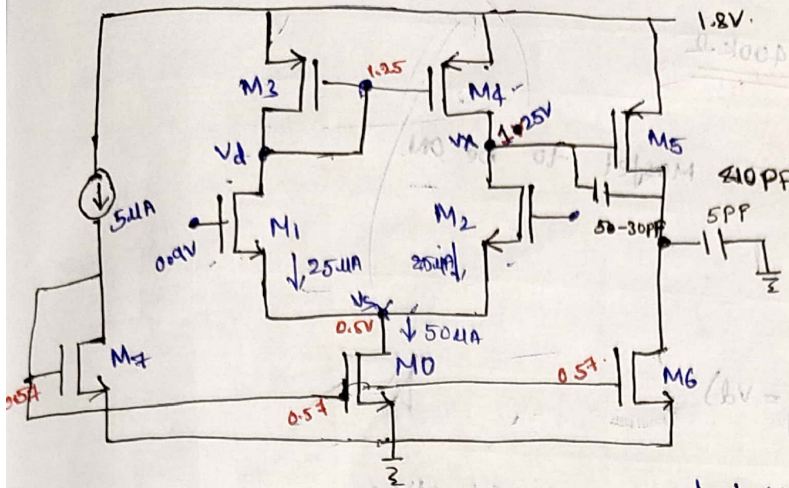


## 2 STAGE OTA DC CALCULATIONS

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Given

$$(V_{th})_n = 0.39V$$

$$(V_{th})_p = 0.39V$$

$$\mu_n C_{ox} = 230 \mu A/V^2$$

$$\mu_p C_{ox} = 100 \mu A/V^2$$

$$L_{min} = 0.18 \mu m$$

$$W_{min} = 0.27 \mu m$$

$$\lambda = 0.01 \text{ for } L = 0.18 \mu m$$

Given the overdrive for initial calculations:  $V_{gs} - V_{th} = 0.2V$ .

1) FOR  $M_0$

$$I_D = 50 \mu A \text{ (let us consider)}$$

$$I_D = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right) (V_{gs} - V_{th})^2$$

$$50 \mu A = \frac{1}{2} (230 \mu A/V^2) \left(\frac{W}{L}\right) (0.2)^2$$

$$\left(\frac{W}{L}\right)_{M_0} = \frac{10}{23(0.2)^2} = 10.87$$

For design in Ltspice I considered  $L = 5 \times 0.18 \mu m = 0.9 \mu m$  for all the Mosfets. of stage 1.

$$g_m = \frac{2I_D}{V_{gs} - V_{th}} = \frac{2(50 \mu A)}{0.2} = 500 \mu S$$

$$r_o \text{ (due to channel length modulation)} = \frac{1}{\lambda I_D} = \frac{1}{0.01 \times 50 \mu A} = 200 k\Omega$$

2) FOR  $M_1$  and  $M_2$

FOR  $M_1$  to be in saturation.

$$V_{gs} > V_{th}$$

$$0.9 - V_s > 0.37$$

$$V_s < 0.53$$

To get max gain,  $g_m$  needs to be high,  $\Rightarrow V_{gs} - V_{th}$  must be low  
So I considered max  $V_s$  of 0.5

Then

$$25 \mu A = \frac{1}{2} (230 \mu A/V^2) \left(\frac{W}{L}\right) (0.9 - 0.5 - 0.37)^2$$

$$\left(\frac{W}{L}\right) = \frac{50}{23(0.03)^2} = 241.55$$

$$g_m = \frac{2(25 \mu A)}{0.03} = 1666.6 \mu S$$



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$$r_D = \frac{1}{\lambda I_D} = \frac{1}{0.1(25 \mu A)} = 400 k\Omega$$

$$V_{DS1} = V_{DS2} = 400 k\Omega$$

3) For  $M_3$  and  $M_4$ .

to be in saturation. / The Mosfet to be ON.

