



16.485: VNAV - Visual Navigation for Autonomous Vehicles

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整理: 范浩



based on slides by Markus Ryll

Lecture Outline

- 四旋翼的动力学模型 (Dynamical model of a Quadrotor)
- 四旋翼无人机的动力模型介绍
- 四旋翼无人机的动力飞控模型介绍

Agile Navigation with Aerial Vehicles

- 一点也不流线型的无人机，要空气动力学有啥用？【差评君】_哔哩哔哩_bilibili
- 四轴无人机的结构及飞行原理_哔哩哔哩_bilibili



设计理念 Design Concepts

- Single rotor



- ⊕ ✓ Good Controllability and maneuverability
- ⊖ - Complex mechanics
- ⊖ - Large rotor

- Tandem rotor



- ⊕ ✓ Good Controllability and maneuverability
- ⊖ - Complex mechanics
- ⊖ - Large size

- Coaxial rotor



- ⊕ ✓ Compactness
- ⊕ ✓ Simple mechanics
- ⊖ - Complex aerodynamics

- Quadrotor



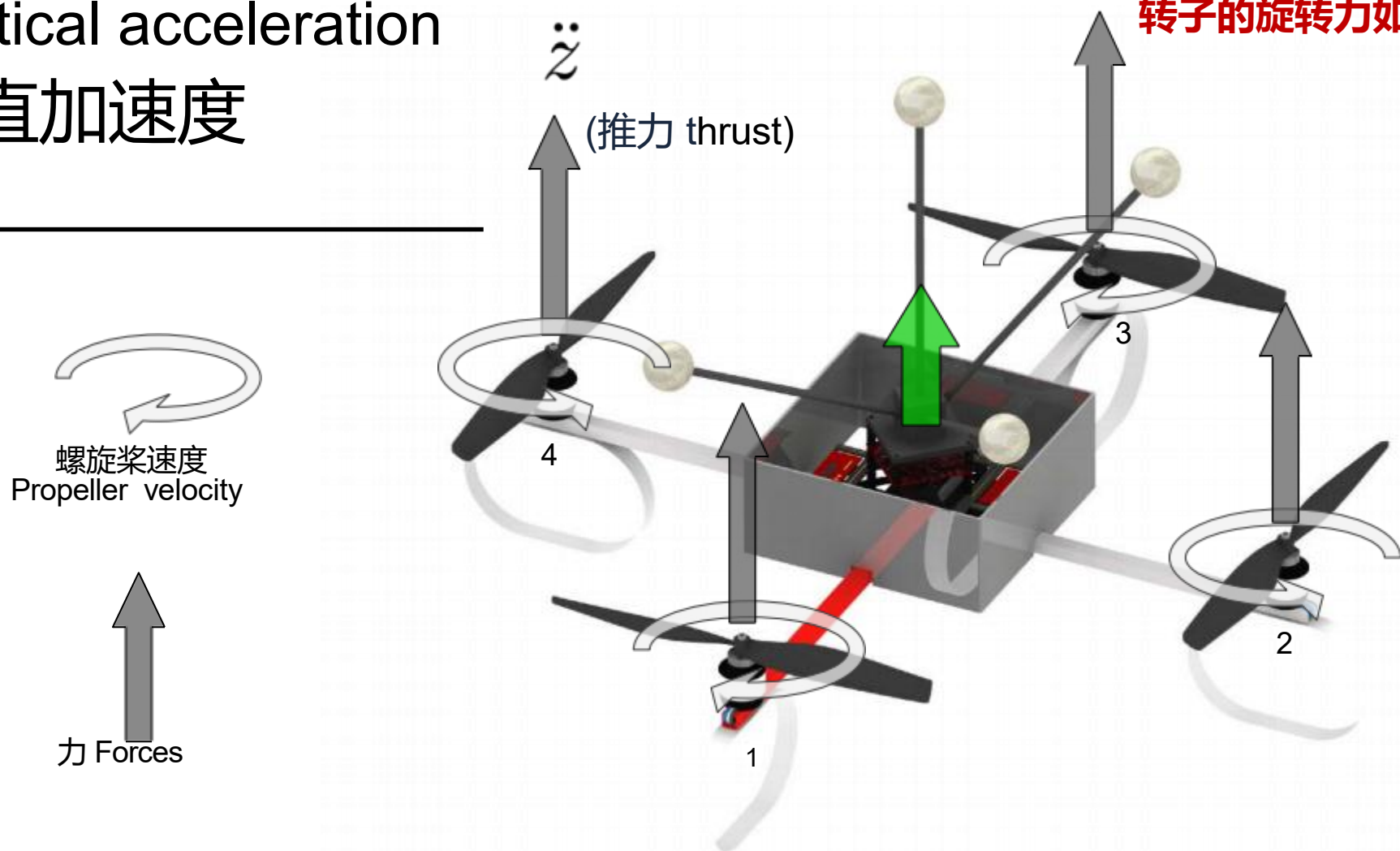
- ⊕ ✓ Good maneuverability
- ⊕ ✓ Simple mechanics
- ⊕ ✓ Big payload
- ⊖ - High energy consumption

设计理念 Design Concepts

[看了这个视频才知道，无刷电机的结构原理原来这么简单_哔哩哔哩_bilibili](#)

