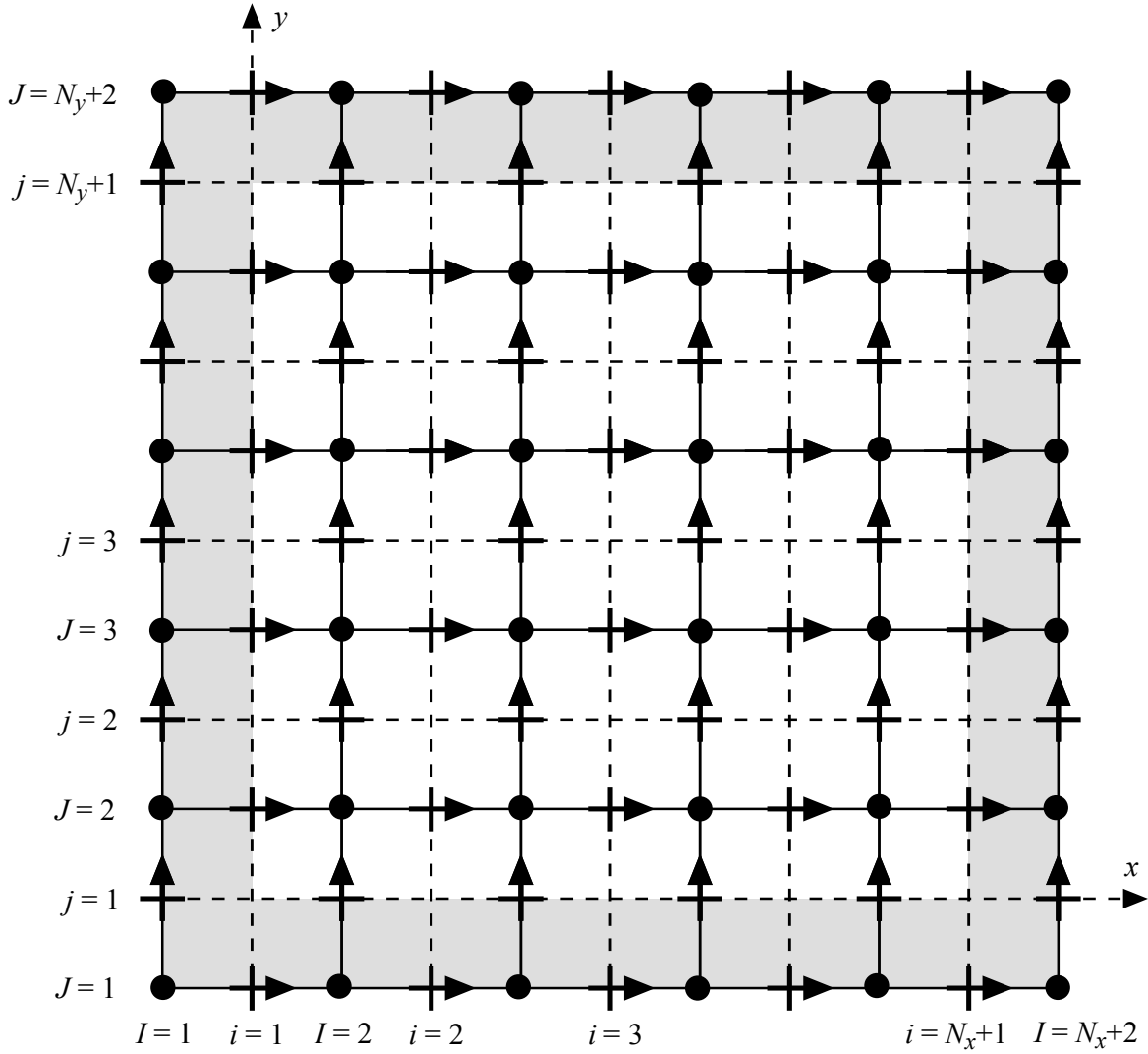


Staggered Grid for SIMPLE with Main Nodes Surrounding Domain:



Nomenclature for Grid Geometry:

I, J main grid points for scalar properties $\phi(I, J)$, $I=1, 2, \dots, N_x+2$ and $J=1, 2, \dots, N_y+2$

i, j staggered grid points for $u(i, J)$ and $v(I, j)$, $i=1, 2, \dots, N_x+1$ and $j=1, 2, \dots, N_y+1$

