864	11.07	9.559	14.5	12.521
				G04	6	0.8	5.16	10	0.01	0.05	0.405	11.9	4.820	20.34	8.239
				G05	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	26.34	8.684
				G06	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	32.34	10.662
				G07	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	38.34	12.641
				G08	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	44.34	14.619
				G09	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	50.34	16.597
				G10	6	0.7	4.2	10	0.01	0.04	0.330	11.95	3.940	56.34	18.575
				G11	6	1	6.3	10	0.01	0.06	0.495	11.8	5.836	62.34	30.830
				G12	6	2	12	10	0.01	0.12	0.942	10.7	10.079	68.4	64.433

	G13	6	2	12	10	0.01	0.12	0.942	7.85	7.395	73.15	68.907
	G14	4	2	8	10	0.01	0.08	0.628	5.73	3.598	77.31	48.551

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>	
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>					
<b><u>H Strake</u></b>				H01	6	2	12	10	0.01	0.12	0.94	5.88	5.54	7.25	6.83
				H02	6	2	12	10	0.01	0.12	0.94	9.57	9.01	10.4	9.80
				H03	5	1.2	3	10	0.01	0.03	0.24	11.53	2.72	69.82	16.44
				H04	6	2	12	10	0.01	0.12	0.94	9.54	8.99	73.5	69.24
				H05	3.75	1.7	3.2	10	0.01	0.032	0.25	7.77	1.95	77.5	19.47

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from keel</u>	<u>Moment</u> <u>from Base</u>	<u>LCG</u> <u>from aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>I Strake</u></b>			I01	6	2	12	10	0.01	0.12	0.94	6.47	6.09	5.8	5.46
<b><u>I Strake</u></b>			I02	6	1.5	9	10	0.01	0.09	0.71	9.98	7.05	8.84	6.25

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from keel</u>	<u>Moment</u> <u>from Base</u>	<u>LCG</u> <u>from aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>J Strake</u></b>			J01	2	2	4	10	0.01	0.04	0.314	5.32	1.670	3.84	1.206
<b><u>J Strake</u></b>			J02	3.5	2	7	10	0.01	0.07	0.550	7.82	4.297	5.05	2.775
<b><u>J Strake</u></b>			J03	3.75	2	7.5	10	0.01	0.075	0.589	10.02	5.899	7.15	4.210

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>L Strake</u></b>		L01	3.75	2	7.5	10	0.01	0.075	0.589	6.52	3.84	2.85	1.68	
<b><u>L Strake</u></b>		L02	3.75	2	7.5	10	0.01	0.075	0.589	9.26	5.45	4.24	2.50	

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>M Strake</u></b>		M01	2	2	4	10	0.01	0.04	0.314	6.36	1.997	1.01	0.317	
<b><u>M Strake</u></b>		M02	4.5	2	9	10	0.01	0.09	0.707	8.8	6.217	2.01	1.420	

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>N Strake</u></b>		N01	3.5	0.5	0.875	10	0.01	0.00875	0.069	8.22	0.565	0.35	0.024	

				<u>Dimensions</u>		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from aft</u>
				<u>m</u>	<u>m</u>	<u>m2</u>	<u>mm</u>	<u>m</u>	<u>m3</u>	<u>tonnes</u>				
<b><u>Sheer Strake</u></b>	S01	1.75	0.5	0.875	11	0.011	0.0096	0.076	9.28	0.701	0.582	0.044		
	S02	6	0.5	3	11	0.011	0.0330	0.259	11	2.850	3.870	1.003		
	S03	6	0.5	3	11	0.011	0.0330	0.259	11.54	2.989	9.820	2.544		
	S04	6	0.5	3	11	0.011	0.0330	0.259	12.3	3.186	15.820	4.098		

S05	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	21.820	5.652
S06	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	27.820	7.207
S07	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	33.820	8.761
S08	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	39.820	10.315
S09	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	45.820	11.870
S10	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	51.820	13.424
S11	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	57.820	14.978
S12	6	0.5	3	11	0.011	0.0330	0.259	12.64	3.274	63.820	16.533
S13	6	0.5	3	11	0.011	0.0330	0.259	12.38	3.207	68.453	17.733
S14	6	0.5	3	11	0.011	0.0330	0.259	10.8	2.798	73.440	19.025
S15	5	0.5	2.5	11	0.011	0.0275	0.216	8.01	1.729	77.600	16.752

**The sum of total weight= 164.74 tonnes**

### WEIGHT OF Other Plates

		<u>Area</u>	<u>Thickness</u>	<u>Thickness</u>	<u>Volume</u>	<u>Weight</u>	<u>VCG</u> <u>from</u> <u>keel</u>	<u>Moment</u> <u>from</u> <u>Base</u>	<u>LCG</u> <u>from</u> <u>aft</u>	<u>Moment</u> <u>from</u> <u>aft</u>
		<u>m<sup>2</sup></u>	<u>mm</u>	<u>m</u>	<u>m<sup>3</sup></u>	<u>tonnes</u>				
<b>Inner bottom</b>		818.55	9	0.009	7.37	57.83	0.87	50.31	47.7	2758.52
<b>Hatch cover 1</b>		368	9	0.009	3.31	29.81	7.02	209.25	34.4	1025.40
<b>Hatch cover 2</b>		178.25	9	0.009	1.60	14.44	7.02	101.36	62.24	898.64
<b>Main deck Parallel middle body(without hatch cover)</b>		272.3	9	0.008	2.18	19.61	7.02	137.63		
<b>Main deck aft</b>		230	9	0.008	1.84	16.56	7.02	116.25	8.18	135.46
<b>Main deck fwd</b>		76.97	9	0.008	0.62	5.54	7.02	38.90	74.53	413.03
<b>Hatch Coaming Plate</b>		50.71	9	0.009	0.46	4.11	6.115	25.12	42.96	176.46
<b>Shell plate behind</b>		15.64	10	0.01	0.16	1.56	6	9.39	0	0.00
<b>Superstructure</b>										
<b>Poop deck</b>	deck	170	8	0.008	1.36	10.68	9.35	99.82	6.08	64.91

	side plate1	51.22	5	0.005	0.26	2.01	7.35	14.78	0	0.00
	side plate2	94.56	5	0.005	0.47	3.71	7.35	27.28	5.92	21.97
	side plate3	61.07	5	0.005	0.31	2.40	7.35	17.62	11.83	28.36
Pilot deck	deck	70.17	8	0.008	0.56	4.41	12	52.88	7.87	34.68
	side plate 1	22.60	5	0.005	0.11	0.89	10.64	9.44	3.79	3.36
	side plate 2	42.54	5	0.005	0.21	1.67	10.64	17.77	7.87	13.14
	side plate 3	22.60	5	0.005	0.11	0.89	10.64	9.44	11.84	10.50
Bridge deck	deck	109.54	8	0.008	0.88	6.88	14.45	99.40	4.9	33.71
	side 1	24.23	4	0.004	0.10	0.76	13.2	10.04	3.79	2.88
	side 2	45	4	0.004	0.18	1.41	13.2	18.65	7.87	11.12
	side 3	43.85	4	0.004	0.18	1.38	13.2	18.17	11.84	16.30
Bridge deck top	deck	38.18	8	0.008	0.31	2.40	17.2	41.24	10.46	25.08

	side1	21.36	4	0.004	0.09	0.67	15	10.06	7.86	5.27
	side2	24.5	4	0.004	0.10	0.77	15	11.54	10.46	8.05
	side3	18.4	4	0.004	0.07	0.58	15	8.67	13.07	7.55
Forecastle	deck	71.9	9	0.009	0.65	5.08	8.62	43.79	74.5	378.44
	side plate	55	6	0.006	0.33	2.59	6.9	17.87	74.5	192.99
Bulwark	side plate	144.5	6	0.006	0.87	6.81	6.42	43.69	42.04	286.12
Void tank		82	11	0.011	0.90	7.08	1.1263	7.97	7.6644	54.27
Machinery space floor plate		149.62	9	0.009	1.35	10.57	0.87	9.20	11.14	102.45

**Total Weight of Steel Plates = 418.98 tonnes**

## Weight of Structural Members

### Bottom Strengthening Member

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
Bottom Center Girder	1	74.891	0.00855	0.640	5.026	37.446	188.220	0.405	2.033
Bottom Side Girder (Port)	4	74.891	0.00855	0.640	20.106	37.446	752.879	0.405	8.133
Bottom Side Girder (Starboard)	4	74.891	0.00855	0.640	20.106	37.446	752.879	0.405	8.133
Floors(Aft)	1	13.490	0.00855	0.115	0.905	0.233	0.211	4.203	3.805
	1	15.218	0.00855	0.130	1.021	8.308	8.486	0.405	0.413
	1	15.542	0.00855	0.133	1.043	10.908	11.379	0.405	0.422
	1	15.700	0.00855	0.134	1.054	13.508	14.234	0.405	0.426
Floors(Parallel Middle body)	1	15.724	0.00855	0.134	1.055	18.058	19.058	0.405	0.427
	1	15.724	0.00855	0.134	1.055	20.658	21.802	0.405	0.427
	1	15.724	0.00855	0.134	1.055	23.258	24.545	0.405	0.427

	1	15.724	0.00855	0.134	1.055	25.858	27.289	0.405	0.427
	1	15.724	0.00855	0.134	1.055	28.458	30.033	0.405	0.427
	1	15.724	0.00855	0.134	1.055	31.058	32.777	0.405	0.427
	1	15.724	0.00855	0.134	1.055	33.658	35.521	0.405	0.427
	1	15.724	0.00855	0.134	1.055	36.258	38.265	0.405	0.427
	1	15.724	0.00855	0.134	1.055	38.858	41.009	0.405	0.427
	1	15.724	0.00855	0.134	1.055	41.458	43.753	0.405	0.427
	1	15.724	0.00855	0.134	1.055	44.058	46.497	0.405	0.427
	1	15.724	0.00855	0.134	1.055	46.658	49.241	0.405	0.427
	1	15.724	0.00855	0.134	1.055	49.258	51.985	0.405	0.427
	1	15.724	0.00855	0.134	1.055	51.858	54.729	0.405	0.427
	1	15.724	0.00855	0.134	1.055	54.458	57.473	0.405	0.427
	1	15.724	0.00855	0.134	1.055	57.058	60.216	0.405	0.427
	1	15.724	0.00855	0.134	1.055	59.658	62.960	0.405	0.427
	1	15.724	0.00855	0.134	1.055	62.258	65.704	0.405	0.427

	1	15.724	0.00855	0.134	1.055	64.858	68.448	0.405	0.427
	1	15.724	0.00855	0.134	1.055	67.458	71.192	0.405	0.427
Floors(Forward)	1	15.604	0.00855	0.133	1.047	70.058	73.372	0.405	0.424
	1	11.296	0.00855	0.097	0.758	76.458	57.967	0.405	0.307
	1	7.316	0.00855	0.063	0.491	78.858	38.722	0.405	0.199

## Side Strengthening Member

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
Side Stringer 1	1	76.0245	0.006656	0.506	3.972	38.01225	150.994	2.314	9.191
Side Stringer 2	1	78.5394	0.006656	0.523	4.104	39.2697	161.149	3.849	15.794
Web Frames(AFT)	1	1.25	0.006656	0.008	0.065	0.233	0.015	5.971	0.390
	1	4.653	0.006656	0.031	0.243	8.308	2.020	2.327	0.566
	1	4.632	0.006656	0.031	0.242	10.908	2.640	2.327	0.563
	1	4.632	0.006656	0.031	0.242	13.508	3.269	2.327	0.563
Web Frames(parallel Middle body)	1	4.618	0.006656	0.031	0.241	18.058	4.357	2.327	0.561
	1	4.618	0.006656	0.031	0.241	20.658	4.985	2.327	0.561
	1	4.618	0.006656	0.031	0.241	23.258	5.612	2.327	0.561
	1	4.618	0.006656	0.031	0.241	25.858	6.239	2.327	0.561
	1	4.618	0.006656	0.031	0.241	28.458	6.867	2.327	0.561
	1	4.618	0.006656	0.031	0.241	31.058	7.494	2.327	0.561

