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Non-Intrusive Polynomial Chaos Expansion Applied to Full-Order Stochastic CFD

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I. Introduction to Uncertainty Quantification (UQ)

Importance of CFD & Deterministic Approach Challenges

- CFD : a critical piece of every engineering projects.
 - Cost & Time efficient.
 - Extensive conditions & designs testing.
 - Pre-experimental decision support.
- Deterministic approach limits.
 - 1 solution for 1 given set of input.
 - Lot of uncertainties in dynamic systems.



Need for **Uncertainty Quantification** !

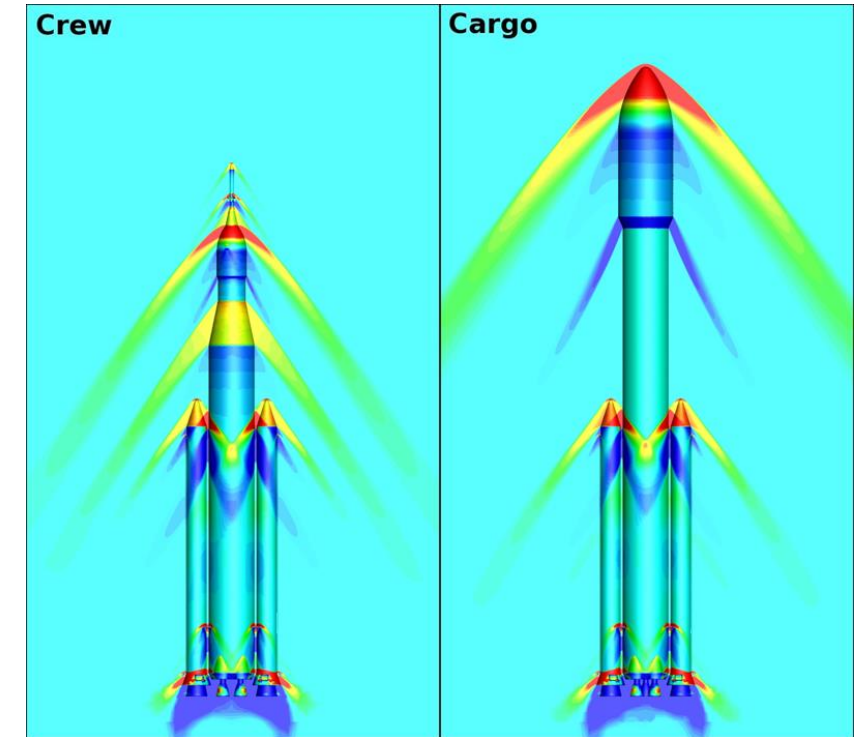


Image Credit :
NASA

Uncertainty Quantification

- UQ Goals :

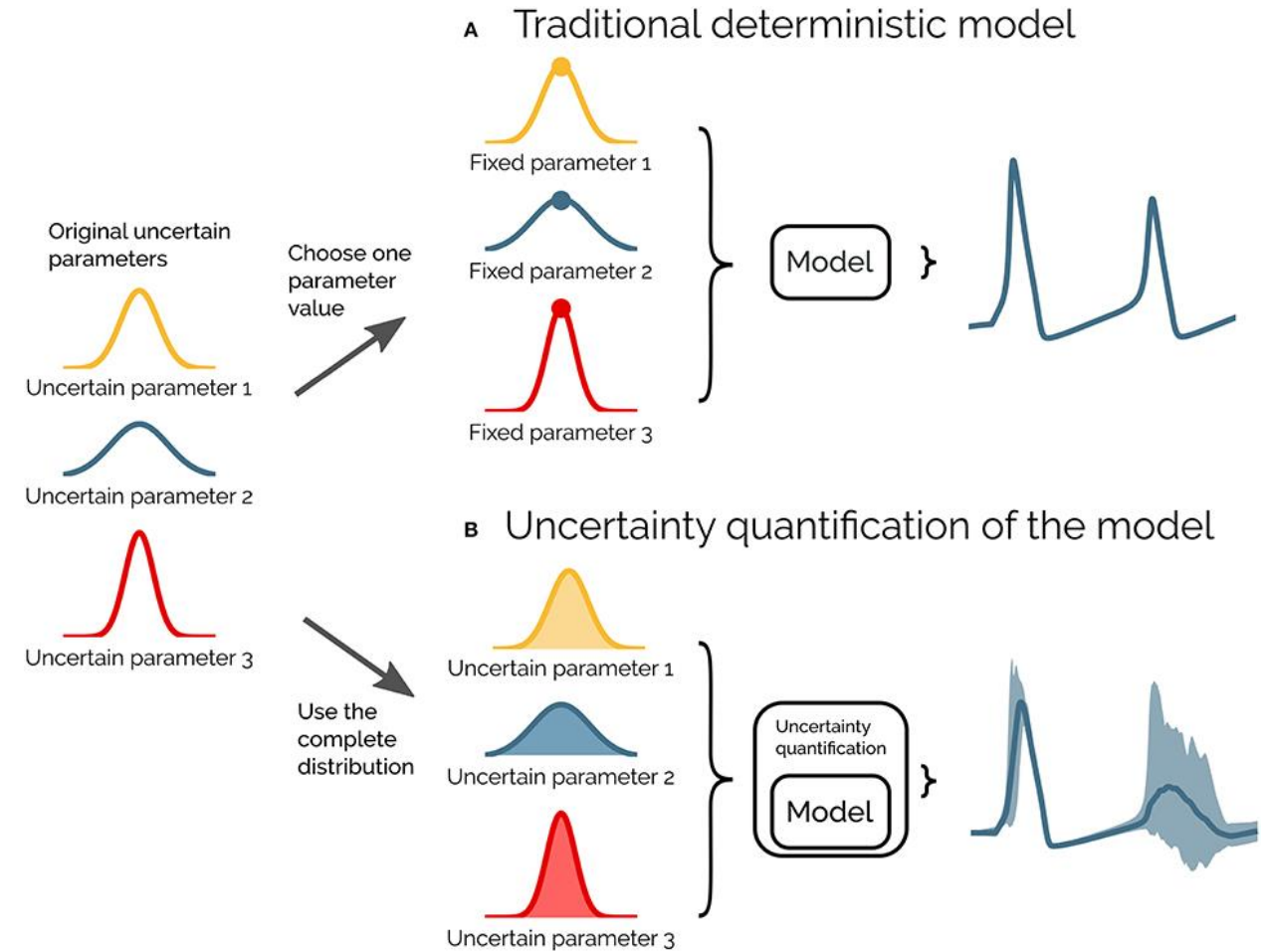
- Assess reliability of predictions.
- Manage variability.
- Assist in decision-making.

- Uncertainty Types :

- **Aleatoric** : Inherent randomness.
- **Epistemic** : Knowledge gaps.

- Key Methods :

- Deterministic : Error propagation using sensitivity derivatives,...
- **Probabilistic** ones : Monte Carlo, PCE,...



Monte Carlo Method and the Push for Alternatives

- **Monte Carlo Basics :**
 - Intuitive and easy implementation.
 - Statistical analysis : calculate mean, variance, determines confidence intervals.
- **Limitations :**
 - High sample requirement.
 - Prohibitive computation cost.

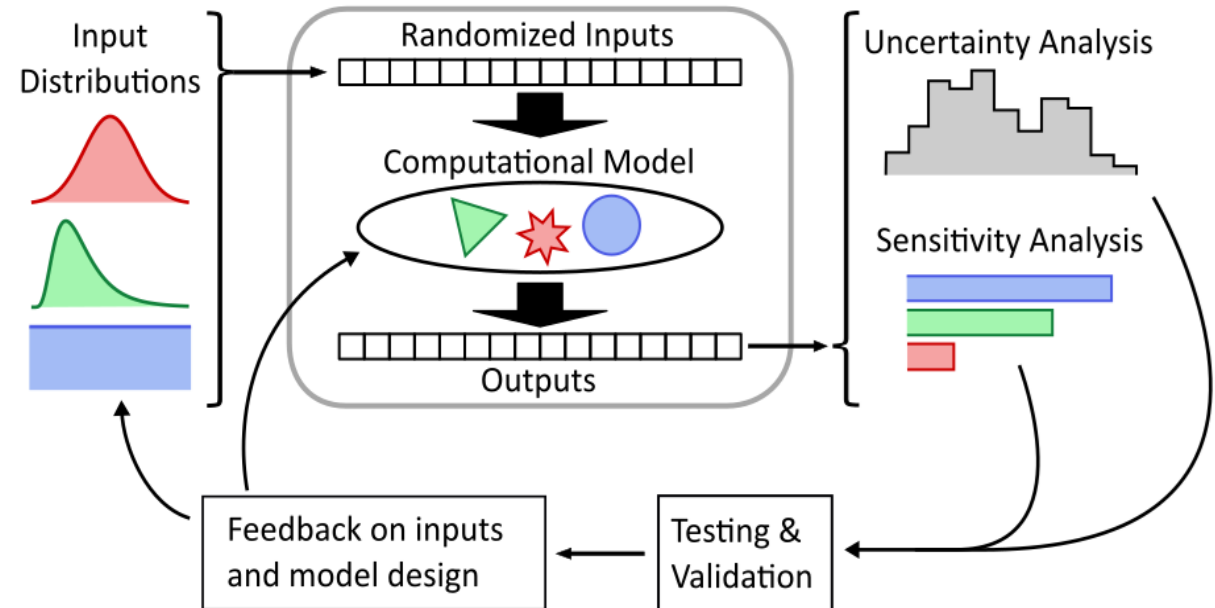


Image Credit : Scott Shambaugh



Need for alternatives : PCE and NIPCE as promising and efficient UQ solutions.

II. Theory of NIPCE

Fundamentals

- Polynomial Chaos Expansion (PCE) is a polynomial surrogate model

$$\Theta(\vec{x}, \vec{\xi}) \approx \sum_{i=0}^P \theta_i(\vec{x}) \psi_i(\vec{\xi})$$

- It is also a linear combination in an orthogonal polynomial basis, weighted by deterministic coefficients

Θ : Stochastic output

$\vec{\xi} = (\xi_1, \xi_2, \dots, \xi_n)$: n-dimensional random variable vector

\vec{x} : Position vector

θ_i : deterministic components

ψ_i : polynomial basis functions

Fundamentals

- Total number of elements of approximation:

$$N_t = P + 1 = \frac{(n + p)!}{n!p!}$$

- Optimal polynomial basis depends on Probability Density Function (PDF) of ξ components, because orthogonality depends on the weight function

For two functions $f(\vec{\xi})$ and $g(\vec{\xi})$ the inner product is defined as:

$$\langle f(\vec{\xi}), g(\vec{\xi}) \rangle = \int_{\Omega} f(\vec{\xi})g(\vec{\xi})w(\vec{\xi})d\vec{\xi}$$

Distribution	PDF	Polynomial family	Weight function	Support range
Normal	$\frac{1}{\sqrt{2\pi}}e^{-\frac{x^2}{2}}$	Hermite $H_n(x)$	$e^{-\frac{x^2}{2}}$	$[-\infty, +\infty]$
Uniform	$\frac{1}{2}$	Legendre $P_n(x)$	1	$[-1, 1]$
Beta	$\frac{(1-x)^\alpha(1+x)^\beta}{2^{\alpha+\beta+1}B(\alpha+1,\beta+1)}$	Jacobi $P_n^{(\alpha,\beta)}(x)$	$(1-x)^\alpha(1+x)^\beta$	$[-1, 1]$
Exponential	e^{-x}	Laguerre $L_n(x)$	e^{-x}	$[0, +\infty]$
Gamma	$\frac{x^\alpha e^{-x}}{\Gamma(\alpha+1)}$	Generalized Laguerre $L_n^\alpha(x)$	$x^\alpha e^{-x}$	$[0, +\infty]$

