

Hands on computer session:

## 2. Compressible flow through a converging diverging nozzle

[Time: 1 h]

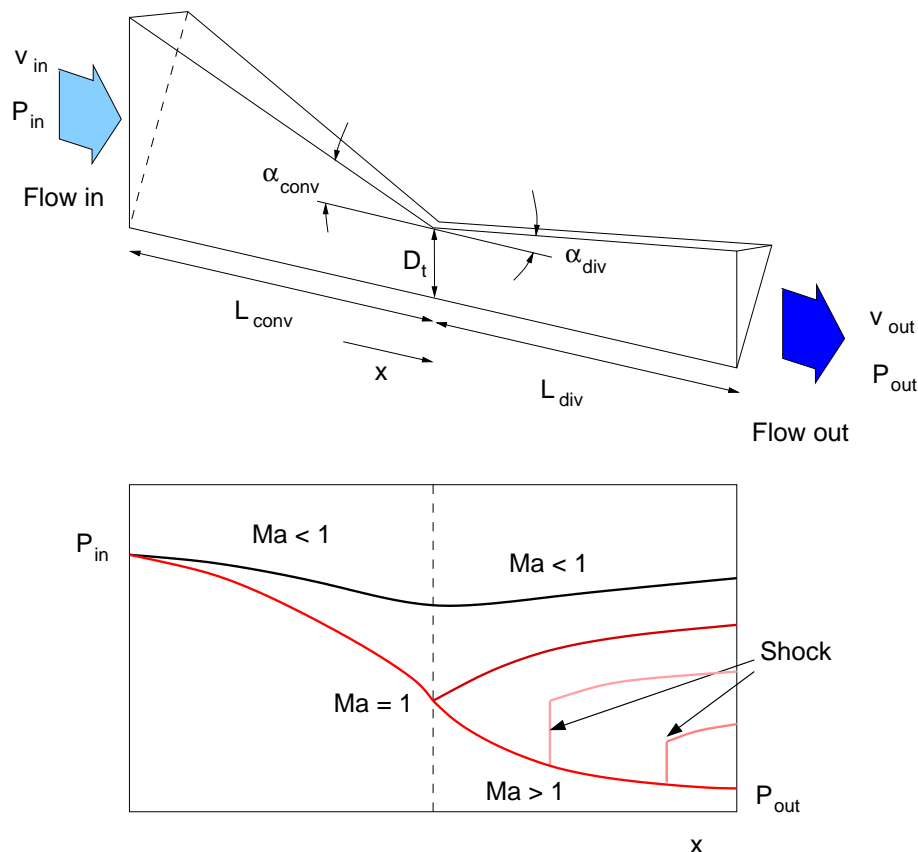
### Objects

- choice of computational domain and definition of optimal boundary conditions
- techniques to obtain a smooth meshing of a “complex” domain, “a posteriori” checks for accuracy against theory, tools for adaptive grid refinement;
- identification of reference data, calculation of global quantities;
- balancing accuracy vs computational time and resources;
- use of MACRO for problem set up and resolution, use of INTERNAL BOUNDARY for post-processing;

### Physical problem

Flow of compressible fluid accelerating in the convergent and decelerating in the divergent part of the nozzle:

- different flow regimes are possible depending on flow rate (or inlet/outlet pressure difference) and geometry of the nozzle (subsonic/sonic/supersonic flow);
- nozzle geometry controls efficient recovery of pressure energy;
- a shock wave may form in the divergent.



## Data

Throat diameter	$D_t = 30 \text{ mm}$
Ratio of exit area ( $A_e$ ) to the throat area ( $A_t$ )	$A_e/A_t = 4$
Convergent length	$L_{conv} = 40 \text{ mm}$
Divergent length	$L_{div} = 160 \text{ mm}$
Inlet Pressure	$P = 600 \text{ kPa}$
Inlet Temperature	$T = 293 \text{ K}$
Outlet Pressure	$P = 600 \text{ kPa} \div 0 \text{ kPa}$