Vertical acceleration
垂直加速度

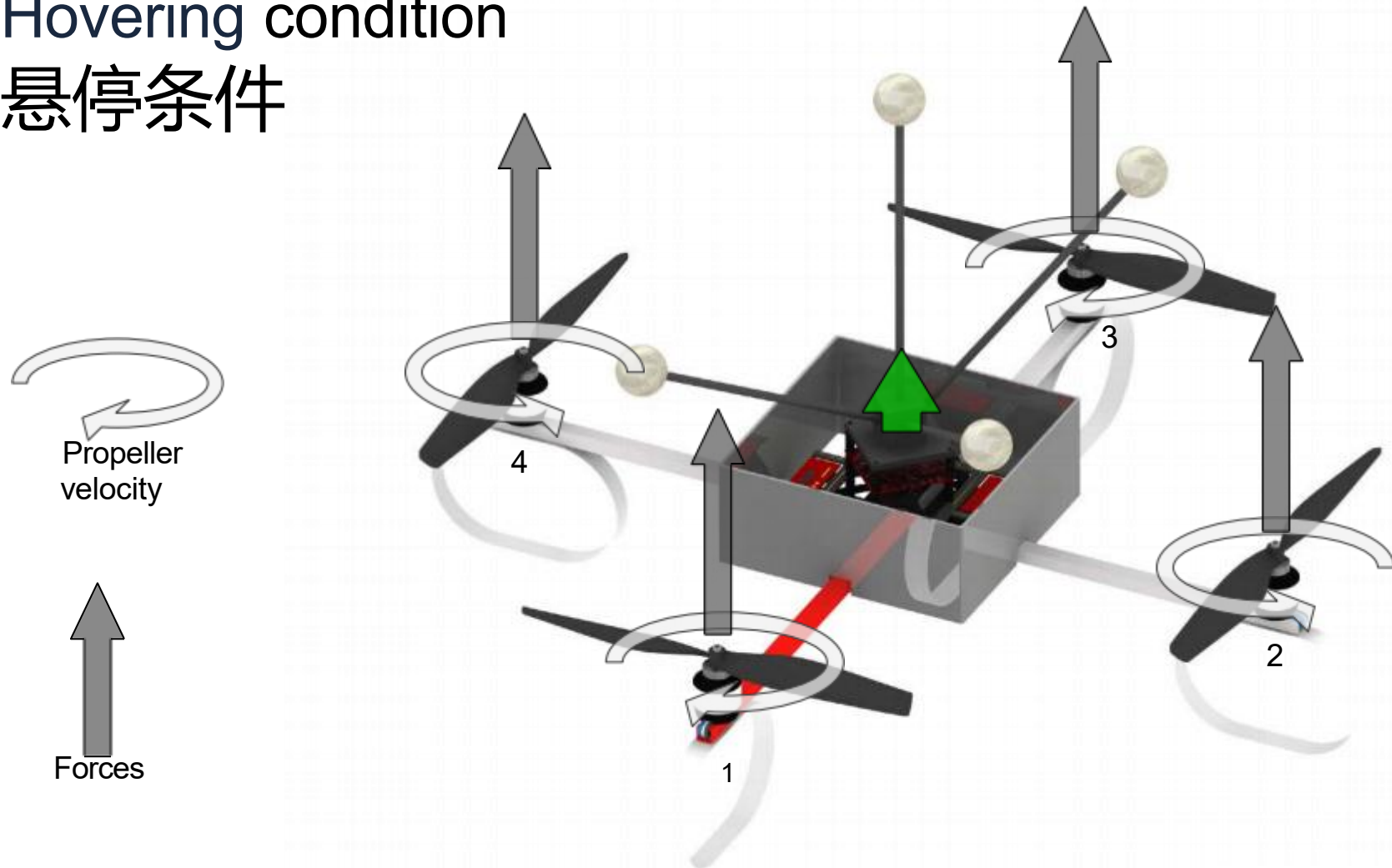
转子的旋转力如何分析？



四旋翼的旋转方向，利用对称力矩抵消自旋。

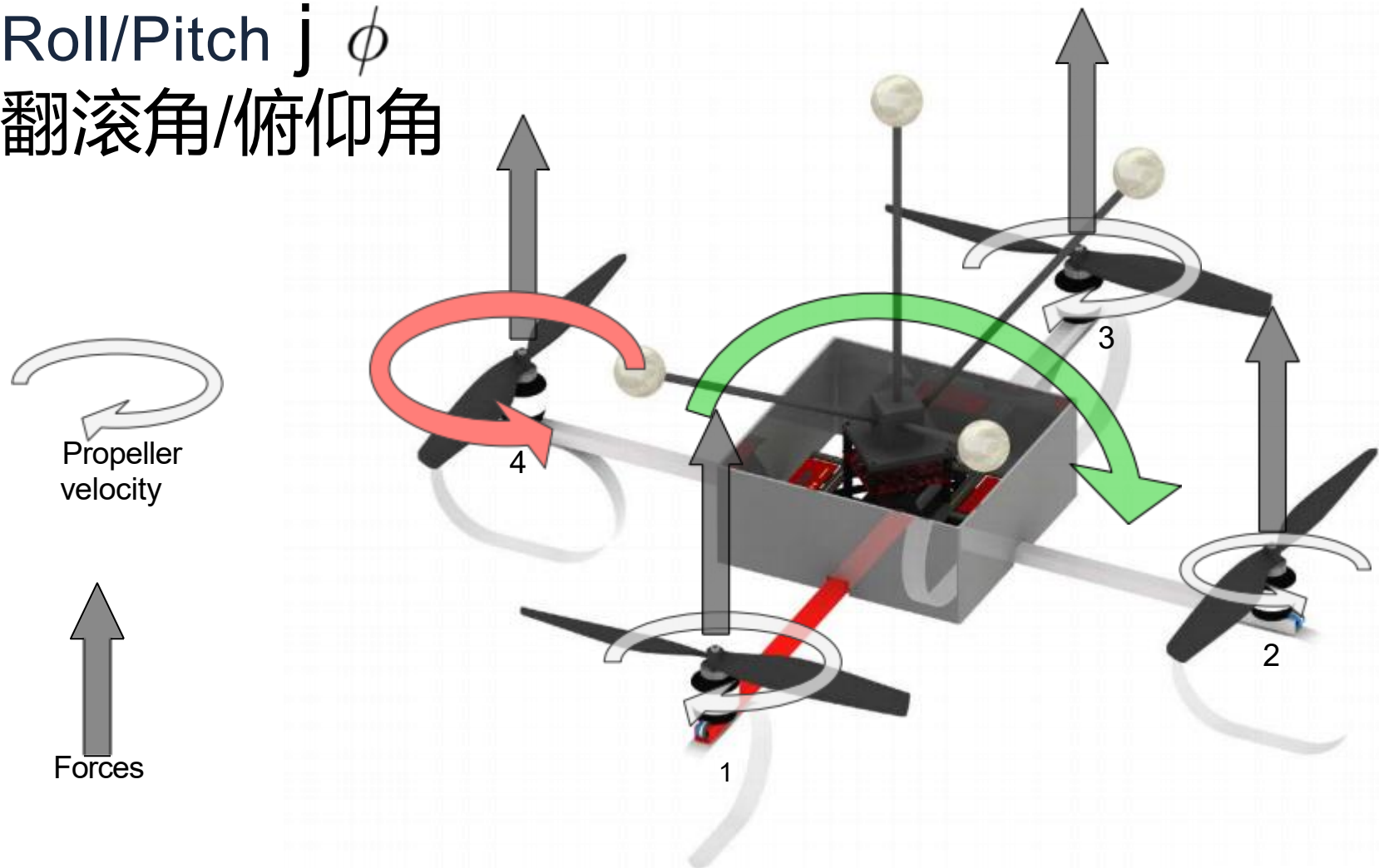
Design Concepts

Hovering condition
悬停条件



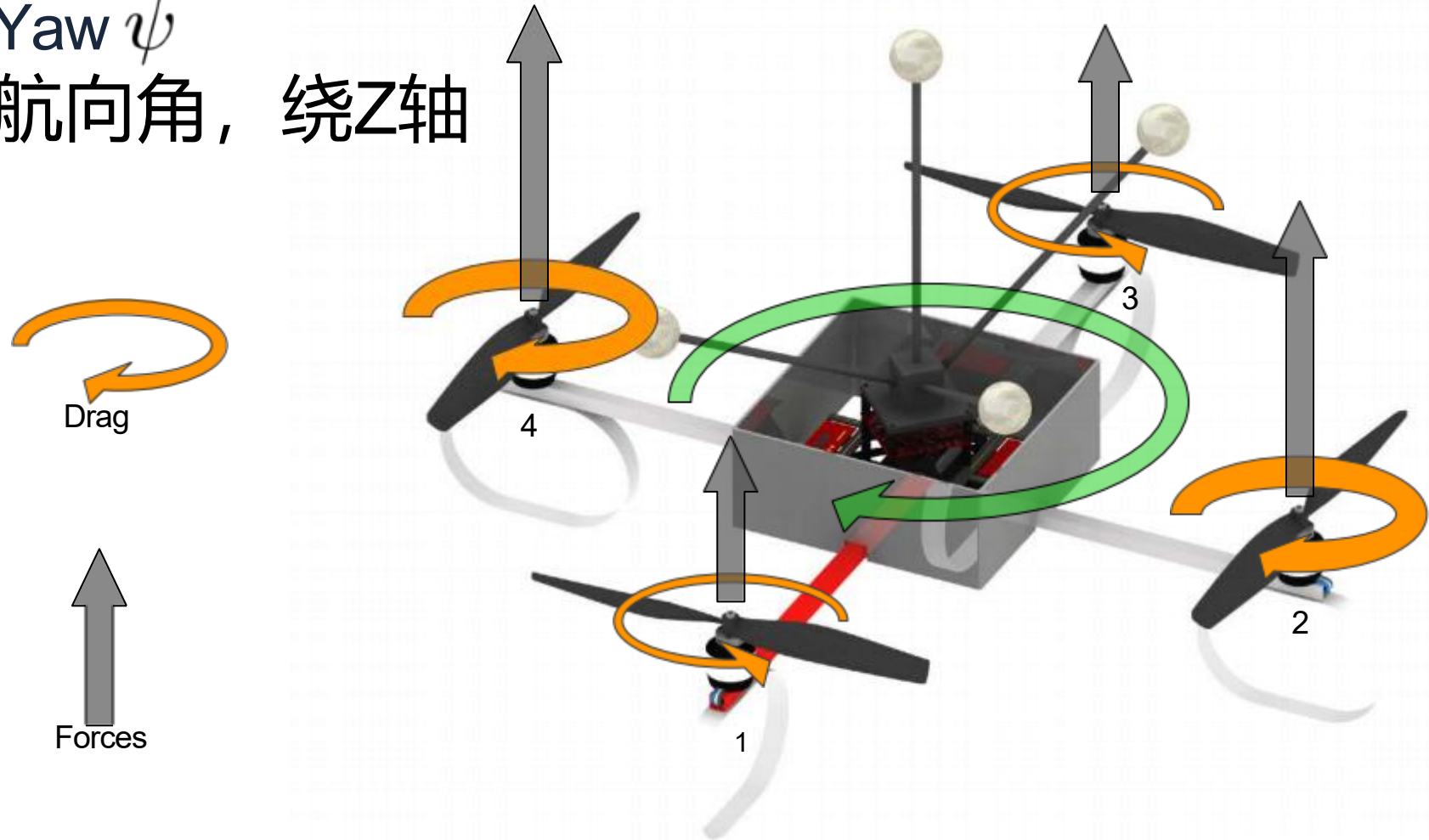
Design Concepts

Roll/Pitch $\ddot{\phi}$
翻滚角/俯仰角



Design Concepts

Yaw $\ddot{\psi}$
航向角，绕Z轴



System view

无人机的工作原理_哔哩哔哩_bilibili

飞行控制器-FC

无线传输

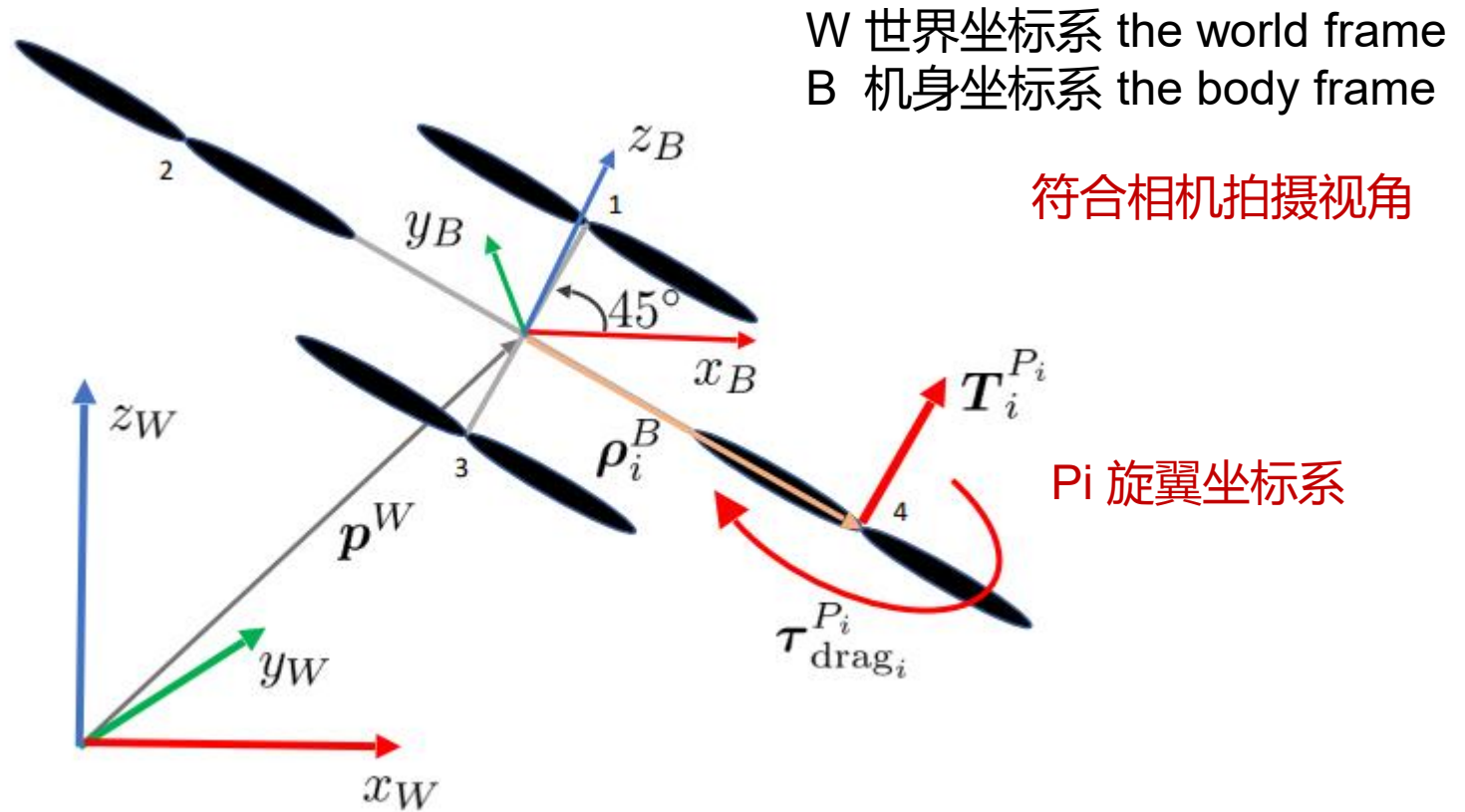
操控信号



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四旋翼无人机模型



Thrust 推力

Tor 力矩, 扭矩

ρ_i^B being the position (vector) of the propeller i in the body frame.

四旋翼无人机模型

- 刚体的旋转与平移.

$$\begin{bmatrix} \mathbf{f}^B \\ \boldsymbol{\tau}^B \end{bmatrix} = \begin{bmatrix} m\mathbf{I}_3 & \mathbf{0} \\ \mathbf{0} & \mathcal{J} \end{bmatrix} \begin{bmatrix} \mathbf{a}^B \\ \boldsymbol{\alpha}^B \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ \boldsymbol{\omega}^B \times \mathcal{J}\boldsymbol{\omega}^B \end{bmatrix}$$

如何理解?

推力 $\mathbf{f}^B \in \mathbb{R}^3$

力矩 $\boldsymbol{\tau}^B \in \mathbb{R}^3$

$m \in \mathbb{R}_+$

$\mathcal{J} \in \mathbb{R}^{3 \times 3}$

\mathbf{I}_n

加速度 $\mathbf{a}^B \in \mathbb{R}^3$

角加速度 $\boldsymbol{\alpha}^B \in \mathbb{R}^3$

$\boldsymbol{\omega}^B \in \mathbb{R}^3$

角速度

applied total forces expressed in the body frame

applied total torques expressed in the body frame

body mass 机身质量 关于质心的转动惯量

moment of inertia about the center of mass

$n \times n$ identity matrix

translational acceleration of the center of mass expressed in the body frame

angular acceleration of the body expressed in the body frame

angular velocity of the body expressed in the body frame

四旋翼无人机模型

- 在世界坐标系 “w” 下的推力:

$$\begin{bmatrix} f^w \\ \tau^B \end{bmatrix} = \begin{bmatrix} R_B^w & 0 \\ 0 & I_3 \end{bmatrix} \begin{bmatrix} mI_3 & 0 \\ 0 & \mathcal{J} \end{bmatrix} \begin{bmatrix} a^B \\ \alpha^B \end{bmatrix} + \begin{bmatrix} 0 \\ \omega^B \times \mathcal{J} \omega^B \end{bmatrix}$$

- 考虑的第一个外力是重力，其他力和扭矩是由于空气动力学效应造成的. 空气动力学的影响

$$\begin{bmatrix} f^w \\ \tau^B \end{bmatrix} = \begin{bmatrix} R_B^w & 0 \\ 0 & I_3 \end{bmatrix} \begin{bmatrix} mI_3 & 0 \\ 0 & \mathcal{J} \end{bmatrix} \begin{bmatrix} a^B \\ \alpha^B \end{bmatrix} + \boxed{\begin{bmatrix} -mg^w \\ \omega^B \times \mathcal{J} \omega^B \end{bmatrix}}$$