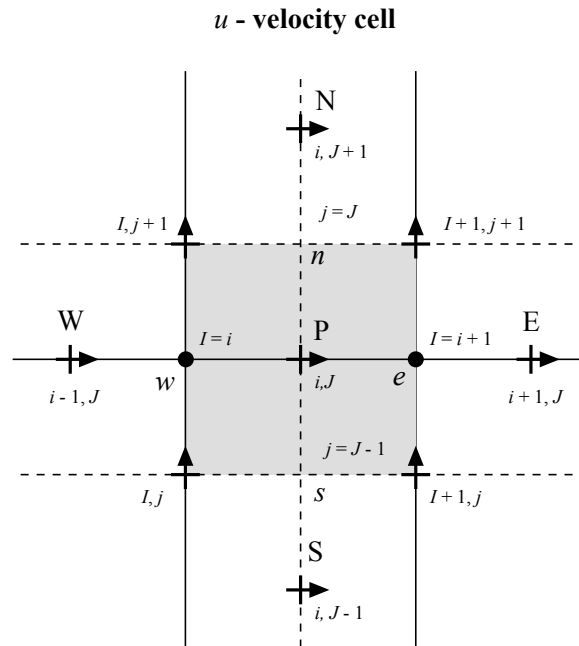
L_x domain length in x -direction N_x number of main grid points in x -direction

L_y domain length in y -direction N_y number of main grid points in y -direction

$$0 \leq x \leq L_x, \quad dx = L_x / N_x, \quad x = (i-1)dx = (I-3/2)dx$$

$$0 \leq y \leq L_y, \quad dy = L_y / N_y, \quad y = (j-1)dy = (J-3/2)dy$$

Derivation of x-Momentum Equation for Interior Node:



Recall steady x -momentum equation for finite volume formulation:

$$\sum_{f=1}^{N_f} u_f (\rho \vec{v} \cdot \vec{n} A)_f = \sum_{f=1}^{N_f} (\mu \nabla u \cdot \vec{n} A)_f - \left(\frac{\partial p}{\partial x} \right)_f \nabla x$$

For two-dimensional domain for interior elements aligned with the x and y axis

$$u_e(\rho u A)_e - u_w(\rho u A)_w + u_n(\rho u A)_n - u_s(\rho u A)_s =$$

$$\left(\mu \frac{\partial u}{\partial x} A\right)_e - \left(\mu \frac{\partial u}{\partial x} A\right)_w + \left(\mu \frac{\partial u}{\partial y} A\right)_n - \left(\mu \frac{\partial u}{\partial y} A\right)_s + (p_w - p_e) dy dz$$

Define the following advection (or *flow*) coefficient, F , and *diffusion* coefficient, D , at the faces where the gradient is evaluated using 2-point central finite difference approximation:

$F_w = (\rho u A)_w = \rho dy dz [u(i-1, J) + u(i, J)]/2$	$D_w = (\mu/dx)_w A_w = (\mu/dx)_w dy dz$
$F_e = (\rho u A)_e = \rho dy dz [u(i, J) + u(i+1, J)]/2$	$D_e = (\mu/dx)_e A_e = (\mu/dx)_e dy dz$
$F_s = (\rho v A)_s = \rho dx dz [v(I, j) + v(I+1, j)]/2$	$D_s = (\mu/dy)_s A_s = (\mu/dy)_s dx dz$
$F_n = (\rho v A)_n = \rho dx dz [v(I, j+1) + v(I+1, j+1)]/2$	$D_n = (\mu/dy)_n A_n = (\mu/dy)_n dx dz$

NOTE: For constant properties: $D_x = D_w = D_e = (\mu/dx)dydz$, $D_y = D_s = D_n = (\mu/dy)dx dz$

$$F_e u_e - F_w u_w + F_n u_n - F_s u_s = \\ D_e (u_E - u_P) - D_w (u_P - u_W) + D_n (u_N - u_P) - D_s (u_P - u_S) + (p_w - p_e) dy dz$$

Evaluate properties at the faces using the *hybrid differencing scheme*.

$Pe_f > 2$	$Pe_f < -2$	$-2 \leq Pe_f \leq 2$
$u_w = u_W$, $D_w = 0$	$u_w = u_P$, $D_w = 0$	$u_w = (u_W + u_P) / 2$
$u_e = u_P$, $D_e = 0$	$u_e = u_E$, $D_e = 0$	$u_e = (u_E + u_P) / 2$
$u_s = u_S$, $D_s = 0$	$u_s = u_P$, $D_s = 0$	$u_s = (u_S + u_P) / 2$
$u_n = u_P$, $D_n = 0$	$u_n = u_N$, $D_n = 0$	$u_n = (u_N + u_P) / 2$

where Pe is the Peclet number (ratio of advection to diffusion rate). At high Pe number this is 1st order upwinding with no diffusion. For moderate Pe this is central differencing.