## Worksheet

Mesh generation	<ul style="list-style-type: none"> <li>• evaluate number of required grid nodes (wall layer and streamwise resolution), with specific attention to the divergent part of the nozzle (flow detachment from the wall, possible shock region)</li> <li>→ use patches to generate blocks of cells</li> </ul>
Boundary conditions	<ul style="list-style-type: none"> <li>→ use cyclic B.C. to set up a bidimensional simulation</li> <li>→ use Pressure at inlet and Pressure at outlet</li> <li>→ use INTERNAL boundary conditions to monitor flow rate at throat</li> <li>→ use a TABLE to decrease the pressure at outlet</li> </ul>
Initial conditions	<ul style="list-style-type: none"> <li>• outlet pressure equal to inlet pressure</li> </ul>
Solution method	<ul style="list-style-type: none"> <li>• transient simulation, with variation of outlet B.C.</li> <li>→ choice of relaxation factor</li> <li>→ choice of differencing scheme</li> <li>• comparison with steady state simulation (at each regime)</li> </ul>
Results	<ul style="list-style-type: none"> <li>→ use of SENSOR to plot pressure and Mach variation along the nozzle axis</li> <li>→ identification of shock region, adaptive grid refinement to capture the sharp pressure gradient at the shock line</li> <li>→ use of MACRO and fortran coding to evaluate thrust at nozzle exit</li> </ul>

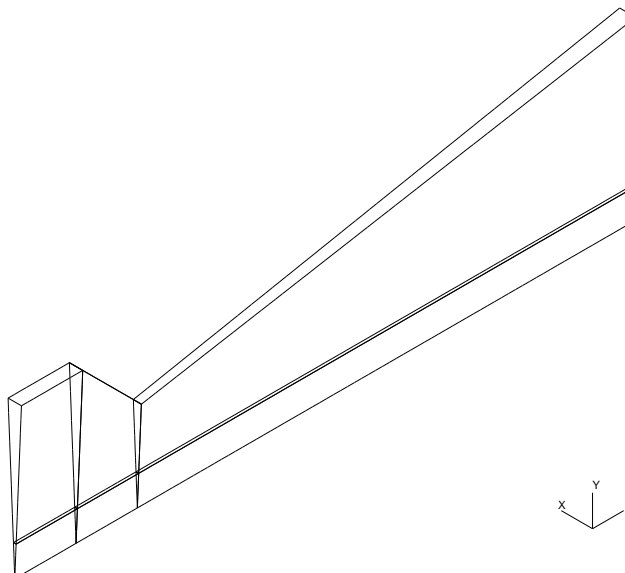
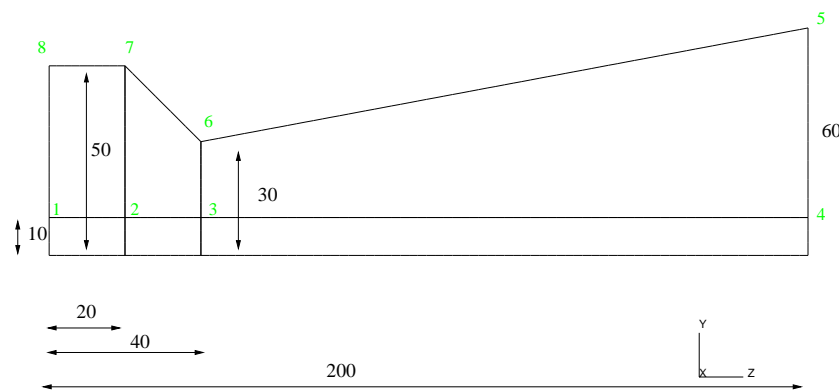
## References

Hadjadj, A., Nebbache, A., Vuillamy, D. and Vandromme, D. (1997), "Numerical simulation of flow separation in rocket nozzle", *Mechanics research Communications*, **24**, 269-276.

Hussaini, M. M., and Korte J. J., (1996), "Investigation of low Reynolds number rocket nozzle design using PNS-based optimization procedure", *NASA Technical Memorandum 110295*.

