# Prof. Faouzi Bellili — ECE Department (University of Manitoba)

# ECE-4260 Communication Systems

# Assignment#4 (Winter 2025)

### Remarks:

- This assignment is due on March 11th, 2025. Please scan your answers and upload them to UM Learn. Do not e-mail pdf documents.
- Make sure to compile a single PDF document that contains all your answers, i.e., do not submit separate pages and make sure to number your pages.
- Presenting clean and well-justified answers helps you get full marks for questions.
- Assignments submitted after the due date will not be marked.
- Clearly show the solution method. Marks are awarded for the method and not the final answer itself.

## 1. Problem 1 (50 points): Validation of the Carson's rule for bandwidth analysis of FM signals

For an FM modulated signal with (angular) carrier frequency is denoted as  $\omega_c = 2\pi f_c$  and amplitude A > 0:

$$x_{\rm FM}(t) = A\cos\left(\omega_c t + k_f \int_{-\infty}^t m(\tau)d\tau\right),$$
 (1)

and a generic message signal m(t) of bandwidth B Hz, it was shown in the notes that its spectral (or bandwidth) analysis requires the use of a staircase signal approximation which lead us to the so-called Carson's rule. The latter provides an estimate of the required bandwidth,  $B_{\rm FM}$ , of the FM-modulated signal:

$$B_{\rm FM} = 2(\Delta f + B),\tag{2a}$$

$$= 2(\beta + 1)B, \tag{2b}$$

wherein  $\Delta f = k_f m_p/2\pi$  is the maximum frequency deviation with  $m_p = \max |m(t)|$  and  $\beta \triangleq \Delta f/B$  is the so-called frequency deviation ratio.

In this problem, we consider the special case when the message signal m(t) is a sinusoid:

$$m(t) = \alpha \cos(\omega_m t),\tag{3}$$

for which a precise spectral analysis is possible (i.e., no staircase signal approximation is required). Here  $\alpha > 0$  is some nonnegative real-valued amplitude and  $\omega_m = 2\pi f_m$  is the angular frequency of the sinusoid, and the bandwidth of m(t) is  $B_m = \omega_m/2\pi$ . We will use this special case along with its precise spectral analysis to verify the FM bandwidth approximation predicted by the general Carson's rule in (2).

**Part I**: To do so, we start by establishing some algebraic properties of the so-called Bessel function of the first kind and the *n*th order,  $J_n(.)$ , which is defined as (will be encountered later on in this problem):

$$J_n(y) = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{j(y\sin x - nx)} dx, \quad y \in \mathbb{R}, \ n \in \mathbb{Z}.$$

$$(4)$$

1.1) Show that if a function g(x) is periodic with period T, then we have (5 points):

$$\int_0^T g(x)dx = \int_{-T/2}^{T/2} g(x)dx.$$
 (5)

**Hint**: Recall the fact that  $\int_a^c g(x)dx = \int_a^b g(x)dx + \int_b^c g(x)dx$ .

1.2) Deduce that  $J_n(y)$  is also given by (5 points):

$$J_n(y) = \frac{1}{2\pi} \int_0^{2\pi} e^{j(y\sin x - nx)} dx, \quad y \in \mathbb{R}.$$
 (6)

1.3) Deduce from (6) the following relationship (5 points):

$$J_{-n}(y) = (-1)^n J_n(y), (7)$$

1.4) Show that for all  $n \in \mathbb{Z}$  the function  $J_n(y)$  is real-valued. In other words, show that (5 points):

$$J_n(y) \in \mathbb{R} \quad \text{for all} \quad y \in \mathbb{R}$$
 (8)

**Hint**: For any complex number  $z, z \in \mathbb{R}$  if and only if  $z^* = z$ .

**Part II**: Now back to the precise spectral analysis of our FM-modulated signal when the message signal is given by (3). In this part,  $\Re\{.\}$  returns the real part of any complex number and we let:

$$a(t) = \int_{-\infty}^{t} m(\tau)d\tau, \tag{9}$$

1.5) Show that the deviation ratio is given by (5 points):

$$\beta = \frac{k_f \alpha}{\omega}.\tag{10}$$

1.6) With the assumtion that initially  $a(-\infty) = 0$ , show that the FM-modulated signal corresponding to m(t) in (3) is given by (5 points):

$$x_{\rm FM}(t) = A \Re \left\{ z(t)e^{j\omega_c t} \right\}, \tag{11}$$

in which z(t) is given by:

$$z(t) = e^{j\beta\sin(\omega_m t)} \tag{12}$$

1.7) Show that the signal z(t) is periodic with period  $2\pi/\omega_m$ . (5 points).