	1	4.618	0.006656	0.031	0.241	33.658	8.121	2.327	0.561
	1	4.618	0.006656	0.031	0.241	36.258	8.749	2.327	0.561
	1	4.618	0.006656	0.031	0.241	38.858	9.376	2.327	0.561
	1	4.618	0.006656	0.031	0.241	41.458	10.003	2.327	0.561
	1	4.618	0.006656	0.031	0.241	44.058	10.631	2.327	0.561
	1	4.618	0.006656	0.031	0.241	46.658	11.258	2.327	0.561
	1	4.618	0.006656	0.031	0.241	49.258	11.885	2.327	0.561
	1	4.618	0.006656	0.031	0.241	51.858	12.513	2.327	0.561
	1	4.618	0.006656	0.031	0.241	54.458	13.140	2.327	0.561
	1	4.618	0.006656	0.031	0.241	57.058	13.767	2.327	0.561
	1	4.618	0.006656	0.031	0.241	59.658	14.395	2.327	0.561
	1	4.618	0.006656	0.031	0.241	62.258	15.022	2.327	0.561
	1	4.618	0.006656	0.031	0.241	64.858	15.649	2.327	0.561
	1	4.618	0.006656	0.031	0.241	67.458	16.277	2.327	0.561
Web Frames Forward	1	4.618	0.006656	0.031	0.241	70.058	16.904	2.327	0.561

	1	4.618	0.006656	0.031	0.241	76.458	18.448	2.327	0.561
	1	4.618	0.006656	0.031	0.241	78.858	19.028	2.327	0.561
Ordinary Frames(AFT)	1	1.95	0.002832	0.006	0.043	0.827	0.036	4.449	0.193
	1	1.95	0.002832	0.006	0.043	1.477	0.064	4.449	0.193
	1	1.95	0.002832	0.006	0.043	2.127	0.092	4.449	0.193
	1	1.95	0.002832	0.006	0.043	2.777	0.120	4.449	0.193
	1	1.95	0.002832	0.006	0.043	3.427	0.149	4.449	0.193
	14	4.632	0.002832	0.013	0.142	2.316	3.339	2.327	3.354
Ordinary Frames(Parallel Middle Body)	1	4.632	0.002832	0.013	0.103	16.63	1.712	2.327	0.240
	1	4.632	0.002832	0.013	0.103	17.28	1.779	2.327	0.240
	1	4.632	0.002832	0.013	0.103	18.58	1.913	2.327	0.240
	1	4.632	0.002832	0.013	0.103	19.23	1.980	2.327	0.240
	1	4.632	0.002832	0.013	0.103	19.88	2.047	2.327	0.240
	1	4.632	0.002832	0.013	0.103	20.53	2.114	2.327	0.240
	1	4.632	0.002832	0.013	0.103	21.83	2.248	2.327	0.240

	1	4.632	0.002832	0.013	0.103	22.48	2.315	2.327	0.240
	1	4.632	0.002832	0.013	0.103	23.13	2.382	2.327	0.240
	1	4.632	0.002832	0.013	0.103	23.78	2.449	2.327	0.240
	1	4.632	0.002832	0.013	0.103	25.08	2.583	2.327	0.240
	1	4.632	0.002832	0.013	0.103	25.73	2.650	2.327	0.240
	1	4.632	0.002832	0.013	0.103	26.38	2.716	2.327	0.240
	1	4.632	0.002832	0.013	0.103	27.03	2.783	2.327	0.240
	1	4.632	0.002832	0.013	0.103	28.33	2.917	2.327	0.240
	1	4.632	0.002832	0.013	0.103	28.98	2.984	2.327	0.240
	1	4.632	0.002832	0.013	0.103	29.63	3.051	2.327	0.240
	1	4.632	0.002832	0.013	0.103	30.28	3.118	2.327	0.240
	1	4.632	0.002832	0.013	0.103	31.58	3.252	2.327	0.240
	1	4.632	0.002832	0.013	0.103	32.23	3.319	2.327	0.240
	1	4.632	0.002832	0.013	0.103	32.88	3.386	2.327	0.240
	1	4.632	0.002832	0.013	0.103	33.53	3.453	2.327	0.240

	1	4.632	0.002832	0.013	0.103	34.83	3.587	2.327	0.240
	1	4.632	0.002832	0.013	0.103	35.48	3.654	2.327	0.240
	1	4.632	0.002832	0.013	0.103	36.13	3.720	2.327	0.240
	1	4.632	0.002832	0.013	0.103	36.78	3.787	2.327	0.240
	1	4.632	0.002832	0.013	0.103	38.08	3.921	2.327	0.240
	1	4.632	0.002832	0.013	0.103	38.73	3.988	2.327	0.240
	1	4.632	0.002832	0.013	0.103	39.38	4.055	2.327	0.240
	1	4.632	0.002832	0.013	0.103	40.03	4.122	2.327	0.240
	1	4.632	0.002832	0.013	0.103	41.33	4.256	2.327	0.240
	1	4.632	0.002832	0.013	0.103	41.98	4.323	2.327	0.240
	1	4.632	0.002832	0.013	0.103	42.63	4.390	2.327	0.240
	1	4.632	0.002832	0.013	0.103	43.28	4.457	2.327	0.240
	1	4.632	0.002832	0.013	0.103	44.58	4.591	2.327	0.240
	1	4.632	0.002832	0.013	0.103	45.23	4.658	2.327	0.240
	1	4.632	0.002832	0.013	0.103	45.88	4.724	2.327	0.240

	1	4.632	0.002832	0.013	0.103	46.53	4.791	2.327	0.240
	1	4.632	0.002832	0.013	0.103	47.83	4.925	2.327	0.240
	1	4.632	0.002832	0.013	0.103	48.48	4.992	2.327	0.240
	1	4.632	0.002832	0.013	0.103	49.13	5.059	2.327	0.240
	1	4.632	0.002832	0.013	0.103	49.78	5.126	2.327	0.240
	1	4.632	0.002832	0.013	0.103	51.08	5.260	2.327	0.240
	1	4.632	0.002832	0.013	0.103	51.73	5.327	2.327	0.240
	1	4.632	0.002832	0.013	0.103	52.38	5.394	2.327	0.240
	1	4.632	0.002832	0.013	0.103	53.03	5.461	2.327	0.240
	1	4.632	0.002832	0.013	0.103	54.33	5.595	2.327	0.240
	1	4.632	0.002832	0.013	0.103	54.98	5.662	2.327	0.240
	1	4.632	0.002832	0.013	0.103	55.63	5.728	2.327	0.240
	1	4.632	0.002832	0.013	0.103	56.28	5.795	2.327	0.240
	1	4.632	0.002832	0.013	0.103	57.58	5.929	2.327	0.240
	1	4.632	0.002832	0.013	0.103	58.23	5.996	2.327	0.240

	1	4.632	0.002832	0.013	0.103	58.88	6.063	2.327	0.240
	1	4.632	0.002832	0.013	0.103	59.53	6.130	2.327	0.240
	1	4.632	0.002832	0.013	0.103	60.83	6.264	2.327	0.240
	1	4.632	0.002832	0.013	0.103	61.48	6.331	2.327	0.240
	1	4.632	0.002832	0.013	0.103	62.13	6.398	2.327	0.240
	1	4.632	0.002832	0.013	0.103	62.78	6.465	2.327	0.240
	1	4.632	0.002832	0.013	0.103	64.08	6.599	2.327	0.240
	1	4.632	0.002832	0.013	0.103	64.73	6.666	2.327	0.240
	1	4.632	0.002832	0.013	0.103	65.38	6.733	2.327	0.240
	1	4.632	0.002832	0.013	0.103	66.03	6.799	2.327	0.240
	1	4.632	0.002832	0.013	0.103	67.33	6.933	2.327	0.240
Ordinary Frames Forward	1	4.632	0.002832	0.013	0.103	71.87	7.401	2.327	0.240
	1	4.632	0.002832	0.013	0.103	72.52	7.468	2.327	0.240
	1	4.632	0.002832	0.013	0.103	73.82	7.602	2.327	0.240
	1	4.632	0.002832	0.013	0.103	74.47	7.669	2.327	0.240

	1	4.632	0.002832	0.013	0.103	75.77	7.802	2.327	0.240
	1	4.632	0.002832	0.013	0.103	76.42	7.869	2.327	0.240
	1	4.632	0.002832	0.013	0.103	77.72	8.003	2.327	0.240
	1	4.632	0.002832	0.013	0.103	78.37	8.070	2.327	0.240
	1	4.632	0.002832	0.013	0.103	79.02	8.137	2.327	0.240
	1	4.632	0.002832	0.013	0.103	80.32	8.271	2.327	0.240
	1	4.632	0.002832	0.013	0.103	80.97	8.338	2.327	0.240

## Deck Strengthening Member

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volum e (m <sup>3</sup> )	weigh t (ton)	LCG(m )	LCG moment from aft	VCG	VCG moment from baseline
<b>Main Deck</b>									
Deck Center Girder	1	81.16	0.0036	0.292	2.294	40.58	93.074	5.2	11.927
Deeck Side Girder 1	2	31.8986	0.0036	0.115	1.803	40.58	73.162	5.2	9.375
Deck Side Girder 2	2	30.6103	0.0036	0.110	1.730	40.58	70.207	5.2	8.996
Deck Side Girder 3	2	28.6056	0.0036	0.103	1.617	40.58	65.609	5.2	8.407
Deck Side Girder 4	2	70.646	0.0036	0.254	3.993	40.58	162.032	5.2	20.763
Deck Web Beam	1	13.49	0.00153125	0.021	0.162	0.233	0.038	5.2	0.843
	1	15.218	0.00153125	0.023	0.183	8.308	1.520	5.2	0.951
	1	15.542	0.00153125	0.024	0.187	10.908	2.038	5.2	0.971

	1	15.7	0.0015312 5	0.024	0.189	13.508	2.549	5.2	0.981
	1	15.724	0.0015312 5	0.024	0.189	18.058	3.413	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	20.658	3.905	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	23.258	4.396	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	25.858	4.887	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	28.458	5.379	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	31.058	5.870	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	33.658	6.362	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	36.258	6.853	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	38.858	7.344	5.2	0.983

	1	15.724	0.0015312 5	0.024	0.189	41.458	7.836	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	44.058	8.327	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	46.658	8.819	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	49.258	9.310	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	51.858	9.802	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	54.458	10.293	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	57.058	10.784	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	59.658	11.276	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	62.258	11.767	5.2	0.983
	1	15.724	0.0015312 5	0.024	0.189	64.858	12.259	5.2	0.983

	1	15.724	0.0015312 5	0.024	0.189	67.458	12.750	5.2	0.983
	1	15.604	0.0015312 5	0.024	0.188	70.058	13.140	5.2	0.975
	1	11.296	0.0015312 5	0.017	0.136	76.458	10.382	5.2	0.706
	1	7.316	0.0015312 5	0.011	0.088	78.858	6.935	5.2	0.457

## Superstructure

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
<b>Poop Deck</b>									
Deck Center girder	1	16.326	0.0036	0.059	0.461	8.163	3.766	9.16	4.226
Deeck Side Girder 1	2	16.326	0.0036	0.059	0.923	8.163	7.532	9.16	8.452
Deck Side Girder 2	2	16.326	0.0036	0.059	0.923	8.163	7.532	9.16	8.452
Deck Side Girder 3	2	16.326	0.0036	0.059	0.923	8.163	7.532	9.16	8.452
Deck Side Girder 4	2	13.206	0.0036	0.048	0.746	6.603	4.928	9.16	6.837
Deck Beam	1	13.2	0.00153125	0.020	0.159	0.204	0.032	9.16	1.453
	1	14.94	0.00153125	0.023	0.180	8.17	1.467	9.16	1.645
	1	15.3564	0.00153125	0.024	0.185	10.77	1.988	9.16	1.691
	1	15.58	0.00153125	0.024	0.187	13.67	2.560	9.16	1.715
Stiffener	2	16.326	0.002832	0.046	0.726	8.163	5.925	6.7	4.863
	2	16.326	0.002832	0.046	0.726	8.163	5.925	8.04	5.836

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
<b>Pilot Deck</b>									
Deck Center girder	1	11.9	0.0036	0.0428	0.3363	9.75	3.279	11.8	3.968
Deeck Side Girder 1	2	11.9	0.0036	0.0428	0.6726	9.75	6.558	11.8	7.937
Deck Side Girder 2	2	11.9	0.0036	0.0428	0.6726	9.75	6.558	11.8	7.937
Deck Side Girder 3	2	11.9	0.0036	0.0428	0.6726	9.75	6.558	11.8	7.937
Deck Side Girder 4	2	9.73	0.0036	0.0350	0.5499	10	5.499	11.8	6.489
Deck Beam	1	6.9	0.00153125	0.0106	0.0829	5.56	0.461	11.8	0.979
	1	7.2	0.00153125	0.0110	0.0865	8.16	0.706	11.8	1.021
	1	7.4	0.00153125	0.0113	0.0890	10.76	0.957	11.8	1.050
	1	7.7	0.00153125	0.0118	0.0926	13.36	1.237	11.8	1.092
Stiffener	2	11.9	0.001152	0.0137	0.2152	9.75	2.098	10.51	2.262

