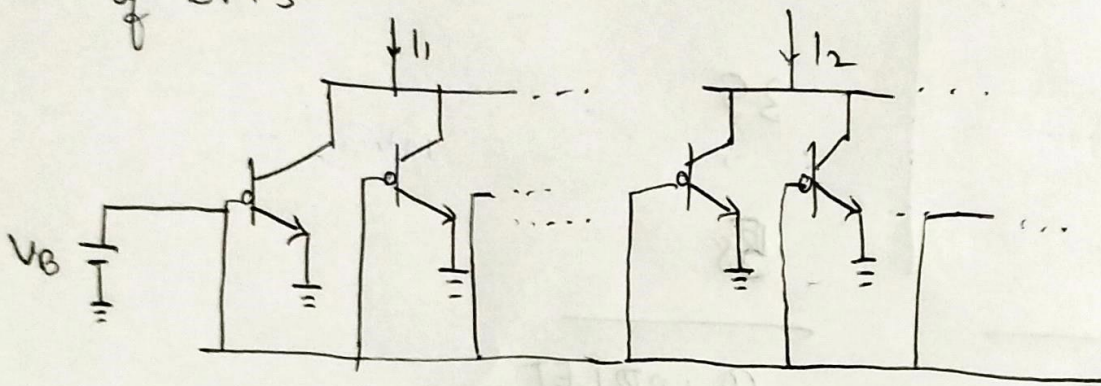


Analog Circuits : Assignment -2

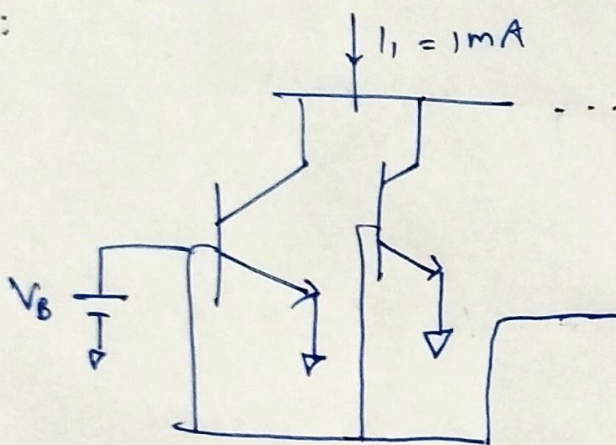
RAHUL MUKUNDHAN
1MT2022S18

Q4) An IC uses $I_1 = 1\text{mA}$ & $I_2 = 1.5\text{mA}$. Assuming only integer multiples of a unit BJT, $(i_s = 3 \times 10^{-16}\text{A})$ can be placed in //, & only V_B is available, make the req. circuit with min. no. of BJTs

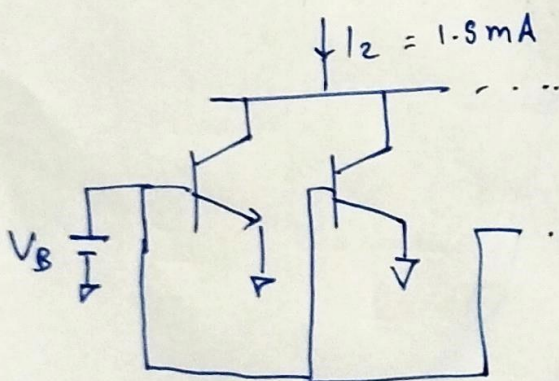


< Assume all BJTs have same i_s , $V_A = \infty$ >
 $V_T = 26\text{mV}$

Ans:



\Rightarrow assume n BJTs



\Rightarrow assume m BJTs

\Rightarrow for I_1 :

$$I_1 = n(I_c) = n(i_s e^{V_{BE}/V_T}) \quad - (1)$$

$$I_2 = m(I_c) = m(i_s e^{V_{BE}/V_T}) \quad - (2)$$

⇒ Divide ① & ②

$$\frac{1}{1.5} = \frac{\eta}{m} \frac{I_s}{I_s} \frac{e^{V_{BE}/V_T}}{e^{V_{BE}/V_T}} = \frac{\eta}{m}$$