$$V_{SG3} > (V_{th})_p$$

$$V_{SG3} = V_G > 0.39$$

$$V_G < 1.41 \quad (\because V_G = V_D)$$

$$V_D < 1.41$$

and, with the  $V_D$ ,  $M_1$  must also be in saturation

$$\therefore (V_{DS})_1 > (V_{GS})_1 - (V_{th})_n$$

$$V_D > V_G - (V_{th})_n$$

$$V_D > 0.9 - 0.39$$

$$V_D > 0.53$$

$$V_D \in (0.53, 1.41)$$

Let us consider  $V_D = 1.25V$

$$\text{then, } 25 \mu = \frac{1}{2} (\mu_p C_{ox}) \left(\frac{W}{L}\right) (V_{SG} - V_{th})^2$$

$$25 \mu = \frac{1}{2} (100 \mu A) \left(\frac{W}{L}\right) (1.8 - 1.25 - 0.39)^2$$

$$\left(\frac{W}{L}\right) = \frac{2(0.16)^2}{2(0.16)^2} = 19.53$$

$$g_m = \frac{2I_D}{V_{SG} - V_{th}} = \frac{2(25 \mu A)}{0.16} = 312.5 \mu S$$

$$(r_D)_{M1} = (r_D)_{M2} = 400 k\Omega$$

4) For  $M_5$  (Let us consider a current of  $100 \mu A$  is flowing in stage-2)

The value of  $V_X$  must be chosen such that  $M_2, M_4$  and  $M_5$  must be on / In saturation.

$$V_{SG5} > (V_{th})_p$$

$$1.8 - V_X > 0.39$$

$$V_X < 1.41 - (1)$$

$$(V_{DS})_4 > (V_{GS})_4 - (V_{th})_p$$

$$-V_X > -V_G - (V_{th})_p$$

$$V_G + V_{th} > V_X$$

$$V_X < 1.25 + 0.39$$

$$V_X < 1.64 - (2)$$

$$\text{and } V_X > 0.53 - (3)$$



To satisfy all (1), (2), (3)  $V_X \in [0.53, 1.41]$

But, the Phase Margin and bandwidth of the overall gain of this design depends on 2nd stage gain i.e.  $(g_m)_5$

If we consider  $(g_m)_5$  very high then overall gain increases but it reduces PM and bandwidth.

$\Rightarrow$  To get a PM of  $50^\circ$  to  $70^\circ$ .

$(g_m)_5$  considered  $6-10 \mu$

Let us consider  $(V_X = 1.00V)$   $V_X = 1.25V$

Then  $100 \mu = \frac{1}{2} (100 \mu) \left( \frac{W}{L} \right)_5 (1.8 - 0.39)^2$

$$\left( \frac{W}{L} \right)_5 = \frac{2}{(0.41)^2} = 11.9$$

$$\left( \frac{W}{L} \right)_5 = \frac{2}{(0.16)^2} = 78.125$$

$$g_{m5} = \frac{2(100 \mu)}{0.41} = 487.8 \mu S$$

$$g_{m5} = \frac{2(100 \mu)}{0.16} = 1250 \mu S$$

$$(r_o)_5 = (r_o)_5 = \frac{1}{\lambda I_D} = \frac{1}{0.1 \times 100 \mu} = 100 K \Omega$$

5) For  $M_7$ .

$$\frac{(I_D)_7}{\left( \frac{W}{L} \right)_7} = \frac{(I_D)_{M_6}}{\left( \frac{W}{L} \right)_{M_6}} \quad (\text{For same overdrive})$$

$$\frac{5 \mu}{\left( \frac{W}{L} \right)_7} = \frac{50 \mu}{10.87}$$

$$\left( \frac{W}{L} \right)_7 = \frac{10.87}{10} = 1.087$$

$$\therefore (V_{GS} - V_{th})_7 = 0.2$$

$$V_G - 0 - 0.37 = 0.2$$

$$V_G = 0.57$$

$$g_{m7} = \frac{2(5 \mu)}{0.2} = 50 \mu S$$

$$r_o = \frac{1}{\lambda I_D} = \frac{1}{0.1(5 \mu)} = 2 M \Omega$$

6) For  $M_6$ .

$$100 \mu = \frac{1}{2} (230 \mu) \left( \frac{W}{L} \right)_6 (0.2)^2$$

$$\left( \frac{W}{L} \right)_6 = \frac{20}{23(0.2)^2} = 21.74$$

$$g_{m6} = \frac{2(100 \mu)}{0.2} = 1000 \mu S$$

For  $M_5$  and  $M_6$ , I have considered  $L = 0.18 \mu m$  as  $\lambda = 0.1$  which depends on  $L$  value.



