

EE 102 Week 5, Lecture 1 (Fall 2025)

Instructor: Ayush Pandey

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1 Goals

2 Review: LTI systems and convolutions

Recall that using the linearity and time-invariance of the system, we can define the output, $y(t)$ of the system to any arbitrary input $x(t)$ in terms of the impulse response of the system $h(t)$ using the following integral:

$$y(t) = (x * h)(t) = \int_{-\infty}^{\infty} x(\tau)h(t - \tau)d\tau. \quad (1)$$

This integral is called the convolution integral.

Pop Quiz 2.1: Check your understanding!

Using the convolution integral, show that you recover the impulse response $h(t)$ when the input is $\delta(t)$. As a consequence, you will have proven that the convolution of a signal (in this case, $h(t)$) with an impulse is equal to the same signal.

Solution on page 8

3 Time-domain system response

In this section, we discuss the response of systems in time-domain. We focus our discussion on linear systems and their responses. The overarching message about linear systems is the following: if you *know* how the system responds under a given condition or an input, then you can construct the system output if any linear combination of the known conditions occur. In other words, you can use the isolated system response to obtain the output to a new input that is a linear combination of the inputs for which you have the data already. This is called the *principle of superposition* (note that the above is only an informal description).

We often find it useful to talk about two kinds of system outputs: (1) the “natural” or the

characteristic output of the system when there are no forcing inputs, and (2) the output of the system to forced inputs. For linear systems, we can add these two outputs to get the full output of the system when both are present simultaneously.

3.1 Building intuition for a system's responses

Consider yourself — a student invested in learning new things — as a system. As you stroll past the lakes in and around the campus, you must have observed that the number of birds increases through late fall and winter and then thins from late spring into the hot, dry summer. Without anyone explicitly teaching you the ecology of bird movement, you self-learn and update your knowledge about bird movement as you observe these patterns and correlate them with the season. This is your natural response as a “system” that is invested in learning new things. Simultaneously, if you enroll in an ecology class as you expand your general education, you might be “forced” to learn (due to the pressure of exams!) that the Central Valley lies on the Pacific Flyway. Large flocks of geese, cranes, and ducks concentrate here from roughly October through February and by early summer many waterfowl have departed north to breeding grounds. This learning will be your response to the external input (the instruction in the ecology course). Your overall learning (if your learning progresses linearly) is the sum of your self-learned concepts and the concepts from the course. In this case, a nonlinear learner can have an advantage — one who accentuates their overall learning by synthesizing new (extra) knowledge by combining the natural (self-learning) and forced learning in innovative ways.

We conclude by writing the output of any general linear system as a combination of the natural/characteristic/initial condition response and the forced response. For a system with initial condition x_0 and an input $u(t)$, we write the output $y(t)$ as

$$y(t) = y_0(t) + y_{\text{forced}}(t)$$

where $y_0(t)$ is the initial condition response to initial condition x_0 . This is the characteristic response of the system without any forced inputs (the self-learning by seeing initial conditions, in the example above). Finally, $y_{\text{forced}}(t)$ is the forced response, that is, the output of the system when only the forced input $u(t)$ is present in isolation (the forced course-based learning, in the example above).

3.2 Example: Analyzing an RC circuit using convolution

Consider a series RC circuit shown in the diagram 1. Assume that we have an input voltage $u_{\text{in}}(t)$ that can be applied to the circuit using a function generator and the capacitor can have an initial voltage v_0 volts at time $t = 0$. We denote the output voltage for the circuit as

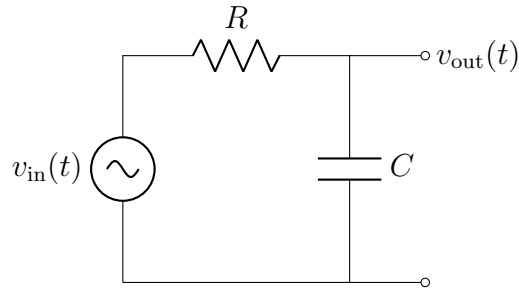


Figure 1: An RC circuit with input voltage $v_{\text{in}}(t)$ and output voltage $v_{\text{out}}(t)$.

the voltage across the capacitor $v_{\text{out}}(t)$. A typical analysis of such circuits uses differential equations to describe and compute the system response (recall pre-requisite #3 where you solved a differential equation to solve this circuit). Here, we will use convolution to find the output of the system to various common types of inputs:

- an impulse input at $t = 0$
- a step input voltage (modeling DC input)
- a sinusoidal voltage input (modeling AC input)
- a generalized complex exponential input signal

Pop Quiz 3.1: Check your understanding!

