

# Hardware-In-the-Loop Testing of Phasor Measurement Unit using Mini-Full Spectrum Simulator

Rathin Dholakia, Roll No: 143076001  
M.Tech, Power Electronics and Power Systems,  
under the guidance of Prof. M. C. Chandorkar,  
Department of Electrical Engineering, IIT Bombay

## I. INTRODUCTION

**D**ay by day power system is becoming more and more complex, which makes it impossible to operate it without automation for higher reliability. Due to wider geographical distribution of the grid, timely detection of faults and taking preventive/corrective counter measure has become a complex task, which requires a reliable, fast-acting and absolute technique to deal with the challenge. This is where the Phasor Measurements Unit (PMU) comes in to the picture. Phasor is a complex number which represents both magnitude and angle of an AC quantity. And the synchronized sampling/ measurement of this phasor at a precise reference (time) is called **synchrophasors** [1]. Using these synchrophasor measurements, different quantities are derived like phase angle, frequency, rate of change of frequency (ROCOF) etc. Frequency is computed as the first derivative of the synchrophasor phase angle, and ROCOF is computed as the second derivative of the same phase angle.

Just like all other engineering devices PMU's reliability, accuracy and precision are very crucial for its application and hence different kinds of test are done to validate its performance. And hence just like other measuring devices to validate t

### A. Background Theory

Phasor representation of sinusoidal signals is commonly used in AC power system analysis. The sinusoidal waveform defined in Equation (1):

$$x(t) = X_m \cos(\omega t + \varphi) \quad (1)$$

is commonly represented as the phasor as shown in Equation (2):

$$\mathbf{X} = \frac{X_m}{\sqrt{2}} \exp^{j\phi} \text{ or } \mathbf{X} = X_r + jX_i \quad (2)$$

The *synchrophasor* representation of the signal  $x(t)$  in Equation (1) is the value  $\mathbf{X}$  in Equation (2) where  $\varphi$  is the instantaneous phase angle relative to a cosine function at the nominal system frequency synchronized to UTC. Before we go into the compliance theory we will go through the basic

definitions for clarity:

**phasor:** A complex equivalent of a sinusoidal wave quantity such that the complex modulus is the cosine wave amplitude, and the complex angle (in polar form) is the cosine wave phase angle.

**UTC:** Its is the time of day at the earth's prime meridian.

**ROCOF:** It is the measure at which the frequency changes in a give instance of time.

**Rate of change of Frequency Error (RFE):** The measure of error between the theoretical ROCOF and the measured ROCOF for the given instant of time.

**Frame:** a data frame or a frame of data is a set of synchrophasor, frequency, and ROCOF measurements that corresponds to the same time stamp.

## II. C37.118 STANDARD COMPLIANCE

**E**very PMU should be able to calculate the value of phasor estimate accurately. The estimate will include positive sequence or single phase values, phase difference, frequency and ROCOF. So it is important to keep in mind that the measurements are actually estimates of certain values.

Now, for a given input wave the computation for estimating the desired quantity are given below: For estimating frequency:

$$f(t) = \frac{1}{2\pi} \frac{d\psi(t)}{dt} \quad (3)$$

The ROCOF is defined as:

$$ROCOF(t) = \frac{df(t)}{dt} \quad (4)$$

important thing to note here is that phasors are always computed in relation to the system nominal frequency ( $f_0$ ). Here  $\psi(t) = \omega_0 t + \varphi(t)$

### A. Measurement Evaluation

To validate the estimation coming from PMUs they are compared with the theoretical results. As results consists of amplitude and phase difference both they are considered combinedly and this quantity is called *total vector error* (TVE). TVE is an expression of difference between "perfect" sample of a theoretical synchrophasor and the estimate given by the

unite at the same instant of time [1]. The value is normalized and expressed in PU of the theoretical phasor:

$$PVE(n) = \sqrt{\frac{(\hat{X}_r(n) - X_r(n))^2 + (\hat{X}_i(n) - X_i(n))^2}{X_r(n)^2 + X_i(n)^2}} \quad (5)$$

