

Hardware-In-the-Loop Testing of Phasor Measurement Unit using Mini-Full Spectrum Simulator

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I. ABSTRACT

PMU are vital in modern power grid due to advancement operation and control. Here in this report description of a PMU being developed using OMAP-L137, its testing and verification using a Full Spectrum Simulator (FSS) is discussed. The tests and its standardization reference is taken by smart grid standard C37.118. While developing the PMU, a custom high speed ADC board is designed, its interfaced to OMAP using EMIFA - a new interfacing method available in L13x processors, is used. This setup will be hooked up to mini-FSS which will provide different test signals.

II. INTRODUCTION

Day by day power system is becoming more and more complex, which makes it impossible to operate it without automation for higher reliability. Due to wider geographical distribution of the grid, timely detection of faults and taking preventive/corrective counter measure has become a complex task, which requires a reliable, fast-acting and absolute technique to deal with the challenge. This is where the Phasor Measurements Unit (PMU) comes in to the picture. Phasor is a complex number which represents both magnitude and angle of an AC quantity. And the synchronized sampling/ measurement of this phasor at a precise reference (time) is called **synchrophasors** [1]. Using these synchrophasor measurements, different quantities are derived like phase angle, frequency, rate of change of frequency (ROCOF) etc. Frequency is computed as the first derivative of the synchrophasor phase angle, and ROCOF is computed as the second derivative of the same phase angle.

Just like all other engineering devices PMU's reliability, accuracy and precision are very crucial for its application and hence different kinds of test are done to validate its performance. And hence just like other measuring devices PMU standards are defined. All device should at least meet the requirement stated by the standards, as per their application.

So, here with this project we are exploring the application of miniaturised Full spectrum simulator as an Hardware -in-loop-testing device for PMUs. We will see the feasibility as well as effectiveness of the platform and how they can be mitigated to make it suitable for C37.118 compliance testing. This report

is largely divided in two parts 1) C37.118 standard, tests and its explanation and 2) implementation. The *compliance* section provides theory section

A. Background Theory

Phasor representation of sinusoidal signals is commonly used in AC power system analysis. The sinusoidal waveform defined in Equation (1):

$$x(t) = X_m \cos(\omega t + \varphi) \quad (1)$$

is commonly represented as the phasor as shown in Equation (2):

$$\mathbf{X} = \frac{X_m}{\sqrt{2}} \exp^{j\varphi} \text{ or } \mathbf{X} = X_r + jX_i \quad (2)$$

The *synchrophasor* representation of the signal $x(t)$ in Equation (1) is the value \mathbf{X} in Equation (2) where φ is the instantaneous phase angle relative to a cosine function at the nominal system frequency synchronized to UTC. Before we go into the compliance theory we will go through the basic definitions for clarity:

phasor: A complex equivalent of a sinusoidal wave quantity such that the complex modulus is the cosine wave amplitude, and the complex angle (in polar form) is the cosine wave phase angle.

UTC: Its is the time of day at the earth's prime meridian.

ROCOF: It is the measure at which the frequency changes in a give instance of time.

Rate of change of Frequency Error (RFE): The measure of error between the theoretical ROCOF and the measured ROCOF for the given instant of time.

Frame: a data frame or a frame of data is a set of synchrophasor, frequency, and ROCOF measurements that corresponds to the same time stamp.

III. C37.118 STANDARD COMPLIANCE

Every PMU should be able to calculate the value of phasor estimate accurately. The estimate will include positive sequence or single phase values, phase difference, frequency and ROCOF. So it is important to keep in mind that the measurements are actually estimates of certain values.

Now, for a given input wave the computation for estimating the desired quantity are given below: For estimating frequency:

$$f(t) = \frac{1}{2\pi} \frac{d\psi(t)}{dt} \quad (3)$$

The ROCOF is defined as:

$$ROCOF(t) = \frac{df(t)}{dt} \quad (4)$$

important thing to note here is that phasors are always computed in relation to the system nominal frequency (f_0). Here $\psi(t) = \omega_0 t + \varphi(t)$

A. Measurement Evaluation

To validate the estimation coming from PMUs they are compared with the theoretical results. As results consists of amplitude and phase difference both they are considered combinedly and this quantity is called *total vector error* (TVE). TVE is an expression of difference between "perfect" sample of a theoretical synchrophasor and the estimate given by the unite at the same instant of time [1]. The value is normalized and expressed in PU of the theoretical phasor:

$$PVE(n) = \sqrt{\frac{(\hat{X}_r(n) - X_r(n))^2 + (\hat{X}_i(n) - X_i(n))^2}{X_r(n)^2 + X_i(n)^2}} \quad (5)$$