推力 thrust force

- 在第一个近似中，单个旋翼 i 的推力，以旋翼 i 的参考系（又名螺旋桨架 P_i ）表示，可以计算为

$$\mathbf{T}_i^{P_i} = c_f w_i |w_i| \mathbf{e}_3 \quad c_f \text{ 是常量, } \mathbf{e}_3 = [0, 0, 1]^T.$$

- $w_i |w_i|$ 是转子旋转速度的有符号平方.

$$\mathbf{f}_{thrust}^B = \sum_{i=1}^4 \mathbf{R}_{P_i}^B \mathbf{T}_i^{P_i};$$

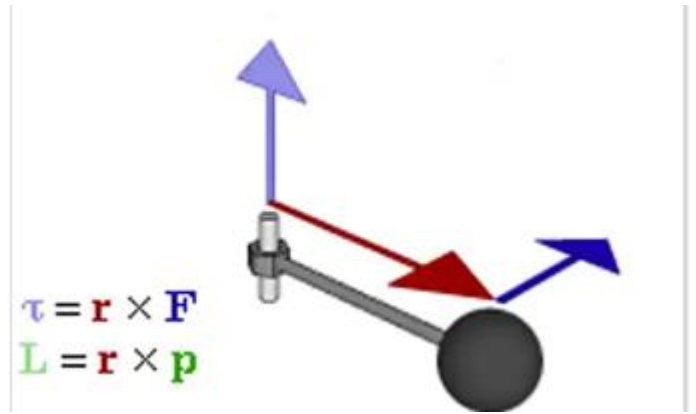
$\mathbf{R}_{P_i}^B$ being the rotation matrix from propeller- to body-frame
($\mathbf{R}_{P_i}^B = \mathbf{I}_3$ for standard quadrotors)

力矩 torque

- 力矩包含2个部分:

转子拖力 + 桨叶升力分力--推力

$$\tau^B = \tau_{drag}^B + \tau_{thrust}^B$$



转子拖力 $\tau_{drag}^B = \sum_{i=1}^4 R_{P_i}^B \tau_{drag_i}^{P_i}$

$$\tau_{drag_i}^{P_i} = (-1)^{(i+1)} c_d w_i |w_i| e_3$$

桨叶升力分力 $\tau_{thrust}^B = \sum_{i=1}^4 (\rho_i^B \times R_{P_i}^B T_i^{P_i})$

ρ_i^B being the position (vector) of the propeller i in the body frame.

- 力矩是一个**矢量**，定义是距离与力的**叉乘**。力矩的**量纲**是 ML^2T^{-2} ，在国际单位制中的单位是 $\text{kg} \cdot \text{m}^2 \cdot \text{s}^{-2}$ 。
- 力矩会改变物体的**角动量**，即物体的转动性质，或者使物体发生扭曲。处于平衡状态的物体不仅受力为零，所受力矩也为零。

四旋翼模型 Quadrotor model

- 模型中的力和力矩 the forces and torques

$$\begin{bmatrix} m\mathbf{a}^w \\ \mathcal{J}\alpha^B \end{bmatrix} = \begin{bmatrix} m\mathbf{g}^w \\ -\omega^B \times \mathcal{J}\omega^B \end{bmatrix} + \begin{bmatrix} R_B^w & 0 \\ 0 & I_3 \end{bmatrix} \begin{bmatrix} f_{thrust}^B \\ \tau_{drag}^B + \tau_{thrust}^B \end{bmatrix} = \begin{bmatrix} -m\mathbf{g}e_3 \\ -\omega^B \times \mathcal{J}\omega^B \end{bmatrix} + \begin{bmatrix} R_B^w & 0 \\ 0 & I_3 \end{bmatrix} Fw$$

$$\begin{bmatrix} f_x^B \\ f_y^B \\ f_z^B \\ \tau_x^B \\ \tau_y^B \\ \tau_z^B \end{bmatrix} = Fw = \begin{bmatrix} c_f e_3 & c_f e_3 & c_f e_3 & c_f e_3 \\ c_d e_3 + c_f \rho_1^B \times e_3 & -c_d e_3 + c_f \rho_2^B \times e_3 & c_d e_3 + c_f \rho_3^B \times e_3 & -c_d e_3 + c_f \rho_4^B \times e_3 \end{bmatrix} w$$

最终想得到的转速向量
W=[w1,w2,w3,w4]T

- 最后，我们观察到（线性和角）速度和加速度由以下方式相关：

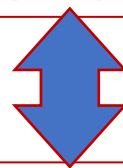
$$\begin{aligned} \dot{p}^w &= v^w & \dot{v}^w &= a^w \\ \dot{R}_B^w &= R_B^w [\omega^B]^\wedge & \dot{\omega}^B &= \alpha^B \end{aligned}$$

四旋翼模型 Quadrotor model

- 基于一阶微分方程的四旋翼动力学模型:

$$\begin{aligned}\begin{bmatrix} m\dot{\boldsymbol{v}}^{\text{w}} \\ \mathcal{J}\dot{\boldsymbol{\omega}}^{\text{B}} \end{bmatrix} &= \begin{bmatrix} -mge_3 \\ -\boldsymbol{\omega}^{\text{B}} \times \mathcal{J}\boldsymbol{\omega}^{\text{B}} \end{bmatrix} + \begin{bmatrix} \boldsymbol{R}_{\text{B}}^{\text{w}} & \mathbf{0} \\ \mathbf{0} & \boldsymbol{I}_3 \end{bmatrix} \boldsymbol{F}\boldsymbol{w} \\ \dot{\boldsymbol{p}}^{\text{w}} &= \boldsymbol{v}^{\text{w}} \\ \dot{\boldsymbol{R}}_{\text{B}}^{\text{w}} &= \boldsymbol{R}_{\text{B}}^{\text{w}}[\boldsymbol{\omega}^{\text{B}}]^{\wedge} \end{aligned}$$

the *state* of the quadrotor is $\boldsymbol{p}^{\text{w}}, \boldsymbol{v}^{\text{w}}, \boldsymbol{R}_{\text{B}}^{\text{w}}, \boldsymbol{\omega}^{\text{B}}$ and the *control actions*



the propeller velocities, included in the vector \boldsymbol{w} .