Before we jump into the application of convolution to the RC circuit example, it is important to ensure that the assumptions for the convolution integral to hold are still met. Your task is to state these assumptions (linearity and time-invariance) and prove that the RC circuit is linear and time-invariant. Additionally, also prove that the RC circuit is a causal system.

Solution on page 8

3.2.1 An impulse input to an RC circuit

An impulse at $t = 0$ is simply given by $v_{\text{in}}(t) = v_0\delta(t)$, where v_0 is the magnitude of the impulse (the area under the curve of this impulse is v_0). That is,

$$\int_{-\infty}^{\infty} v_{\text{in}}(t)dt = v_0.$$

From the pop quiz at the beginning of this lecture, you know that the output of the system (with zero initial conditions) to an impulse is just the impulse response. Since the system is linear (see pop quiz above), the output of the system to a scaled impulse $v_0\delta(t)$ will be equal to

$$y(t) = v_0 h(t)$$

where v_0 is the magnitude of the input impulse (the area under curve). To find the impulse response of the RC circuit, we will have to rely on our circuits knowledge — signal processing can only get us so far! From circuit theory, we know that an initial impulse on the circuit will cause a jump in the voltage and then an exponential decay (with a time constant of RC) through the resistor in the circuit. Full proof of this fact can be found in the solution of the pop-quiz below. We have the impulse response of an RC circuit (response to unit impulse)

$$h(t) = \frac{1}{RC} e^{-\frac{t}{RC}} u(t) \quad (4)$$

Therefore, the output to the scaled impulse is $y(t) = \frac{v_0}{RC} e^{-\frac{t}{RC}} u(t)$.

Pop Quiz 3.2: Check your understanding!

Prove that the impulse response of an RC circuit is given by equation (4).

Solution on page 9

3.2.2 A step input to an RC circuit

Let's compute the forced input response of the RC circuit for a scaled step input that models a DC voltage applied to the circuit $x(t) = v_{\text{DC}}u(t)$. By applying the convolution integral, we can compute the system output $y(t)$ as

$$y(t) = \int_{-\infty}^{\infty} v_{\text{DC}}u(\tau)h(t-\tau)d\tau$$

which can be evaluated as

$$y(t) = v_{\text{DC}} \int_0^t h(t-\tau)d\tau$$

since the step function is zero for $\tau < 0$ and $h(t-\tau)$ is zero for $\tau > t$ (causality of the real-life RC circuit's voltage response). To further understand this, you can see that the step input of the DC voltage is only applied at time $t = 0$. So, anything for negative time is 0 (**important note:** we must account for this by multiplying a $u(t)$ to the final output expression!). Similarly, you will see that the impulse response of the system will be zero for

any negative time. Therefore, we can limit the integration limits to 0 and t . Next, we can substitute the impulse response from equation (4) to get

$$y(t) = \frac{v_{\text{DC}}}{RC} \int_0^t e^{-\frac{t-\tau}{RC}} d\tau.$$

Evaluating this integral, we get

$$y(t) = v_{\text{DC}} \left(1 - e^{-\frac{t}{RC}}\right) u(t). \quad (5)$$

This is the forced response of the RC circuit to a step input voltage.

Pop Quiz 3.3: Check your understanding!

Verify the above equation from your circuit theory notes. Does it match up with the the output of an RC circuit when a DC voltage is applied as input?