< Common V_{BE} , same type of BJT's >

$$\rightarrow \frac{\eta}{m} = \frac{1}{1.5} = \frac{1}{3/2} = \frac{2}{3}$$

$$\therefore \boxed{\eta=2, m=3} \text{ < Assuming integral of BJT's >}$$

⇒ f.f. V_{BE} : use ① or ②

$$\Rightarrow 10^{-3} \times 1 = 2 \times e^{(V_{BE}/V_T)} \times I_s$$

$$\Rightarrow 10^{-3} \times 1/2 I_s = e^{V_{BE}/V_T}$$

$$\Rightarrow V_{BE}^T = 26 \text{ mV} \quad , \quad V_{BE} = V_T \ln \left(\frac{10^{-3}}{2 \times 3} \right)$$

$$< 1 \text{ mA} = 2 \times e^{V_{BE}/V_T} \text{ --- ①, } V_T = 26 \text{ mV} >$$

$$\therefore \boxed{V_{BE} = 731.69 \text{ mV}} \quad (0.73 \text{ V approx})$$

Q2> BJT's relation b/w $I_C - V_{BE}$ is as follows:

$$I_C = I_s e^{V_{BE}/\eta V_T}$$

< same assumptions >

→ η is a constant < like I_s, V_T >

→ Given: $I_C = \beta I_B$. Find small signal model.

Ans: ⇒ Given:

$$I_C = I_s e^{V_{BE}/\eta V_T}$$

$$= \beta I_B$$

Q2)

⇒ For small signal model (π model):

find r_{π} , r_o , r_u , g_m

↳ ignored generally:

⇒ We know that:

$$g_m = \frac{\partial i_c}{\partial V_{BE}}, \quad 1/r_{\pi} = \frac{\partial i_B}{\partial V_{BE}} = \frac{1}{\beta} \frac{\partial i_c}{\partial V_{BE}}$$

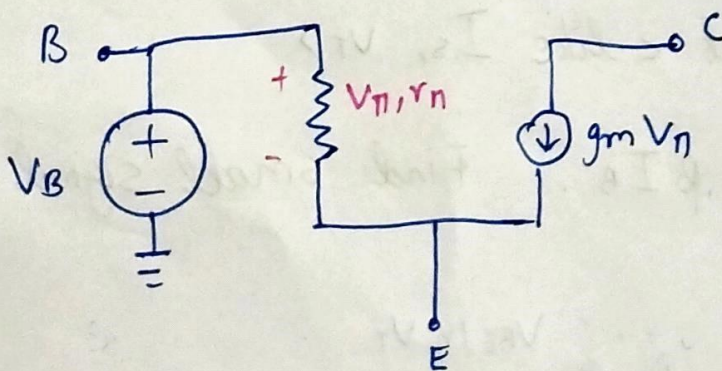
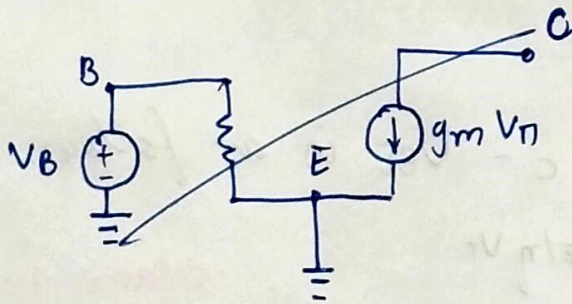
$$\Rightarrow r_{\pi} = \beta / g_m$$

$$\Rightarrow g_m = \frac{\partial}{\partial V_{BE}} (i_s e^{V_{BE}/\eta V_T}) = \frac{i_s e^{V_{BE}/\eta V_T}}{(\eta V_T)} = \frac{i_c}{\eta V_T}$$

$$\Rightarrow r_{\pi} = \frac{\beta \cdot \eta V_T}{i_c} = \beta \eta \left(\frac{V_T}{i_c} \right)$$

⇒ ~~Assume~~ Assuming $V_A = \infty$: ~~$r_o \rightarrow \infty$~~
 $r_o \rightarrow \infty$, so it is ignored

⇒ Small Signal Model:



(V_E can be 0 due to ground)