	2	11.9	0.001152	0.0137	0.2152	9.75	2.098	11.135	2.397
	2	11.9	0.001152	0.0137	0.2152	9.75	2.098	11.76	2.531

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
<b>Bridge Deck</b>									
Deck Center girder	1	9.4	0.0036	0.034	0.266	8.5	2.258	14.3	3.799
Deeck Side Girder 1	2	9.4	0.0036	0.034	0.531	8.5	4.516	14.3	7.597
Deck Side Girder 2	2	9.4	0.0036	0.034	0.531	8.5	4.516	14.3	7.597
Deck Side Girder 3	2	9.4	0.0036	0.034	0.531	8.5	4.516	14.3	7.597
Deck Side Girder 4	2	1.95	0.0036	0.007	0.110	9	0.992	14.3	1.576
Deck Beam	1	9.28	0.00153125	0.014	0.112	6.83	0.762	14.3	1.595
	1	9.28	0.00153125	0.014	0.112	9.43	1.052	14.3	1.595
	1	9.28	0.00153125	0.014	0.112	12.03	1.342	14.3	1.595

stiffener	2	9.4	0.001152	0.011	0.170	8.5	1.445	12.55	2.134
	2	9.4	0.001152	0.011	0.170	8.5	1.445	13.175	2.240
	2	9.4	0.001152	0.011	0.170	8.5	1.445	13.8	2.346

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
<b>Bridge Deck Top</b>									
Deck Center Girder	1	5.207	0.0036	0.019	0.147	10.7	1.575	17.2	2.531
Deck Side Girder 1	2	5.207	0.0036	0.019	0.294	10.7	3.149	17.2	5.062
Deck Side Girder 2	2	4.6	0.0036	0.017	0.260	10.4	2.704	17.2	4.472
Deck Beam 1	1	7.52	0.00153125	0.012	0.090	9.72	0.879	17.2	1.555
	1	7.52	0.00153125	0.012	0.090	12.32	1.114	17.2	1.555
stiffener	2	5.207	0.001152	0.006	0.094	10.7	1.008	15.12	1.424
	2	5.207	0.001152	0.006	0.094	10.7	1.008	15.75	1.483
	2	5.207	0.001152	0.006	0.094	10.7	1.008	16.4	1.544

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
<b>Forcastle Deck</b>									
Deck Center Girder	1	10.66	0.0036	0.038	0.301	75.83	22.844	8.4	2.531
Deeck Side Girder 1	2	10.32	0.0036	0.037	0.583	75.66	44.131	8.4	4.900
Deck Side Girder 2	2	7.78	0.0036	0.028	0.440	74.39	32.711	8.4	3.694
Deck Side Girder 3	2	6.1	0.0036	0.022	0.345	73.55	25.358	8.4	2.896
Deck Side Girder 4	2	3.16	0.0036	0.011	0.179	72.08	12.874	8.4	1.500
Deck Beam 1	1	12.72	0.00153125	0.019	0.153	76.328	11.670	8.4	1.284
Deck Beam 2	1	9.2	0.00153125	0.014	0.111	78.928	8.728	8.4	0.929

## Bulkheads

ITEM	Amount	Length(m)	Height(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
Collision BHD	1	12.9293	7.505	97.03956822	0.679	5.332	76.162	406.120	3.753	20.011
vertical stiffeners	3		7.505	0.002112	0.016	0.373	76.162	28.431	3.753	1.401
BHD 1	1	14.6377	7.478	109.4577931	0.766	6.015	73.178	440.144	3.739	22.488
vertical stiffeners	3		7.478	0.002112	0.016	0.050	73.178	3.640	3.739	0.186
BHD 2	1	15.2637	5.525	84.32888976	0.590	4.634	71.229	330.066	2.762	12.801
vertical stiffeners	3		5.525	0.002112	0.012	0.275	71.229	19.573	2.762	0.759
BHD 3	1	15.728	5.525	86.8940544	0.608	4.775	52.378	250.096	2.762	13.190
vertical stiffeners	3		5.525	0.002112	0.012	0.275	52.378	14.393	2.762	0.759
BHD 4 (machinery space)	1	15.728	5.656	88.9638592	0.623	4.889	15.978	78.109	2.828	13.826
vertical stiffeners	3		5.656	0.002112	0.012	0.281	15.978	4.495	2.828	0.796
BHD 5 (machinery Space)	1	15.8957	5.176	82.28250148	0.576	4.521	6.246	28.241	2.726	12.326
vertical stiffeners	3		5.176	0.002112	0.011	0.257	6.246	1.608	2.726	0.702

ITEM	Amount	Length(m)	area (m <sup>2</sup> )	volume (m <sup>3</sup> )	weight (ton)	LCG(m)	LCG moment from aft	VCG	VCG moment from baseline
Main Hull Brackets(upper)	192	0.182	0.002832	0.000515424	0.777	40.5805	31.525	2.703	2.0998
Main Hull Brackets lower	192	0.312	0.002832	0.000883584	1.332	40.5805	54.043	2.703	3.5997
Super Structure Brackets upper and lower	72	0.182	0.001511	0.000275002	0.155	5.95145	0.925	8.5	1.3212

**Total weight of Structural members = 154.048 tonnes**

**Total moment of LCG = 6379.963**

## Machinery Weight

<b>Items</b>	<b>Quantity</b>	<b>Unit weight (tonne)</b>	<b>Total weight (tonnes)</b>	<b>LCG (m)</b>	<b>Moment (about aft)</b>	<b>VCG (m)</b>	<b>Moment (about keel)</b>
Main Engine	2	6.5	13	10.52	136.760	2	26
Generator	2	0.2	0.4	10.52	4.208	2	0.8
Pump	2	0.102	0.204	10.52	2.146	2	0.408
	2	0.102	0.204	10.52	2.146	2	0.408
	1	0.102	0.102	10.52	1.073	2	0.204
	1	0.102	0.102	10.52	1.073	2	0.204
Rudder & Steering Arrangement	2	0.8	1.6	2.02	3.232	2.9586	4.734
Anchor forward	2	3.5	7	77.94	5.820		0
anchor aft1	1	3.5	3.5	0.1735	0.607	6.535	22.873
Stud Link Chain Cable	1	3	3	0.8817	2.645	7.8951	23.685
Stud Link Chain Cable	2	3	6	75.8152	454.891	7.8951	47.371
Towline	1	0.25	0.25	40.58	10.145	8.13	2.033

Mooring Ropes	3		0.5	40.58	20.290	8.13	4.065
Windlass	3	1	3	40.58	121.740	8.13	24.39
Bollard	12	0.05	0.6	40.58	24.348	8.13	4.878
Propeller, Propeller Shaft	2	2	4	3.7	14.800	1.0812	4.325
Complete Piping		0.5	0.5	40.58	20.290	3	1.5
Gear box	2	0.36	0.72	10.52	7.574	2	1.44

**Total machinery weight = 45.61tonnes**

## **WOOD AND OUTFIT Weight**

Item	No. of Items	Weight (kg)	Total Weight (ton)	LCG (m)	Moment about aft	VCG (m)	Moment about keel
Control Panel	1	450.00	0.45	47.92	21.56	14.40	6.48
Wing Control Panel (Starboard)	1	20.00	0.02	47.92	0.96	14.40	0.29
Wing Control Panel (Port side)	1	20.00	0.02	47.92	0.96	14.40	0.29
Cabinet	2	50.00	0.05	32.10	1.61	10.40	0.52
Chart Table	1	15.00	0.015	45.00	0.68	14.00	0.21
Chart Table-Chair	1	12.00	0.012	45.00	0.54	14.00	0.17
Map Table	1	18.00	0.018	45.00	0.81	14.00	0.25
Map Table- Chair	1	15.00	0.015	45.00	0.68	14.00	0.21
Control Panel- Chair	2	15.00	0.015	45.00	0.68	14.00	0.21
Radio Instrument Table	1	50.00	0.05	32.10	1.61	14.00	0.70
Radio Operator's Chair	1	20.00	0.02	21.10	0.42	10.40	0.21
Sofa	1	40.00	0.04	32.10	1.28	10.40	0.42

Shower	1	20.00	0.02	13.50	0.27	6.25	0.13
Shower	1	20.00	0.02	11.05	0.22	9.25	0.19
Shower	1	20.00	0.02	15.2	0.30	9.25	0.19
Washing Machine	2	150	0.15	5.85	0.88	8.18	1.23
Single bed	1	50.00	0.05	32.74	1.64	10.40	0.52
Locker	1	25.00	0.025	32.74	0.82	10.40	0.26
Table	1	15.00	0.015	32.74	0.49	10.40	0.16
chair	1	6.00	0.006	32.74	0.20	10.40	0.06
Single bed	1	50.00	0.05	10.70	0.54	6.54	0.33
Table	1	15.00	0.015	10.70	0.16	6.54	0.10
chair	1	6.00	0.006	10.70	0.06	6.54	0.04
Locker	1	25.00	0.025	10.70	0.27	6.54	0.16

Single bed	1	50.00	0.05	32.74	1.64	10.40	0.52
Cabinet	1	25.00	0.025	32.74	0.82	10.40	0.26
Table	1	15.00	0.015	32.74	0.49	10.40	0.16
Chair	1	6.00	0.006	32.74	0.20	10.40	0.06
Single Bed	2	100.00	0.1	10.70	1.07	6.54	0.65
locker	0	0.00	0	10.70	0.00	6.54	0.00
Table	1	15.00	0.015	10.70	0.16	6.54	0.10
Chair	1	6.00	0.006	10.70	0.06	6.54	0.04
Double bed	1	80.00	0.08	32.74	2.62	10.40	0.83
Cabinet	1	25.00	0.025	32.74	0.82	10.40	0.26
Table	1	20.00	0.02	32.74	0.65	10.40	0.21
Chair	1	6.00	0.006	32.74	0.20	10.40	0.06

TV	1	25.00	0.025	32.74	0.82	10.40	0.26
Mini Refrigerator	1	50.00	0.05	32.74	1.64	10.40	0.52
Single bed	2	100.00	0.1	10.70	1.07	6.54	0.65
Table	1	15.00	0.015	10.70	0.16	6.54	0.10
Chair	1	6.00	0.006	10.70	0.06	6.54	0.04
Locker	2	50.00	0.05	10.70	0.54	6.54	0.33
Single bed	2	100.00	0.1	10.70	1.07	6.25	0.63
Table	1	15.00	0.015	10.70	0.16	6.25	0.09
Chair	1	6.00	0.006	10.70	0.06	6.25	0.04
Locker	1	25.00	0.025	10.70	0.27	6.25	0.16
						6.25	
Single bed	2	100.00	0.1	10.70	1.07	6.25	0.63
Table	1	15.00	0.015	10.70	0.16	6.25	0.09

Chair	1	6.00	0.006	10.70	0.06	6.25	0.04
Locker	2	50.00	0.05	10.70	0.54	6.25	0.31
				10.70	0.00	6.25	0.00
Single bed	2	100.00	0.1	10.70	1.07	6.25	0.63
Table	1	15.00	0.015	10.70	0.16	6.25	0.09
Chair	1	6.00	0.006	10.70	0.06	6.25	0.04
Cabinet	1	25.00	0.025	10.70	0.27	6.25	0.16
				10.70	0.00	6.25	0.00
Single bed	2	100.00	0.1	10.70	1.07	6.25	0.63
Table	1	15.00	0.015	10.70	0.16	6.25	0.09
Chair	1	6.00	0.006	10.70	0.06	6.25	0.04
Cabinet	2	50.00	0.05	10.70	0.54	6.25	0.31
				10.70	0.00	6.25	0.00

Single bed	1	50.00	0.05	8.40	0.42	6.25	0.31
Locker	1	25.00	0.025	8.40	0.21	6.25	0.16
Table	1	15.00	0.015				
Chair	1	6.00	0.006				
Cooker Gas	1	45.00	0.045	11.20	0.50	6.25	0.28
Dish washer	1	50.00	0.05	11.20	0.56	6.25	0.31
Cabinet	1	25.00	0.025	8.40	0.21	6.25	0.16
Table	1	80.00	0.08	8.40	0.67	6.25	0.50
Chair	6	36.00	0.216	8.40	1.81	6.25	1.35
Vegetable Storage		100.00	0.1	13.50	1.35	6.25	0.63