Fundamentals

- With the inner product defined, we can project the PCE on the k-th basis

$$\langle \Theta(\vec{x}, \vec{\xi}), \psi_k(\vec{\xi}) \rangle = \sum_{i=0}^P \langle \theta_i(\vec{x}) \psi_i(\vec{\xi}), \psi_k(\vec{\xi}) \rangle$$

- Due to orthogonality of the basis:

$$\theta_k(\vec{x}) = \frac{\langle \Theta(\vec{x}, \vec{\xi}), \psi_k(\vec{\xi}) \rangle}{\langle \psi_k(\vec{\xi}), \psi_k(\vec{\xi}) \rangle}$$

Point-collocation method

- NIPCE: Non-Intrusive Polynomial Chaos Expansion
- Many methods are available for a non-intrusive approach, but the selected one is point-collocation
- Take N+1 different input scenarios.

$$\begin{bmatrix} \psi_0(\vec{\xi}_0) & \psi_1(\vec{\xi}_0) & \psi_2(\vec{\xi}_0) & \cdots & \psi_P(\vec{\xi}_0) \\ \psi_0(\vec{\xi}_1) & \psi_1(\vec{\xi}_1) & \psi_2(\vec{\xi}_1) & \cdots & \psi_P(\vec{\xi}_1) \\ \psi_0(\vec{\xi}_2) & \psi_1(\vec{\xi}_2) & \psi_2(\vec{\xi}_2) & \cdots & \psi_P(\vec{\xi}_2) \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \psi_0(\vec{\xi}_N) & \psi_1(\vec{\xi}_N) & \psi_2(\vec{\xi}_N) & \cdots & \psi_P(\vec{\xi}_N) \end{bmatrix} \begin{Bmatrix} \theta_0 \\ \theta_1 \\ \theta_2 \\ \vdots \\ \theta_N \end{Bmatrix} = \begin{Bmatrix} \Theta_0 \\ \Theta_1 \\ \Theta_2 \\ \vdots \\ \Theta_N \end{Bmatrix}$$

- if N=P, then we have a square linear system, thus there is a unique solution

Point-collocation method

- Common practice: take more samples than needed
- Oversampling ratio:

$$N_p = \frac{\text{number of samples}}{P + 1}$$

- Solve oversampled system by using regression: least squares minimization
- Stochastic post-processing:

$$\mu_{\Theta} = \int \left(\sum_{i=0}^P \theta_i \psi_i(\vec{\xi}) \right) w(\vec{\xi}) d\vec{\xi} = \theta_0 \quad \left| \quad \sigma_{\Theta}^2 = \int \left(\sum_{i=0}^P \theta_i \psi_i(\vec{\xi}) \right)^2 w(\vec{\xi}) d\vec{\xi} = \sum_{i=1}^P \theta_i^2$$

Methodology

Open  FOAM®

- Full Order Model (FOM) used: OpenFOAM
- 2 test cases studied:
 - Lid-driven cavity problem
 - Dynamical characterization of NACA0012 airfoil
- 1st test case: demonstrate the use of the NIPCE method with the chaospy
- 2nd test case: parametric study
- We will validate the PCE results by comparing with the FOM and literature

III. Case study : Lid-driven cavity problem

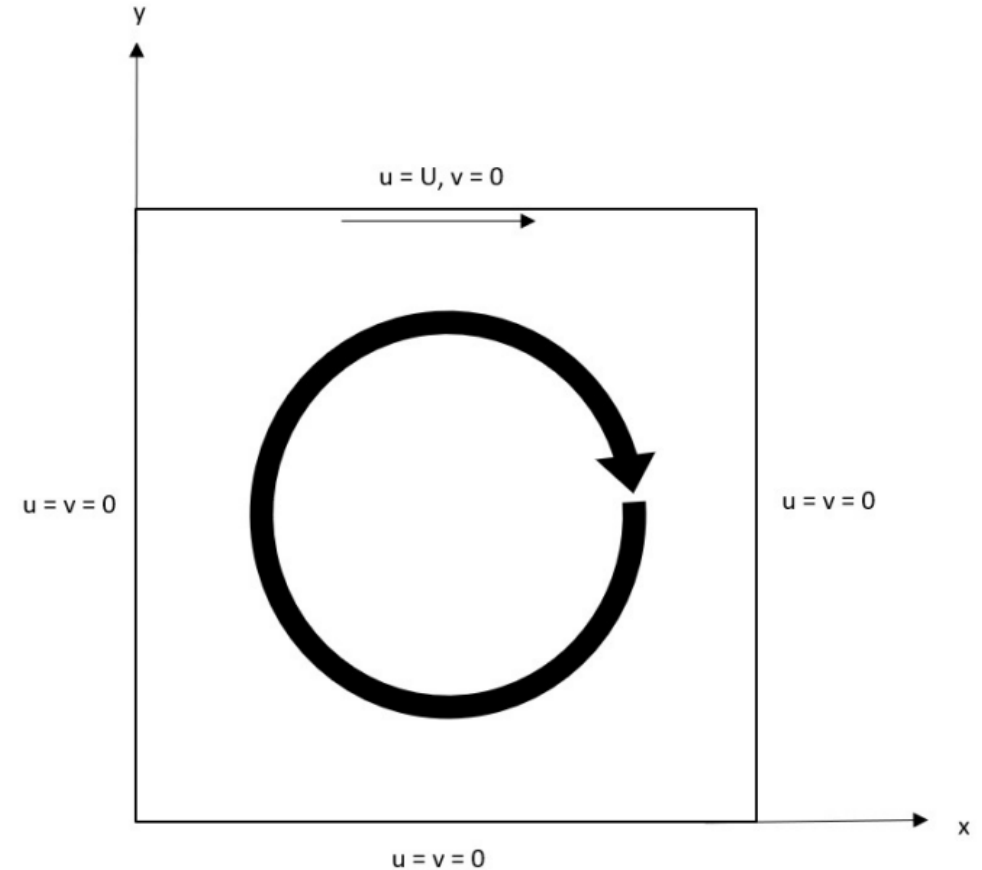
Formulation of the problem

- Domain: square with side length L
- Physics behind the problem:

$$\nabla \cdot \vec{u} = 0$$

$$\frac{\partial \vec{u}}{\partial t} = -(\vec{u} \cdot \nabla) \vec{u} - \nabla p + \frac{1}{Re} \Delta \vec{u}$$

- Reynolds number is the only parameter influencing the simulation
- Literature to compare: Ghia et al.
- Boundary conditions:
 - pressure: $\nabla p = 0$
 - velocity:
$$\begin{cases} u = U \text{ and } v = 0, & \text{if } y = L \\ u = v = 0, & \text{otherwise} \end{cases}$$

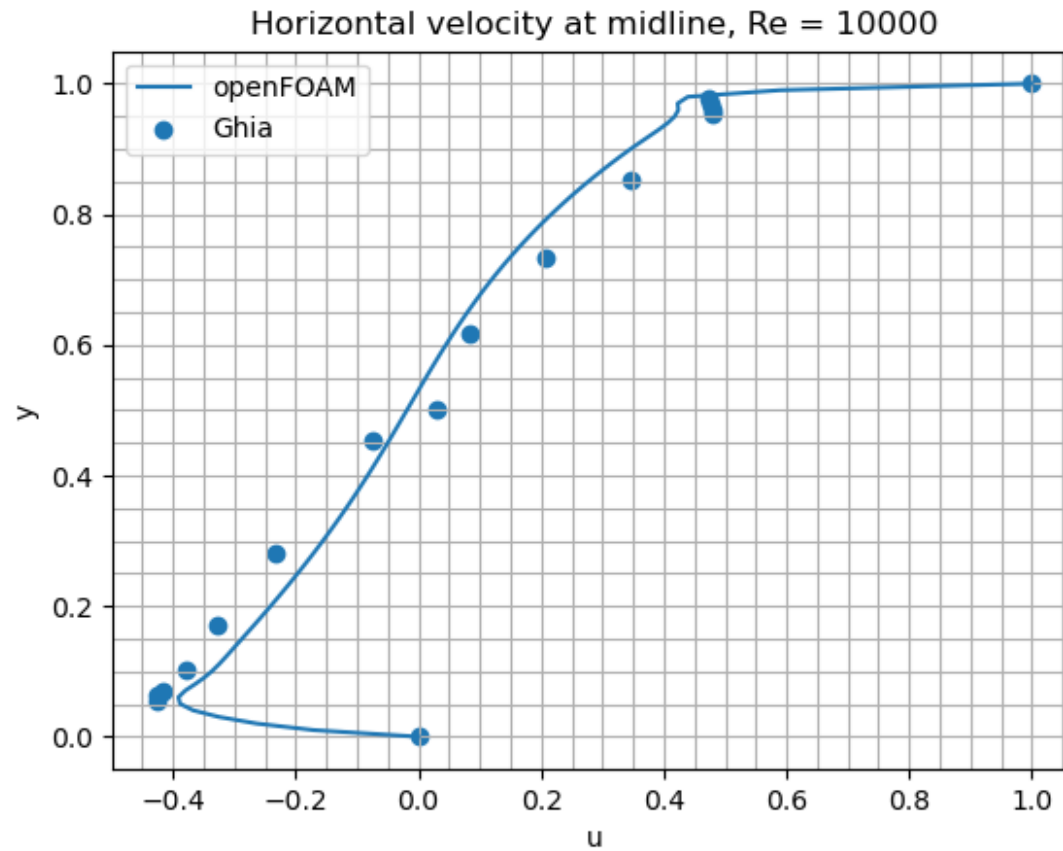


Ghia, UKNG, Kirti N Ghia, and CT Shin: *High-re solutions for incompressible flow using the navier-stokes equations and a multigrid method*. Journal of computational physics, 48(3):387–411, 1982.