差平整度特性

- 在本节中，我们表明以螺旋桨 w 的四个角速度为输入的四旋翼动力学是微分平坦的。
- 状态和输入可以写成四个精心挑选的平面输出及其导数的代数函数。我们选择的平坦输出由下式给出

$$\boldsymbol{\sigma} = [\sigma_1 \ \sigma_2 \ \sigma_3 \ \sigma_4]^T = [x, \ y, \ z, \ \psi]^T,$$

where $\mathbf{p}^w = [x, \ y, \ z]^T$ are the coordinates of the center of mass of the quadrotor in the world coordinate system and ψ is the yaw angle. We will define a trajectory, $\boldsymbol{\sigma}(t)$, as a smooth curve in the space of flat outputs:

$$\boldsymbol{\sigma}(t) : [t_o, t_m] \rightarrow \mathbb{R}^3 \times SO(2). \quad (6.26)$$

➤ [四旋翼动力模型推导_哔哩哔哩_bilibili](#)

[多旋翼无人机偏航运动与反扭力的深度解析](#)

Lecture Outline

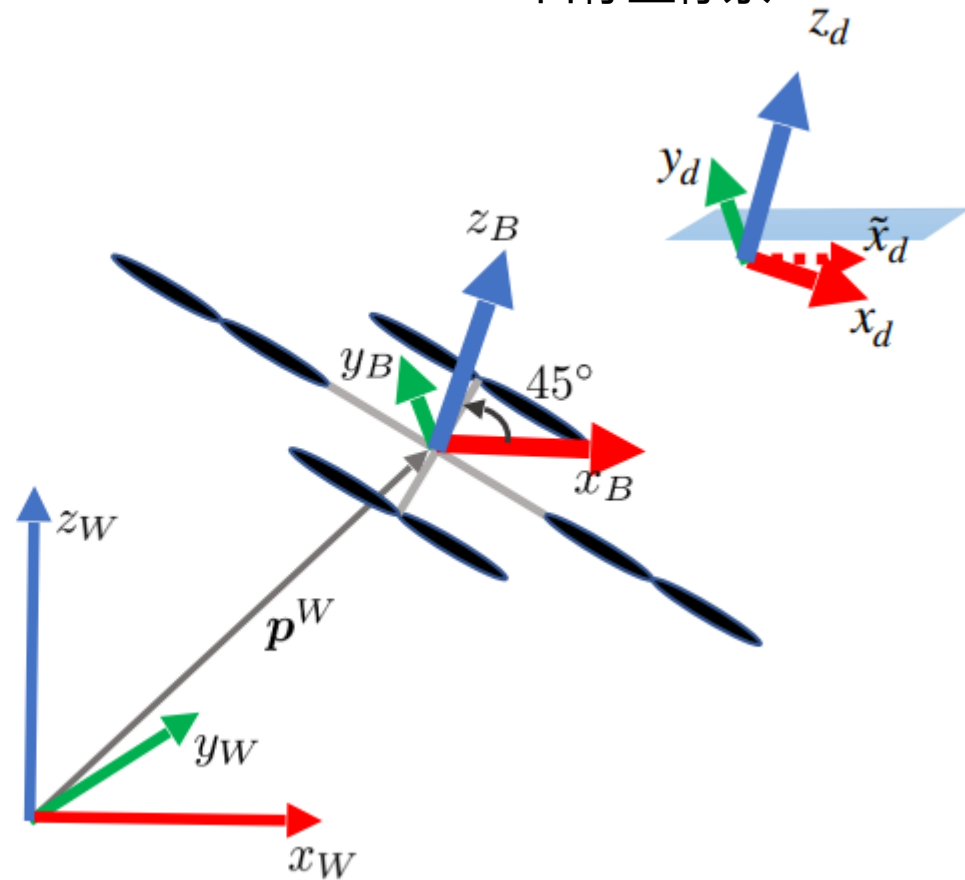
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四旋翼控制器