$$Pe_f = \frac{(\rho u)_f}{(\mu/dx)_f} = \frac{F_f}{D_f}$$

For $2 \leq Pe \leq -2$ for all faces we get

$$\begin{aligned} \frac{F_e}{2}(u_E + u_P) - \frac{F_w}{2}(u_W + u_P) + \frac{F_n}{2}(u_N + u_P) - \frac{F_s}{2}(u_S + u_P) = \\ D_e (u_E - u_P) - D_w (u_P - u_W) + D_n (u_N - u_P) - D_s (u_P - u_S) + (p_w - p_e) dy dz \\ \left(\frac{F_e}{2} + D_e - \frac{F_w}{2} + D_w + \frac{F_n}{2} + D_n - \frac{F_s}{2} + D_s \right) u_P = \\ \left(D_e - \frac{F_e}{2} \right) u_E + \left(D_w + \frac{F_w}{2} \right) u_W + \left(D_n - \frac{F_n}{2} \right) u_N + \left(D_s + \frac{F_s}{2} \right) u_S + (p_w - p_e) dy dz \end{aligned}$$

Rewrite as

$$\begin{aligned} a_P u_P &= a_W u_W + a_E u_E + a_S u_S + a_N u_N + b \\ a_E &= D_e - F_e/2 , \quad a_W = D_w + F_w/2 , \quad a_N = D_n - F_n/2 , \quad a_S = D_s + F_s/2 \\ a_P &= a_W + a_E + a_S + a_N + \Delta F , \quad \Delta F = F_e - F_w + F_n - F_s , \quad b = (p_w - p_e) dy dz \end{aligned}$$

For $Pe > 2$ for all faces we get

$$F_e u_P - F_w u_W + F_n u_P - F_s u_S = (p_w - p_e) dy dz$$

$$(F_e + F_n) \phi_P = F_w \phi_W + F_s \phi_S + (p_w - p_e) dy dz$$

$$a_E = 0, \quad a_W = F_w, \quad a_N = 0, \quad a_S = F_s$$

For $Pe < -2$ for all faces we get

$$F_e u_E - F_w u_P + F_n u_N - F_s u_P = 0$$

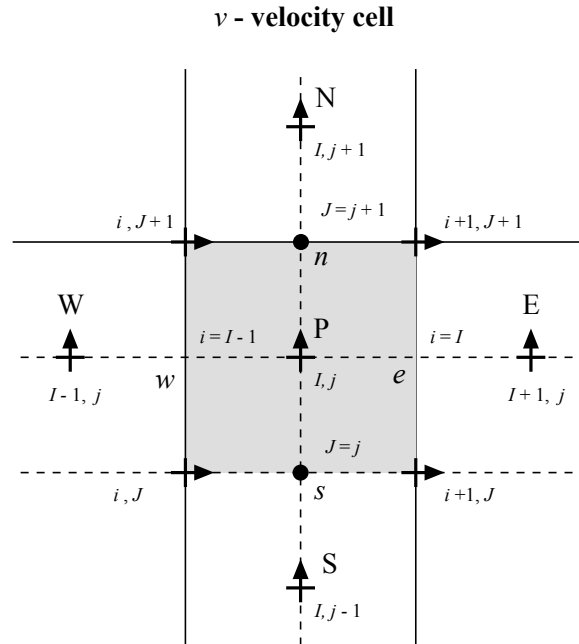
$$-(F_w + F_s) u_P = -F_e u_W - F_n u_S$$

$$a_E = -F_e, \quad a_W = 0, \quad a_N = -F_n, \quad a_S = 0$$

These three possibilities can be programed using the following:

$a_W = \max(0, F_w, D_w + F_w/2)$	$a_S = \max(0, F_s, D_s + F_s/2)$
$a_E = \max(0, -F_e, D_e - F_e/2)$	$a_N = \max(0, -F_n, D_n - F_n/2)$

Derivation of y-Momentum Equation for Interior Node:



Recall steady y-momentum equation for finite volume formulation:

$$F_w = (\rho u A)_w = \rho dy dz [u(i, j) + u(i, j+1)]/2$$

For two-dimensional domain for interior elements aligned with the x and y axis

$$v_e(\rho v A)_e - v_w(\rho v A)_w + v_n(\rho v A)_n - v_s(\rho v A)_s =$$

$$\left(\mu \frac{\partial v}{\partial x} A \right)_e - \left(\mu \frac{\partial v}{\partial x} A \right)_w + \left(\mu \frac{\partial v}{\partial y} A \right)_n - \left(\mu \frac{\partial v}{\partial y} A \right)_s + (p_s - p_n) dx dz$$