<http://www.engapplets.vt.edu/fluids/CDnozzle>

## Geometry



## MACROS

```

|*****
! Geometry.MAC *
|*****
|_____
|*** generation of points and splines
|_____
csys 2
v 1 10 92.5 0
v 2 10 92.5 20
v 3 10 92.5 40
v 4 10 92.5 200
v 5 60 92.5 200
v 6 30 92.5 40
v 7 50 92.5 20
v 8 50 92.5 0
|_____
|*** generation of patches and 2D geometry
|_____
ctab 4 shell 2
patch 1 2 7 8 10 10
ctab 5 shell 3
patch 2 3 6 7 10 10
patch 3 4 5 6 70 10
vmer all
c
vcomp all
y
cset all
cplo
|_____
|*** extrusion of 2D geometry and creation of 3D mesh
|_____
csys 2
vcextrude,1,mini,cset,,,local,,-5,,both
cset news fluid
view,-1,1,1
cset news shell
cdel cset
ccomp all
y
cset all
ctype 1
cmod cset
get coff mxce
cflip,1,coff,1,right
vc3d 0 10 3 87.5 92.5 1 0 20 10
vc3d 0 10 3 87.5 92.5 1 20 40 10
vc3d 0 10 3 87.5 92.5 1 40 200 70
cset all
vmer all
c

```

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```
vcomp all
```

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y
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cset all
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view,-1,0,0
```

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cplo
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!_____
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```
!*** save the model
```

```
!_____
```

```
save exe2.mdl
```

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!*****
```

```
! scalar-axis.MAC *
```

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!*****
```

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!_____
```

```
!*** load transient solution
```

```
!_____
```

```
trload,exe2.pstt,nomvgr,,c
```

```
_____
```

```
—*** loop definition
```

```
!_____
```

```
!*define
```

```
stor next
```

```
getv,T
```

```
greset
```

```
y
```

```
sens dele all
```

```
cset all
```

```
gpost,points,nomap,50,1,0,0.1,0,0,0.1,200
```

```
frame,1,xreg,init,2
```

```
frame,1,xrange,0,200
```

```
frame,1,xtitle,4.3,1.5
```

```
DISTANCE
```

```
frame,1,yreg,init,9
```

```
frame,1,yrange,200,300
```

```
frame,1,ytitle,0.5,5.5
```

```
T
```

```
!scdu,gif,frm
```

```
gdraw,1
```

```
!scdu,off
```

```
!*END
```

```
!*loop 1 70
```

```
!*****
```

```
! animation.MAC *
```

```
!*****
```

```
!_____
```

```
!*** load transient solution
```

```
!_____
```

```
trload,exe2.pstt,nomvgr,,c
```

```
cset news fluid
```

```
cplo
csca,20,user,0,4,,
!csca,20,auto
!_____
!*** loop definition
!_____
DEFI
STOR NEXT
!GETC all
oper,getc,t,1,absolute
oper,smul,402.768,1,1
oper,sqrt,1,2
oper,getc,sw,3
oper,divi,3,2,4
CAVER CSET
PLTB ON
REPLOT
PLTB OFF
END
LOOP 1 101

!*****
! film-2windows.MAC *
!*****
!_____
!*** load transient solution
!_____
TRLOAD,,
N
window,default
window,divi,2,1
POPT,CONT
PLTY EHID
CSET NEWS FLUID
TRINTERPOLATE,ON,CAVER CSET
!_____
!*** loop definition
!_____
SET FRM 1001 1
DEFI NOEX
STOR NEXT
window,activate,1,1
pldi,off,all
oper,getc,t,1,absolute
oper,smul,402.768,1,1
oper,sqrt,1,2
oper,getc,sw,3
oper,divi,3,2,4
caver,cset
CSCA,20,user,0,4,,
pldi,on,scale
PLDI,ON,TITLE
```

TITLE

NOZZLE - Mach Field and Axis Pressure

CPLO

window,activate,next

getv,pstat,relative

greset

y

sens dele all

csys 1

gpost,points,nomap,50,1,0,1,0,0,1,200

frame,1,xreg,init,2

frame,1,xrange,0,200

frame,1,xtick,50,0,integer,

frame,1,yreg,init,9

frame,1,yrange,-600000,0

frame,1,ytick,0,1000,real,right

frame,1,ytitle,0.5,3.5

PRESSURE

grdisp,1,off,yscale

SCDU,GIF,FRM

gdraw,1

SCDU,OFF

END

LOOP,1,300,1