## 1 Fitness means and standard deviations

Table 1: Averages and standard deviations for Thirty-six benchmark problems with 100.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	1.93066E-6	0E0	0E0	0E0	4.63924E-9	0E0	3.38218E-6	4.3202E-4
$f_1$	$\pm 2.04174\text{E-}6$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 7.91031\text{E-}9$	$\pm 0 E0$	$\pm 4.15411\text{E-}6$	$\pm 3.76789\text{E}4$
$f_2$	-9.96098E-1	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-8.094E-1
J2	$\pm 6.86823$ E-3	$\pm 0E0$	$\pm 0E0$	±0E0	$\pm 3.92281$ E-7	$\pm 0E0$	$\pm 1.60367 E-9$	$\pm 1.649 \text{E-}1$
$f_3$	1.78454E-5	8.21455E-284	1.49378E-285	0E0	2.12395E-10	6.18242E-84	6.09334E-8	1.44255E-4
	±3.66086E-5	±0E0	±0E0	±0E0	±2.54804E-10	±1.54814E-83	±6.90648E-8	±1.54542E-4
$f_4$	0E0	0E0	0E0	0E0	9.69351E-7	0E0	4.56024E-8	6.28907E-1
	±0E0	±0E0	±0E0 0E0	±0E0 0E0	±1.53885E-6	±0E0 0E0	±8.36922E-8	±3.10524E-1
$f_5$	3.47188E-14 ±1.75E-13	0E0 ±0E0	±0E0	±0E0	7.66673E-9 ±9.22051E-9	±0E0	8.71627E-8 ±8.81188E-8	3.16944E-3 $\pm 2.62437E-3$
	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80054E0
$f_6$	±0E0	±0E0	±0E0	±0E0	±4.40662E-10	±0E0	±7.00796E-8	±8.05768E-4
	0E0	0E0	0E0	0E0	7.03141E-17	0E0	2.08775E-4	8.30756E-4
$f_7$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 2.87867 \text{E-}16$	$\pm 0 E0$	$\pm 5.41374\text{E4}$	$\pm 1.42424E-3$
	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03102E0
$f_8$	$\pm 1.10639 \text{E-}16$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 5.8919\text{E-}9$	$\pm 0E0$	$\pm 1.29547\text{E8}$	$\pm 6.43456 \text{E}4$
$f_9$	0E0	0E0	0E0	0E0	1.89663E-6	0E0	3.89669E-8	4.5356E-1
	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	±0E0	$\pm 3.09064$ E-6	$\pm 0E0$	$\pm 5.50056$ E-8	$\pm 2.19903$ E-1
$f_{10}$	1.44256E-6	0E0	0E0	0E0	2.40094E-6	0E0	4.31245E-6	3.59242E-1
	±2.16808E-6	±0E0	±0E0	±0E0	±2.52746E-6	±0E0	±4.50154E-6	±2.08713E-1
$f_{11}$	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86543E2
	±1.07732E-14 6.08171E-1	±1.69383E-14 0E0	±2.36164E-11 2.09853E-3	±2.02353E-14 5.91646E-33	±1.30768E-5 1.73839E-1	±2.32262E-14 3.74316E-3	±3.84458E-6 2.69272E-1	±2.13937E-1 1.50376E1
$f_{12}$	±5.03955E-1	±0E0	±4.99115E-3	±3.24058E-32	±1.39158E-1	±5.29167E-3	±1.46728E-1	±7.5733E0
	-4.68766E0	-4.68487E0	-4.68627E0	-4.53989E0	-4.67231E0	-4.55567E0	-4.68343E0	-3.70998E0
$f_{13}$	±1.62158E-16	±1.05956E-2	±7.62481E-3	±1.85262E-1	±1.22212E-2	±3.06727E-1	±1.27407E-2	±1.91807E-1
	2.98001E2	5.12453E-19	5.86293E1	4.24214E-24	1.3874E2	3.18773E2	1.36442E0	3.40161E2