Final Designed Values:  $V_{DD} = 1.8V$ ;  $I_{ref} = 5\mu A$ ;  $V_{in,cm} = 0.9V$

$V_{ds} = 20mV$

Parameters	$M_0$	$M_1$	$M_2$	$M_3$	$M_4$	$M_5$	$M_6$	$M_7$
$V_{gs} - (V_{th})$ $V_{sg} - (V_{th})_p$	0.2V	0.03V	0.08V	0.16V	0.16V	0.16V	0.2	0.2
$(\frac{W}{L})$	10.869	241.54	241.50	19.5	19.5	78.125	21.439	1.0869
$g_m$	500 $\mu S$	1666.6 $\mu S$	1666.6 $\mu S$	312.5 $\mu S$	312.5 $\mu S$	1250 $\mu S$	1000 $\mu S$	50 $\mu S$
$r_o$	200 k $\Omega$	400 k $\Omega$	400 k $\Omega$	400 k $\Omega$	400 k $\Omega$	400 k $\Omega$	100 k $\Omega$	20 k $\Omega$
$I_D$	5 $\mu A$	25 $\mu A$	25 $\mu A$	25 $\mu A$	25 $\mu A$	100 $\mu A$	100 $\mu A$	5 $\mu A$
$W$	9.78 $\mu m$	0.22 mm	0.22 mm	17.55 $\mu m$	17.55 $\mu m$	14.06 $\mu m$	3.9 $\mu m$	0.98 $\mu m$
$L$	0.9 $\mu m$	0.9 $\mu m$	0.9 $\mu m$	0.9 $\mu m$	0.9 $\mu m$	0.18 $\mu m$	0.18 $\mu m$	0.9 $\mu m$

Theoretical values:

$$\text{stage 1 gain} = g_{m1}(r_{o1} || r_{o2}) = 1666.6 \times 10^{-6} (200 \times 10^3) = 333.32 = 50.457 \text{ dB}$$

$$\text{stage 2 gain} = g_{m5}(r_{o5} || r_{o6}) = 1250 \times 10^{-6} (50 \times 10^3) = 62.5$$

$$\text{Total gain} = 333.32 \times 62.5 = 20832.5 = 86.4 \text{ dB (Total)}$$

Observed values from LT spice:

$$\text{For stage 1 } A_v = \frac{1.184334 - 1.176524}{40 \mu V} = 195.125 = 45.8 \text{ dB}$$

for stage 2: Total gain at stage 2:

$$A_v = \frac{0.9881 - 0.7753V}{40 \mu V} = \frac{0.2128}{40 \mu V} = 5320 = 74.5 \text{ dB}$$

power consumed:

$$P = IV$$

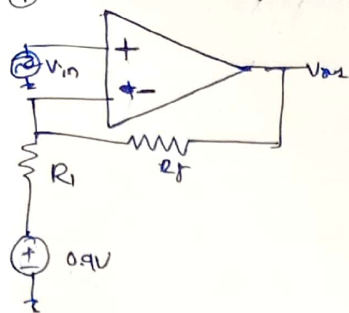
$$= (5\mu A + 50\mu A + 100\mu A)(1.8V)$$

$$= 279 \mu W$$

$$= 0.279 \text{ mW}$$

①

Non Inverting amplifier of gain 2.



$$1 + \frac{R_f}{R_1} = 2$$

$$\frac{R_f}{R_1} = 1$$

$$R_f = R_1$$

I have considered  $R_f = R_1 = 10\text{ k}\Omega$

We have connected 0.9V DC to  $R_1$  because to provide biasing to the MOSFET's.