Here  $\hat{X}_r(n)$  and  $\hat{X}_i(n)$  are the estimated values of the given phasor and  $X_r$  and  $X_i$  are the theoretical values. to be compliant with standard, PMU shall provide synchrophasor, frequency, and ROCOF measurements that meet the requirements as per the standards at a given time instance  $n$ . Similarly for freq and ROCOF the validation will be done using following equations:

$$FE == |f_{true} - f_{measured}| = |\Delta f_{true} - \Delta f_{measured}| \quad (6)$$

$$RFE == |(df/dt)_{true} - (df/dt)_{measured}| \quad (7)$$

Apart from the above 3 quantitative parameters other three important parameters to be considered are measurement response time & delay and reporting delay. *Measurement response time* is the time to transition between two steady-state measurements before and after a step change is applied to the input. *Measurement delay time* is defined as the time interval between the instant that a step change is applied to the input of a PMU and measurement time that the stepped parameter achieves a value that is halfway between the initial and final steady-state values [1]. The reason of measuring time delay is to verify that the time tagging has been compensated properly or not. *Latency in reporting* is the time taken between the occurrence of even in power system and that being reflected in the output of the PMU. This parameter largely depends on the class of PMU and the sampling and filtering algorithm used. Which brings us to the classification of the PMU, they are divided in two parts:

- 1) **Protection Class (P class):** This PMU is used for protection purposes and hence its response time should be as much less as possible.
- 2) **Measurement Class (M class):** This PMU class emphasies on the accuracy of the reported data and hence timing requirement are not as stringent as P class PMUs.

On the basis of above class PMU's TVE tolerance limit is set, as discribed in above points protection class is for application requiring fast response and M class is for application requiring higher accuracy.the TVE norm for P class is more stringent compared to M class.

### B. Validation & Testing

To get the TVE, compliance tests are performed and during the test only the quantity under test is varied from the reference condition as per the test and other relevant quantities are maintained at reference condition. There are following kind of compliance tests:

- 1) Steady-state compliance
  - a) Steady-state synchrophasor measurement requirements
  - b) Steady-state frequency and ROCOF measurement requirements
- 2) Dynamic compliance

- a) Synchrophasor measurement bandwidth requirements using modulated test signals
- b) Ramp of system frequency
- c) Step changes in phase and magnitude

The TVE tolerance for each case wont be mentioned here as those tables can be looked into the standards.

## III. IMPLEMENTATION

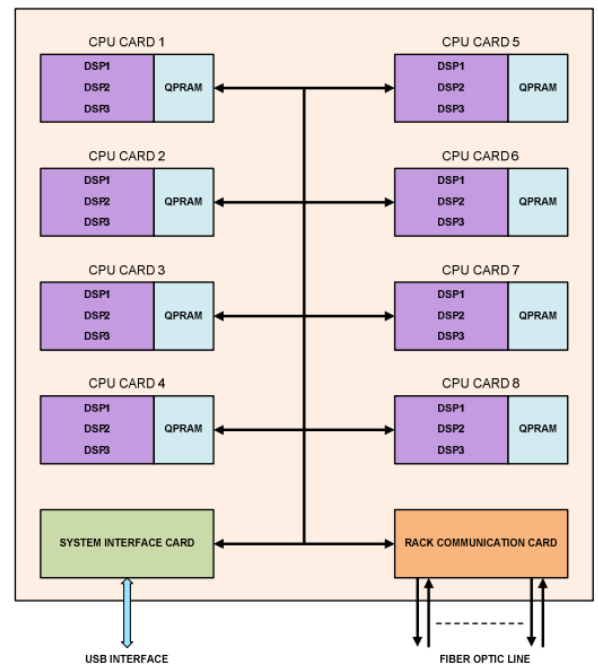
Overview of the test setup can be seen in FIGURE, Implementation can be divided in three parts

- 1) **Full Spectrum Simulator (FSS):** Which will have the power system model, through which different test conditions will be given
- 2) **PMU:** Which will consist of a ADC interfacing board and OMAP-L 137 EVM
- 3) **PC:** It will have a Phasor Data Concentrator (PDC), which receives data from the PMU and record it for future analysis.

During the initial phase of the project intention was to use indigenously PMU developed C-DAC but due to the hardware issues and lack of documentation and support, it was decided that a minimalistic PMU will be developed by ourself.

### A. Full Spectrum Simulator:

As per the requirement of the implementation, miniature-Full spectrum Simulator will be used for this purpose. FSS is a card based, multi CPU - parallel processing hardware.It uses TI's MSP430 DSPs as building block. It was developed by IIT Bombay and CDAC for both, offline & real-time simulation purposes in Power Electronics and Power Systems.



## REFERENCES

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