Define the following advection (or *flow*) coefficient, F , and *diffusion* coefficient, D , at the faces where the gradient is evaluated using 2-point central finite difference approximation:

$F_w = (\rho u A)_w = \rho dy dz [u(i, J) + u(i, J+1)]/2$	$D_w = (\mu/dx)_w A_w = (\mu/dx)_w dy dz$
$F_e = (\rho u A)_e = \rho dy dz [u(i+1, J) + u(i+1, J+1)]/2$	$D_e = (\mu/dx)_e A_e = (\mu/dx)_e dy dz$
$F_s = (\rho v A)_s = \rho dx dz [v(I, j-1) + v(I, j)]/2$	$D_s = (\mu/dy)_s A_s = (\mu/dy)_s dx dz$
$F_n = (\rho v A)_n = \rho dx dz [v(I, j) + v(I, j+1)]/2$	$D_n = (\mu/dy)_n A_n = (\mu/dy)_n dx dz$

NOTE: For constant properties: $D_x = D_w = D_e = (\mu/dx) dy dz$, $D_y = D_s = D_n = (\mu/dy) dx dz$

$$F_e v_e - F_w v_w + F_n v_n - F_s v_s =$$

$$D_e (v_E - v_P) - D_w (v_P - v_W) + D_n (v_N - v_P) - D_s (v_P - v_S) + (p_s - p_n) dx dz$$

Again, use hybrid differencing scheme (with same coefficients as above) and rewrite as:

$$a_P v_P = a_w v_W + a_E v_E + a_S v_S + a_N v_N + b \quad , \quad b = (p_s - p_n) dx dz$$

Derivation of Advection-Diffusion Equation for Property at Main Node:

Recall general steady, advection-diffusion equation for finite volume formulation:

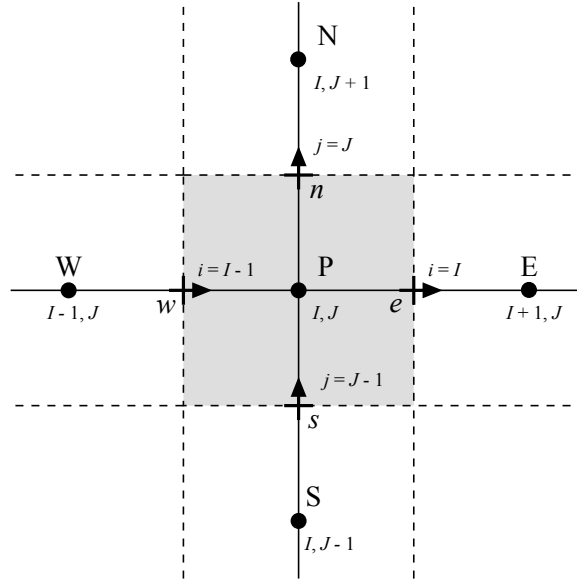
$$\sum_{f=1}^{N_f} \phi_f (\rho \vec{V} \cdot \vec{n} A)_f = \sum_{f=1}^{N_f} (\Gamma \nabla \phi \cdot \vec{n} A)_f + S_\phi \nabla$$

For two-dimensional domain for interior elements aligned with the x and y axis

$$\phi_e (\rho u A)_e - \phi_w (\rho u A)_w + \phi_n (\rho u A)_n - \phi_s (\rho u A)_s =$$

$$\left(\Gamma \frac{\partial \phi}{\partial x} A \right)_e - \left(\Gamma \frac{\partial \phi}{\partial x} A \right)_w + \left(\Gamma \frac{\partial \phi}{\partial y} A \right)_n - \left(\Gamma \frac{\partial \phi}{\partial y} A \right)_s + S_\phi \nabla$$

scalar property cell



Define the following advection (or *flow*) coefficient, F , and *diffusion* coefficient, D , at the faces where the gradient is evaluated using 2-point central finite difference approximation:

$F_w = (\rho u A)_w = \rho u(i-1, J) dy dz$	$D_w = (\Gamma / dx)_w A_w = (\Gamma / dx)_w dy dz$
$F_e = (\rho u A)_e = \rho u(i, J) dy dz$	$D_e = (\Gamma / dx)_e A_e = (\Gamma / dx)_e dy dz$
$F_s = (\rho v A)_s = \rho v(I, j-1) dx dz$	$D_s = (\Gamma / dy)_s A_s = (\Gamma / dy)_s dx dz$
$F_n = (\rho v A)_n = \rho v(I, j) dx dz$	$D_n = (\Gamma / dy)_n A_n = (\Gamma / dy)_n dx dz$