② For poles and zeroes location to be fixed. And Phase margin Miller capacitance used for compensation  $C_c = 5\text{ pF}$

$$C_c = 0.22 C_L$$

$$\Rightarrow C_L = \frac{C_c}{0.22} = \frac{5\text{ pF}}{0.22} = 22.72\text{ pF}$$

$$C_L = 22.72\text{ pF}$$

$$\Rightarrow R_Z = \frac{1}{g_{m5}} = \frac{1}{1250\text{ }\mu\text{S}} = 800\text{ }\Omega$$

But for getting a phase margin of  $60^\circ$  I have tuned the capacitors and resistors.

Final values to get  $60^\circ$  PM:

$$C_c = 5\text{ pF}$$

$$C_L = 22.72\text{ pF}$$

$$R_Z = 6\text{ k}\Omega$$

from simulation:

Frequency at 0dB  $\omega_{gc} = 27.97\text{ MHz}$ .

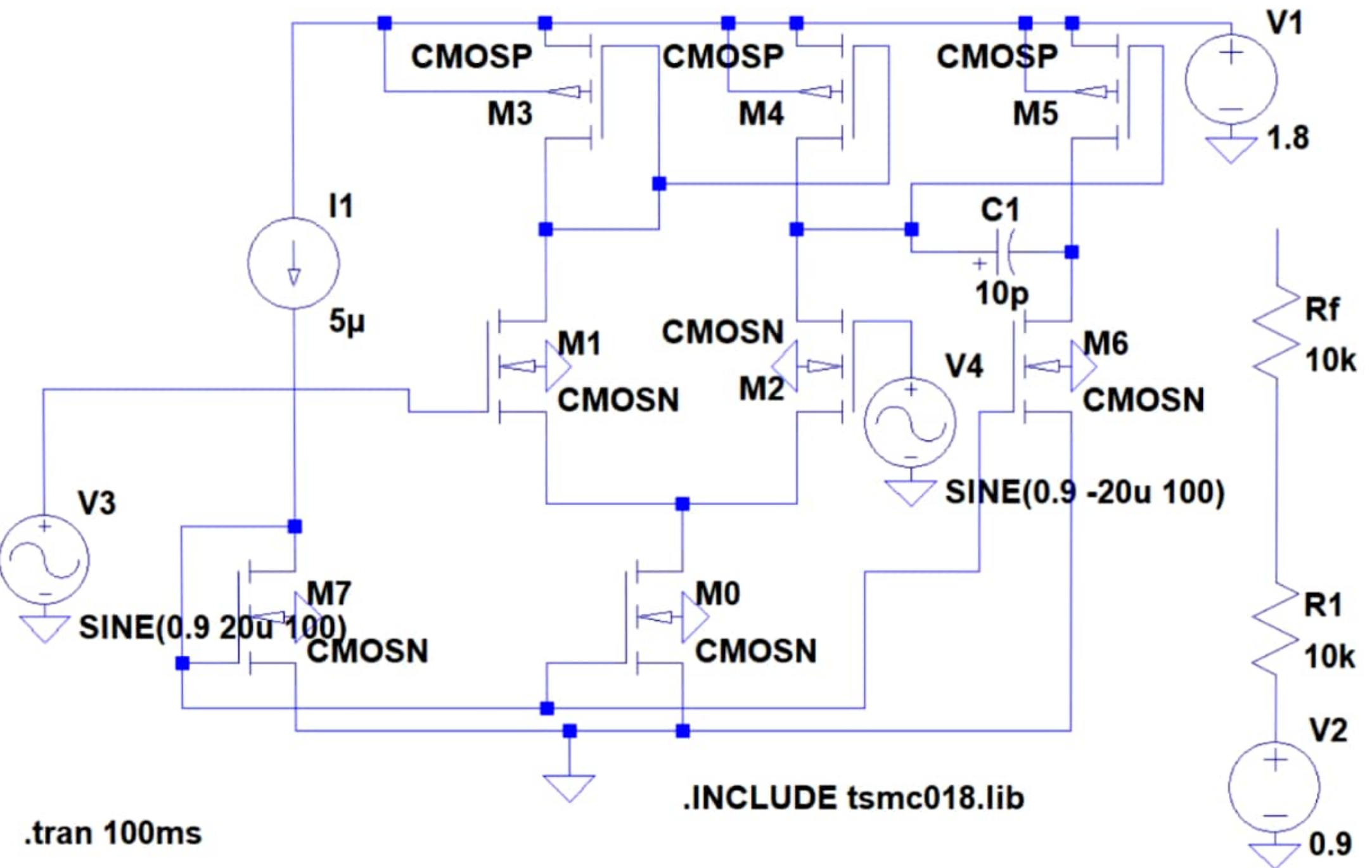
At that  $\omega_{gc}$  phase of open loop circuit  $\angle G_{OL}(j\omega) = -119.37^\circ$