Frogen Food Storage		400.00	0.4	13.50	5.40	6.25	2.50
Cabinet		50.00	0.05	13.50	0.68	6.25	0.31
Table	1	100.00	0.1	13.50	1.35	6.25	0.63
chair	6	36.00	0.036	13.50	0.49	6.25	0.23
aft	9	630.00	0.63	12.00	7.56	7.75	4.88
Fwd	4	280.00	0.28	62.50	17.50	6.25	1.75
		300.00	3	45.30	135.90	5.50	16.50
	1	200.00	2	8.90	17.80	12.25	24.50
			2	0.00	0.00	0.00	0.00

**Total wood and outfit weight = 12.60 tonnes**

## **Weight Calculation Summary**

**Steel Weight = 630.20 tonnes**

**Machinery Weight = 45.61 tonnes**

**Wood and Outfit Weight = 12.60 tonnes**

**Total Lightweight = 688.41 tonnes**

**Appendix 7**

**Stability Calculation:**

**Lightship condition ordinates**

0 degree		
	immerse	emmersed
<b>st 0</b>	0	0
<b>st 0.5</b>	0	0
<b>st 1</b>	0	0
<b>st 1.5</b>	6642	6642
<b>st 2</b>	7710	7710
<b>st 3</b>	7799	7799
<b>st 4</b>	7799	7799
<b>st 5</b>	7799	7799
<b>st 6</b>	7799	7799
<b>st 7</b>	7799	7799
<b>st 8</b>	7786	7786
<b>st 8.5</b>	7709	7709
<b>st 9</b>	6756	6756
<b>st 9.5</b>	4220	4220

<b>st 10</b>	0	0
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<b>15 degree</b>		
	<b>immerse</b>	<b>emmersed</b>
<b>st 0</b>	0	0
<b>st 0.5</b>	0	0
<b>st 1</b>	7375	0
<b>st 1.5</b>	7924	765
<b>st 2</b>	8130	2493
<b>st 3</b>	8149	2493
<b>st 4</b>	8149	2493
<b>st 5</b>	8149	2493
<b>st 6</b>	8149	2493
<b>st 7</b>	8149	2493
<b>st 8</b>	8147	2493

<b>st 8.5</b>	8129	2493
<b>st 9</b>	7425	2493
<b>st 9.5</b>	4913	2493
<b>st 10</b>	0	0

30 degree		
	immerse	emmersed
st 0	0	0
st 0.5	8070	0
st 1	8672	0
st 1.5	9016	409
st 2	9086	1297
st 3	9107	1297
st 4	9107	1297
st 5	9107	1297
st 6	9107	1297
st 7	9107	1297
st 8	9099	1297
st 8,5	9091	1297
st 9	8442	1297

st 9.5	5443	1297
st 10	0	0

45 degree		
	immerse	emmersed
st 0	9624	0
st 0.5	10230	0
st 1	10785	0
st 1.5	11130	291
st 2	11167	917
st 3	11177	917
st 4	11177	917
st 5	11177	917

<b>st 6</b>	11177	917
<b>st 7</b>	11177	917
<b>st 8</b>	11205	917
<b>st 8,5</b>	11201.2	917
<b>st 9</b>	10931	917
<b>st 9.5</b>	7943	917
<b>st 10</b>	0	0

60 degree		
	immerse	emmersed
st 0	9419	0
st 0.5	9419	0
st 1	9419	0
st 1.5	9419	241
st 2	9419	757
st 3	9419	757
st 4	9419	757
st 5	9419	757
st 6	9419	757
st 7	9419	757
st 8	9419	757
st 8,5	9419	757
st 9	9419	757
st 9.5	9419	757
st 10	2060	0

75 degree		
	immerse	emmersed
<b>st 0</b>	8412	0
<b>st 0.5</b>	8412	0
<b>st 1</b>	8412	0
<b>st 1.5</b>	8412	216
<b>st 2</b>	8412	676
<b>st 3</b>	8412	676
<b>st 4</b>	8412	676
<b>st 5</b>	8412	676
<b>st 6</b>	8412	676
<b>st 7</b>	8412	676
<b>st 8</b>	8412	676
<b>st 8,5</b>	8412	676
<b>st 9</b>	8412	676

<b>st 9.5</b>	8412	676
<b>st 10</b>	8412	0

90 degree		
	<b>immerse</b>	<b>emmersed</b>
<b>st 0</b>	8115	0
<b>st 0.5</b>	8115	0
<b>st 1</b>	8115	0
<b>st 1.5</b>	8115	209
<b>st 2</b>	8115	653
<b>st 3</b>	8115	653
<b>st 4</b>	8115	653
<b>st 5</b>	8115	653
<b>st 6</b>	8115	653
<b>st 7</b>	8115	653
<b>st 8</b>	8115	653

<b>st 8,5</b>	8115	653
<b>st 9</b>	8115	653
<b>st 9.5</b>	8115	653
<b>st 10</b>	8115	0

## **Loaded condition ordinates**

0 degree		
	immerse	emmersed
<b>st 0</b>	0	0
<b>st 0.5</b>	6515	6515
<b>st 1</b>	7386	7386
<b>st 1.5</b>	7775	7775
<b>st 2</b>	7849	7849
<b>st 3</b>	7864	7864
<b>st 4</b>	7864	7864
<b>st 5</b>	7864	7864
<b>st 6</b>	7864	7864
<b>st 7</b>	7864	7864
<b>st 8</b>	7862	7862
<b>st 8.5</b>	7849	7849
<b>st 9</b>	7212	7212
<b>st 9.5</b>	4725	4725
<b>st 10</b>	279	

15 degree		
	immerse	emmersed
st 0	6569	0
st 0.5	7326	3608
st 1	7782	6631
st 1.5	8070	7875
st 2	8136	8135
st 3	8149	8149
st 4	8149	8149
st 5	8149	8149
st 6	8149	8149
st 7	8149	8149
st 8	8147	8148
st 8,5	8135	8134
st 9	7611	7362
st 9.5	5224	4190
st 10	241	362

30 degree		
	immerse	emmersed
st 0	7819	0
st 0.5	8308	1948
st 1	8753	4119
st 1.5	9039	6139
st 2	9101	7128
st 3	9107	7128
st 4	9107	7128
st 5	9107	7128
st 6	9107	7128
st 7	9107	7128
st 8	9.105	7128
st 8,5	9100	7128
st 9	8815	7128
st 9.5	6850	7128
st 10	230	582

<b>45 degree</b>		
	<b>immerse</b>	<b>emmersed</b>
<b>st 0</b>	7303	0
<b>st 0.5</b>	7303	1395
<b>st 1</b>	7730	2953
<b>st 1.5</b>	7730	4363
<b>st 2</b>	7730	5036
<b>st 3</b>	7730	5036
<b>st 4</b>	7730	5036
<b>st 5</b>	7730	5036
<b>st 6</b>	7730	5036
<b>st 7</b>	7730	5036
<b>st 8</b>	7730	5036
<b>st 8,5</b>	7730	5036
<b>st 9</b>	7730	5036
<b>st 9.5</b>	7730	5036
<b>st 10</b>	232	1369

**60 degree**

	<b>immerse</b>	<b>emmersed</b>
<b>st 0</b>	6016	0
<b>st 0.5</b>	6016	1160
<b>st 1</b>	6016	2458
<b>st 1.5</b>	6016	3621
<b>st 2</b>	6016	4159
<b>st 3</b>	6016	4159
<b>st 4</b>	6016	4159
<b>st 5</b>	6016	4159
<b>st 6</b>	6016	4159
<b>st 7</b>	6016	4159
<b>st 8</b>	6016	4159
<b>st 8,5</b>	6016	4159
<b>st 9</b>	6016	4159
<b>st 9.5</b>	6016	4159
<b>st 10</b>	6016	2053

75 degree		
	immerse	emmersed
st 0	5373	0
st 0.5	5373	1042
st 1	5373	2210
st 1.5	5373	3245
st 2	5373	3712
st 3	5373	3712
st 4	5373	3712
st 5	5373	3712
st 6	5373	3712
st 7	5373	3712
st 8	5373	3712
st 8,5	5373	3712
st 9	5373	3712
st 9.5	5373	3712
st 10	5373	2272

90 degree		
	immerse	emmersed
st 0	5189	0
st 0.5	5189	1011
st 1	5189	2146
st 1.5	5189	3144
st 2	5189	3588
st 3	5189	3588
st 4	5189	3588
st 5	5189	3588
st 6	5189	3588
st 7	5189	3588
st 8	5189	3588
st 8,5	5189	3588
st 9	5189	3588
st 9.5	5189	3588
st 10	5189	2519

L(ship length)	77.942	m
INTERVAL(radians)	0.262	
DEPTH	5.406	m
VOLUME	6.87E+11	mm <sup>3</sup>
KB	326	mm

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 0 degree									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	0	0	0	0	0	0	0	0
0.5	1	0	0	0	0	0	0	0	0

1	0.5	0	0	0	0	0	0	0	0
1.5	1	6642	6642	44116164	2.93E+11	6642	6642	44116164	2.93E+11
2	0.75	7710	5782.5	44583075	3.44E+11	7710	5782.5	44583075	3.44E+11
3	2	7799	15598	121648802	9.49E+11	7799	15598	121648802	9.49E+11
4	1	7799	7799	60824401	4.74E+11	7799	7799	60824401	4.74E+11
5	2	7799	15598	121648802	9.49E+11	7799	15598	121648802	9.49E+11
6	1	7799	7799	60824401	4.74E+11	7799	7799	60824401	4.74E+11
7	2	7799	15598	121648802	9.49E+11	7799	15598	121648802	9.49E+11
8	0.75	7786	5839.5	45466347	3.54E+11	7786	5839.5	45466347	3.54E+11
8.5	1	7709	7709	59428681	4.58E+11	7709	7709	59428681	4.58E+11
9	0.5	6756	3378	22821768	1.54E+11	6756	3378	22821768	1.54E+11
9.5	1	4220	4220	17808400	75151448000	4220	4220	17808400	75151448000
10	0.25	0	0	0	0	0	0	0	0
$\Sigma$			95963	720819643	5.47E+12		95963	720819643	5.47E+12
(EW+ IW) of $\sum(y^3 \times SM) =$									1.09E+13

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 15 degree									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	0	0	0	0	0	0	0	0
0.5	1	0	0	0	0	0	0	0	0
1	0.5	7375	3687.5	27195312.5	2.01E+11	0	0	0	0
1.5	1	7924	7924	62789776	4.98E+11	765	765	585225	447697125
2	0.75	8130	6097.5	49572675	4.03E+11	2493	1869.75	4661286.75	11620587868
3	2	8149	16298	132812402	1.08E+12	2493	4986	12430098	30988234314
4	1	8149	8149	66406201	5.41E+11	2493	2493	6215049	15494117157
5	2	8149	16298	132812402	1.08E+12	2493	4986	12430098	30988234314
6	1	8149	8149	66406201	5.41E+11	2493	2493	6215049	15494117157

7	2	8149	16298	132812402	1.08E+12	2493	4986	12430098	30988234314
8	0.75	8147	6110.25	49780206.75	4.06E+11	2493	1869.75	4661286.75	11620587868
8.5	1	8129	8129	66080641	5.37E+11	2493	2493	6215049	15494117157
9	0.5	7425	3712.5	27565312.5	2.05E+11	2493	1246.5	3107524.5	7747058579
9.5	1	4913	4913	24137569	1.19E+11	2493	2493	6215049	15494117157
10	0.25	0	0	0	0	0	0	0	0
$\Sigma$			105765.75	838371100.8	6.70E+12		30681	75165813	1.86E+11
(EW+ IW) of $\Sigma(y^3 \times SM) =$									6.88E+12

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 30 degree									
STATION	SM MULTIPLIERS	IMMersed WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	0	0	0	0	0	0	0	0
0.5	1	8070	8070	65124900	5.26E+11	0	0	0	0
1	0.5	8672	4336	37601792	3.26E+11	0	0	0	0
1.5	1	9016	9016	81288256	7.33E+11	409	409	167281	68417929
2	0.75	9086	6814.5	61916547	5.63E+11	1297	972.75	1261656.75	1636368805
3	2	9107	18214	165874898	1.51E+12	1297	2594	3364418	4363650146
4	1	9107	9107	82937449	7.55E+11	1297	1297	1682209	2181825073
5	2	9107	18214	165874898	1.51E+12	1297	2594	3364418	4363650146
6	1	9107	9107	82937449	7.55E+11	1297	1297	1682209	2181825073

7	2	9107	18214	165874898	1.51E+12	1297	2594	3364418	4363650146
8	0.75	9099	6824.25	62093850.75	5.65E+11	1297	972.75	1261656.75	1636368805
8.5	1	9091	9091	82646281	7.51E+11	1297	1297	1682209	2181825073
9	0.5	8442	4221	35633682	3.01E+11	1297	648.5	841104.5	1090912537
9.5	1	5443	5443	29626249	1.61E+11	1297	1297	1682209	2181825073
10	0.25	0	0	0	0	0	0	0	0
$\Sigma$			126671.75	1119431150	9.97E+12		15973	20353789	26250318805
(EW+ IW) of $\Sigma(y^3 \times SM) =$									9.99E+12

