

Report

GETEC project



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1 Introduction

bla bla bla

1.1 Subsection

Hello Juliana

(Carrasco-Munoz et al., 2022).

Example of how to reference a figure:

In Fig. 1 shows... blablabla.

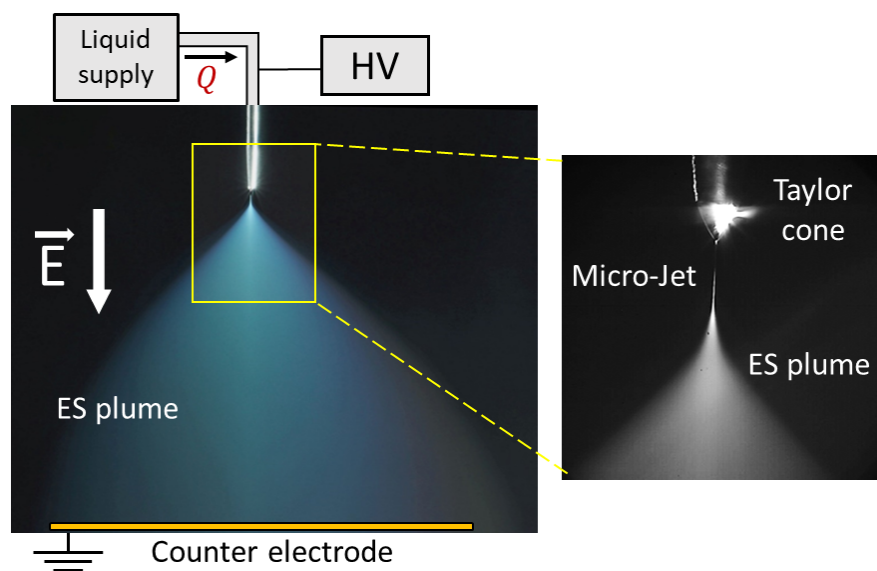


Figure 1. EXAMPLE OF FIGURE. Left: Conventional ES setup. Right: Droplet emission region.

1.2 Subsection

1.2.1 Subsubsection

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1.2.2 Specific objectives

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2 First Approach: PID Controller

2.1 Time Response Analysis

Before developing a proof-of-concept PID controller for the multinozzle, we first need to understand the time response of system to changes in the input.

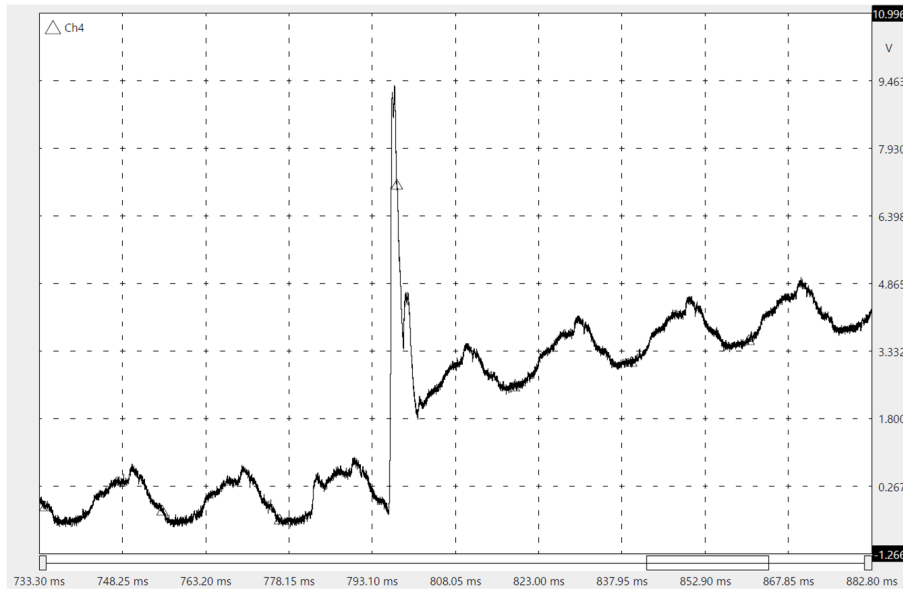


Figure 2. Inrush current on the positive HV+ line.

2.1.1 Subsubsection

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3 Second Approach: Current-based Classification and Control

Once identified the issues with the first approach, we attempted to design a controller based on the classification suggested by Verdoold (add reference).

The strategy adopted will be to first classify the electrospray mode by looking a current values on the system, and then experimentally design a controller that can move from an intermittent to a cone-jet spray mode.

However, Verdoold's method was designed for the single nozzle, and it is not clear if we can extend his classification to a multinozzle configuration. Therefore, part of this work includes an attempt to extend his classification to the system developd by Gilbert.

3.1 Measuring the currents by spray mode

The first test done was to measure the current on all three lines of the sprayhead and verify if we see a pattern in the shape of current that can be used to classify the spray mode. Figure 3 shows the setup used for this test.



Figure 3. Setup to measure all three currents on the sprayhead.

Using three oscilloscopes, all three currents were sampled at 5 kHz, collecting 20.000

samples of each (totalling a 4 seconds time window). Notice that, although the oscilloscope has multiple channels, we cannot use the same oscilloscope as the channels are interconnected internally: the high voltage differences would damage the instrument. Therefore, we use one oscilloscope for each line.