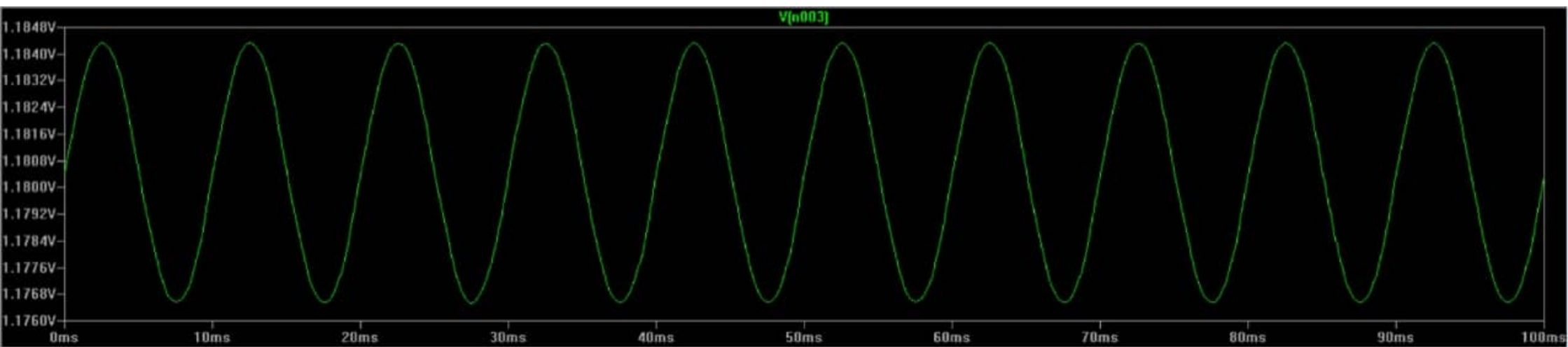
$$\text{phase margin} = 180 + \phi$$