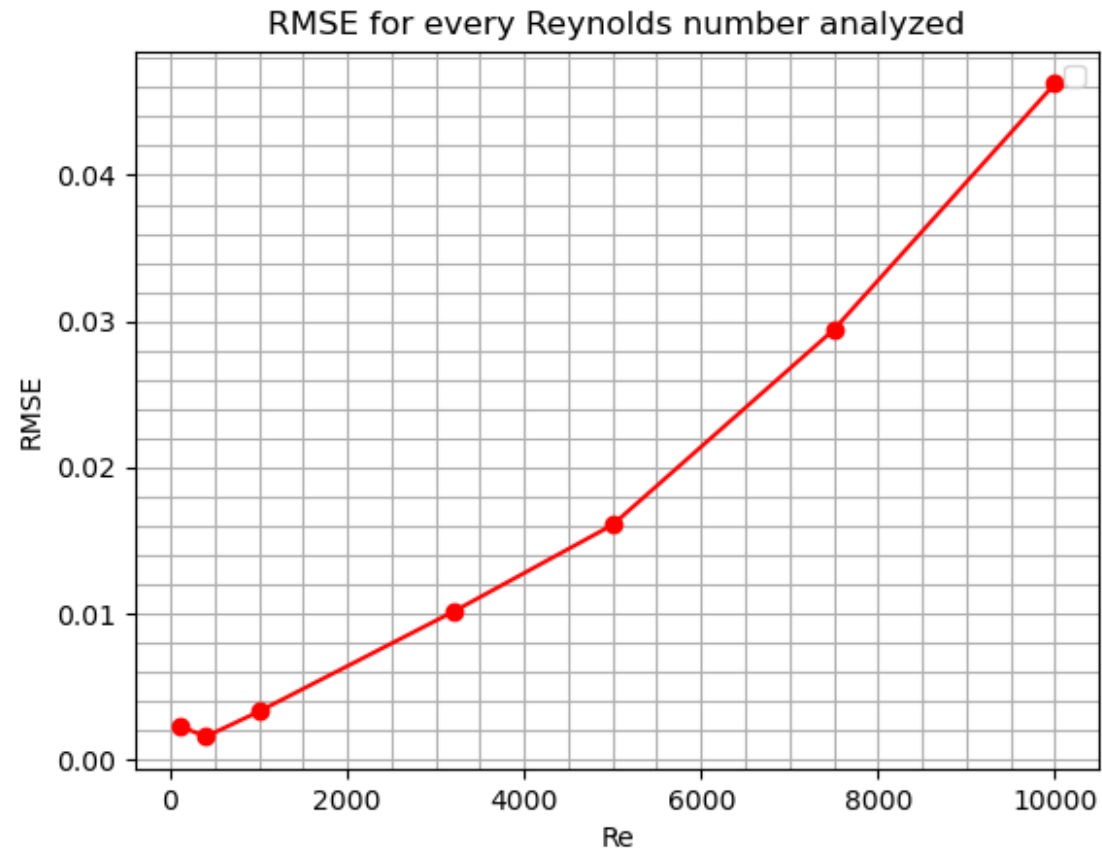
OpenFOAM implementation

- First step: determine where the solver used is reliable
- OpenFOAM solver selected is icoFoam
 - solves the incompressible laminar Navier-Stokes equations using the PISO (Pressure-Implicit with Splitting of Operators) algorithm
 - Transient code
- Secondly: Determine the minimum final step and number of cells to achieve convergence
- Finally: Reynolds number will be the only parameter influencing results, thus we can use the PCE method and assess its validity

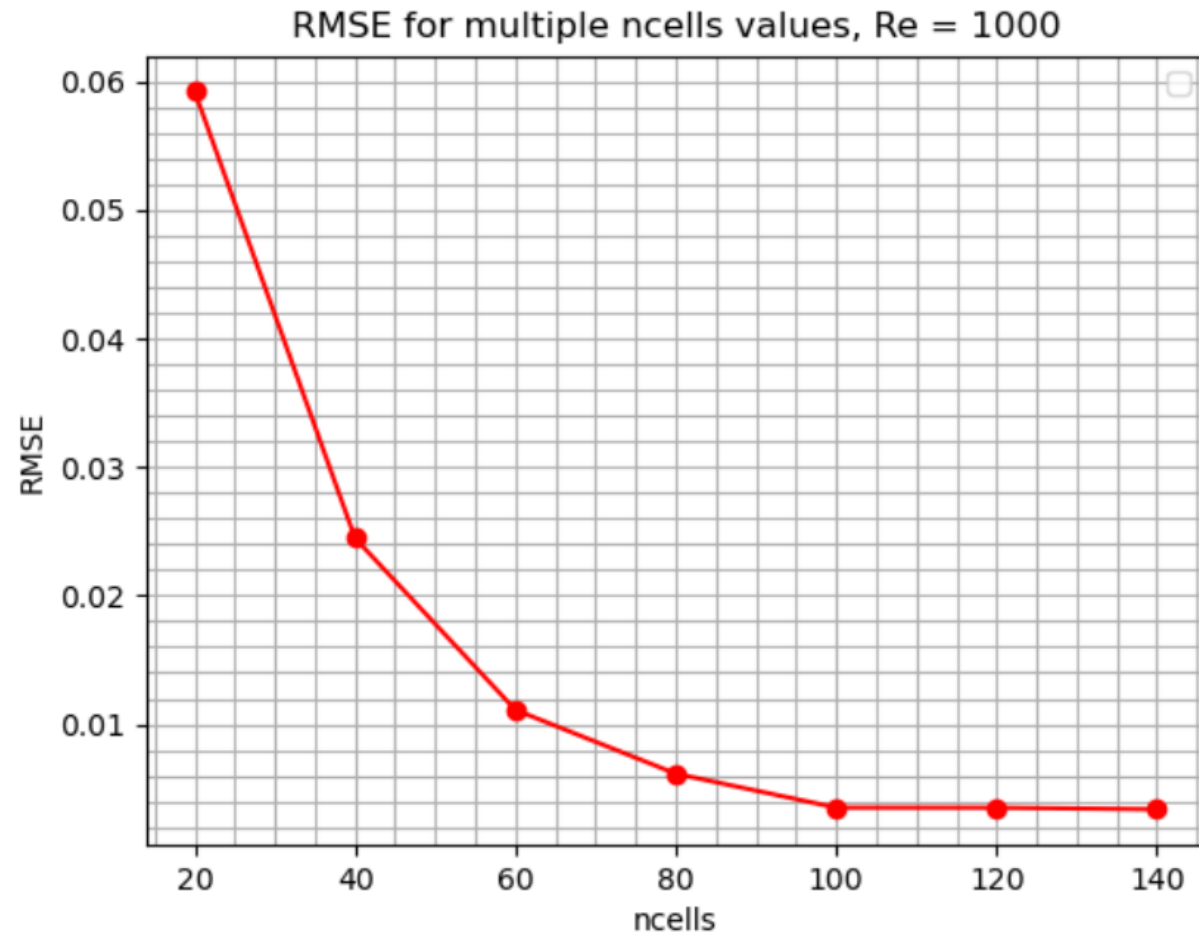
First step of analysis: Determine where the solver is reliable



First step of analysis: Determine where the solver is reliable



Second step of analysis: Convergence study



Final step of analysis: Implementing NIPCE

- Vary the Reynolds number as follows:

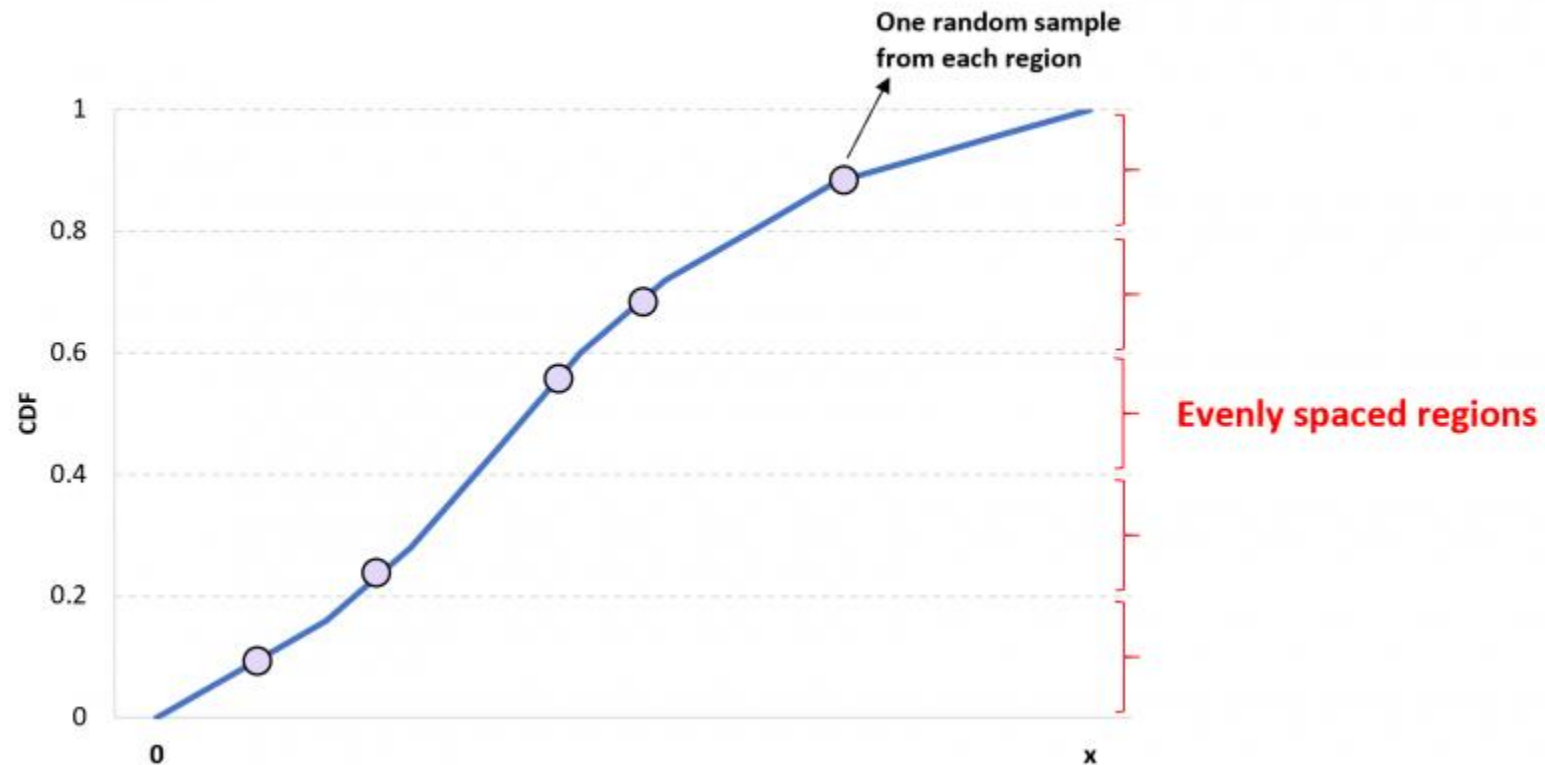
$$R_e \sim \mathcal{N}(\hat{R}_{e,avg}, \hat{R}_{e,std}) \longrightarrow R_e \sim \mathcal{N}(\hat{1000}, \hat{100})$$

- Necessity to build a PCE surrogate for each y coordinate of OpenFOAM results
- Simulations for polynomial chaos order and oversampling ratio following:

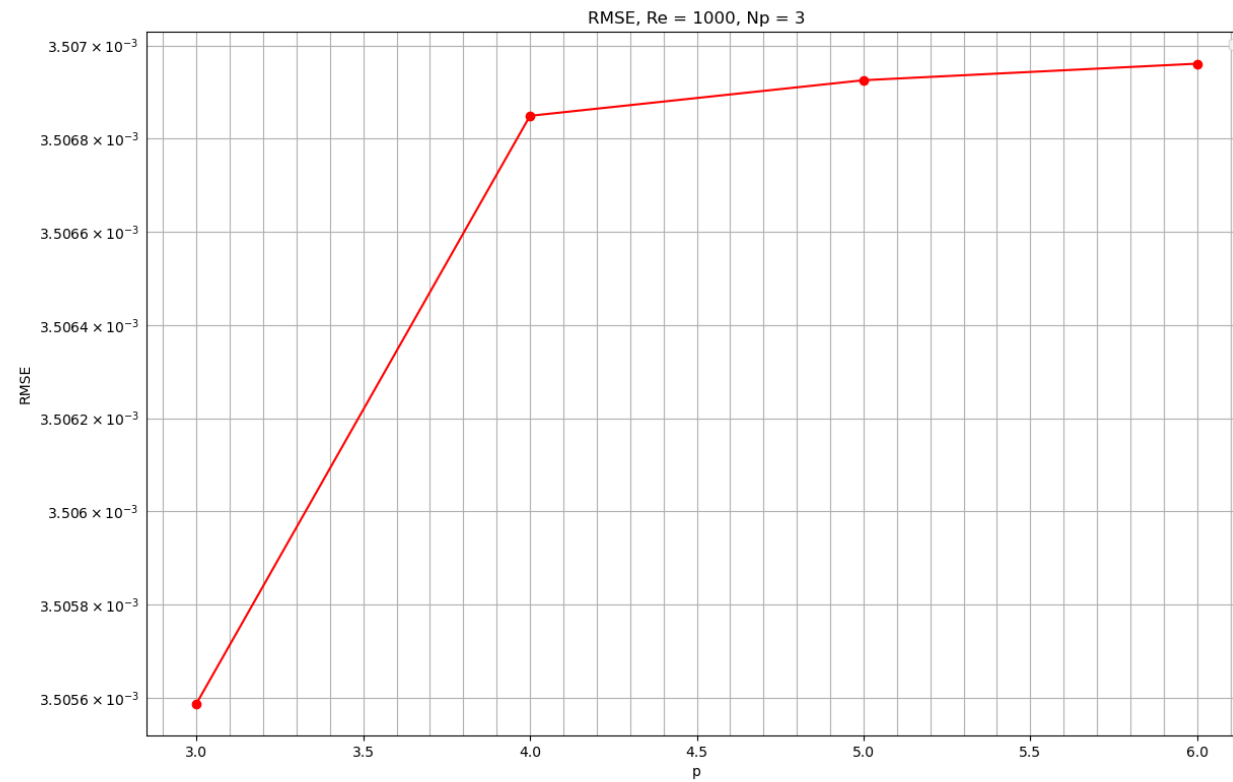
$$p \in \llbracket 3, 6 \rrbracket \text{ and } N_p \in \llbracket 1, 3 \rrbracket$$

Final step of analysis: Implementing NIPCE

- Sampling method used: Latin Hypercube Sampling (LHS)



Final step of analysis: Implementing NIPCE

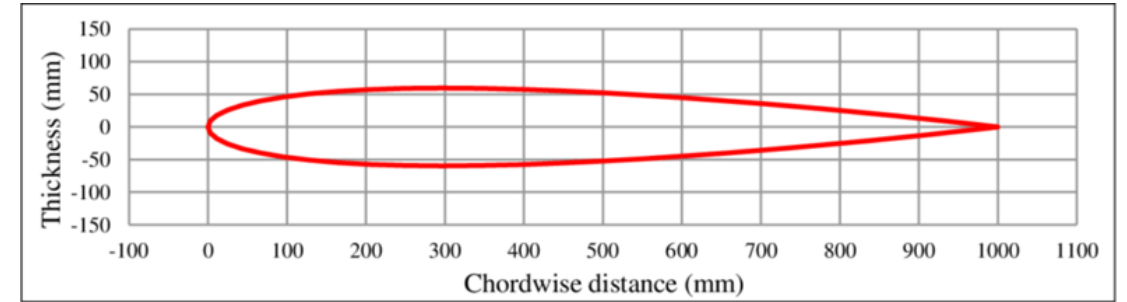


IV. Case study : NACA0012 Airfoil

Case Presentation

- NACA0012 profile : Standard aerodynamic test model.
- Focus on two critical parameters :
 - Angle of Attack.
 - Upstream Mach Number.
- Simulation Goals :
 - Compute C_L (Lift Coefficient)
 - Compute C_D (Drag Coefficient)

$$C_L = \frac{L}{\frac{1}{2}\rho V^2 S} \quad C_D = \frac{D}{\frac{1}{2}\rho V^2 S}$$



NACA0012 Profile

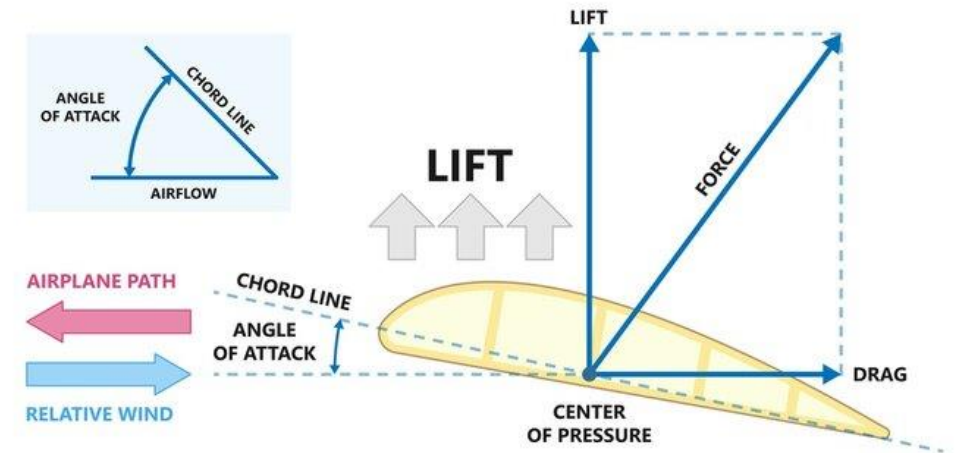
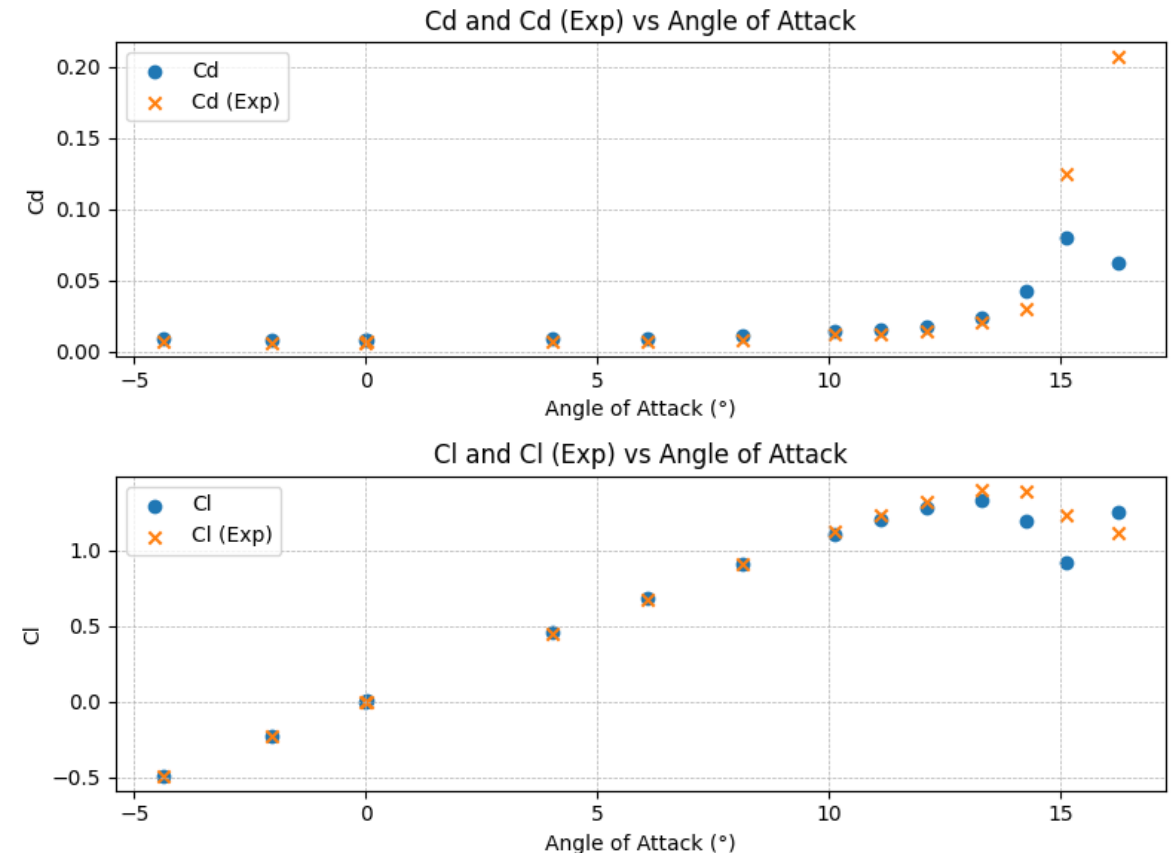


Image Credit : Adobe Stock

Numerical Implementation on OpenFOAM

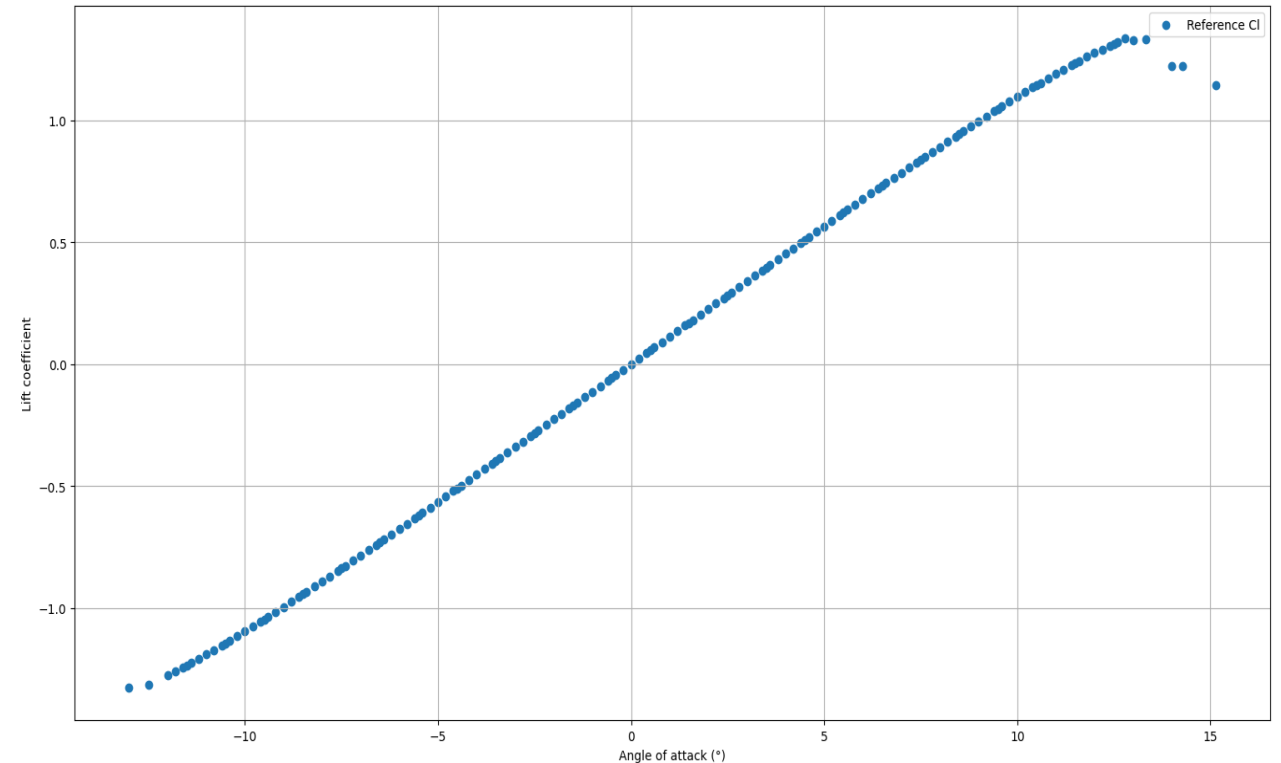
- Adapted from an existing OpenFOAM case (cf. Appendices for key simulation parameters).
- Convergence issues encountered:
 - High Mach Number instabilities (~ 0.7)
 - Stall phenomena at high Angles of Attack ($\sim 13^\circ$)
- Streamlining with Python and validation against NASA Data.