The Fourier series expansion of z(t) is thus given by

$$z(t) = \sum_{n = -\infty}^{+\infty} z_n e^{jn\omega_m t},\tag{13}$$

with

$$z_n = \frac{\omega_m}{2\pi} \int_{-\pi/\omega_m}^{\pi/\omega_m} z(t)e^{-jn\omega_m t} dt.$$
 (14)

1.8) Show that the *n*th Fourier series coefficient  $z_n$  is given by (5 points):

$$z_n = J_n(\beta). (15)$$

The general algebraic properties of the Bessel function we already established in Part I show that the Fourier series coefficients  $z_n$ 's are real-valued and also  $z_{-n} = (-1)^n z_n$ .

1.9) Show that the FM-modulated signal corresponding to the message signal in (3) is given by (5 points):

$$x_{\rm FM}(t) = A \sum_{n=-\infty}^{+\infty} J_n(\beta) \cos\left(2\pi [f_c + nf_m]t\right). \tag{16}$$

The plots of  $J_n(\beta)$  as a function of n for various values of  $\beta$  are depicted in Fig. 1. There the plots of  $J_n(\beta)$  are depicted for for positive values of n only since you can deduce the values for negative n from the symmetry property shown in (7).

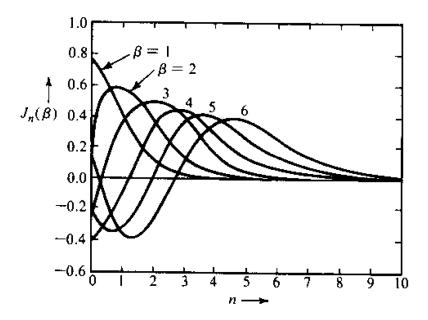


Figure 1: Variations of  $J_n(\beta)$  as a function of n for various values of  $\beta$ .

1.10) Suppose A=2,  $f_m=300$  KHz,  $k_f=2\pi\times 10^5$ , and  $\alpha=6$ . Find and sketch the Fourier transform,  $X_{\rm FM}(f)$  of the modulated signal  $x_{\rm FM}(t)$ . (5 points).

Carson's rule verification: From the plots of  $J_n(\beta)$  in Fig. 1, it can be seen that for a given  $\beta$ ,  $J_n(\beta)$  decreases with n, and there are only a finite number of significant spectral lines (or harmonics). It can be seen from Fig. 1 that  $J_n(\beta)$  is negligible for  $n > \beta + 1$ . Hence the number of significant harmonics (or sideband impulses) is  $\beta + 1$ . The bandwidth of the FM-modulated signal,  $x_{\rm FM}(t)$ , is thus given by:

$$B_{\text{FM}} = 2(\beta + 1)f_m$$
  
=  $2(\Delta f + B)$ 

which is in line with the general Carson's rule in (2).

#### 2. **Problem 2** (25 points): How can you build a spectrum analyzer?

In this problem, you will understand how you can build a real-time spectrum analyzer based on the concept of frequency modulation. The spectrum analyzer equipment which you have used extensively in the labs plots the magnitude spectrum of any input real-valued signal g(t).

## **Part I**: Consider a band-pass real-valued signal g(t) whose Fourier Transform G(f) is depicted in. Fig. 2.

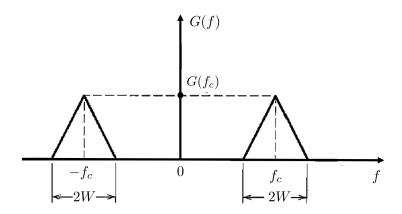


Figure 2: Fourier transform of a band-pass real-valued signal q(t).