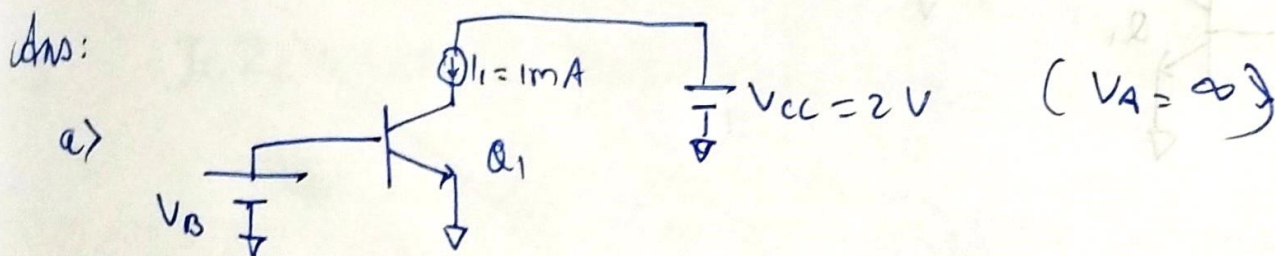
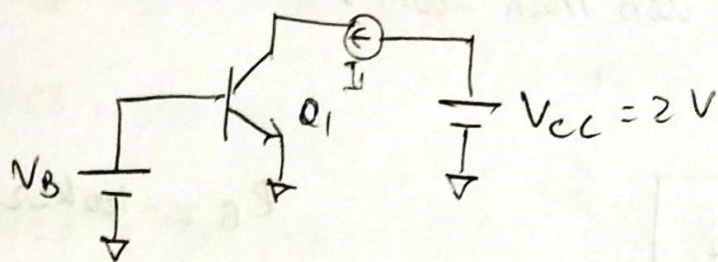
< $V_{\pi} = V_B$, r_{π} is found out >

< Not assuming R_L , R_C here >

Q3) $I_1 = 1 \text{ mA}$, $I_S = 3 \times 10^{-17} \text{ A}$

a) $V_A = \infty$, V_B s.t. $I_C = 1 \text{ mA}$

b) $V_A = 5 \text{ V}$, make V_B s.t. $I_C = 1 \text{ mA}$, $V_{CE} = 3/2 \text{ V}$



\Rightarrow If $V_A = \infty$, it is an ideal BJT:

$$I_1 = I_C = 1 \text{ mA}$$

$$\Rightarrow V_{BE} = V_T \ln \left(\frac{I_C}{I_S} \right)$$

$$= 26 \times 10^{-3} \times \ln \left(\frac{10^{-3}}{3 \times 10^{-17}} \right)$$

$$\boxed{V_{BE} = 809.577 \text{ mV} \approx 0.81 \text{ V}}$$

b) now $V_A = 5 \text{ V}$

$$\Rightarrow I_1 = I_C = 1 \text{ mA}$$

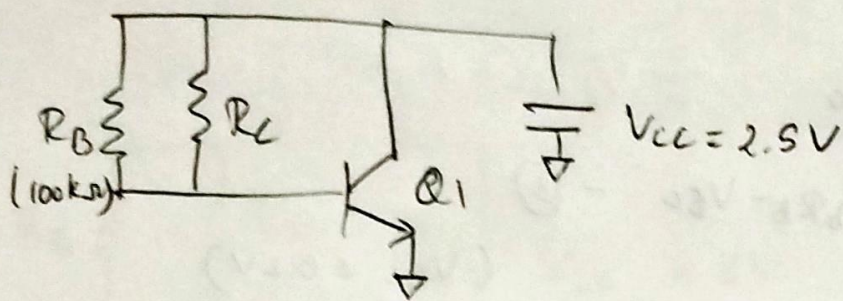
$$\Rightarrow I_C = I_S \left(e^{\frac{V_{BE}}{V_T}} \right) \left[1 + \frac{V_{CE}}{V_A} \right] \quad // \text{ Due to Early Effect}$$

$$\Rightarrow V_{CE} = 3/2 \text{ V}, V_A = 5 \text{ V}$$

$$\rightarrow 10^{-3} = (3 \times 10^{-17}) \times (e^{V_{BE}/V_T}) \times \left(1 + \frac{3}{10} \right)$$

$$\Rightarrow V_{BE} = 26 \times 10^{-3} \times \ln \left(10^{14} / 3.9 \right) \Rightarrow \boxed{V_{BE} = 802.76 \text{ mV} \approx 0.8 \text{ V}}$$

Q4) $V_A = \infty$, $I_S = 2 \times 10^{-17} \text{ A}$, $\beta = 100$. Max value of R_C s.t. collector-base must experience a forward bias $< 200 \text{ mV}$.