Here $\hat{X}_r(n)$ and $\hat{X}_i(n)$ are the estimated values of the given phasor and X_r and X_i are the theoretical values. to be compliant with standard, PMU shall provide synchrophasor, frequency, and ROCOF measurements that meet the requirements as per the standards at a given time instance n . Similarly for freq and ROCOF the validation will be done using following equations:

$$FE == |f_{true} - f_{measured}| = |\Delta f_{true} - \Delta f_{measured}| \quad (6)$$

$$RFE == |(df/dt)_{true} - (df/dt)_{measured}| \quad (7)$$

Apart from the above 3 quantitative parameters other three important parameters to be considered are measurement response time & delay and reporting delay. *Measurement response time* is the time to transition between two steady-state measurements before and after a step change is applied to the input. *Measurement delay time* is defined as the time interval between the instant that a step change is applied to the input of a PMU and measurement time that the stepped parameter achieves a value that is halfway between the initial and final steady-state values [1]. The reason of measuring time delay is to verify that the time tagging has been compensated properly or not. *Latency in reporting* is the time taken between the occurrence of even in power system and that being reflected in the output of the PMU. This parameter largely depends on the class of PMU and the sampling and filtering algorithm used. Which brings us to the classification of the PMU, they are divided in two parts:

- 1) **Protection Class (P class):** This PMU is used for protection purposes and hence its response time should be as much less as possible.
- 2) **Measurement Class (M class):** This PMU class emphasies on the accuracy of the reported data and hence timing requirement are not as stringent as P class PMUs.

On the basis of above class PMU's TVE tolerance limit is set, as discribed in above points protection class is for application requiring fast response and M class is for application requiring higher accuracy.the TVE norm for P class is more stringent compared to M class.

B. Validation & Testing

To get the TVE, compliance tests are performed and during the test only the quantity under test is varied from the reference condition as per the test and other relevant quantities are maintained at reference condition. There are following kind of compliance tests:

- 1) Steady-state compliance
 - a) Steady-state synchrophasor measurement requirements
 - b) Steady-state frequency and ROCOF measurement requirements
- 2) Dynamic compliance
 - a) Synchrophasor measurement bandwidth requirements using modulated test signals
 - b) Ramp of system frequency
 - c) Step changes in phase and magnitude

The TVE tolerance for each case wont be mentioned here as those tables can be looked into the standards.

Main Category of PMU Testing	Sub-Category of PMU Testing	System Conditions (Cases) for Sub-Category
Dynamic Performance Tests	Magnitude Response to Step Change Tests	Balanced, Unbalanced, Off-nominal Frequency
	Phase Angle Response to Step Change Tests	Balanced, Unbalanced, Off-nominal Frequency
Tests	Frequency Response to Step Change Tests	Balanced, Unbalanced with Harmonics
	ROCOF Response to Step Change Tests	Balanced, Unbalanced, with Harmonics

IV. IMPLEMENTATION

Overview of the test setup can be seen in FIGURE, Implementation can be divided in three parts

- 1) **Full Spectrum Simulator (FSS):** Which will have the power system model, through which different test conditions will be given
- 2) **PMU:** Which will consist of a ADC interfacing board and OMAP-L 137 EVM
- 3) **PC:** It will have a Phasor Data Concentrator (PDC), which receives data from the PMU and record it for future analysis.

During the initial phase of the project intention was to use indigenously PMU developed C-DAC but due to the hardware issues and lack of documentation and support, it was decided that a minimalistic PMU will be developed by ourself.

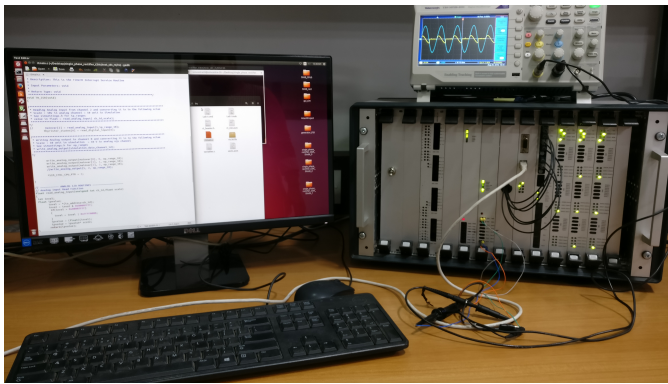


Fig. 1: Mini-FSS setup in laboratory

A. Full Spectrum Simulator:

As per the requirement of the implementation, miniature-Full spectrum Simulator will be used for this purpose. FSS is a card based, multi CPU - parallel processing hardware. It uses TI's MSP430 DSPs as building block. It was developed by IIT Bombay and CDAC for both, offline & real-time simulation purposes in Power Electronics and Power Systems.