W 世界坐标系 the world frame
B 机身坐标系 the body frame
d 目标坐标系

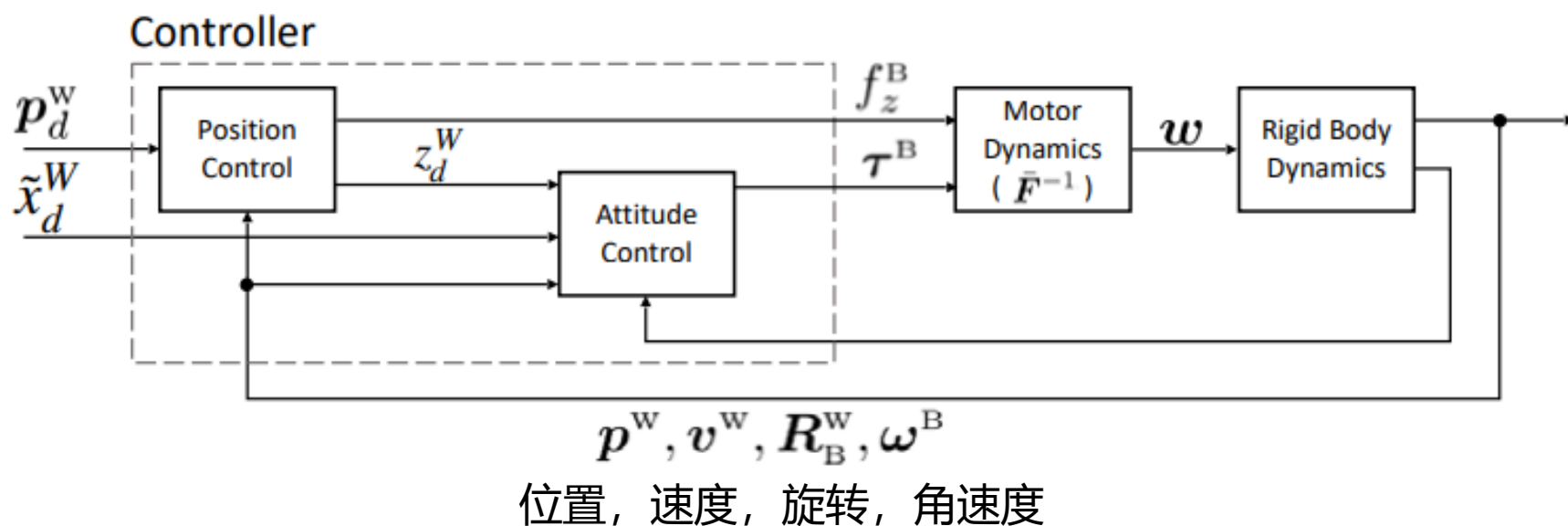
$$R_B^W = [x_B^W \ y_B^W \ z_B^W]$$

$$R_d^W = [x_d^W \ y_d^W \ z_d^W]$$



四旋翼控制器

- 用于位置和姿态控制的几何控制回路。



几何控制器1

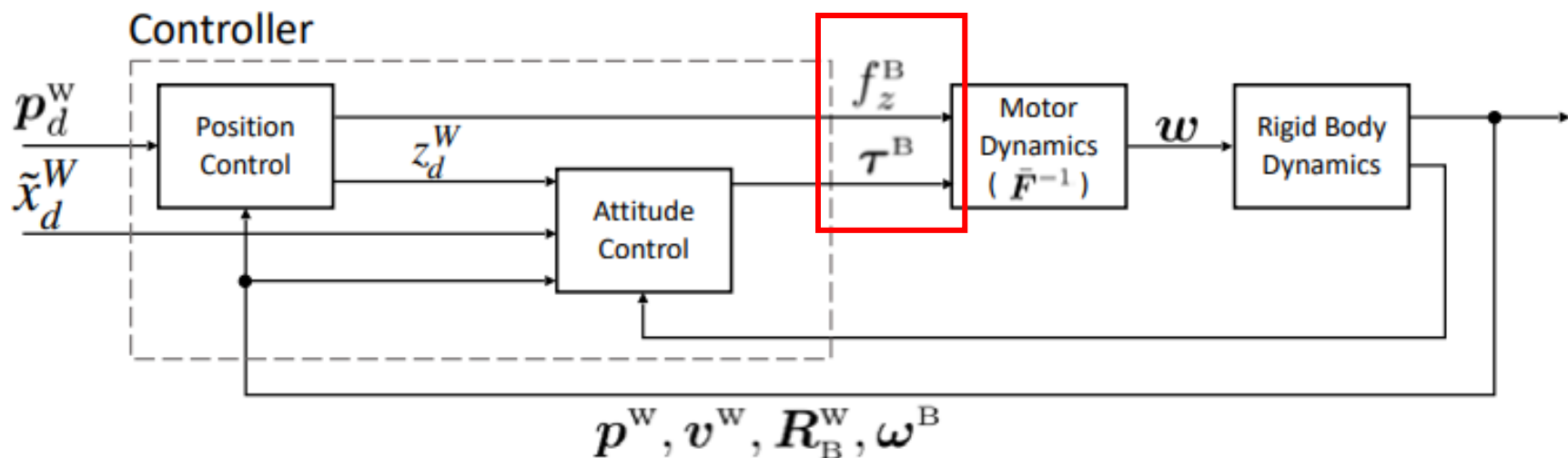
- 四旋翼有 4 个控制输入（4 个转子的速度），但有 6 个自由度（3 个用于平移，3 个用于旋转）。由于我们的输入比控制少，因此我们将无法独立控制所有自由度。
- 直观地说，如果四旋翼具有俯仰角或横滚角，其动力学将迫使其移动，因此四旋翼无法同时保持所需的位置以及所需的横滚和俯仰。横滚和俯仰时，机身必然移动！
- 因此，在本次讲座中，我们将只讨论如何控制 4 个自由度。

跟踪误差和控制设计

- 在第 6 讲中，我们已经看到四旋翼动力学满足：

$$\begin{bmatrix} m\ddot{\mathbf{p}}^{\mathbf{w}} \\ \mathcal{J}\dot{\boldsymbol{\omega}}^{\mathbf{B}} \end{bmatrix} = \begin{bmatrix} -mge_3 \\ -\boldsymbol{\omega}^{\mathbf{B}} \times \mathcal{J}\boldsymbol{\omega}^{\mathbf{B}} \end{bmatrix} + \begin{bmatrix} \mathbf{z}_B^{\mathbf{w}} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_3 \end{bmatrix} \begin{bmatrix} f_z^{\mathbf{B}} \\ \boldsymbol{\tau}^{\mathbf{B}} \end{bmatrix}$$

- 由于 **F 是常数**，我们总是可以从 \mathbf{w} 到 $[f; \tau]$ 来回移动，
- 因此，在下文中我们将直接将 $[f; \tau]$ 视为我们的控制输入。



跟踪错误

- 人们可能会将几何控制器视为 PD（比例导数）控制器，但具有尊重旋转的李群结构的误差指标。错误定义如下：

$$e_p = p^w - p_d^w \quad (\text{position error})$$

$$e_v = v^w - v_d^w \quad (\text{linear velocity error})$$

$$e_R = \frac{1}{2} [(R_d^w)^\top R_B^w - (R_B^w)^\top R_d^w]^\vee \quad (\text{rotation error})$$

$$e_\omega = \omega^B - (R_B^w)^\top R_d^w \omega_d \quad (\text{angular velocity error})$$