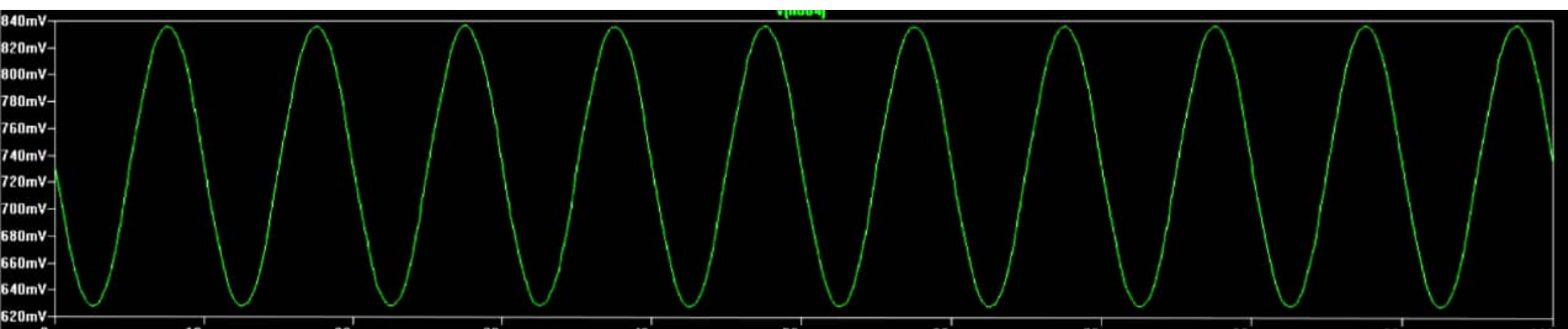
$$= 180 - 119.37$$

$$\text{PM} = 60.63^\circ$$