Solution on page 10

3.2.3 A sinusoidal input to an RC circuit

We can compute the forced response of the RC circuit to a sinusoidal input voltage $x(t) = v_{\text{AC}} \cos(\omega t)u(t)$. Using the convolution integral, we can write

$$y(t) = \int_{-\infty}^{\infty} x(\tau)h(t-\tau)d\tau.$$

Substituting the expressions for $x(t)$ and $h(t)$, we get

$$y(t) = \int_0^t v_{\text{AC}} \cos(\omega\tau) \frac{1}{RC} e^{-\frac{t-\tau}{RC}} d\tau. \quad (6)$$

Evaluating this integral will give us the forced response of the RC circuit to the sinusoidal input. This is same as the pre-requisite #3 problem set! As you might remember, integrating the above requires a bit of effort as it is an integration by parts. Keep reading this section to learn a much easier way to do the same.

3.2.4 A generalized complex exponential signal input to an RC circuit

For a complex exponential signal, note that we are aiming for analysis of a broader variety of possible real signals. As we have seen before, complex exponentials can be used to define sinusoids, exponentials, and their combinations. By isolating the real and imaginary parts

as needed, we can get a large class of signals as a subset of the general complex exponential signal $x(t) = Ae^{st}$ where A and s are complex numbers. We can apply the convolution integral (1) to compute the output of the signal $y(t)$ to this input. As expected, the output will also be a complex signal and its special cases will lead to the computation of the output of the system for the input signal represented in that special case. For zero initial conditions, we write the convolution equation for this input as

$$y(t) = \int_0^t Ae^{s\tau} \frac{1}{RC} e^{-\frac{t-\tau}{RC}} d\tau = \frac{A}{RC} e^{-t/(RC)} \int_0^t e^{(s+\frac{1}{RC})\tau} d\tau.$$

Evaluating the integral,

$$y(t) = \frac{A}{RC} e^{-t/(RC)} \frac{e^{(s+\frac{1}{RC})t} - 1}{s + \frac{1}{RC}} = A \frac{e^{st} - e^{-t/(RC)}}{1 + sRC} u(t).$$

By further manipulating the above, we can see that it is made up of two parts:

$$y(t) = Ae^{st} \frac{1}{1 + sRC} u(t) - A \frac{e^{-t/(RC)}}{1 + sRC} u(t). \quad (7)$$

This is an interesting result due to many properties that we can observe from the output:

Observation 1: The system is linear. We observe the output that the output has the same “shape” as the input. Because the system is linear, the complex exponential input Ae^{st} reappears in the output multiplied by a constant factor $\frac{1}{1+sRC}$. That first term,

$$y_{\text{forced}}(t) = A \frac{e^{st}}{1 + sRC} u(t),$$

is the *forced (particular) response*. This is what you would derive by integrating the differential equation by parts! Here, we did the same but in two lines of algebra and a very simple integration instead — the power of exponentials!

Observation 2: The transient term decays to 0. The second term,

$$y_{\text{transient}}(t) = -A \frac{e^{-t/(RC)}}{1 + sRC} u(t),$$

is the *transient (natural) response*. It always decays like $e^{-t/(RC)}$, so for large t the output approaches the forced response, the transient part will disappear to 0 as $t \rightarrow \infty$.

Observation 3: As promised, the complex exponential is useful because it specializes to many other simple cases we derived individually above.

Special case 1: Unit step. Note that by setting $s = 0$, $A = v_{\text{DC}}$, we get

$$y(t) = v_{\text{DC}}(1 - e^{-t/(RC)})u(t),$$

which matches the step-response derived above in equation (5).

Special case 2: Real exponential. Although we did not derive this earlier, we can now easily compute the output of the RC circuit to an exponential input $x(t) = Ae^{\alpha t}$. For this, set $s = \alpha \in \mathbb{R}$, and choose A to be a real in the general form. Then, we have

$$y(t) = A \frac{e^{\alpha t} - e^{-t/(RC)}}{1 + \alpha RC} u(t).$$

Pop Quiz 3.4: Check your understanding!