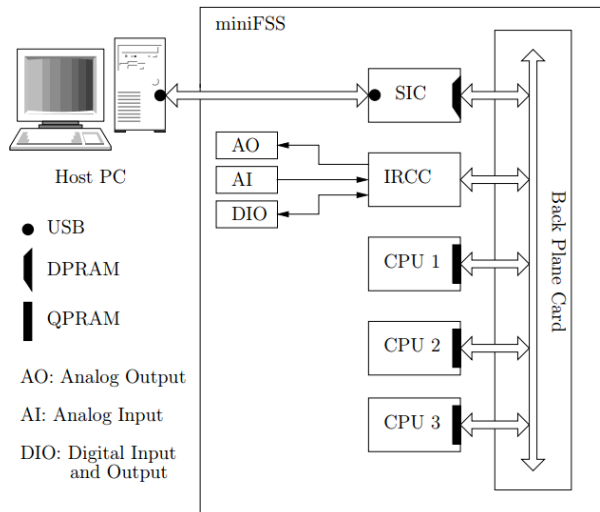


Fig. 2: FSS architecture

As shown in 2 above it is a card base setup which contains:

- System Interface Card (SIC)
- Intra Rack Control Card (IRC Card)
- Three CPU Cards (CPU 0, CPU 1 and CPU 2), each having 3 digital signal processors on it. So there are total 9 processors allowing for parallel computation.
- One Analog Output Card (AO Card), having 6 analog output channels (10 V range).
- One Analog Input Card (AI Card), having 6 differential analog input channels (10 V range).
- One Digital Input/Output Card (DIO Card), having 24 digital inputs and 24 digital outputs (0 - 5 V).
- One Back Plane PCB.

• System Interface Card:

It is called SiC, its acts as a communication layer between host PC and the device. Its consists of TUSB chip which connects it to the host PC, a TMS320 to interface SIC with IRC card and a MSP430 to have RS-232 interfacing.

- **IRC Card:** IRC is designed as a master control, which eventually control other cards, peripheral communication, timer triggered execution and host pc communication. Further more IRC card handles analog as well as digital input-output also. Apart from that IRC processor also controls the simulation execution using it's timer on the respective CPU card. IRC card has protocol implemented to communicate between CPU cards and SIC so that simulation can be controlled and it's result can be sent to respective peripheral and/or can be downloaded to host PC.

• CPU card:

mini-FSS has 3 CPU cards, each having TI's MSP430 DSPs. This card is heart of the FSS. They handle all the mathematical algorithm associated with the simulation. Data flowing from and to the cards are controlled by IRC card via **back plane** PCB.

B. PMU

OMAP-L137 EVM is being used as the platform to design a PMU. OMAP-L137 EVM doesnt have Analog to Digital Converter on board hence a interfacing circuit is developed. While designing the ADC board following criteria were kept considered.

- Good sampling rate: 200 Samples/Sec
- No of channels: 3 + 3 = 6 (3 - ϕ voltage and current)
- Interfacing type: It should be memory addressable and voltage level compatible to the EVM.
- Input type: FSS analog output is differential which can be configured as single. their voltage level is $\pm 10V$

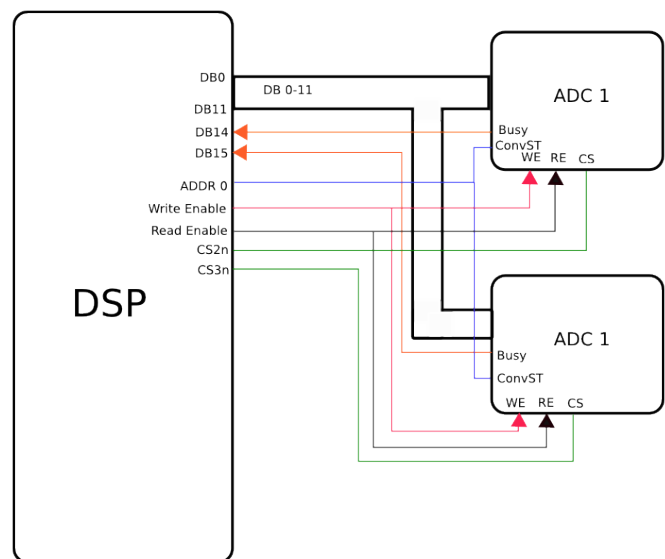


Fig. 3: ADC Board block diagram

Above Fig:3 shows the design logic of ADC board. Two AD7864-1 are used as ADC chips due to their high sampling

rate of 500 kbps and direct input voltage compatibility range of ± 10 V. AD7864 is a high speed 4 channel simultaneous sampling successive approximation ADC with conversion time as low as $1.65\mu\text{sec}$. its conversion sequence can be controlled through hardware as well as software, its default operating voltage is 5v but has a special output voltage shifter for interfacing it with 3.3v processors and controllers. This ADCs are fairly advance hence they have been interfaced with a special asynchronous peripheral interfacing architecture called EMIF-A, which is exclusively available in OMAP-L13x series processors. Extended Memory InterFace (EMIF) has two parts A & B out of which EMIF-B is having *Enhanced Direct Memory Access* controller (EDMA3) which enables the processor for multi-threaded rapid memory access and hence it is exclusively for highspeed SDRAM interfacing where as interface A (EMIF-A) is developed for generic purposes more details are given below:

1) *EMIF-A*: EMIF-A controller is a 16-bit databus based versatile controller [7], designed to interact with variety of devices like

- Single Data Rate (SDR) RAM
- Asynchronous devices like NAND & NOR flash memory and SRAM

It contains lot of features to ease and facilitate the usage of asynchronous devices. A functional block diagram is given here in Fig: 4 It is apparent from figure-4, that it has 4 chip selects and, one read and write and 16 data channels. which makes it very convenient for interfacing multiple peripherals at a time.

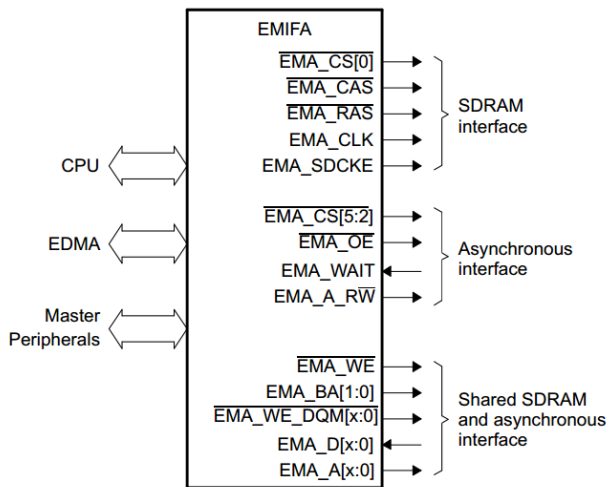


Fig. 4: EMIFA Block Diagram [7]

2) *ADC board Logic*: Due to EMIFA, interfacing of ADC board became quite convenient rather than using pins in GPIO mode. So the logical flow of the board is as follows:

- 6 input channels are required hence 2 ICs are used
- Chip Select (CS), Read, Write, and databits from 0 - 11 are directly available from the EMIFA interface, and they are shared with both the chips.
- AD7864 has sequence selection which has been configured through hardware, and Clock source has been kept

internal. because of this both the pins INT/EXT_CLK & H/S select

- AD7864 has 3 control output Busy, FIRSTDATA and EOC. Out of these only busy is observed via a data line (data bits 16 & 15). Data is **anded** is not read until data line 15 & 14 are not zero.
- AD7864 supports two kinds of data reading 1) Reading during the conversion 2) Reading after the conversion. Here we are going to use *Reading After the conversion*, below is the timing diagram of the chip for understanding the proper functioning of the circuit.

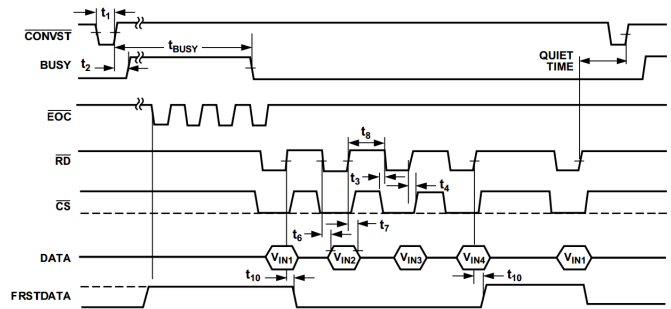


Fig. 5: ADC Reading After the Conversion timing

Now we will see the operation that takes place when sampling is to be done:

- Assert start of conversion (CONVST) is asserted via EMA_CS[4]
- Due to this chip will start the conversion processes which will make BUSY high,
- Status of BUSY will be checked via DB15 & DB14 pins of the EMIFA header, for both the chips until they are low again.
- The moment BUSY goes low, EMA_CS[2] and EMA_A_RE are asserted with which AD7864 starts putting data on data lines. this processes of asserting is repeated for 4 times, for each channel. The same is done using EMA_CS[3] for getting data from 2nd ADC chip.

3) *Computer*: It will have the Phasor Data Concentrator (PDC) program, which will collate the data coming from our PMU coming over serial bus. PDC usually has two functions one is to archive the data for historic reference and to send the data upward to higher level PDC for control actions and analytics. Here a PDC program developed by other M.Tech students is going to be used which is called **iPDC** [3]. iPDC has two parts, one part controls the data sources and the communication of configuration frame. The other part DBserver works as a data storage manager, which archives the data received at a given port. Configuration frame is first communicated before starting the transmission of data to know the number of channels, digital status word etc. Though for existing setup config frame wont be required so program can be modified accordingly to function without it.

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