Ans: Given:

$$V_{CC} = I_B R_B + V_{BE}$$

$$V_{CC} = I_C R_C + V_{CE}$$

$$V_{CE} = V_{BE} - 0.2 \text{ V} \quad (V_{BE} \leq 0.2 \text{ V})$$

$$\Rightarrow I_C / I_B = 100, R_B = 100 \text{ k}\Omega$$

$$\Rightarrow 2.5 = \frac{I_C}{100} \times 100 \times 10^3 + V_{BE} = 1000 I_C + V_{BE}$$

$$2.5 = I_C R_C + V_{CE}$$

$$\Rightarrow \text{Also, } V_{BE} = V_T \ln \left(\frac{I_C}{I_S} \right)$$

$$V_{BE} = 26 \times 10^{-3} \times \ln \left(\frac{I_C}{I_S} \right)$$

$$\Rightarrow 2.5 = 1000 \left[I_S e^{V_{BE}/V_T} \right] + V_{BE}$$

$$\text{// cross verify with } V_{BE} = 2.5 - 0.8335 \text{ V} \approx 833.5 \text{ mV}$$

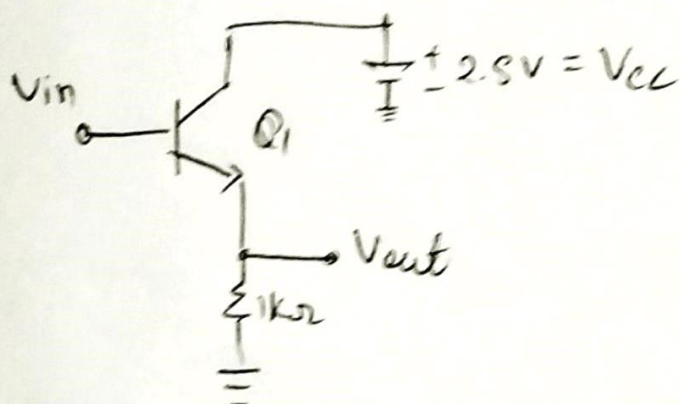
$$\Rightarrow V_{BE} = 833.5 \text{ mV}, I_C = 2 \times 10^{-17} \times e^{(0.8335/0.026)}$$

$$V_{CE} = 633.5 \text{ mV} \quad = 0.00169305$$

$$\Rightarrow R_C = \frac{V_{CC} - V_{CE}}{I_C} = \frac{2.5 - 0.6335}{2 \times 10^{-17} \times 0.00169305} = 1115.63 \Omega \approx 1.12 \text{ k}\Omega$$

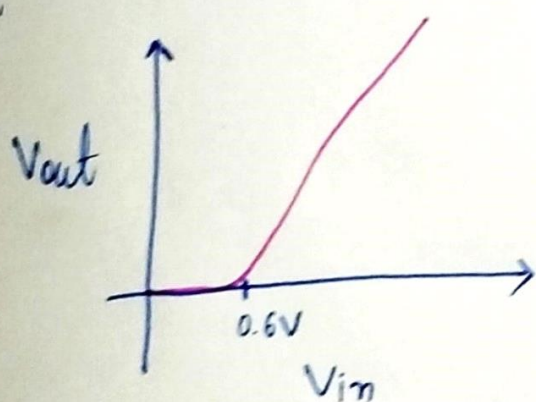
Q5) $V_{in} \in (0, 2.5) V$. What value of V_{in} places transistor at the edge of saturation?

Value of V_{in} s.t. Q_1 has $i_c = 1 mA$

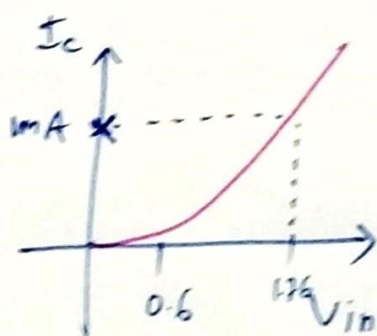
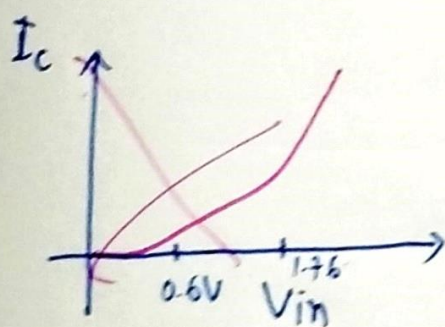


[Assume: $I_s = 5 \times 10^{-16} A$, $\beta = 100$, $V_A = 5V$]

Ans:



$V_{in} = 0.6 V$: edge of saturation



$V_{in} = 1.76 V$, $I_c = 1 mA$