Cl as the only output for UQ. AOA range limited to $[-12^\circ, 12^\circ]$ for reliable analysis.

NIPCE Implementation : AOA uncertainty analysis

- Study Parameters:
 - Mach Number set at 0.3
 - AOA : Normal Distribution, mean 0°, STD 5°
- NIPCE Python Implementation:
 - Inputs : FOM, AOA distribution, Expansion order, Sample size, Sampling method, Fitting Method
 - Point Collocation Technique to compute the PCE
- Parametric study:
 - Creation of a reference database to assess the surrogate models accuracy
 - L2 relative error as accuracy metric



Reference values for the Lift Coefficient

$$\epsilon = 100 \times \frac{\sqrt{\sum_{t=1}^n (C_{l_t}^{\text{FOM}} - C_{l_t}^{\text{PCE}})^2}}{\sqrt{\sum_{t=1}^n (C_{l_t}^{\text{FOM}})^2}} \%$$

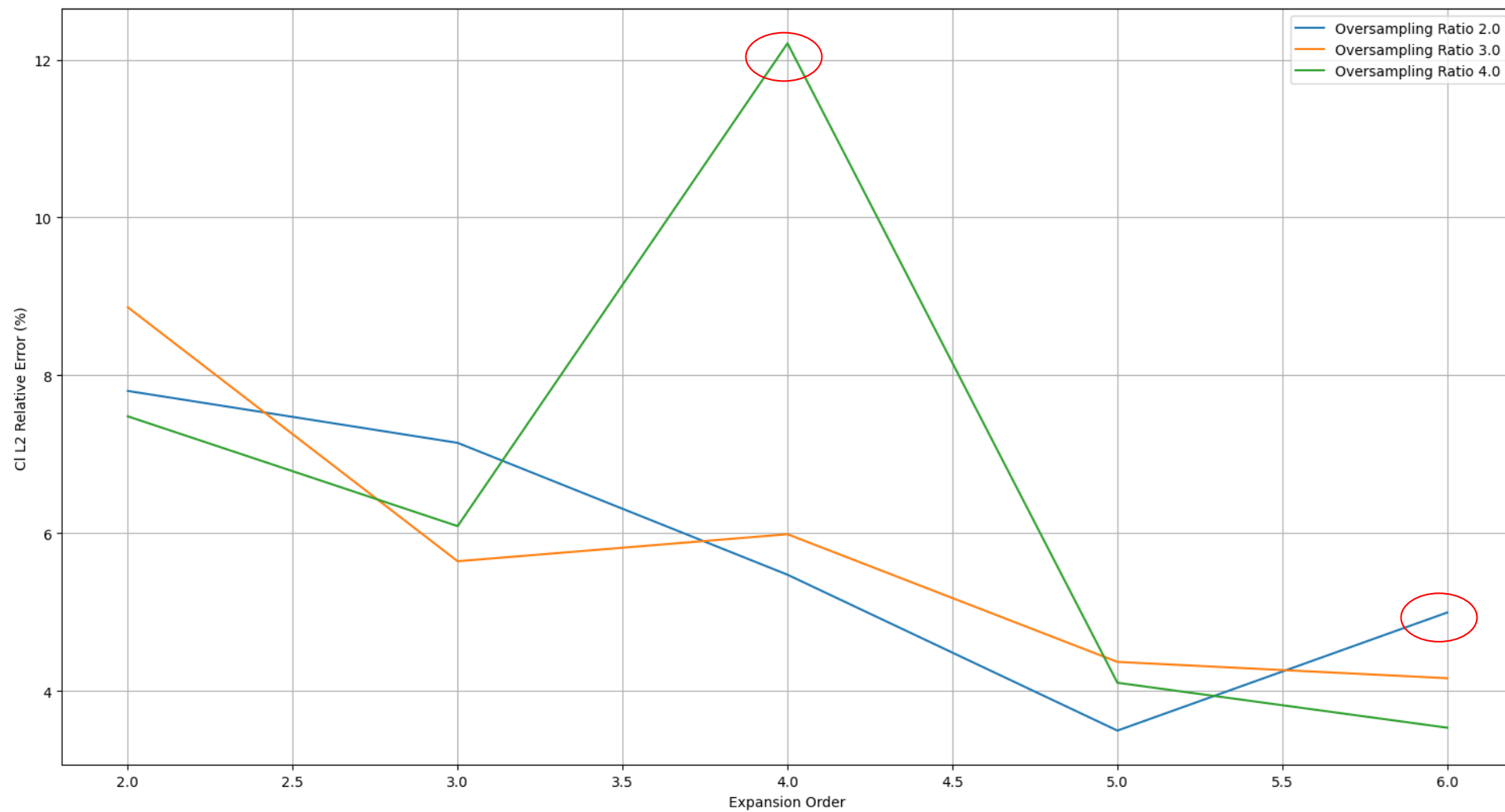
Impact of Sampling Technique : LHS vs Random

Expansion order	Number of Samples	Sampling method	Cl L2 relative error (%)
3	6	Random	8.7
3	6	LHS	6.1
3	9	Random	6.2
3	9	LHS	6.1
4	8	Random	7.5
4	8	LHS	7.3
4	12	Random	7.5
4	12	LHS	5.6
5	10	Random	3.4
5	10	LHS	7.3
2	4	Random	8.9
2	4	LHS	8.1
5	15	Random	3.34
5	15	LHS	2.7

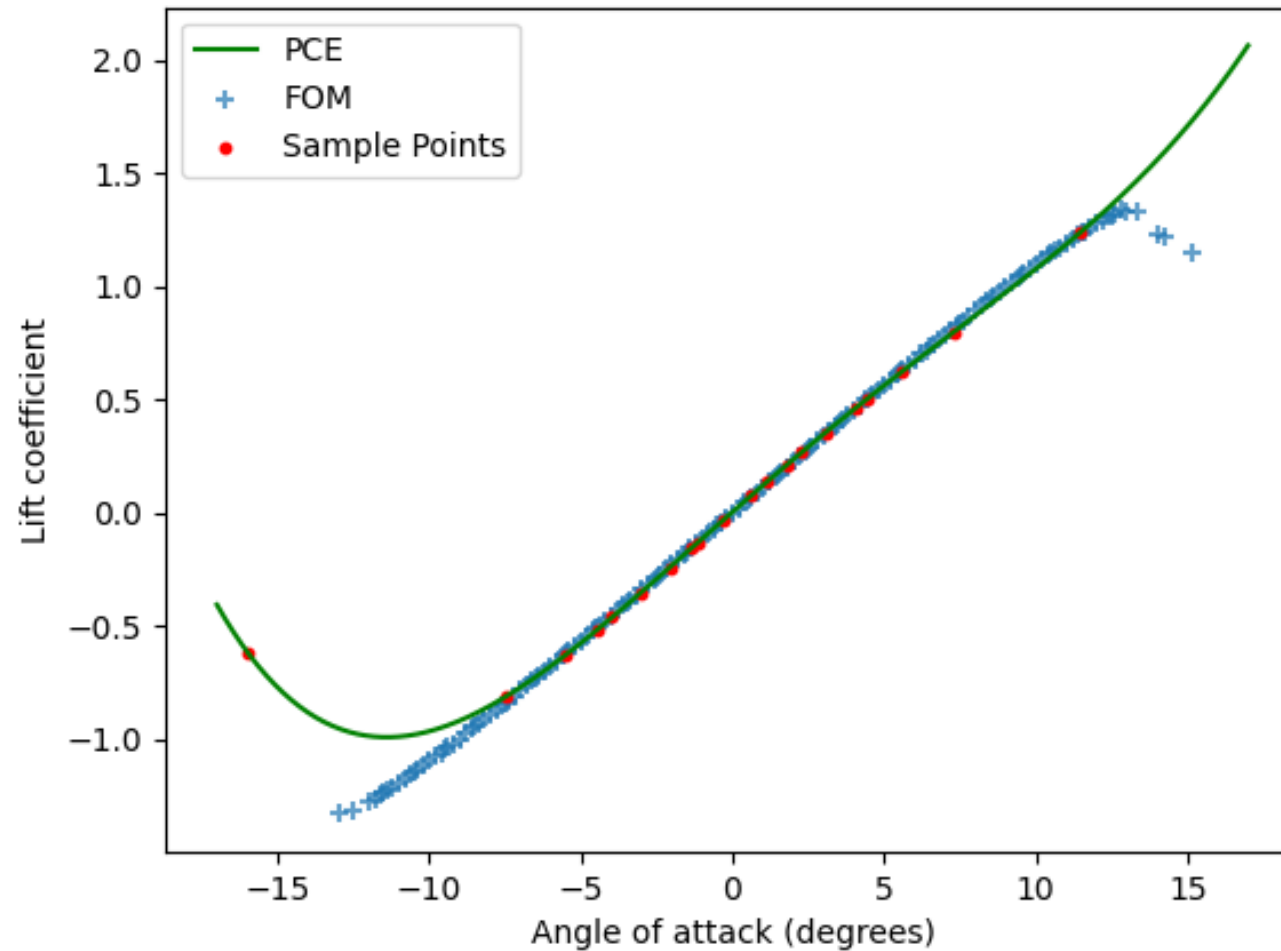


LHS outperforms the Random sampling in most cases.