TABLE FOR STABILITY

WATER SECTION INCLINED AT 45 degree

STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	9624	2406	23155344	2.23E+11	0	0	0	0
0.5	1	10230	10230	104652900	1.07E+12	0	0	0	0
1	0.5	10785	5392.5	58158112.5	6.27E+11	0	0	0	0
1.5	1	11130	11130	123876900	1.38E+12	291	291	84681	24642171
2	0.75	11167	8375.25	93526416.75	1.04E+12	917	687.75	630666.75	578321409.8
3	2	11177	22354	249850658	2.79E+12	917	1834	1681778	1542190426
4	1	11177	11177	124925329	1.40E+12	917	917	840889	771095213
5	2	11177	22354	249850658	2.79E+12	917	1834	1681778	1542190426
6	1	11177	11177	124925329	1.40E+12	917	917	840889	771095213

7	2	11177	22354	249850658	2.79E+12	917	1834	1681778	1542190426
8	0.75	11205	8403.75	94164018.75	1.06E+12	917	687.75	630666.75	578321409.8
8.5	1	11201.2	11201.2	125466881.4	1.41E+12	917	917	840889	771095213
9	0.5	10931	5465.5	59743380.5	6.53E+11	917	458.5	420444.5	385547606.5
9.5	1	7943	7943	63091249	5.01E+11	917	917	840889	771095213
10	0.25	0	0	0	0	0	0	0	0
$\Sigma$			159963.2	1745237835	1.91E+13		11295	10175349	9277784727
(EW+ IW) of $\sum(y^3 \times \text{SM}) =$									1.91E+13

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 60 degree									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	9419	2354.75	22179390.25	2.09E+11	0	0	0	0
0.5	1	9419	9419	88717561	8.36E+11	0	0	0	0
1	0.5	9419	4709.5	44358780.5	4.18E+11	0	0	0	0
1.5	1	9419	9419	88717561	8.36E+11	241	241	58081	13997521
2	0.75	9419	7064.25	66538170.75	6.27E+11	757	567.75	429786.75	325348569.8
3	2	9419	18838	177435122	1.67E+12	757	1514	1146098	867596186
4	1	9419	9419	88717561	8.36E+11	757	757	573049	433798093
5	2	9419	18838	177435122	1.67E+12	757	1514	1146098	867596186
6	1	9419	9419	88717561	8.36E+11	757	757	573049	433798093

7	2	9419	18838	177435122	1.67E+12	757	1514	1146098	867596186
8	0.75	9419	7064.25	66538170.75	6.27E+11	757	567.75	429786.75	325348569.8
8.5	1	9419	9419	88717561	8.36E+11	757	757	573049	433798093
9	0.5	9419	4709.5	44358780.5	4.18E+11	757	378.5	286524.5	216899046.5
9.5	1	9419	9419	88717561	8.36E+11	757	757	573049	433798093
10	0.25	2060	515	1060900	2185454000	0	0	0	0
$\Sigma$			139445.25	1309644925	1.23E+13		9325	6934669	5219574637
(EW+ IW) of $\Sigma(y^3 \times SM) =$									1.23E+13

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 75 degree									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	8412	2103	17690436	1.49E+11	0	0	0	0
0.5	1	8412	8412	70761744	5.95E+11	0	0	0	0
1	0.5	8412	4206	35380872	2.98E+11	0	0	0	0
1.5	1	8412	8412	70761744	5.95E+11	216	216	46656	10077696
2	0.75	8412	6309	53071308	4.46E+11	676	507	342732	231686832
3	2	8412	16824	141523488	1.19E+12	676	1352	913952	617831552
4	1	8412	8412	70761744	5.95E+11	676	676	456976	308915776
5	2	8412	16824	141523488	1.19E+12	676	1352	913952	617831552
6	1	8412	8412	70761744	5.95E+11	676	676	456976	308915776

7	2	8412	16824	141523488	1.19E+12	676	1352	913952	617831552
8	0.75	8412	6309	53071308	4.46E+11	676	507	342732	231686832
8.5	1	8412	8412	70761744	5.95E+11	676	676	456976	308915776
9	0.5	8412	4206	35380872	2.98E+11	676	338	228488	154457888
9.5	1	8412	8412	70761744	5.95E+11	676	676	456976	308915776
10	0.25	8412	2103	17690436	1.49E+11	0	0	0	0
$\Sigma$			126180	1061426160	8.93E+12		8328	5530368	3717067008
(EW+ IW) of $\sum(y^3 \times SM) =$									8.93E+12

TABLE FOR STABILITY									
WATER SECTION INCLINED AT 90 degree									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	8115	2028.75	16463306.25	1.34E+11	0	0	0	0
0.5	1	8115	8115	65853225	5.34E+11	0	0	0	0
1	0.5	8115	4057.5	32926612.5	2.67E+11	0	0	0	0
1.5	1	8115	8115	65853225	5.34E+11	209	209	43681	9129329
2	0.75	8115	6086.25	49389918.75	4.01E+11	653	489.75	319806.75	208833807.8
3	2	8115	16230	131706450	1.07E+12	653	1306	852818	556890154
4	1	8115	8115	65853225	5.34E+11	653	653	426409	278445077
5	2	8115	16230	131706450	1.07E+12	653	1306	852818	556890154
6	1	8115	8115	65853225	5.34E+11	653	653	426409	278445077

7	2	8115	16230	131706450	1.07E+12	653	1306	852818	556890154
8	0.75	8115	6086.25	49389918.75	4.01E+11	653	489.75	319806.75	208833807.8
8.5	1	8115	8115	65853225	5.34E+11	653	653	426409	278445077
9	0.5	8115	4057.5	32926612.5	2.67E+11	653	326.5	213204.5	139222538.5
9.5	1	8115	8115	65853225	5.34E+11	653	653	426409	278445077
10	0.25	8115	2028.75	16463306.25	1.34E+11	0	0	0	0
$\Sigma$			121725	987798375	8.02E+12		8045	5160589	3350470253
(EW+ IW) of $\sum(y^3 \times SM) =$									8.02E+12

COMBINATION TABLE FOR STABILITY														
CALCULATION OF GZ AT 15°														
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF ORDINATE S FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBES FOR RADIAL PLANES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARERS OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARERS OF ORDINATES FOR BOTH SIDES	INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARERS OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARERS OF ORDINATES FOR BOTH SIDES					
0°	95963	720819 643	5	360409 8215	0°	95963	720819 643	5	360409 8215	1.09E+13	5	5.47E+13	0.86602 5404	4.74E+13
15°	105765	838371	8	670696	15°	30681	751658	8	601326	6.88E+	8	5.51E+	0.96592	5.32E+

	.75	100.8		8806			13		504	12		13	5826	13
30°	126671 .75	111943 1150	-1	- 111943 1150	30°	15973	203537 89	-1	- 203537 89	9.99E+ 12	-1	- 9.99E+ 12	1	- 9.99E+ 12
			$\Sigma=$	919163 5871				$\Sigma=$	418507 0930				$\Sigma=$	9.06E+ 13
IMMERSED WEDGE				9191635 871								UNCORRECTED MOMENT		3.42E+ 15
EMERGED WEDGE				4185070 930								CORRECTION OF LAYER		7.94E+ 14
DIFFERENCE				5006564 941								DIFFERENCE		2.63E+ 15
VOLUME OF LAYER				2.84E+1 1								VOLUME OF DISPLACEMENT		6.87E+ 11
AREA AND POSITION OF C.G. OF RADIAL PLANE												BR		3829.9 16
Area	2*(1/3)*(L*1000/10)*A.F											KG		3604
	708995505.9											BG		KG- KB
C.G. OF RADIAL PLANE		(1/2)*( M.F/A.F												3982

ON IMMERSED SIDE =	)									
	2796.714791									
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA							GZ		BR-BG*SI N(15)
	400.25									2799.299

COMBINATION TABLE FOR STABILITY														
CALCULATION OF GZ AT 30°														
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF FUNCTIONS OF CUBE PLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBE PLIERS	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES	
INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARING OF ORDINATES OF RADIAL PLANES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARING OF ORDINATES OF RADIAL PLANES	INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF SQUARING OF ORDINATES OF RADIAL PLANES	MULTIPLIERS	FUNCTIONS OF SQUARING OF ORDINATES OF RADIAL PLANES FOR BOTH SIDES						
0°	95963	720819 643	1	720819 643	0°	95963	720819 643	1	720819 643	1.09E+13	1	1.09E+13	0.866	9.48E+12
15°	105765	838371	4	335348	15°	30681	751658	4	300663	6.88E+	4	2.75E+	0.966	2.66E+

	.75	100.8		4403			13		252	12		13		13
30°	126671 .75	111943 1150	1	111943 1150	30°	15973	203537 89	1	203537 89	9.99E+ 12	1	9.99E+ 12	1	9.99E+ 12
			$\Sigma=$	519373 5196				$\Sigma=$	104183 6684				$\Sigma=$	4.61E+ 13
IMMERSED WEDGE				5193735 196						degree	UNCORRECTED MOMENT			6.96E+ 15
EMERGED WEDGE				1041836 684					30	CORRECTION OF LAYER			3.63E+ 15	
DIFFERENCE				4151898 512					15	DIFFERENCE			3.34E+ 15	
VOLUME OF LAYER				9.41E+1 1					0	VOLUME OF DISPLACEMENT			6.87E+ 11	
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR			6.54E+ 03	
Area	$2*(1/3)*(L*1000/10)*A.F$									KG			3604	
	741201140.3									BG			KG- KB	
C.G. OF RADIAL PLANE		$(1/2)*(M.F/A.F)$											3278	

ON IMMERSSED SIDE =	3852.498								GZ	BR-BG*SI N(30)
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA									4900.5 80768
	1270.013									

COMBINATION TABLE FOR STABILITY													
CALCULATION OF GZ AT $45^\circ$													
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTION S OF CUBE S OF ORDINATE S FOR BOTH SIDES	PRODUCTS OF SUMS OF FUNCTION S OF CUBE S OF ORDINATE S FOR BOTH SIDES	COSINES OF INCLINATION S OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUMES OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUMES OF WEDGES	INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUMES OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUMES OF WEDGES	MULTIPLIERS	FUNCTIONS OF CUBE S OF ORDINATE S FOR BOTH SIDES	COSINES OF INCLINATION S OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES

0°	95963	72081 9643	1	72081 9643	0°	95963	72081 9643	1	72081 9643	1.09E +13	1	1.09E +13	0.866	9.48E +12
15°	10576 5.75	83837 1100.8	4	33534 84403	15°	30681	75165 813	4	30066 3252	6.88E +12	4	2.75E +13	0.966	2.66E +13
30°	12667 1.75	11194 31150	1	11194 31150	30°	15973	20353 789	1	20353 789	9.99E +12	1	9.99E +12	1	9.99E +12
			Σ=	51937 35196				Σ=	10418 36684				Σ=	4.61E +13
45°	15996 3.2	17452 37835	5	87261 89175	45°	11295	10175 349	5	50876 745	1.91E +13	5	9.57E +13	0.966	9.24E +13
30°	12667 1.75	11194 31150	8	89554 49198	30°	15973	20353 789	8	16283 0312	9.99E +12	8	8.00E +13	0.866	6.92E +13
15°	10576 5.75	83837 1100.8	-1	- 83837 1100.8	15°	30681	75165 813	-1	- 75165 813	6.88E +12	-1	- 6.88E +12	0.707	- 4.87E +12
			Σ=	16843 26727 2				Σ=	13854 1244				Σ=	1.57E +14
IMMERSED WEDGE					9.55E+11	1.18E +12				UNCORRECTED MOMENT			5.93E +15	
EMERGED WEDGE					7852659285	2.36E +11				CORRECTION OF LAYER			9.56E +15	

DIFFERENCE		1.89E+12						DIFFERENCE	3.32E +15
VOLUME OF LAYER		1.89E+12						VOLUME OF DISPLACEMENT	6.87E +11
AREA AND POSITION OF C.G. OF RADIAL PLANE								BR	8906.6 46774
Area	$2*(1/3)*(L*1000/10)*A.F$							KG	3604
	889880441.6							BG	KG- KB
C.G. OF RADIAL PLANE ON IMMERSED SIDE =	$(1/2)*(M.F/A.F)$							GZ	3278
	5065.633								BR- BG*S IN(45)
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA								6588.7 50745
	2121.831								