Now, consider the following two complex-valued signals:

$$g_{+}(t) = g(t) + j\,\widehat{g}(t), \tag{17}$$

$$\widetilde{g}(t) = g_{+}(t)e^{-j2\pi f_{c}t} \tag{18}$$

wherein  $\widehat{q}(t)$  is given by (\* stands for convolution):

$$\widehat{g}(t) = \frac{1}{\pi t} * g(t). \tag{19}$$

- 2.1) Determine and sketch  $G_{+}(f)$ , the Fourier transform of  $g_{+}(t)$ . (5 points):
- 2.2) Determine and sketch  $\widetilde{G}(f)$ , the Fourier transform of  $\widetilde{g}(t)$  (5 points).
- 2.3) Show that we have (5 points):

$$g(t) = \Re\left\{\widetilde{g}(t)e^{j2\pi f_c t}\right\} \tag{20}$$

The signal  $\widetilde{g}(t)$  is called the complex envelope of the pass-band real-valued signal g(t) or its basebandequivalent representation. Now, consider an LTI system (e.g., filter, channel, etc.) with real-valued impulse response h(t). Assume that the system is also band-pass, i.e., its symmetric frequency response H(f) is non-zero around  $\pm f_c$ . Then using the exact same procedure described above (for band-pass signals) we can also define the low-pass equivalent system with complex impulse response h(t) which satisfies:

$$h(t) = \Re\left\{\widetilde{h}(t)e^{j2\pi f_c t}\right\} \tag{21}$$

Using baseband-equivalent representations, we can easily find the pass-band output, y(t), of a pass-band LTI system to a pass-band input signal, x(t), by simply convolving the (baseband) complex impulse response h(t) with the (baseband) complex envelope of the input signal x(t). In other words, by letting:

$$x(t) = \Re\left\{\widetilde{x}(t)e^{j2\pi f_c t}\right\} \tag{22}$$

$$x(t) = \Re\left\{\widetilde{x}(t)e^{j2\pi f_c t}\right\}$$

$$h(t) = \Re\left\{\widetilde{h}(t)e^{j2\pi f_c t}\right\}$$
(22)

(24)

then the pass-band output y(t) is obtained straightforwardly as:

$$y(t) = \Re\left\{\widetilde{y}(t)e^{j2\pi f_c t}\right\},\tag{25}$$

with

$$\widetilde{y}(t) = \widetilde{h}(t) * \widetilde{x}(t)$$
 (26)

**Part II**: Consider the block diagram shown Fig. 3 with real-valued input signal q(t) and output signal z(t).

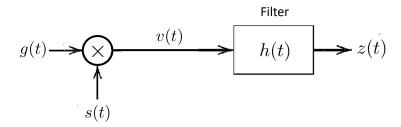


Figure 3: Block diagram of a spectrum analyzer working on the principle of frequency modulation.

The signals s(t) and the filter impulse response h(t) are under our control and are chosen carefully so that the output signal z(t) is the magnitude spectrum of g(t), which a spectrum analyzer would plot for you. One possible choice that does the job as we will now show is to use the following frequency-modulated signals:

$$s(t) = \cos\left(2\pi f_c t - \pi k t^2\right),\tag{27}$$

$$h(t) = \cos\left(2\pi f_c t + \pi k t^2\right),\tag{28}$$

(29)

where k is a constant.

2.4) Show that the complex envelopes  $\widetilde{v}(t)$  and  $\widetilde{h}(t)$  of v(t) and h(t) are given by (5 points):

$$\widetilde{v}(t) = g(t)e^{-j\pi kt^2}, \qquad (30)$$

$$\widetilde{h}(t) = e^{j\pi kt^2}. \qquad (31)$$

$$\widetilde{h}(t) = e^{j\pi kt^2}. (31)$$

(32)

2.5) Deduce that the complex envelope of z(t) is given by (5 points):

$$\widetilde{z}(t) = e^{j\pi kt^2} G(kt),$$
(33)

(34)

where G(f) is the Fourier transform of g(t).