NOTE: For constant properties: $D_x = D_w = D_e = (\Gamma / dx) dy dz$, $D_y = D_s = D_n = (\Gamma / dy) dx dz$

$$F_e \phi_e - F_w \phi_w + F_n \phi_n - F_s \phi_s = D_e (\phi_e - \phi_P) - D_w (\phi_P - \phi_w) + D_n (\phi_n - \phi_P) - D_s (\phi_P - \phi_s) + S_\phi \quad \nabla$$

Again, use hybrid differencing scheme (with same coefficients as above) and rewrite as:

$$a_P \phi_P = a_w \phi_w + a_e \phi_e + a_s \phi_s + a_n \phi_n + b, \quad b = S_\phi \quad \nabla$$

Velocity Correction Equations:

Define actual, guessed (or starred) and corrected (or primed) values as follows:

$$u = u^* + u', \quad v = v^* + v', \quad \text{and} \quad p = p^* + p'$$

Calculate an updated velocity field, u^* and v^* , using x and y -momentum equations with guessed pressure field, p^* , and coefficients estimated using guessed velocity fields:

$$a_p u_p^* = a_w u_w^* + a_e u_e^* + a_s u_s^* + a_n u_n^* + (p_w^* - p_e^*) dy dz$$

$$a_p v_p^* = a_w v_w^* + a_e v_e^* + a_s v_s^* + a_n v_n^* + (p_s^* - p_n^*) dx dz$$

Subtract these equations from original momentum equation and substitute in corrections to get:

$$a_p u_p' = a_w u_w' + a_e u_e' + a_s u_s' + a_n u_n' + (p_w' - p_e') dy dz$$

$$a_p v_p' = a_w v_w' + a_e v_e' + a_s v_s' + a_n v_n' + (p_s' - p_n') dx dz$$

Simplify by neglecting neighboring correction values and rewrite as:

$$u_p' = du_p (p_w' - p_e') , \quad du_p = \begin{cases} dy dz / a_p & \text{SIMPLE} \\ dy dz / (a_p - \sum a_{nb}) & \text{SIMPLE-C} \end{cases}$$

$$v_p' = dv_p (p_s' - p_n') , \quad dv_p = \begin{cases} dy dz / a_p & \text{SIMPLE} \\ dy dz / (a_p - \sum a_{nb}) & \text{SIMPLE-C} \end{cases}$$

Finally, substituting back into definitions for

$$u_p = u_p^* + du_p (p_w' - p_e') \quad \text{or} \quad u_{i,j} = u_{i,j}^* + du_{i,j} (p'_{i,j} - p'_{i+1,j})$$

$$v_p = v_p^* + dv_p (p_s' - p_n') \quad \text{or} \quad v_{i,j} = v_{i,j}^* + dv_{i,j} (p'_{i,j} - p'_{i,j+1})$$

Pressure Correction Equation from Conservation of Mass for Main Node

Recall conservation of mass for finite volume formulation:

$$\sum_{f=1}^{N_f} (\rho \vec{V} \cdot \vec{n} A)_f = 0$$

For two-dimensional domain for interior elements aligned with the x and y axis

$$(\rho u A)_e - (\rho u A)_w + (\rho v A)_n - (\rho v A)_s = 0$$

Substitute in corrected velocities to get

$$\begin{aligned} & \rho dy dz [u_e^* + du_e(p'_P - p'_E) - u_w^* - du_w(p'_W - p'_P)] + \\ & \rho dx dz [v_n^* + dv_n(p'_P - p'_N) - v_s^* - dv_s(p'_S - p'_P)] = 0 \\ & [\rho dy dz (du_e + du_w) + \rho dx dz (dv_n + dv_s)] p'_P = (\rho dy dz du_e) p'_E + (\rho dy dz du_w) p'_W + \\ & (\rho dx dz dv_n) p'_N + (\rho dx dz dv_s) p'_S + [\rho dy dz (u_w^* - u_e^*) + \rho dx dz (v_s^* - v_n^*)] \end{aligned}$$

Rewrite as

$$\begin{aligned} a_P p'_P &= a_W p'_W + a_E p'_E + a_S p'_S + a_N p'_N + b' \\ a_P &= a_W + a_E + a_S + a_N, \quad b' = \rho dy dz (u_w^* - u_e^*) + \rho dx dz (v_s^* - v_n^*) \end{aligned}$$

$a_W = \rho dy dz du_w$	$a_S = \rho dx dz dv_s$
$a_E = \rho dy dz du_e$	$a_N = \rho dx dz dv_n$