COMBINATION TABLE FOR STABILITY														
CALCULATION OF GZ AT 60°														
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBE S OF ORDINATE S FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBE S FOR MOMENTS OF WEDGES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARIES OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARIES OF ORDINATES FOR VOLUME OF WEDGES	INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARIES OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARIES OF ORDINATES FOR VOLUME OF WEDGES					
0°	95963	720819 643	1	720819 643	0°	95963	720819 643	1	720819 643	1.09E+13	1	1.09E+13	0.5	5.47E+12
15°	105765 .75	838371 100.8	4	335348 4403	15°	30681	751658 13	4	300663 252	6.88E+12	4	2.75E+13	0.70710 6781	1.95E+13
30°	126671 .75	111943 1150	2	223886 2300	30°	15973	203537 89	2	407075 78	9.99E+12	2	2.00E+13	0.86602 5404	1.73E+13
45°	159963	174523	4	698095	45°	11295	101753	4	407013	1.91E+	4	7.66E+	0.96592	7.39E+

	.2	7835		1340			49		96	13		13	5826	13
60°	139445 .25	130964 4925	1	130964 4925	60°	9325	693466 9	1	693466 9	1.23E+ 13	1	1.23E+ 13	1	1.23E+ 13
			$\Sigma=$	146037 62610				$\Sigma=$	110982 6538				$\Sigma=$	1.29E+ 14
IMMERSED WEDGE				1460376 2610						UNCORRECTED MOMENT				1.94E+ 16
EMERGED WEDGE				1109826 538						CORRECTION OF LAYER				1.34E+ 16
DIFFERENCE				1349393 6072						DIFFERENCE				6.03E+ 15
VOLUME OF LAYER				3.06E+1 2						VOLUME OF DISPLACEMENT				6.87E+ 11
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR				8271.7 4532
Area	2*(1/3)*(L*1000/10)*A.F									KG				3604
	773030055									BG				KG- KB
C.G. OF RADIAL PLANE		(1/2)*(M.F/A.F)												3278

ON IMMERESED SIDE =	4378.26197								GZ	BR-BG*SI N(60)
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA									5433.2 37888
	3957.67									

COMBINATION TABLE FOR STABILITY														
CALCULATION OF GZ AT $75^\circ$														
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF ORDINATE S FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBE S FOR MOMENTS OF RADIAL PLANES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLN ATIONS OF RADIA L PLANES	FUNC TIONS OF ORDI NATE S OF RADI AL PLAN ES	FUNC TIONS OF SQUA RES OF ORDI NATE S FOR RADIAL PLAN ES	MULTI PLIERS	FUNC TIONS OF SQUA RES OF ORDI NATE S FOR VOLUM E OF WEDG ES	INCLN ATIONS OF RADIA L PLAN ES	FUNC TIONS OF ORDI NATE S OF RADIA L PLAN ES	FUNC TIONS OF SQUA RES OF ORDI NATE S	MULTI PLIERS	FUNC TIONS OF SQUA RES OF ORDI NATE S FOR VOLUM E OF WEDG ES					
0°	95963	720819 643	1	720819 643	0°	95963	720819 643	1	720819 643	1.09E+13	1	1.09E+13	0.5	5.47E+12
15°	105765 .75	838371 100.8	4	335348 4403	15°	30681	751658 13	4	300663 252	6.88E+12	4	2.75E+13	0.70710 6781	1.95E+13
30°	126671 .75	111943 1150	2	223886 2300	30°	15973	203537 89	2	407075 78	9.99E+12	2	2.00E+13	0.86602 5404	1.73E+13
45°	159963	174523	4	698095	45°	11295	101753	4	407013	1.91E+	4	7.66E+	0.96592	7.39E+

	.2	7835		1340			49		96	13		13	5826	13
60°	139445 .25	130964 4925	1	130964 4925	60°	9325	693466 9	1	693466 9	1.23E+ 13	1	1.23E+ 13	1	1.23E+ 13
			Σ=	146037 62610				Σ=	110982 6538				Σ=	1.29E+ 14
75°	126180	106142 6160	5	530713 0800	75°	8328	553036 8	5	276518 40	8.93E+ 12	5	4.47E+ 13	0.70710 6781	3.16E+ 13
60°	139445 .25	130964 4925	8	104771 59398	60°	9325	693466 9	8	554773 52	1.23E+ 13	8	9.87E+ 13	0.5	4.93E+ 13
45°	159963 .2	174523 7835	-1	- 174523 7835	45°	11295	101753 49	-1	- 101753 49	1.91E+ 13	-1	- 1.91E+ 13	0.25881 9045	- 4.95E+ 12
			Σ=	140390 52363				Σ=	729538 43				Σ=	7.60E+ 13
IMMERSED WEDGE					7.96E+1	3.31E+ 12						UNCORRECTED MOMENT		2.87E+ 15
EMERGED WEDGE					4135098 373	2.52E+ 11						CORRECTION OF LAYER		1.51E+ 16
DIFFERENCE					3.85E+1 2							DIFFERENCE		7.18E+ 15
VOLUME OF LAYER					3.85E+1							VOLUME OF		6.87E+

	2						DISPLACEMENT	11
AREA AND POSITION OF C.G. OF RADIAL PLANE							BR	6054.4 74513
Area	2*(1/3)*(L*1000/10)*A.F						KG	3604
	874463514						BG	KG- KB
C.G. OF RADIAL PLANE ON IMMERSED SIDE =	(1/2)*(M.F/A.F)							3278
	3925.0297						GZ	2888.1 69655

COMBINATION TABLE FOR STABILITY														
CALCULATION OF GZ AT 90° for WL - 1														
IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF ORDINATE S FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBE S FOR ORDINATE S FOR BOTH SIDES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLN ATIONS OF RADIA L PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUA RES OF ORDINATE S FOR RADIAL PLANES	MULTIPLIERS	FUNCTIONS OF SQUA RES OF ORDINATE S FOR VOLUME OF WEDGES	INCLN ATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUA RES OF ORDINATE S FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUA RES OF ORDINATE S FOR BOTH SIDES					
0°	95963	720819 643	1	720819 643	0°	95963	720819 643	1	720819 643	1.09E+13	1	1.09E+13	6.13E-17	0.000670546
15°	105765 .75	838371 100.8	4	335348 4403	15°	30681	751658 13	4	300663 252	6.88E+12	4	2.75E+13	0.25881 9045	7.13E+12
30°	126671 .75	111943 1150	2	223886 2300	30°	15973	203537 89	2	407075 78	9.99E+12	2	2.00E+13	0.5	9.99E+12
45°	159963	174523	4	698095	45°	11295	101753	4	407013	1.91E+	4	7.66E+	0.70710	5.41E+

	.2	7835		1340			49		96	13		13	6781	13
60°	139445 .25	130964 4925	2	261928 9850	60°	9325	693466 9	2	138693 38	1.23E+ 13	2	2.47E+ 13	0.86602 5404	2.14E+ 13
75°	126180	106142 6160	4	424570 4640	75°	8328	553036 8	4	221214 72	8.93E+ 12	4	3.57E+ 13	0.96592 5826	3.45E+ 13
90°	121725	987798 375	1	987798 375	90°	8045	516058 9	1	516058 9	8.02E+ 12	1	8.02E+ 12	1	8.02E+ 12
			Σ=	211469 10550				Σ=	114404 3268				Σ=	1.35E+ 14
IMMERSED WEDGE				2114691 0550						UNCORRECTED MOMENT			2.04E+ 16	
EMERGED WEDGE				1144043 268						CORRECTION OF LAYER			1.72E+ 16	
DIFFERENCE				2000286 7282						DIFFERENCE			3.26E+ 15	
VOLUME OF LAYER				4.54E+1 2						VOLUME OF DISPLACEMENT			6.87E+ 11	
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR			4743.1 25377	
Area		2*(1/3)*(L*1000/10)*A.F								KG			3604	

	674302222.7								KG-KB
C.G. OF RADIAL PLANE ON IMMERESED SIDE =	(1/2)*(M.F/A.F)							BG	3278
	3786.0745								BR-BG*SI N(90)
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA							GZ	- 1465.1 25377
	6725.666								



Stability calculation for Fully loaded Condition

L(ship length)	77.942	m
INTERVAL(radians)	0.261799388	
DEPTH	5.406	m
VOLUME	3.78E+12	mm <sup>3</sup>
KB	1.881	mm

WATER SECTION INCLINED AT 0 degree ABOUT WL - 4									
STATION	SM MULTIPLIERS	IMMersed WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	0	0	0	0	0	0	0	0
0.5	1	6515	6515	42445225	2.77E+11	6515	6515	42445225	2.77E+11
1	0.5	7386	3693	27276498	2.01E+11	7386	3693	27276498	2.01E+11
1.5	1	7775	7775	60450625	4.70E+11	7775	7775	60450625	4.70E+11
2	0.75	7849	5886.75	46205100.75	3.63E+11	7849	5886.75	46205100.75	3.63E+11
3	2	7864	15728	123684992	9.73E+11	7864	15728	123684992	9.73E+11
4	1	7864	7864	61842496	4.86E+11	7864	7864	61842496	4.86E+11
5	2	7864	15728	123684992	9.73E+11	7864	15728	123684992	9.73E+11
6	1	7864	7864	61842496	4.86E+11	7864	7864	61842496	4.86E+11
7	2	7864	15728	123684992	9.73E+11	7864	15728	123684992	9.73E+11
8	0.75	7862	5896.5	46358283	3.64E+11	7862	5896.5	46358283	3.64E+11
8.5	1	7849	7849	61606801	4.84E+11	7849	7849	61606801	4.84E+11
9	0.5	7212	3606	26006472	1.88E+11	7212	3606	26006472	1.88E+11
9.5	1	4725	4725	22325625	1.05E+11	4725	4725	22325625	1.05E+11

10	0.25	279	69.75	19460.25	5429409.75	279	69.75	19460.25	5429409.75
$\Sigma$			108928	827434058	6.34E+12		108928	827434058	6.34E+12
(EW+ IW) of $\sum(y^3 \times SM) =$								1.27E+13	

WATER SECTION INCLINED AT 30 degree ABOUT WL - 4									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	7819	1954.75	15284190.25	1.20E+11	0	0	0	0
0.5	1	8308	8308	69022864	5.73E+11	1948	1948	3794704	7392083392
1	0.5	8753	4376.5	38307504.5	3.35E+11	4119	2059.5	8483080.5	34941808580
1.5	1	9039	9039	81703521	7.39E+11	6139	6139	37687321	2.31E+11
2	0.75	9101	6825.75	62121150.75	5.65E+11	7128	5346	38106288	2.72E+11
3	2	9107	18214	165874898	1.51E+12	7128	14256	101616768	7.24E+11
4	1	9107	9107	82937449	7.55E+11	7128	7128	50808384	3.62E+11
5	2	9107	18214	165874898	1.51E+12	7128	14256	101616768	7.24E+11
6	1	9107	9107	82937449	7.55E+11	7128	7128	50808384	3.62E+11
7	2	9107	18214	165874898	1.51E+12	7128	14256	101616768	7.24E+11
8	0.75	9.105	6.82875	62.17576875	566.1103745	7128	5346	38106288	2.72E+11
8.5	1	9100	9100	82810000	7.54E+11	7128	7128	50808384	3.62E+11
9	0.5	8815	4407.5	38852112.5	3.42E+11	7128	3564	25404192	1.81E+11
9.5	1	6850	6850	46922500	3.21E+11	7128	7128	50808384	3.62E+11

10	0.25	230	57.5	13225	3041750	582	145.5	84681	49284342
$\Sigma$			123781.8288	1098536722	9.79E+12		95828	659750394.5	4.62E+12
(EW+ IW) of $\sum(y^3 \times SM) =$									1.44E+13

## WATER SECTION INCLINED AT 45 degree ABOUT WL - 4

STATION	SM MULTIPLIER S	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATE S	FUNCTION S OF ORDINATE S	FUNCTION S OF SQUARES	FUNCTION S OF CUBES	ORDINATE S	FUNCTION S OF ORDINATE S	FUNCTION S OF SQUARES	FUNCTION S OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	7303	1825.75	13333452.25	9737420178 2	0	0	0	0
0.5	1	7303	7303	53333809	3.89E+11	1395	1395	1946025	2714704875
1	0.5	7730	3865	29876450	2.31E+11	2953	1476.5	4360104.5	1287538858 9
1.5	1	7730	7730	59752900	4.62E+11	4363	4363	19035769	8305306014 7
2	0.75	7730	5797.5	44814675	3.46E+11	5036	3777	19020972	9578961499 2
3	2	7730	15460	119505800	9.24E+11	5036	10072	50722592	2.55E+11
4	1	7730	7730	59752900	4.62E+11	5036	5036	25361296	1.28E+11
5	2	7730	15460	119505800	9.24E+11	5036	10072	50722592	2.55E+11
6	1	7730	7730	59752900	4.62E+11	5036	5036	25361296	1.28E+11
7	2	7730	15460	119505800	9.24E+11	5036	10072	50722592	2.55E+11
8	0.75	7730	5797.5	44814675	3.46E+11	5036	3777	19020972	9578961499 2