控制器

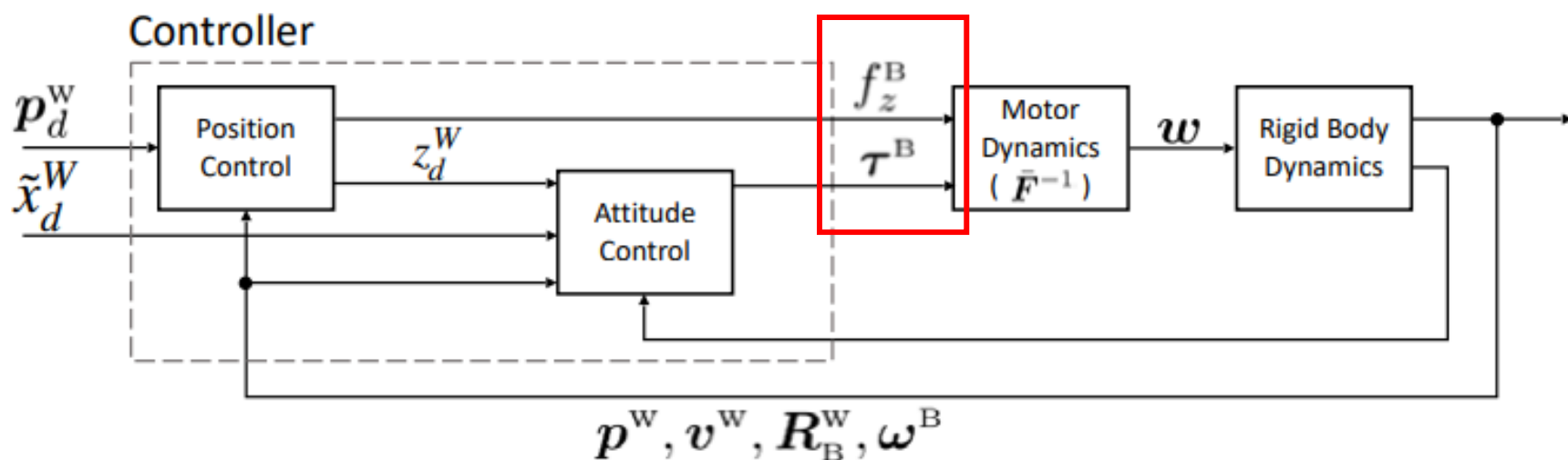
- 我们现在可以介绍几何控制器。

$$f_z^B = (-k_p e_p - k_v e_v + m g e_3 + m \ddot{p}_d^w) \cdot R_B^w e_3,$$

$$\tau^B = -k_R e_R - k_\omega e_\omega + \omega^B \times J \omega^B - J([\omega^B]_\times (R_B^w)^\top R_d^w \omega_d - (R_B^w)^\top R_d^w \dot{\omega}_d),$$

where the desired attitude R_d^w is computed as $R_d^w = [\frac{(z_d^w \times \tilde{x}_d^w) \times z_d^w}{\|(z_d^w \times \tilde{x}_d^w) \times z_d^w\|}, \frac{z_d^w \times \tilde{x}_d^w}{\|z_d^w \times \tilde{x}_d^w\|}, z_d^w] \in \text{SO}(3)$, and:

$$z_d^w = R_d^w e_3 = \frac{-k_p e_p - k_v e_v + m g e_3 + m \ddot{p}_d^w}{\|-k_p e_p - k_v e_v + m g e_3 + m \ddot{p}_d^w\|},$$



近悬停控制器

- 课程介绍了两个标准和众所周知的**四旋翼控制器**的原理。
- 首先，我们讨论了一个几乎全局稳定的几何控制器，它提供了一种最先进的方法来执行四旋翼机的激进机动。
- 第二个控制器（Near-Hovering Controller）是**轻量级级联比例微分（PD）控制器**，它在悬停附近工作得很好。

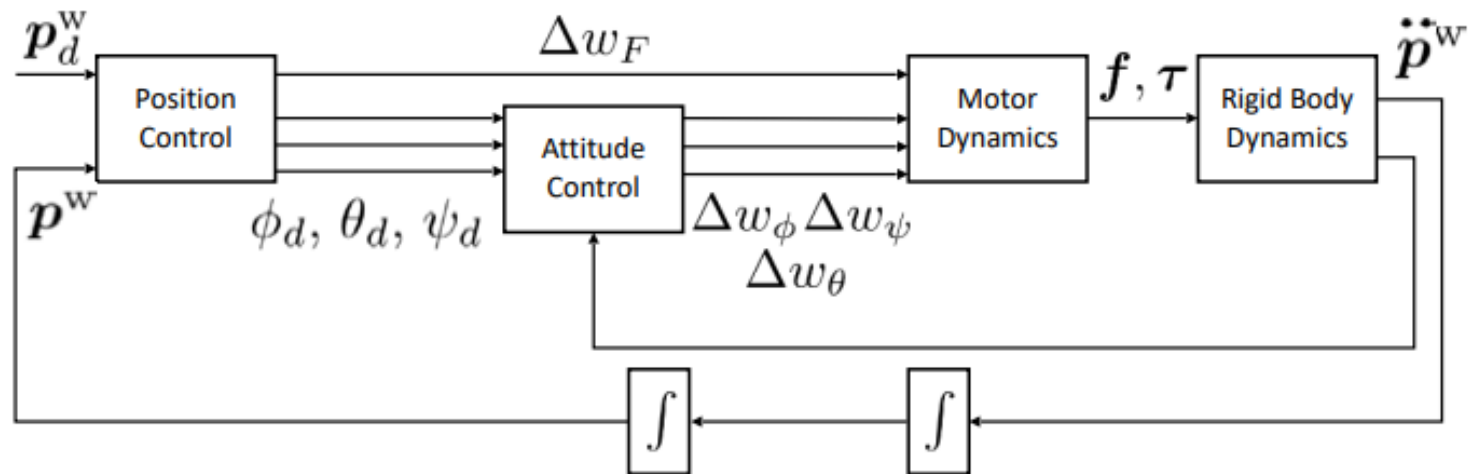


Figure 7.3: The nested control loops for position and attitude control.

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- [1] Samir Bouabdallah. Design and control of quadrotors with application to autonomous flying. Technical report, Epfl, 2007.
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- [4] Nathan Michael, Daniel Mellinger, Quentin Lindsey, and Vijay Kumar. The grasp multiple micro-uav testbed. *IEEE Robot. Automat. Mag.*, 17(3):56–65, 2010.

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