This shows that  $|\tilde{z}(t)| = |G(kt)|$  which means that the envelope of the filter output is equal to the magnitude spectrum of the Fourier transform of the input signal g(t), with kt playing the role of frequency f. In other words, by plotting  $|\tilde{z}(t)|$  you are basically plotting the magnitude spectrum of g(t) and that is how a spectrum analyzer works. FM signals are not just for radio stations!

#### 3. Problem 3 (25 points)

Consider the periodic message signal m(t) shown in Fig. 4 with fundamental period  $T_0$  (i.e., with fundamental angular frequency  $\omega_0 = \frac{2\pi}{T_0}$ ). The Fourier series expansion of m(t) is written as:

$$m(t) = \sum_{-\infty}^{+\infty} m_n e^{jn\omega_0 t} \tag{35}$$

Assume that m(t) is angle-modulated (either FM or PM) to produce  $x(t) = A\cos(\omega_c t + \phi(t))$  whose bandwidth,  $B_x$ , can be estimated using the Carson's rule already studied in Problem 1:

$$B_x = 2(\Delta f + B_m), \tag{36}$$

where  $B_m$  is the essential bandwidth of the message signal m(t) and  $\Delta f$  is the maximum instantaneous frequency deviation from the carrier frequency  $f_c = \omega_c/2\pi$ .

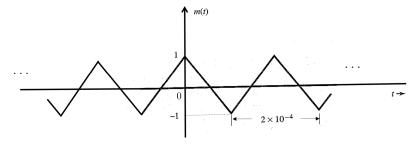


Figure 4: Plot of the periodic message signal m(t).

Now, let g(t) be any periodic signal with fundamental period  $T_0$  (i.e., with fundamental angular frequency  $\omega_0 = \frac{2\pi}{T_0}$ ) and let  $\dot{g}(t) = \frac{dg(t)}{dt}$  which is also periodic with period  $T_0$ . The Fourier series expansion of g(t) and  $\dot{g}(t)$  are given by:

$$g(t) = \sum_{-\infty}^{+\infty} g_n e^{jn\omega_0 t} \qquad \text{and} \qquad \dot{g}(t) = \sum_{-\infty}^{+\infty} \dot{g}_n e^{jn\omega_0 t}$$
(37)

where

$$g_n = \frac{\omega_0}{2\pi} \int_{-\pi/\omega_0}^{+\pi/\omega_0} g(t)e^{-jn\omega_0 t} dt \qquad \text{and} \qquad \dot{g}_n = \frac{\omega_0}{2\pi} \int_{-\pi/\omega_0}^{+\pi/\omega_0} \dot{g}(t)e^{-jn\omega_0 t} dt.$$
 (38)

3.1) Show that the Fourier series coefficients of g(t) and  $\dot{g}(t)$  are related as (5 points):

$$\dot{q}_n = jn\omega_0 q_n \tag{39}$$

3.2) In light of (39), show that the Fourier series coefficients of m(t) are given by (5 points):

$$m_n = \begin{cases} \frac{4}{\pi^2 n^2} & \text{if } n \text{ is odd} \\ 0 & \text{if } n \text{ is even} \end{cases}$$
 (40)

- 3.3) Find the power  $P_m$  of m(t) using direct integration. (2.5 points).
- 3.4) Find  $P_m$  again using Parseval's theorem for periodic signals. (2.5 points).

**Note:** we have  $\sum_{k=0}^{+\infty} \frac{1}{(2k+1)^4} = \frac{\pi^4}{96}$ .

- 3.5) Assume the essential bandwidth of the periodic signal m(t) as the frequency of its third harmonic. Estimate the bandwidth  $B_{\rm FM}$  and  $B_{\rm PM}$  of the frequency-modulated and phase-modulated signals associated with the message signal m(t). Take  $k_f = 2\pi \times 10^5$  and  $k_p = 5\pi$ . (5 points).
- 3.6) Assume that the amplitude of m(t) is doubled to produce another message signal m'(t) = 2m(t). Find  $B'_{FM}$  and  $B'_{PM}$  associated with m'(t) for the same values of  $k_f$  and  $k_p$  given in the previous question. (5 points).