8.5	1	7730	7730	59752900	4.62E+11	5036	5036	25361296	1.28E+11
9	0.5	7730	3865	29876450	2.31E+11	5036	2518	12680648	6385974332 8
9.5	1	7730	7730	59752900	4.62E+11	5036	5036	25361296	1.28E+11
10	0.25	232	58	13456	3121792	1369	342.25	468540.25	641431602.3
$\sum$			113541.75	873344867.3	6.72E+12		68008.75	330145990.8	1.63E+12
(EW+ IW) of $\sum(y^3 \times SM) =$									8.35E+12

WATER SECTION INCLINED AT 60 degree ABOUT WL - 4									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	6016	1504	9048064	54433153024	0	0	0	0
0.5	1	6016	6016	36192256	2.18E+11	1160	1160	1345600	1560896000
1	0.5	6016	3008	18096128	1.09E+11	2458	1229	3020882	7425327956
1.5	1	6016	6016	36192256	2.18E+11	3621	3621	13111641	47477252061
2	0.75	6016	4512	27144192	1.63E+11	4159	3119.25	12972960.75	53954543759
3	2	6016	12032	72384512	4.35E+11	4159	8318	34594562	1.44E+11
4	1	6016	6016	36192256	2.18E+11	4159	4159	17297281	71939391679
5	2	6016	12032	72384512	4.35E+11	4159	8318	34594562	1.44E+11
6	1	6016	6016	36192256	2.18E+11	4159	4159	17297281	71939391679
7	2	6016	12032	72384512	4.35E+11	4159	8318	34594562	1.44E+11
8	0.75	6016	4512	27144192	1.63E+11	4159	3119.25	12972960.75	53954543759
8.5	1	6016	6016	36192256	2.18E+11	4159	4159	17297281	71939391679
9	0.5	6016	3008	18096128	1.09E+11	4159	2079.5	8648640.5	35969695840
9.5	1	6016	6016	36192256	2.18E+11	4159	4159	17297281	71939391679

10	0.25	6016	1504	9048064	54433153024	2053	513.25	1053702.25	2163250719
$\Sigma$		90240	542883840	3.27E+12		56431.25	226099197.3	9.22E+11	
(EW+ IW) of $\sum(y^3 \times SM) =$									4.19E+12

WATER SECTION INCLINED AT 75 degree ABOUT WL - 4									
STATION	SM MULTIPLIER S	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATE S	FUNCTION S OF ORDINATE S	FUNCTION S OF SQUARES	FUNCTION S OF CUBES	ORDINATE S	FUNCTION S OF ORDINATE S	FUNCTION S OF SQUARES	FUNCTION S OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	5373	1343.25	7217282.25	3877845752 9	0	0	0	0
0.5	1	5373	5373	28869129	1.55E+11	1042	1042	1085764	1131366088
1	0.5	5373	2686.5	14434564.5	7755691505 9	2210	1105	2442050	5396930500
1.5	1	5373	5373	28869129	1.55E+11	3245	3245	10530025	3416993112 5
2	0.75	5373	4029.75	21651846.75	1.16E+11	3712	2784	10334208	3836058009 6
3	2	5373	10746	57738258	3.10E+11	3712	7424	27557888	1.02E+11
4	1	5373	5373	28869129	1.55E+11	3712	3712	13778944	5114744012 8
5	2	5373	10746	57738258	3.10E+11	3712	7424	27557888	1.02E+11
6	1	5373	5373	28869129	1.55E+11	3712	3712	13778944	5114744012 8
7	2	5373	10746	57738258	3.10E+11	3712	7424	27557888	1.02E+11

8	0.75	5373	4029.75	21651846.75	1.16E+11	3712	2784	10334208	3836058009 6
8.5	1	5373	5373	28869129	1.55E+11	3712	3712	13778944	5114744012 8
9	0.5	5373	2686.5	14434564.5	7755691505 9	3712	1856	6889472	2557372006 4
9.5	1	5373	5373	28869129	1.55E+11	3712	3712	13778944	5114744012 8
10	0.25	5373	1343.25	7217282.25	3877845752 9	2272	568	1290496	2932006912
$\Sigma$			80595	433036935	2.33E+12		50504	180695663	6.57E+11
(EW+ IW) of $\sum(y^3 \times SM) =$									2.98E+12

WATER SECTION INCLINED AT 90 degree ABOUT WL - 4									
STATION	SM MULTIPLIERS	IMMERSED WEDGE				EMERGED WEDGE			
		ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES	ORDINATES	FUNCTIONS OF ORDINATES	FUNCTIONS OF SQUARES	FUNCTIONS OF CUBES
		$y_i$	$y_i \times SM$	$y_i^2 \times SM$	$y_i^3 \times SM$	$y_e$	$y_e \times SM$	$y_e^2 \times SM$	$y_e^3 \times SM$
0	0.25	5189	1297.25	6731430.25	34929391567	0	0	0	0
0.5	1	5189	5189	26925721	1.40E+11	1011	1011	1022121	1033364331
1	0.5	5189	2594.5	13462860.5	69858783135	2146	1073	2302658	4941504068
1.5	1	5189	5189	26925721	1.40E+11	3144	3144	9884736	31077609984
2	0.75	5189	3891.75	20194290.75	1.05E+11	3588	2691	9655308	34643245104
3	2	5189	10378	53851442	2.79E+11	3588	7176	25747488	92381986944
4	1	5189	5189	26925721	1.40E+11	3588	3588	12873744	46190993472
5	2	5189	10378	53851442	2.79E+11	3588	7176	25747488	92381986944
6	1	5189	5189	26925721	1.40E+11	3588	3588	12873744	46190993472
7	2	5189	10378	53851442	2.79E+11	3588	7176	25747488	92381986944
8	0.75	5189	3891.75	20194290.75	1.05E+11	3588	2691	9655308	34643245104
8.5	1	5189	5189	26925721	1.40E+11	3588	3588	12873744	46190993472
9	0.5	5189	2594.5	13462860.5	69858783135	3588	1794	6436872	23095496736
9.5	1	5189	5189	26925721	1.40E+11	3588	3588	12873744	46190993472

10	0.25	5189	1297.25	6731430.25	34929391567	2519	629.75	1586340.25	3995991090
$\Sigma$		77835	403885815	2.10E+12		48913.75	169280783.3	5.95E+11	
(EW+ IW) of $\Sigma(y^3 \times SM) =$									2.69E+12

CALCULATION OF GZ AT 15°for WL - 4

IMMERSED WEDGE				EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF ORDINATES FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBES OF ORDINATES FOR BOTH SIDES	COSINES OF INCLINATION S OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATION S OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARED RADIAL PLANES	MULTIPLIERS	INCLINATION S OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARED RADIAL PLANES	MULTIPLIERS	FUNCTIONS OF ORDINATES OF RADIAL PLANES	MULTIPLIERS				
0°	10892 8	82743 4058	5	41371 70290	0°	10892 8	82743 4058	5	41371 70290	1.27E +13	5	6.34E +13	0.866 5.49E +13
15°	11555 8.25	91298 5146.8	8	73038 81174	15°	10829 8.25	83854 4413.3	8	67083 55306	1.39E +13	8	1.11E +14	0.966 1.07E +14
30°	12378 1.8288	10985 36722	-1	- 10985	30°	95828	65975 0394.5	-1	- 65975	1.44E +13	-1	- 1.44E	1 - 1.44E

				36722				0394.5			+13		+13
			$\Sigma =$	10342 51474 2				$\Sigma =$	10185 77520 2			$\Sigma =$	1.48E +14
IMMERSED WEDGE				103425 14742						UNCORRECTED MOMENT			5.59E +15
EMERGED WEDGE				101857 75202						CORRECTION OF LAYER			1.48E +12
DIFFERENCE				156739 540.3						DIFFERENCE			5.59E +15
VOLUME OF LAYER				888415 7318						VOLUME OF DISPLACEMENT			3.78E +12
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR			2.02E +03
Area	$2*(1/3)*(L*1000/10)*A.F$									KG			3188.6
	1163188222									BG			KG- KB
C.G. OF RADIAL PLANE ON IMMERSED SIDE =	$(1/2)*(M.F/A.F)$												3186.7 19
	166.2689									GZ			BR- BG*SI

												N(15)
THICKNESS OF LAYER =	VOLUME OF LAYER/AREA											1199.9 82
	7.638											

CALCULATION OF GZ AT 30°for WL - 4

IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBE S OF ORDINATE S FOR VOLU ME OF WEDG ES	MULTI PLIERS	PROD UCTS OF SUMS OF FUNC TIONS OF RADIA L PLANE S	COSIN ES OF INCLIN ATIONS OF RADIA L PLANE S	FUNC TIONS OF CUBE S FOR MOM ENTS OF WEDG ES
INCLN ATIONS OF RADIA L PLANE S	FUNC TIONS OF ORDI NATE S OF RADIA L PLAN ES	FUNC TIONS OF SQUA RES OF ORDI NATE S FOR VOLU ME OF WEDG ES	MULTI PLIERS	FUNC TIONS OF SQUA RES OF ORDI NATE S OF RADIA L PLANE S	INCLN ATIONS OF RADIA L PLANE S	FUNC TIONS OF ORDI NATE S OF RADIA L PLANE S	MULTI PLIERS	FUNC TIONS OF SQUA RES OF ORDI NATE S FOR VOLU ME OF WEDG ES						
0°	108928	827434 058	1	827434 058	0°	108928	827434 058	1	827434 058	1.2684 7E+13	1	1.2684 7E+13	0.866	1.0985 3E+13
15°	115558 .25	912985 146.8	4	365194 0587	15°	108298	838544 .25 413.3	4	335417 7653	1.3896 2E+13	4	5.5585 E+13	0.966	5.3691 E+13
30°	123781 .8288	109853 6722	1	109853 6722	30°	95828	659750 394.5	1	659750 394.5	1.4411 8E+13	1	1.4411 8E+13	1	1.4411 8E+13

			$\Sigma =$	557791 1367				$\Sigma =$	484136 2106				$\Sigma =$	7.9088 1E+13
IMMERSED WEDGE			5577911 367							UNCORRECTED MOMENT			1.1954 1E+16	
EMERGED WEDGE			4841362 106							CORRECTION OF LAYER			1.6682 9E+14	
DIFFERENCE			7365492 61.7							DIFFERENCE			1.1787 3E+16	
VOLUME OF LAYER			1.66993 E+11							VOLUME OF DISPLACEMENT			3.78E+ 12	
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR			3119.7 74165	
Area	$2*(1/3)*(L*1000/10)*A.F$									KG			3188.6	
	1141121951									BG			KG- KB	
C.G. OF RADIAL PLANE ON IMMERSED SIDE =		(1/2)*( M.F/A.F )											3186.7 19	
		999.013								GZ			BR- BG*SI N(30)	

THICKNESS OF LAYER =	VOLUME OF LAYER/AREA								2179.0
	146.3414661								34665

**CALCULATION OF GZ AT  $45^\circ$  for WL - 4**

IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBE S OF ORDI NATE S FOR BOTH SIDES	MULTI PLIERS	PROD UCTS OF SUMS OF FUNC TIONS OF RADIA L PLANE S	COSIN ES OF INCLIN ATIONS OF RADIA L PLANE S	FUNC TIONS OF CUBE S FOR MOME NTS OF WEDG ES
INCLN ATION S OF RADIA L PLAN E S	FUNC TIONS OF ORDI NATE S OF RADIA L PLAN E S	FUNC TIONS OF SQUA RES OF RADIA L PLAN E S	MULTIP LIERS	FUNC TIONS OF SQUA RES OF RADIA L PLAN E S OF VOLU ME OF WEDG ES	INCLN ATION S OF RADIA L PLAN E S	FUNC TIONS OF ORDI NATE S OF RADIA L PLAN E S	MULTI PLIERS	FUNC TIONS OF SQUA RES OF RADIA L PLAN E S	MULTI PLIERS					
0°	108928	827434 058	1	827434 058	0°	108928	827434 058	1	827434 058	1.2684 7E+13	1	1.2684 7E+13	0.86602 5404	1.0985 3E+13
15°	115558 .25	912985 146.8	4	365194 0587	15°	108298	838544 .25 413.3	4	335417 7653	1.3896 2E+13	4	5.5585 E+13	0.96592 5826	5.3691 E+13
30°	123781 .8288	109853 6722	1	109853 6722	30°	95828	659750 394.5	1	659750 394.5	1.4411 8E+13	1	1.4411 8E+13	1	1.4411 8E+13