Remind yourself and derive the sine signal from the complex exponential: Prove that a real input signal $x(t) = A_{AC} \sin(\omega t)$ can be obtained from the general complex exponential $x_c(t) = Ae^{st}$ by taking an appropriate real (or imaginary) part. In particular, show that $x(t)$ is the imaginary part of the general complex exponential for a suitable choice of A and s .

Solution on page 10

Special case 3: Sinusoidal input. With $s = j\omega$, A real (see pop quiz above), take the real part of

$$y(t) = A \frac{e^{j\omega t} - e^{-t/(RC)}}{1 + j\omega RC} u(t).$$

For large t , the transient dies out and the output is a sinusoid with scaled amplitude and a phase lag, consistent with the earlier sinusoidal case (see equation (6)). In fact, note that we did not derive the output in closed form earlier (due to fear of the ugly integration by parts!). Now we have the answer to the same input but obtained in a much easier way.

Observation 4: If the input grows ($\text{Re}\{s\} > 0$), the forced term grows accordingly; the RC remains stable (its transient decays), but a growing input produces a growing output.

Pop Quiz 3.5: Check your understanding!

Is the RC circuit bounded input bounded output stable?

Solution on page 10

4 Next class

In the next class, we will talk about an image processing example using convolution and will visualize convolution further.

Pop Quiz Solutions

Pop Quiz 2.1: Solution(s)

Substitute $x(t) = \delta(t)$ in equation (1) to write

$$y(t) = (x * h)(t) = \int_{-\infty}^{\infty} \delta(\tau) h(t - \tau) d\tau.$$

Since $\delta(\tau)$ is non-zero only when $\tau = 0$, we have

$$y(t) = h(t) \int_{-\infty}^{\infty} \delta(\tau) d\tau$$

with $h(t)$ out of the integral since it does not depend on τ (the integration variable). Notice that the integral is equal to 1 (definition of the impulse signal). So, we get the desired result $y(t) = h(t)$. Additionally, notice that $\delta(t) * x(t) = x(t)$ — holds true in general for any signal.

Pop Quiz 3.1: Solution(s)

Hints:

For linearity, prove that the principle of superposition holds for the system. Assume that for inputs u_1 and u_2 , the outputs are y_1 and y_2 . Then, write the system description using KVL (forward refer to the next pop quiz for a simple derivation of the following):

$$\dot{y}_1(t) + \frac{1}{RC} y_1(t) = \frac{1}{RC} u_1(t), \quad (8)$$

$$\dot{y}_2(t) + \frac{1}{RC} y_2(t) = \frac{1}{RC} u_2(t), \quad (9)$$

Now, for an input $k_1 u_1 + k_2 u_2$, find the output y^* and show that it is equal to $k_1 y_1 + k_2 y_2$ by using equations (8) and (9).

For time-invariance, consider one of the input-output pairs, say equation (8) and a time-shifted input $u_1(t - t_1)$. Prove that the output to the time-shifted input is the same as applying time-shift in the original output y_1 .

For causality, note that the impulse response (voltage output to an impulse) is zero for all negative time in a RC circuit. You will need to closed-form expression for the impulse response to show this formally.

Pop Quiz 3.2: Solution(s)

Start by writing the KVL for the series RC circuit. The input is the applied source voltage $v_{\text{in}}(t)$ and the output is the capacitor voltage $v_{\text{out}}(t)$. KVL gives

$$v_{\text{in}}(t) = v_R(t) + v_C(t) = R i(t) + v_{\text{out}}(t),$$

where $i(t)$ is the series current and

$$v_{\text{out}}(t) = \frac{1}{C} \int i(t) dt,$$

with the constant of integration set by the initial capacitor voltage. Differentiating v_{out} yields $i(t) = C \dot{v}_{\text{out}}(t)$. Substituting into KVL gives a first-order ODE in one variable:

$$\dot{v}_{\text{out}}(t) + \frac{1}{RC} v_{\text{out}}(t) = \frac{1}{RC} v_{\text{in}}(t).$$

The homogeneous (natural) solution for arbitrary initial condition $v_{\text{out}}(0^-) = v_0$ is

$$v_{\text{out}}(t) = v_0 e^{-t/(RC)}.$$

This is the *natural response* of the system due to the initial capacitor voltage.