Impact of Expansion Order

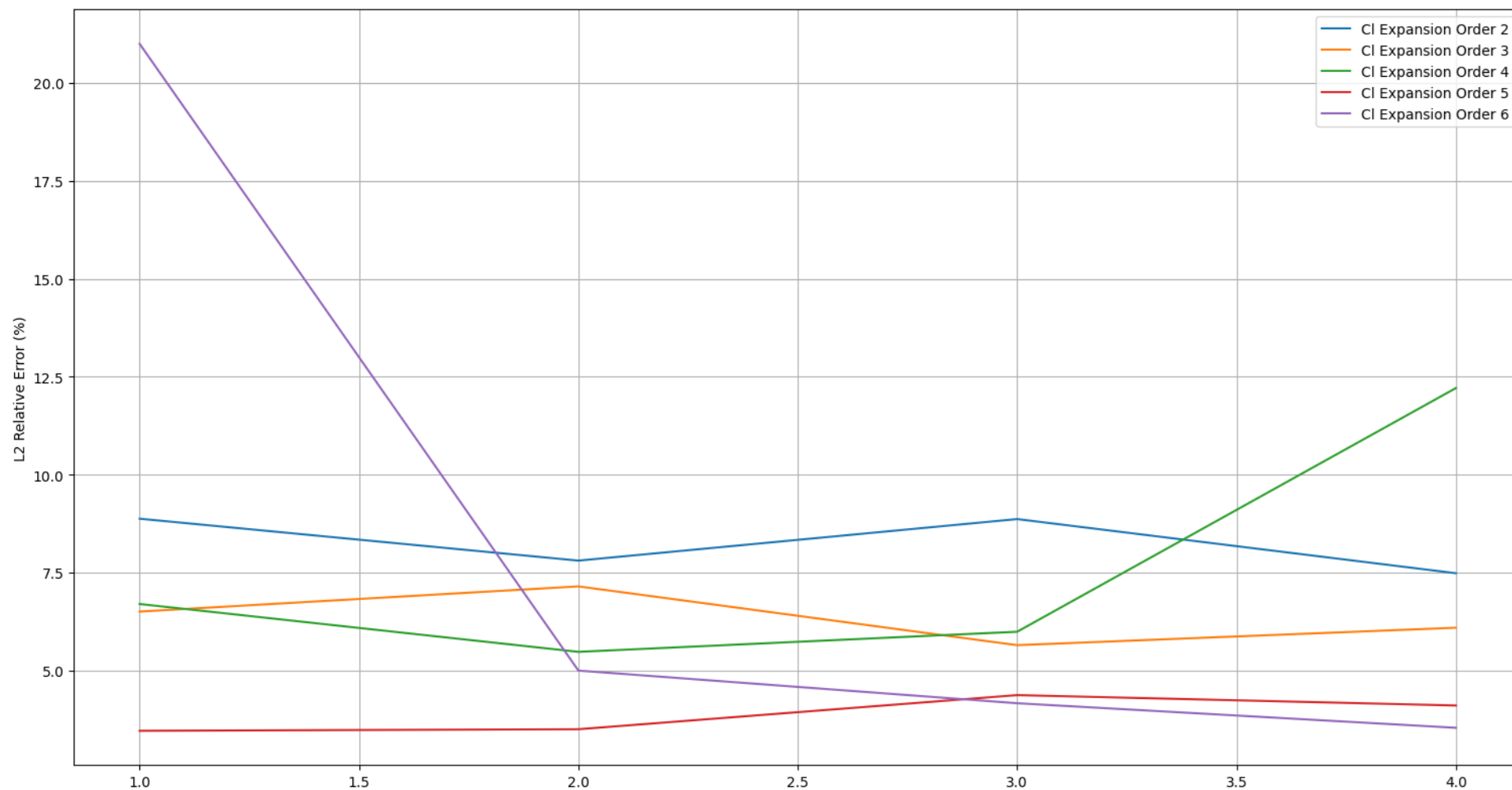


Impact of Expansion Order : Anomaly Explained



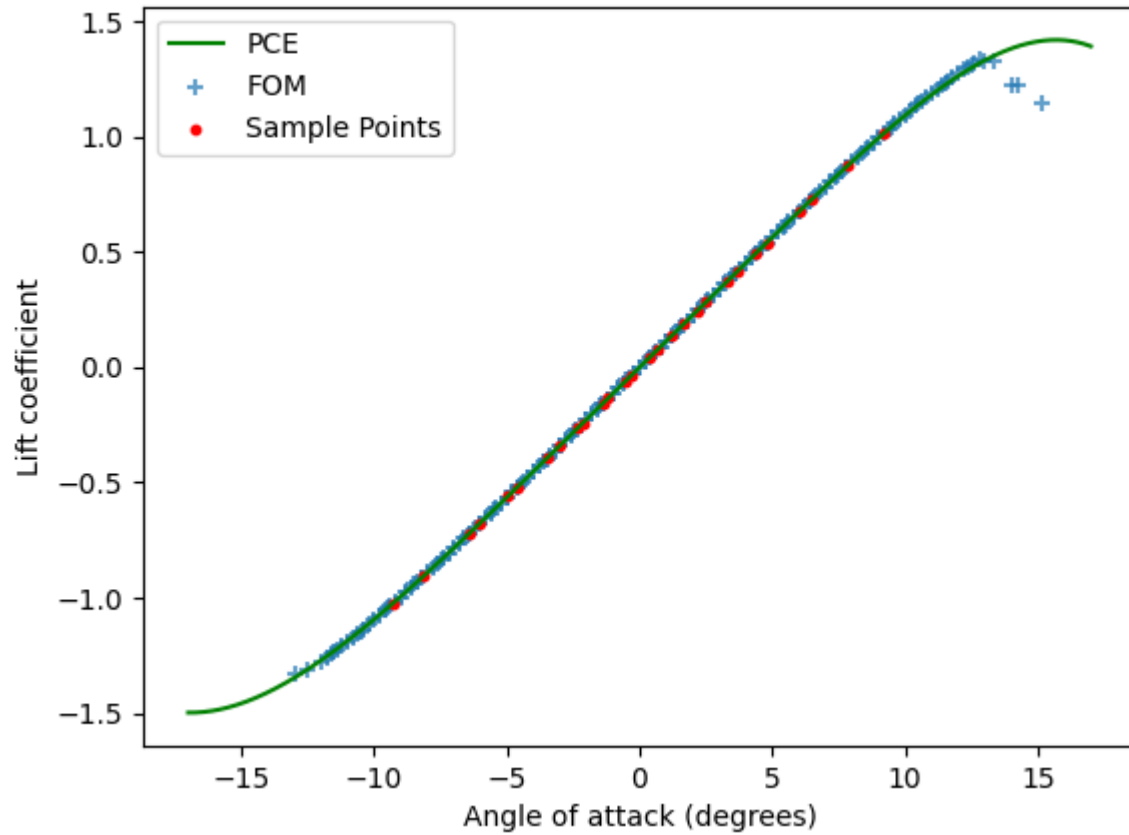
PCE obtained with an Expansion order of 4 and an oversampling ratio of 4

Impact of Oversampling Ratio



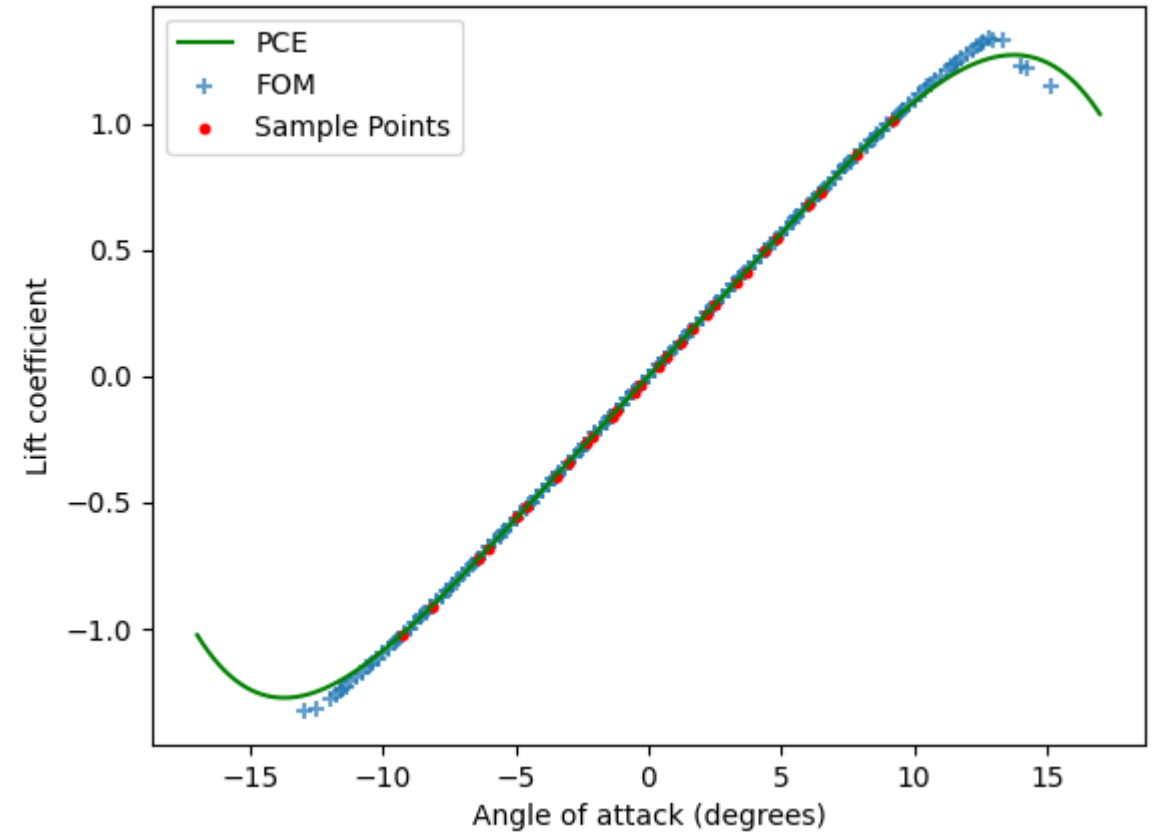
Impact of Fitting Method : Least Squares vs LASSO Regression

Lift coefficient



Best PCE obtained with Least Squares Regression
(Expansion order of 6 and oversampling ratio of 4)

Lift coefficient



Best PCE obtained with LASSO Regression, $\alpha = 0.001$
(Expansion order of 6 and oversampling ratio of 4)

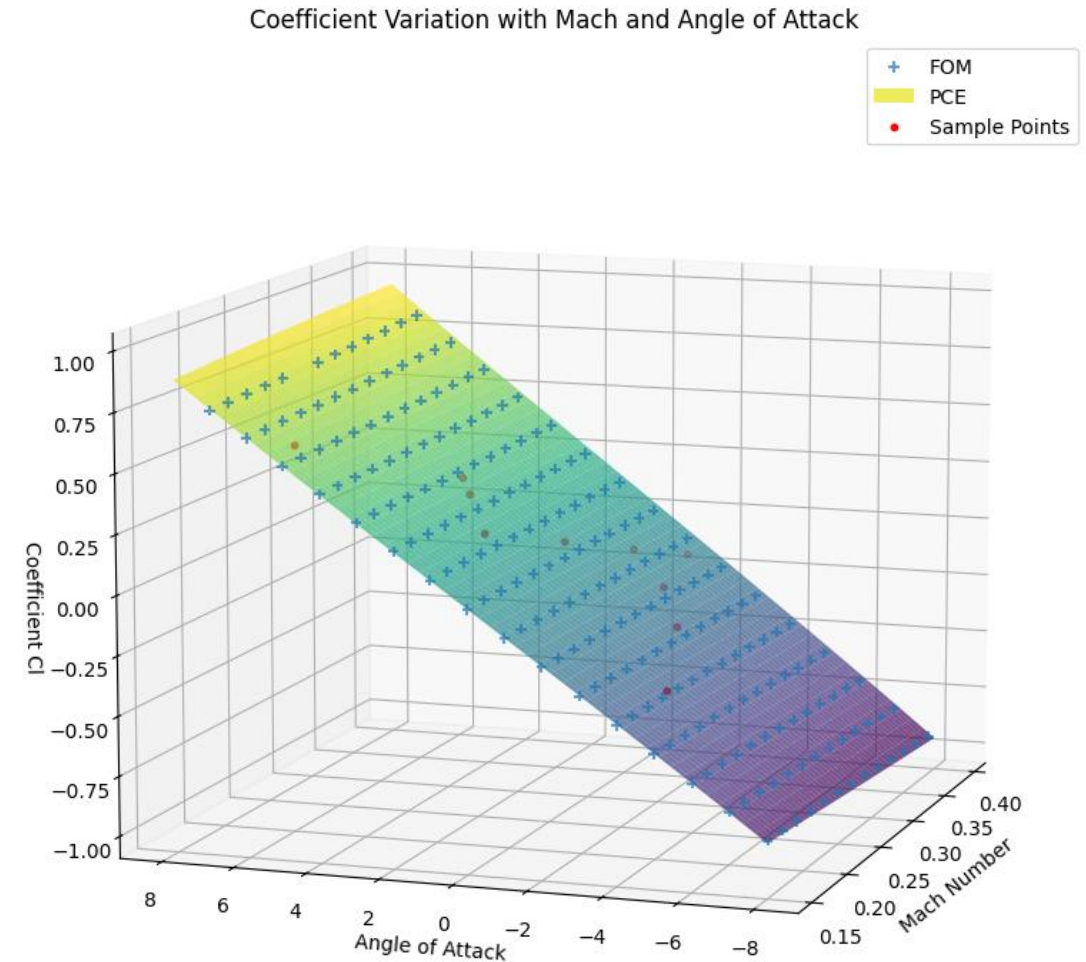
Discussion



- NIPCE Efficacy:
 - Delivers accurate models with few FOM evaluations
 - Versatility in handling untrained data points.
- Considerations for critical perspective:
 - Use of L2 relative error and dataset construction could be seen as arbitrary
 - Some models might better predict specific phenomena despite overall larger error
 - Dependency on FOM robustness

Mach & Two Parameters Uncertainty Analysis

- Mach Number as sole parameter: the same study yielded similar outcomes (cf. Appendices)
- Two uncertain parameters:
 - Initial results are promising
 - Higher computational costs due to additional sample evaluations



PCE obtained for an expansion order of 3 and an oversampling ratio of 1

V. Conclusion and Outlook

Conclusion and Outlook

- Theoretical and practical exploration of the NIPCE for method for UQ in CFD simulations.
 - Effective integration using Chaospy
 - Parametric investigation
- Limitations
 - Dependent on the FOM's robustness
 - Computational capabilities
- Future directions:
 - Deeper dual-parameter uncertainty analysis
 - Robust FOM solver use
 - Transition to Object Oriented Programming
 - Potential comparison of NIPCE results with Monte Carlo simulations
 - Investigate other libraries
 - Machine Learning integration (Gaussian Process Modeling, ...)