			$\Sigma =$	557791 1367				$\Sigma =$	484136 2106				$\Sigma =$	7.9088 1E+13
45°	113541 .75	873344 867.3	5	436672 4336	45°	68008. 75	330145 990.8	5	165072 9954	8.3543 1E+12	5	4.1771 5E+13	0.96592 5826	4.0348 2E+13
30°	123781 .8288	109853 6722	8	878829 3777	30°	95828	659750 394.5	8	527800 3156	1.4411 8E+13	8	1.1529 4E+14	0.86602 5404	9.9847 8E+13
15°	115558 .25	912985 146.8	-1	- 912985 146.8	15°	108298 .25	838544 413.3	-1	- 838544 413.3	1.3896 2E+13	-1	- 1.3896 2E+13	0.70710 6781	- 9.8261 3E+12
			$\Sigma =$	122420 32967				$\Sigma =$	609018 8697				$\Sigma =$	1.3037 E+14
IMMERSED WEDGE				6.93891 E+11	1.2646 5E+12					UNCORRECTED MOMENT			4.9263 3E+15	
EMERGED WEDGE				3.45198 E+11	1.0976 5E+12					CORRECTION OF LAYER			7.7146 6E+14	
DIFFERENCE				5.15686 E+11						DIFFERENCE			1.6109 E+16	
VOLUME OF LAYER				5.15686 E+11						VOLUME OF DISPLACEMENT			3.78E+ 12	
AREA AND POSITION OF C.G. OF RADIAL PLANE										BR			4263.6 09543	

Area	=2*(1/3)*(L*1000/10)*A.F						KG			3188.6
	943360604.7						BG			= KG-KB
C.G. OF RADIAL PLANE ON IMMERESED SIDE =	= $(1/2) * (M.F/A.F)$									3186.7 19
THICKNESS OF LAYER =	=VOLUME OF LAYER/AREA						GZ			=BR-BG*SI N(45)
	546.6480968									2510.2 58928

CALCULATION OF GZ AT  $60^\circ$  for WL - 4

IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBES OF ORDINATE S FOR BOTH SIDES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBES FOR BOTH SIDES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATION S OF RADIAL PLANES	FUNCTIONS OF ORDINATES OF RADIAL PLANES	FUNCTIONS OF SQUARES OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARES OF ORDINATES OF RADIAL PLANES	INCLINATION S OF RADIAL PLANES	FUNCTIONS OF SQUARES OF ORDINATES FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARES OF ORDINATES FOR BOTH SIDES						
$0^\circ$	108928	827434 058	1	827434 058	$0^\circ$	108928	827434 058	1	827434 058	1.2684 7E+13	1	1.2684 7E+13	0.5	6.3423 7E+12
$15^\circ$	115558 .25	912985 146.8	4	365194 0587	$15^\circ$	108298 .25	838544 413.3	4	335417 7653	1.3896 2E+13	4	5.5585 E+13	0.70710 6781	3.9304 5E+13
$30^\circ$	123781 .8288	109853 6722	2	219707 3444	$30^\circ$	95828	659750 394.5	2	131950 0789	1.4411 8E+13	2	2.8823 6E+13	0.86602 5404	2.4962 E+13
$45^\circ$	113541	873344	4	349337	$45^\circ$	68008.	330145	4	132058	8.3543	4	3.3417	0.96592	3.2278

	.75	867.3		9469		75	990.8		3963	1E+12		2E+13	5826	6E+13
60°	90240	542883 840	1	542883 840	60°	56431. 25	226099 197.3	1	226099 197.3	4.1878 9E+12	1	4.1878 9E+12	1	4.1878 9E+12
			$\Sigma=$	107127 11398				$\Sigma=$	704779 5660			$\Sigma=$	1.0707 5E+14	
IMMERSED WEDGE				1071271 1398								UNCORRECTED MOMENT		1.6184 4E+16
EMERGED WEDGE				7047795 660								CORRECTION OF LAYER		8.9732 7E+14
DIFFERENCE				3664915 738								DIFFERENCE		1.5287 E+16
VOLUME OF LAYER				8.30925 E+11								VOLUME OF DISPLACEMENT		3.78E+ 12
AREA AND POSITION OF C.G. OF RADIAL PLANE												BR		4046.0 63882
Area	$=2*(1/3)*(L*1000/10)*A.F$											KG		3188.6
	762123371.2											BG		=KG- KB

	= $(1/2) * (M.F/A.F)$								3186.7 19
C.G. OF RADIAL PLANE ON IMMERSED SIDE =		1079.913898							=BR- BG*SI N(60)
	=VOLUME OF LAYER/AREA								1786.2 84273
THICKNESS OF LAYER =		1090.275811							

CALCULATION OF GZ AT $75^\circ$ for WL - 4														
IMMERSED WEDGE					EMERGED WEDGE					MULTIPLIER S	SUMS OF FUNCTIONS OF CUBES OF ORDINATE S FOR VOLUME OF WEDGES	PRODUCTS OF SUMS OF FUNCTIONS OF RADIAL PLANES	COSINES OF INCLINATION S OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATION S OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUME OF WEDGES	MULTIPLIERS	FUNCTIONS OF SQUARRES OF RADIAL PLANES	INCLINATION S OF RADIAL PLANES	FUNCTIONS OF SQUARRES OF ORDINATE S FOR RADIAL PLANES	MULTIPLIERS	FUNCTIONS OF SQUARRES OF ORDINATE S FOR VOLUME OF WEDGES						
0°	10892 8	82743 4058	1	82743 4058	0°	10892 8	82743 4058	1	82743 4058	1.2684 7E+13	1	1.2684 7E+13	0.5	6.34237 E+12
15°	11555 8.25	91298 5146.8	4	36519 40587	15°	10829 8.25	83854 4413.3	4	33541 77653	1.3896 2E+13	4	5.5585 E+13	0.7071 06781	3.93045 E+13
30°	12378 1.8288	10985 36722	2	21970 73444	30°	95828	65975 0394.5	2	13195 00789	1.4411 8E+13	2	2.8823 6E+13	0.8660 25404	2.4962E +13
45°	11354 1.75	87334 4867.3	4	34933 79469	45°	68008. 75	33014 5990.8	4	13205 83963	8.3543 1E+12	4	3.3417 2E+13	0.9659 25826	3.22786 E+13

60°	90240	54288 3840	1	54288 3840	60°	56431. 25	22609 9197.3	1	22609 9197.3	4.1878 9E+12	1	4.1878 9E+12	1	4.18789 E+12
			Σ=	10712 71139 8				Σ=	70477 95660				Σ=	1.07075 E+14
75°	80595	43303 6935	5	21651 84675	75°	50504	18069 5663	5	90347 8315	2.9841 1E+12	5	1.4920 5E+13	0.7071 06781	1.05504 E+13
60°	90240	54288 3840	8	43430 70720	60°	56431. 25	22609 9197.3	8	18087 93578	4.1878 9E+12	8	3.3503 1E+13	0.5	1.67516 E+13
45°	11354 1.75	87334 4867.3	-1	- 87334 4867.3	45°	68008. 75	33014 5990.8	-1	- 33014 5990.8	8.3543 1E+12	-1	- 8.3543 1E+12	0.2588 19045	- 2.16225 E+12
			Σ=	56349 10528				Σ=	23821 25902				Σ=	2.51397 E+13
IMMERSED WEDGE					3.19392 E+11	2.4288 3E+12				UNCORRECTED MOMENT				9.49963 E+14
EMERGED WEDGE					1.35021 E+11	1.5979 1E+12				CORRECTION OF LAYER				9.77128 E+14

DIFFERENCE		1.0153 E+12					DIFFERENCE	1.61572 E+16
VOLUME OF LAYER		1.0153 E+12					VOLUME OF DISPLACEMENT	3.78E+1 2
AREA AND POSITION OF C.G. OF RADIAL PLANE							BR	3.90E+0 3
Area	$=2*(1/3)*(L*1000/10)*A.F$						KG	3188.6
	852403589.8						BG	=KG- KB
C.G. OF RADIAL PLANE ON IMMERSED SIDE =	$=(1/2)*(M.F/A.F)$							3186.71 9
	962.4073105							
THICKNESS OF LAYER =	=VOLUME OF LAYER/AREA							

			1191.097557									GZ	=BR-BG*SIN (75)
													818.237 9421

CALCULATION OF GZ AT 90° for WL - 4

IMMERSED WEDGE					EMERGED WEDGE					SUMS OF FUNCTIONS OF CUBE S OF ORDINATE S FOR VOLUME OF WEDGES	MULTIPLIERS	PRODUCTS OF SUMS OF FUNCTIONS OF CUBE S FOR BOTH SIDES	COSINES OF INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF CUBES FOR MOMENTS OF WEDGES
INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	FUNCTIONS OF SQUARES OF ORDINATE S	MULTIPLIERS	FUNCTIONS OF SQUARES OF RADIAL PLANES	INCLINATIONS OF RADIAL PLANES	FUNCTIONS OF ORDINATE S OF RADIAL PLANES	MULTIPLIERS	FUNCTIONS OF ORDINATE S FOR VOLUME OF WEDGES						
0°	108928	827434 058	1	827434 058	0°	108928	827434 058	1	827434 058	1.2684 7E+13	1	1.2684 7E+13	6.12574 E-17	0.0007 77035
15°	115558 .25	912985 146.8	4	365194 0587	15°	108298	838544 .25 413.3	4	335417 7653	1.3896 2E+13	4	5.5585 E+13	0.25881 9045	1.4386 5E+13
30°	123781 .8288	109853 6722	2	219707 3444	30°	95828	659750 394.5	2	131950 0789	1.4411 8E+13	2	2.8823 6E+13	0.5	1.4411 8E+13

$45^\circ$	113541 .75	873344 867.3	4	349337 9469	$45^\circ$	68008. 75	330145 990.8	4	132058 3963	8.3543 1E+12	4	3.3417 2E+13	0.70710 6781	2.3629 5E+13
$60^\circ$	90240	542883 840	2	108576 7680	$60^\circ$	56431. 25	226099 197.3	2	452198 394.5	4.1878 9E+12	2	8.3757 8E+12	0.86602 5404	7.2536 4E+12
$75^\circ$	80595	433036 935	4	173214 7740	$75^\circ$	50504	180695 663	4	722782 652	2.9841 1E+12	4	1.1936 4E+13	0.96592 5826	1.1529 7E+13
$90^\circ$	77835	403885 815	1	403885 815	$90^\circ$	48913. 75	169280 783.3	1	169280 783.3	2.6911 E+12	1	2.6911 E+12	1	2.6911 E+12
			$\Sigma=$	133916 28793				$\Sigma=$	816595 8293			$\Sigma=$	7.3902 2E+13	
IMMERSED WEDGE					1339162 8793					UNCORRECTED MOMENT			1.1170 3E+16	
EMERGED WEDGE					8165958 293					CORRECTION OF LAYER			1.0964 9E+15	
DIFFERENCE					5225670 501					DIFFERENCE			1.0073 8E+16	
VOLUME OF LAYER					1.18479 E+12					VOLUME OF DISPLACEMENT			3.78E+ 12	

AREA AND POSITION OF C.G. OF RADIAL PLANE							BR	2666.2 58897
Area	=2*(1/3)*(L*1000/10)*A.F						KG	3188.6
	658603404.8						BG	=KG-KB
C.G. OF RADIAL PLANE ON IMMERESED SIDE =	= $(1/2) * (M.F/A.F)$						GZ	3186.7 19
	925.472763							=BR-BG*SI N(90)
THICKNESS OF LAYER =	=VOLUME OF LAYER/AREA							- 520.46 01032
	1798.936003							

Water plane	SM	SM	SM	SM	Area
	1	4	1		

	1	3	3	1	
WL-1	0	2.799298717	4.900580768	6.588750745	
Area up to 30	0	11.19719487	4.900580768		1.404795935
Area up to 45	0	8.39789615	14.7017423	6.588750745	2.914650794
Area up to 40					2.159723365
WL-4	0	1.199982283	2.179034665	2.510258928	
Area up to 30	0	4.799929133	2.179034665		0.609029483
Area up to 45	0	3.59994685	6.537103996	2.510258928	1.241646734
Area up to 40					0.925338108