To compute the *impulse response*, drive the circuit with a unit impulse input and set zero initial voltage:

$$v_{\text{in}}(t) = \delta(t), \quad v_{\text{out}}(0^-) = 0.$$

Using the ODE above,

$$\dot{v}_{\text{out}}(t) + \frac{1}{RC} v_{\text{out}}(t) = \frac{1}{RC} \delta(t).$$

Using the integrating factor method, you can write

$$\frac{d}{dt} (e^{t/(RC)} v_{\text{out}}(t)) = \frac{1}{RC} e^{t/(RC)} \delta(t).$$

Since the system is causal, $v_{\text{out}}(t) = 0$ for $t < 0$ and the initial voltage is zero, so $v_{\text{out}}(0^-) = 0$. Integrating from 0^- to $t > 0$ gives

$$e^{t/(RC)} v_{\text{out}}(t) - 0 = \frac{1}{RC} \int_{0^-}^t e^{\tau/(RC)} \delta(\tau) d\tau = \frac{1}{RC}.$$

Hence, for $t > 0$, the impulse response is

$$h(t) = v_{\text{out}}(t) = \frac{1}{RC} e^{-t/(RC)}.$$

For a general definition of the impulse response that holds for all time, we can include causality using the unit step $u(t)$ function as

$$h(t) = \frac{1}{RC} e^{-t/(RC)} u(t).$$

Note that the units of the impulse response are 1/seconds so that the convolution $(h * x)(t)$ has units of volts (the units of output signal — $v_{\text{out}}(t)$).

Pop Quiz 3.3: Solution(s)

You should work on finding your circuit theory (ENGR/EE 065) notes and make sure that you understand why the two output expressions match.

Pop Quiz 3.4: Solution(s)

For $s = j\omega$ and $A = A_{AC}$ and taking the imaginary part, we get

$$\text{Im}\{A_{AC}e^{j\omega t}\} = \text{Im}\{A_{AC}\cos(\omega t) + jA_{AC}\sin(\omega t)\} = A_{AC}\sin(\omega t).$$

where we used the Euler's identity $e^{j\omega t} = \cos(\omega t) + j\sin(\omega t)$ to expand the complex exponential. This is not the only way to obtain the sine function from the generalized complex exponential. An alternative is to set $s = j\omega$ and $A = -jA_{AC}$ and take the real part:

$$\begin{aligned}\text{Re}\{(-jA_{AC})e^{j\omega t}\} &= \text{Re}\{-jA_{AC}\cos(\omega t) - j^2A_{AC}\sin(\omega t)\} \\ &= \text{Re}\{-jA_{AC}\cos(\omega t) + A_{AC}\sin(\omega t)\}.\end{aligned}$$

The first term is purely imaginary, so its real part is 0, and the second term is real. Hence

$$\text{Re}\{(-jA_{AC})e^{j\omega t}\} = A_{AC}\sin(\omega t).$$

Pop Quiz 3.5: Solution(s)

For any bounded input $x(t)$, we have $|x(t)| < M$ for some finite M and all time t . The output is given by the convolution integral

$$y(t) = \int_{-\infty}^{\infty} x(\tau)h(t-\tau)d\tau.$$

Since $|x(\tau)| < M$, we can write

$$|y(t)| \leq \int_{-\infty}^{\infty} |x(\tau)||h(t-\tau)|d\tau < M \int_{-\infty}^{\infty} |h(t-\tau)|d\tau.$$

Since the impulse response of the RC circuit is given by equation (4), we can evaluate the integral to get

$$|y(t)| < M \int_0^{\infty} \frac{1}{RC} e^{-\frac{t-\tau}{RC}} d\tau = M.$$

Therefore, the output is bounded by M for all time t . Hence, the RC circuit is bounded input bounded output stable.

An alternative way is to start from equation (7) to show in a single step that $y(t)$ is bounded as long as the input Ae^{st} is bounded.