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Thank you all for the attention

Any questions ?

Appendix I : Numerical Implementation of NACA0012 Case on OpenFOAM

Parameter	Value
Pressure (p)	10^5 Pa
Temperature (T)	293 K
Gas Model	Air at room temperature (polytropic perfect gas)
Dynamic Viscosity (μ)	1.82×10^{-5}
Prandtl Number (Pr)	0.71
Turbulence Model	k-omega SST
Solver	rhoSimpleFoam

Fixed Parameter of the CFD simulation

First cell size ~0.2mm

```
aerofoil
{
    xLead    0;
    zLead    0;
    xTrail   1;
    zTrail   0;
    xUpper   0.3;
    zUpper   0.06;

    xLower   $xUpper;
    zLower   #neg $zUpper;
}
```

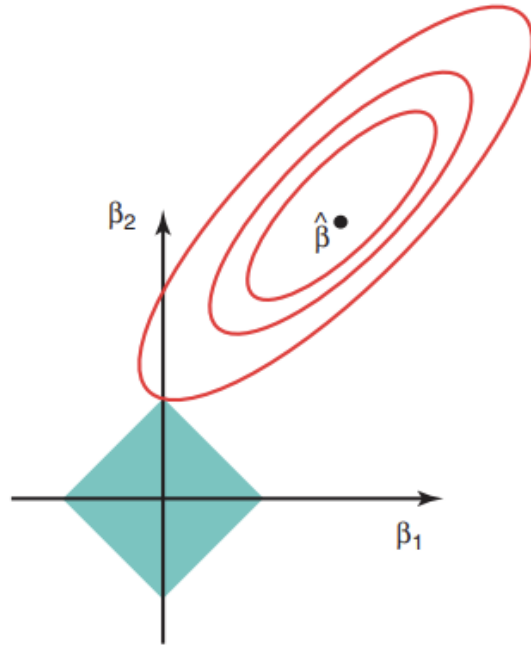
```
domain
{
    xMax 100;
    zMax 50;

    xMin #neg $xMax;
    zMin #neg $zMax;

    // Number of cells
    zCells 60; // aerofoil to far field
    xUCells 60; // upstream
    xMCells 25; // middle
    xDCells 50; // downstream

    // Mesh grading
    zGrading 30000; // aerofoil to far field
    xUGrading 10; // towards centre upstream
    leadGrading 0.005; // towards leading edge
    xDGrading 400; // downstream
}
```

Appendix II : LASSO Regression



Contours of the error and constraint functions for the lasso. The solid blue areas are the constraint regions, $|\beta_1| + |\beta_2| \leq s$, while the red ellipses are the contours of the RSS

The sum of the squares of residuals :

$$\text{RSS} = \sum_{i=1}^n \left(y_i - \beta_0 - \sum_{j=1}^p \beta_j x_{ij} \right)^2.$$

The Lasso regression :

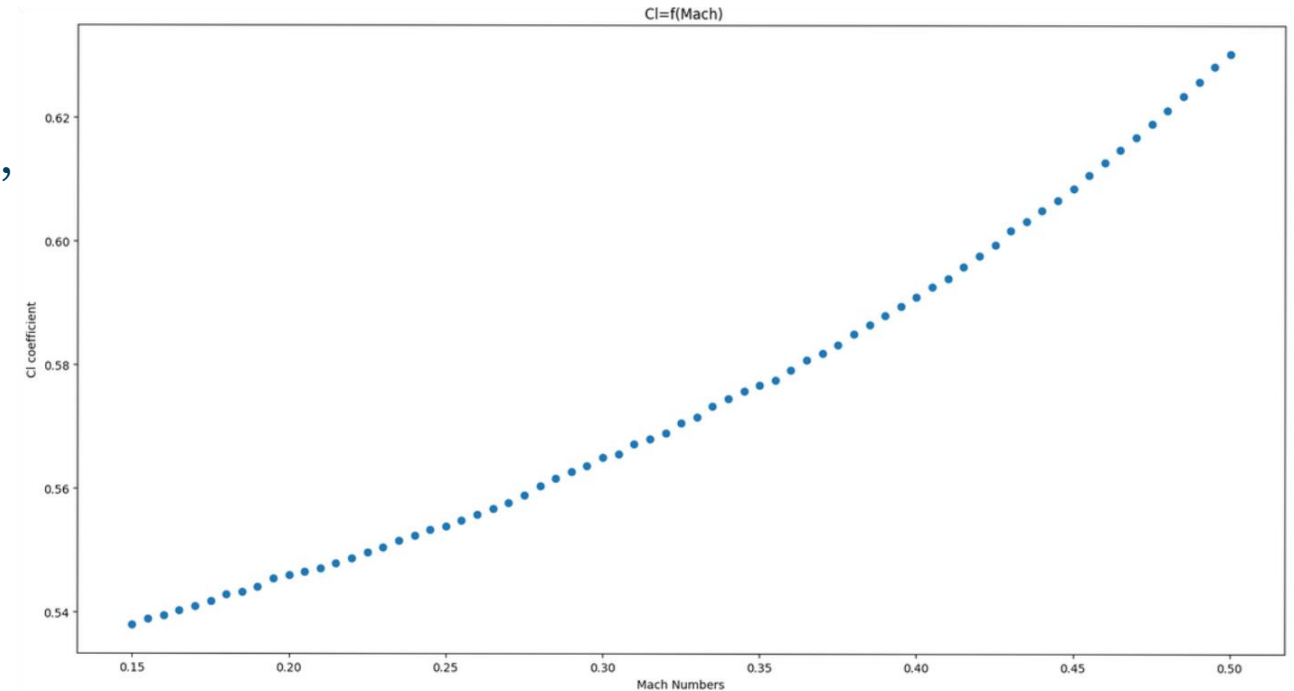
$$\sum_{i=1}^n \left(y_i - \beta_0 - \sum_{j=1}^p \beta_j x_{ij} \right)^2 + \lambda \sum_{j=1}^p |\beta_j| = \text{RSS} + \lambda \sum_{j=1}^p |\beta_j|.$$

Another formulation :

$$\underset{\beta}{\text{minimize}} \left\{ \sum_{i=1}^n \left(y_i - \beta_0 - \sum_{j=1}^p \beta_j x_{ij} \right)^2 \right\} \quad \text{subject to} \quad \sum_{j=1}^p |\beta_j| \leq s$$

Appendix III : NIPCE Implementation : Mach Number uncertainty analysis

- Study Parameters:
 - AOA set at 5°
 - Mach : Normal Distribution, mean 0.325, STD 0.85
- NIPCE Python Implementation:
 - Inputs : FOM, AOA distribution, Expansion order, Sample size, Sampling method, Fitting Method
 - Point Collocation Technique to compute the PCE
- Parametric study:
 - Creation of a reference database to assess the surrogate models accuracy
 - L2 relative error as accuracy metric



Reference values for the Lift Coefficient

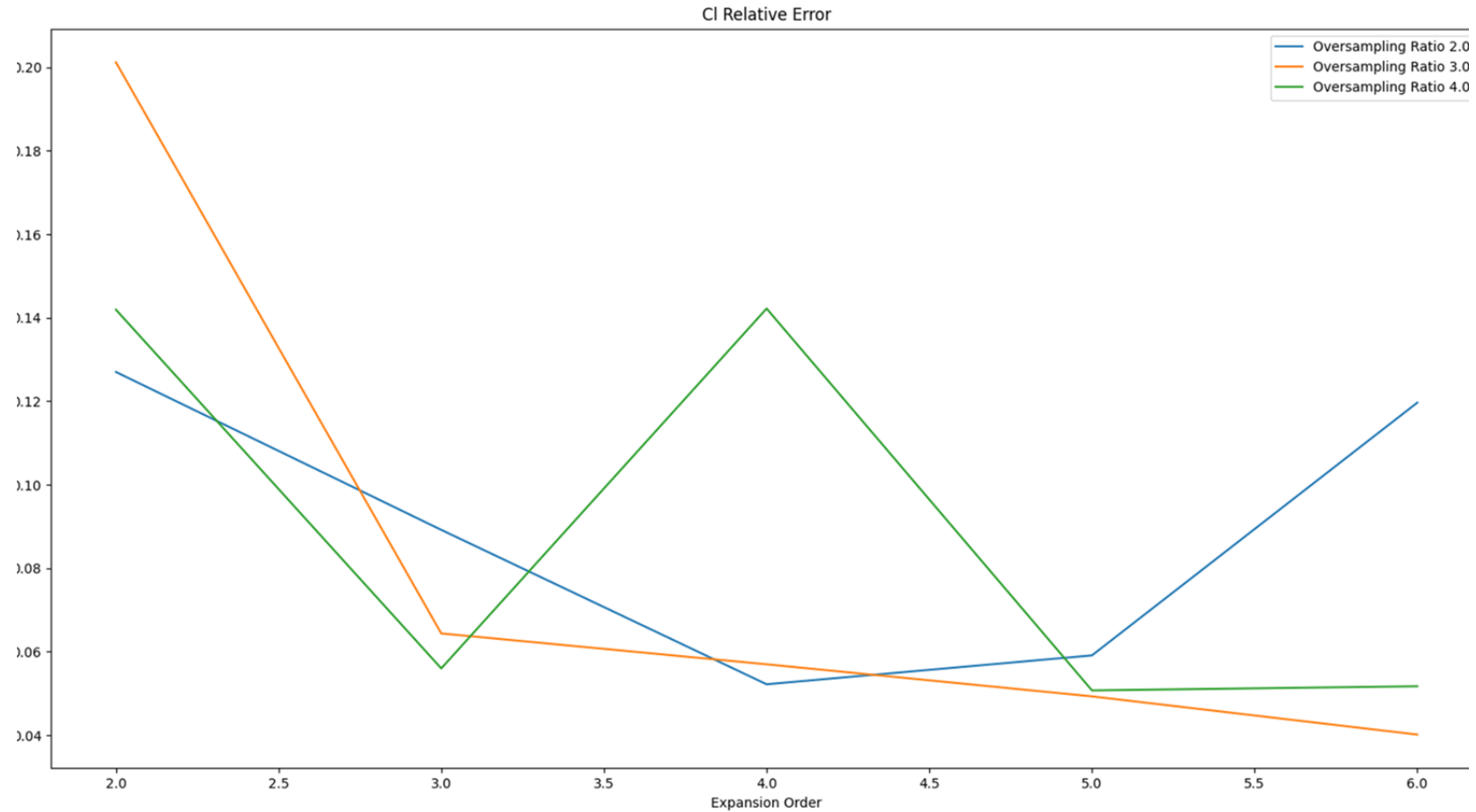
$$\epsilon = 100 \times \frac{\sqrt{\sum_{t=1}^n (C_{l_t}^{\text{FOM}} - C_{l_t}^{\text{PCE}})^2}}{\sqrt{\sum_{t=1}^n (C_{l_t}^{\text{FOM}})^2}} \%$$