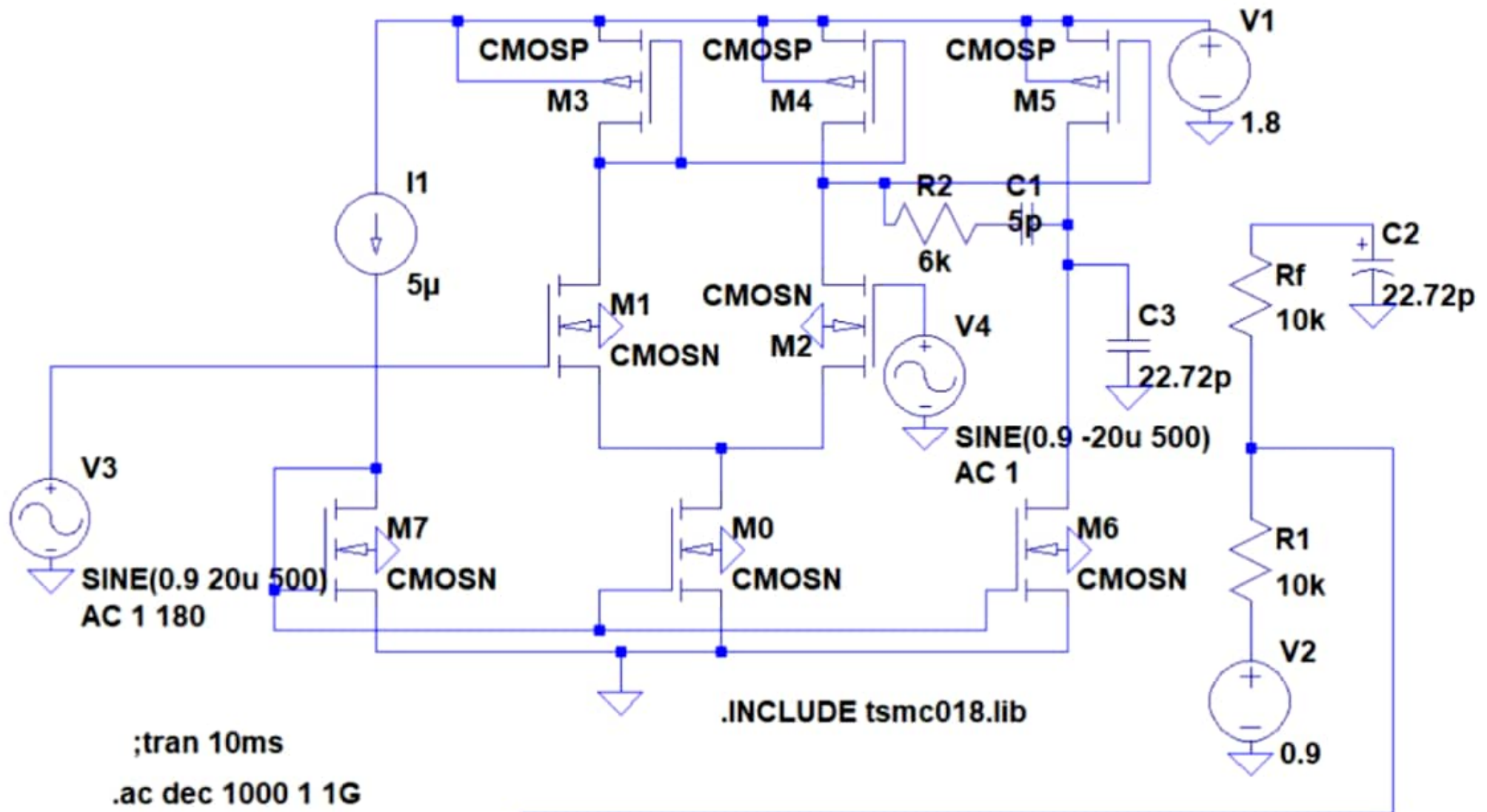


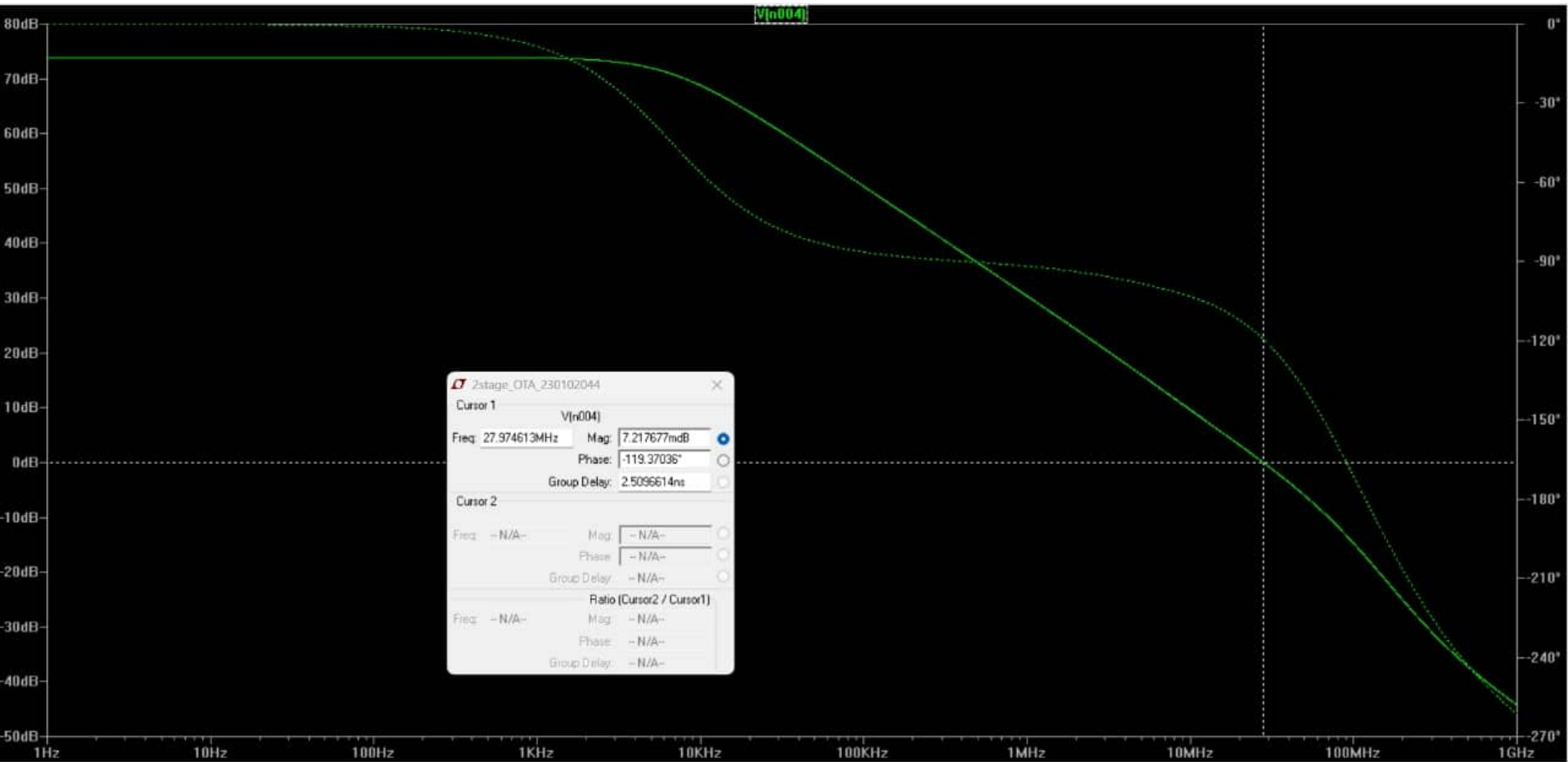