Figure 4 shows the waveforms obtained for $\phi = 20 \text{ mL/h}$.



Figure 4. i_N , i_{GND} and i_C by different spray modes.

As we can see in Figure 4, we don't see a clear distinction in the shape of the current by different spray modes, in both time windows. We repeated the test for $\phi = 30 \text{ mL/h}$ and $\phi = 50 \text{ mL/h}$, obtaining the same result, as shown in Figure 5



Figure 5. i_N , i_{GND} and i_C by different spray modes for all ϕ .

Without a clear distinction in the current waveforms it is not possible to continue with this approach. Therefore, we need to first understand why we are not seeing

distinctions in the shape of the current, particularly between the intermittent and cone-jet spray modes, as it is clear in the literature that there should be a difference.

To do this, we'll begin by attempting to reproduce Verdoold's results, with the goal of isolating if the problem is our measurement strategy or if it is something related to the sprayhead itself.

3.2 Reproducing Verdoold's Results

Figure 6 shows the setup used to reproduce Verdoold's approach. We used a sampling frequency of 5 kHz and $\phi = 1$ mL/h.



Figure 6. Setup used to reproduce Verdoold's classification method.

The results obtained are shown in Figure 7.

As we can see in Figure 7, we see a clear distinction between the spray modes, which is what we wish to see in the multinozzle. We can conclude that our measurement methodology can reproduce the results, therefore it must be something in the multinozzle that is "hiding" the intermittent spray signal.

Comparing the single nozzle setup on Figure 6 and the multinozzle on Figure 3, the most significant difference is indeed the presence of the crown. Therefore, let's begin by understand the influence of the crown on i_{GND} , which is the current that we know is capable of showing a distinction of spraying modes.

3.3 Crown influences on i_{GND}

To understand the influence of the crown on the ground current, we'll use the same setup shown on Figure 3, but we'll make $V_+ = 0$ V, $\phi = 0$ mL/h and measure i_{GND}



Figure 7. Setup used to reproduce Verdoold's classification method.

for different crown voltages. Since there is no flow and no positive voltage, we'll be measuring the current on the grounding ring introduced by the crown only.

Figure 8 shows the shape of i_{GND} for different values of V_- .



Figure 8. i_{GND} for different values of V_- . (a) Waveform and (b) standard deviation

As seen of Figure 8 (a), the crown alone introduces a signal on i_{GND} starting from $V_- = -4\text{ kV}$, which increases in both average value and standard deviation as V_- increases. This is consistent with what happens at the crown: from $V_- = 4\text{ kV}$ the sharp needles of the crown begin to ionize the air, which produces ions that can be directed to ground ring. This results in a current $i_{GND} > 0$ induced by the crown.

In addition, on Figure 8 (b) we see that the standard deviation introduced by the crown is significant. As we saw on Figure 7, the intermittent spray mode presents peaks in the current signal in order of 100 nA, but the "noise" introduced by the crown alone is already over 50 nA. Therefore, it is reasonable to assume that the reason we are not seeing a good distinction between the spray modes on Figure 4 is because of this signal introduced by the crown.

3.3.1 Attenuating Crown Influences on i_{GND}

In order to verify the above hypothesis, we can try to reduce the influence of the crown in the signal and verify if the intermittent signal becomes distinguishable. We can achieve this in two ways:

- Reduce crown voltage
- Add filters in the signal

As we saw in Figure 8 (a), the smaller V_- , the smaller the introduced noise in i_{GND} . Then, we can redo the measurements with a smaller crown voltage.

In addition, we can add digital filters in the oscilloscope to remove the following unwanted frequencies:

- 50 Hz frequency from the electric grid: use a stop band in the range 48 - 52 Hz
- All frequencies above 100 Hz: use low pass filter with cut-off frequency 100 Hz.

Note that, as shown by Verdoold, the intermittent peaks are usually under 100 Hz. Therefore, we can remove anything above this frequency from the signal as it is not what we wish to measure.

Using this, we get ...

3.3.2 8 vs 16 Needle in the Crown

3.4 Optimizing Signal Acquisition

In the previous sections, the signal was acquired using the minimum sampling frequency suggested by the Verdoold of $f_s = 5$ kHz. A sample size of $N_s = 20.000$ was used to obtain a spectral resolution of 0.25 Hz for frequency domain analysis, also suggested by Verdoold as the minimum. However, talks with Gilbert showed that the sampling frequency was too computationally expensive and the sample size was too slow, as it resulted in a sampling time window of 4 seconds, which is too large.

Therefore, to attempt to meet these requirements, we need to find the minimum sampling frequency and minimum sample size that can still reliably distinguish the signal of the intermittent from the cone-jet.

To do this, we'll use the following method:

- Collect a time window of 100 seconds for different values of f_s
- Break the 100 seconds into smaller time windows - denoted as S_i - of size S . Note that $i = 1, 2, \dots$
- Calculate the relevant statistical parameters in each S_i and store these values
- Plot a boxplot of the calculated statistical parameters

We'll use the same setup shown in COMPLETE. The results obtained are shown below on

4 Conclusions

These are the conclusions:

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