Appendix III : NIPCE Implementation : Mach Number uncertainty analysis

EXPANSION ORDER	# SAMPLES	SAMPLING TECHNIQUE	Cd RELATIVE ERROR (%)	CI RELATIVE ERROR (%)
3	6	Random	3,9	0,71
3	6	LHS	0,27	0,06
3	9	Random	1,5	0,34
3	9	LHS	0,38	0,1
4	8	Random	5,7	1
4	8	LHS	0,59	0,11
4	12	Random	4,1	0,75
4	12	LHS	0,309	0,056
5	10	Random	0,78	0,15
5	10	LHS	1,55	0,31
2	4	Random	1,04	0,33
2	4	LHS	0,31	0,12
5	15	Random	1,2	0,26
5	15	LHS	0,47	0,08

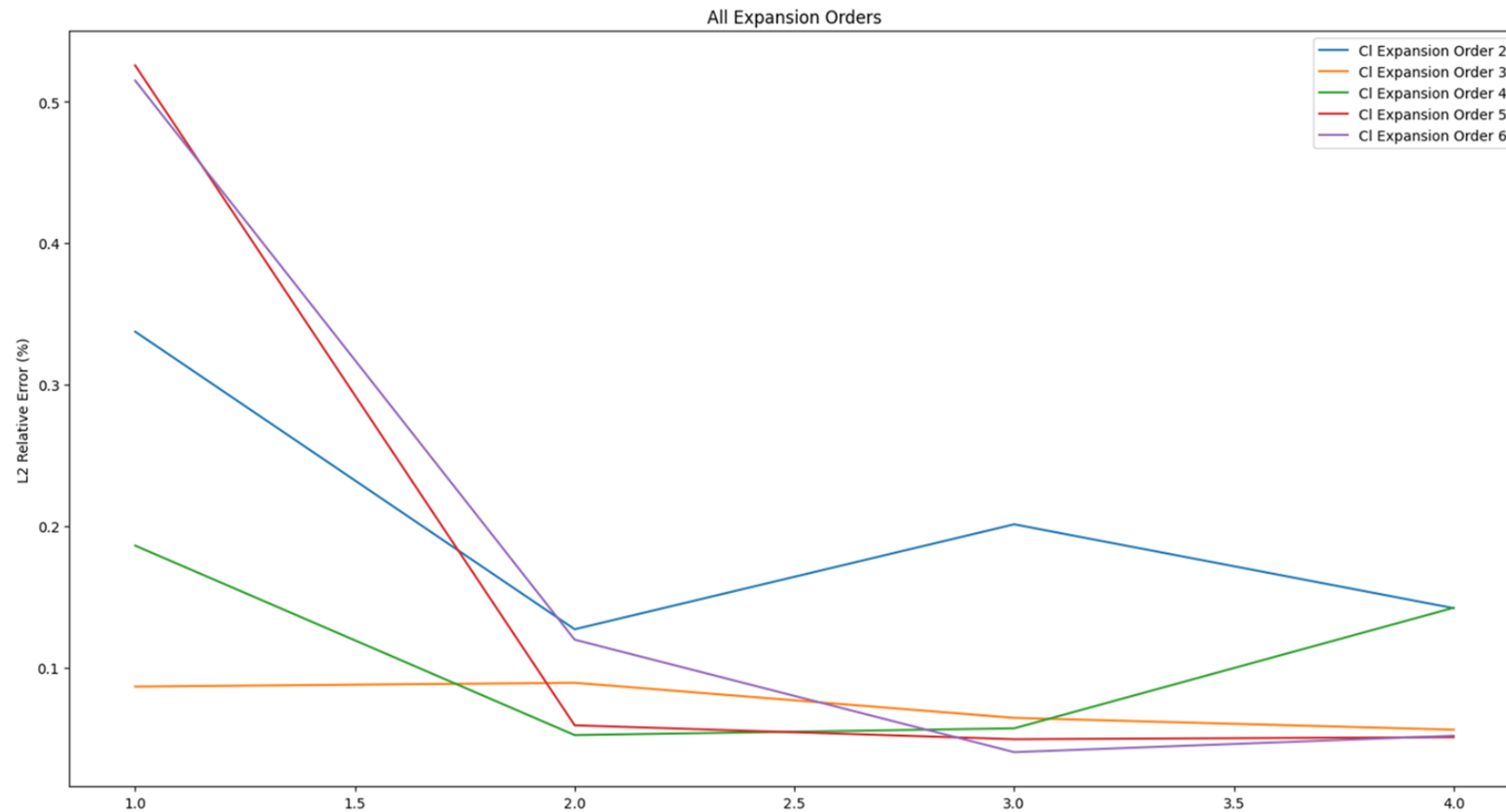
LHS vs Random Sampling

Appendix III : NIPCE Implementation : Mach Number uncertainty analysis



Impact of Expansion Order

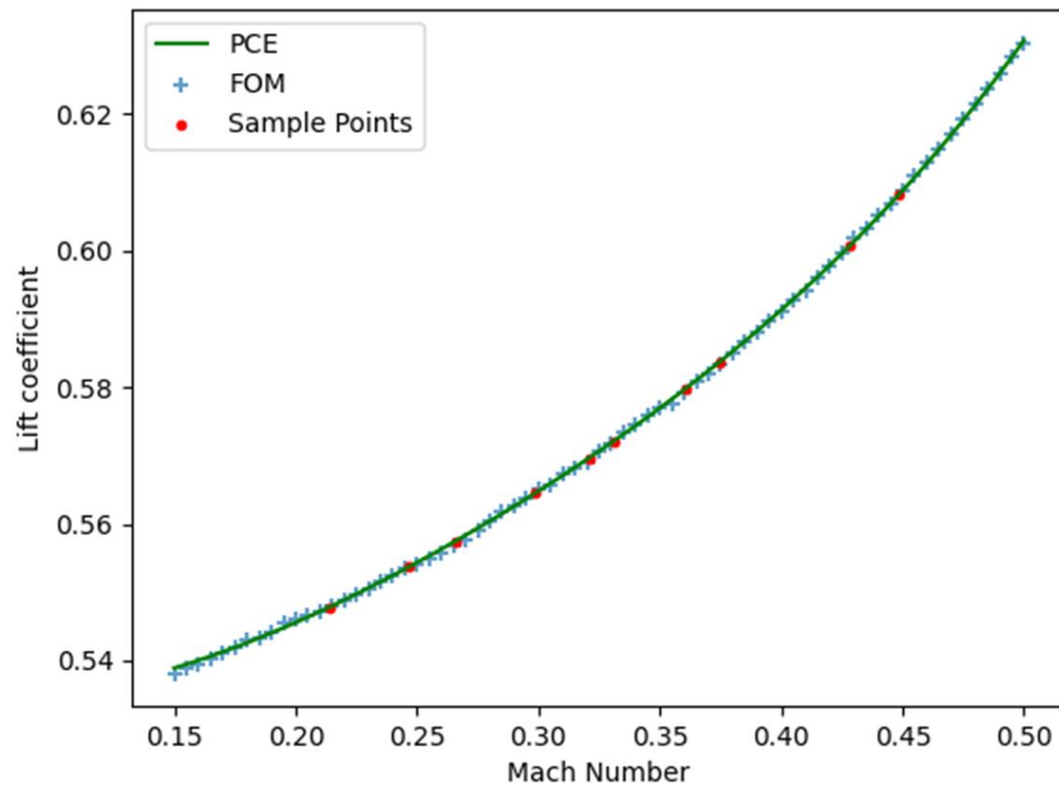
Appendix III : NIPCE Implementation : Mach Number uncertainty analysis



Impact of Oversampling Ratio

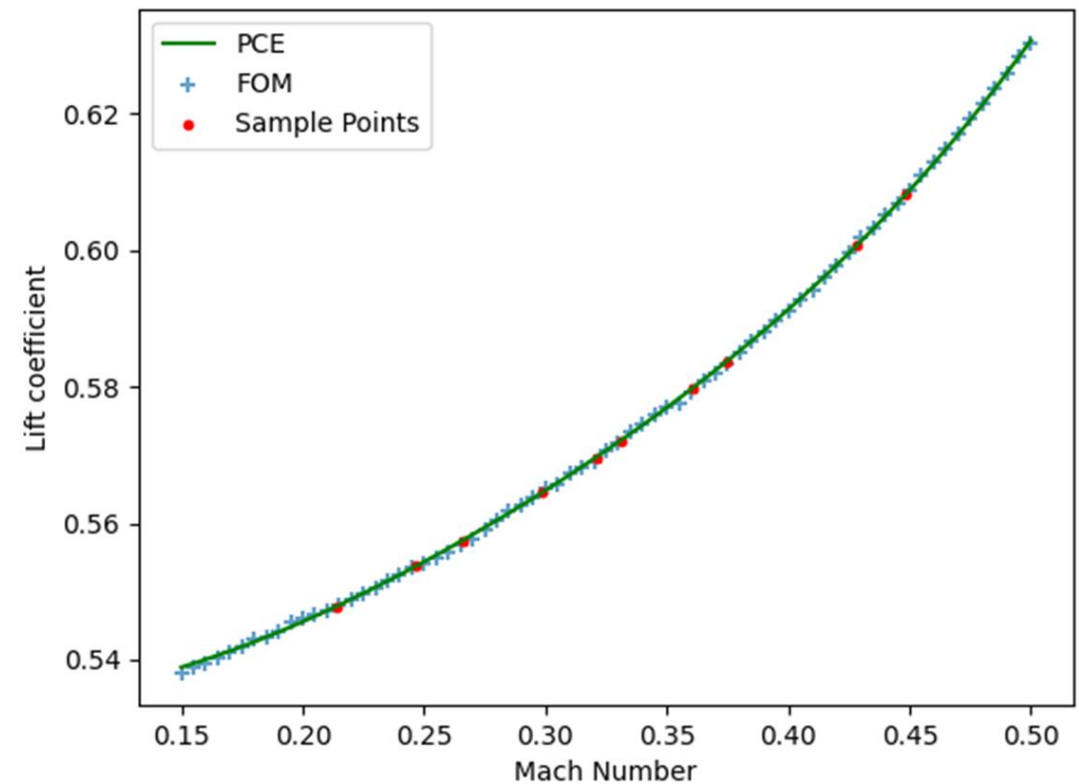
Appendix III : NIPCE Implementation : Mach Number uncertainty analysis

Lift coefficient



Expansion Order = 4
Oversampling Ratio = 2

Lift coefficient



Expansion Order = 4
Oversampling Ratio = 4