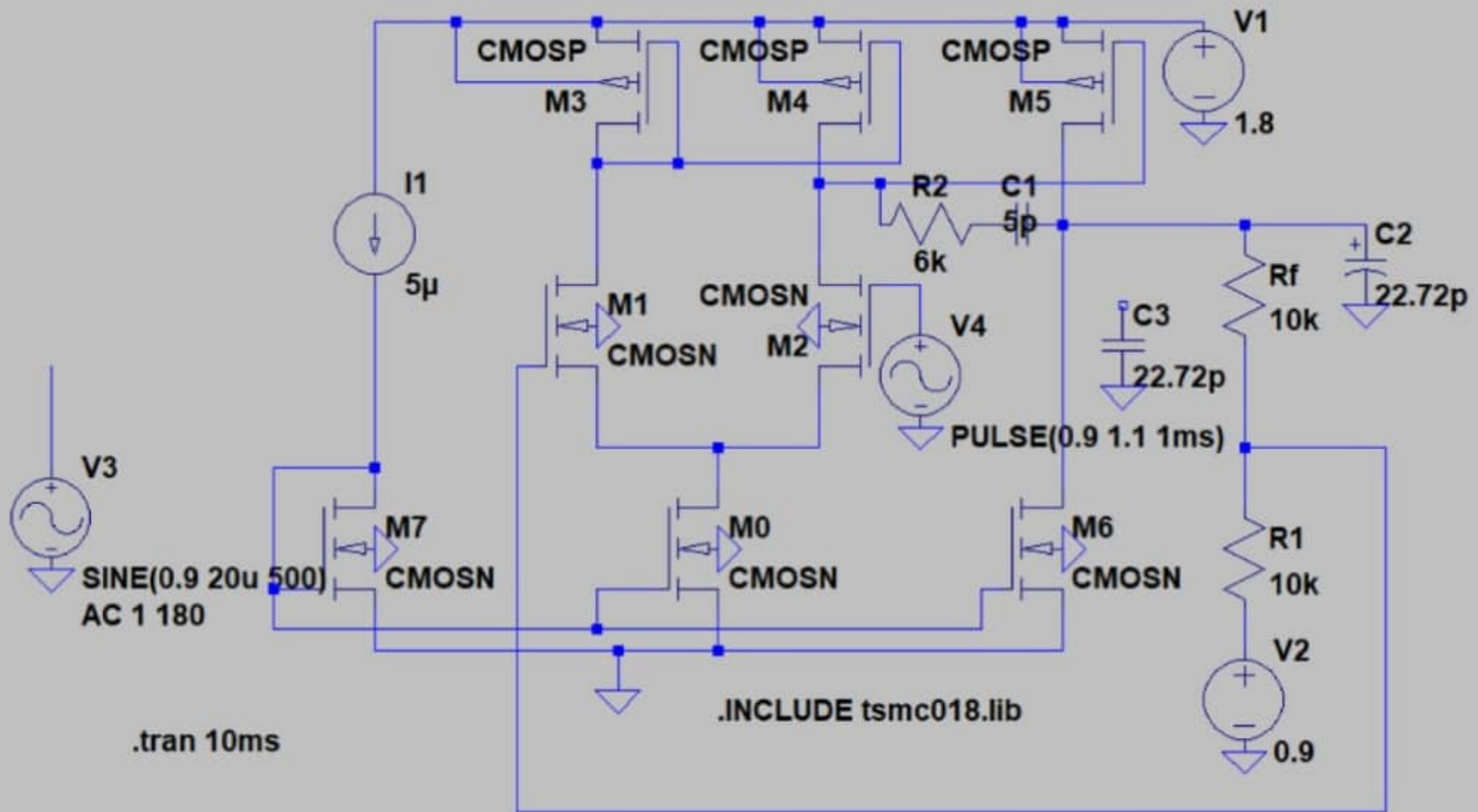












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