$f_{14}$	$\pm 4.03708 E1$	$\pm 2.54234$ E-18	$\pm 1.91011E1$	$\pm 2.32351$ E-23	$\pm 1.88427E1$	$\pm 1.09242E2$	$\pm 2.29904$ E-1	$\pm 4.75691E1$
	-9.66015E0	-9.66015E0	-9.46735E0	-7.65611E0	-8.56808E0	-8.2148E0	-9.46201E0	-5.44624E0
$f_{15}$	$\pm 3.48994\text{E-}12$	$\pm 6.73326 \text{E-}16$	$\pm 1.53716\text{E-}1$	$\pm 6.61462\text{E}1$	$\pm 2.4341\text{E-}1$	$\pm 7.81092\text{E-}1$	$\pm 1.16853\text{E-}1$	$\pm 3.03607 \text{E-}1$
$f_{16}$	0E0	0E0	2.33333E-1	0E0	4.87307E3	1.35517E3	0E0	-1.33357E3
J 16	±0E0	±0E0	$\pm 5.04007$ E-1	±0E0	$\pm 7.61852E2$	$\pm 3.45383E3$	±0E0	±7.03899E1
$f_{17}$	4.25068E-16	5.25187E-62	1.16956E-21	4.37117E-172	4.80514E3	6.74637E2	3.95531E-1	3.69277E4
	±8.66061E-17	$\pm 2.87574$ E-61	±1.64724E-21	±0E0	$\pm 8.27391E2$	$\pm 2.53624E3$	±5.79905E-2	±2.29885E3
$f_{18}$	3.97096E-16	7.97742E-62	1.25033E-22	1.29293E-172	6.11961E2	6.30588E2	5.08604E0	4.77875E3
•	±6.3762E-17 1.24185E-16	±4.36932E-61 8.5529E-79	±1.60361E-22 1.04503E-32	±0E0 1.9E-322	±6.90504E1 1.11257E0	±4.82844E2 3.13431E0	±6.73829E-1 2.27713E-1	±4.19816E2 3.52315E1
$f_{19}$	±2.9789E-17	±4.67061E-78	±3.1168E-32	±0E0	±3.20809E-1	±5.37156E0	±4.59572E-2	±5.6683E0
	6.87922E-14	1.00459E-11	3.17077E-12	2.71856E-85	4.71283E16	1.68509E6	2.27784E0	6.35575E34
$f_{20}$	±2.86633E-14	±5.52611E-12	±7.03593E-12	±7.6679E-85	$\pm 1.43937E17$	±9.22494E6	±1.78263E-1	$\pm 2.06719E35$
	8.36169E-24	0E0	0E0	0E0	6.81741E-20	1.70909E-135	2.56726E-10	1.51232E-6
$f_{21}$	$\pm 1.34414 E-23$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.17765 E-19$	$\pm 9.25867\text{E-}135$	$\pm 4.66692 \text{E-}10$	$\pm 2.12431 \text{E-}6$
f	4.38082E-1	7.97325E-1	2.18596E1	2.88284E1	2.02695E4	1.107E5	1.15746E2	3.3034E5
$f_{22}$	$\pm 4.96995$ E-1	$\pm 1.62191 E0$	$\pm 2.99135 E1$	$\pm 8.15531\text{E-}2$	$\pm 5.10706 E3$	$\pm 5.66658 \text{E}4$	$\pm 4.28929 E1$	$\pm 6.89751 E4$
$f_{23}$	3.10407E-2	6.66667E-1	6.78789E-1	7.17169E-1	1.71332E4	2.4162E4	8.21049E0	5.08544E5
	±1.22118E-1	±5.11961E-17	±6.63947E-2	±5.55783E-2	±6.36219E3	±5.25871E4	±1.25124E0	±1.16568E5
$f_{24}$	2.84217E-14	0E0	3.22808E1	0E0	1.63405E2	1.70014E2	7.66338E1	3.21309E2
	±3.57956E-14	±0E0	±1.4253E1	±0E0 6.77319E-4	±1.19914E1	±2.69807E1 7.06348E0	±6.72321E0	±1.47593E1 3.25851E2
$f_{25}$	2.46547E-4 ±1.35038E-3	2.46535E-4 ±1.35033E-3	5.73635E-3 ±1.1988E-2	±2.63939E-3	4.14885E1 ±6.14688E0	±2.28215E1	6.20956E-2 ±4.39821E-2	±3.13196E1
-	5.74563E-13	7.07582E-15	6.71176E-12	4.82577E-15	1.29845E1	7.36842E0	9.49081E-1	1.95868E1
$f_{26}$	±2.48402E-13	±1.22834E-15	±3.20046E-12	±1.52832E-15	±6.24893E-1	±7.41812E0	±1.10908E-1	±2.03434E-1
	-1E0	-1E0	-1E0	-1E0	-9.99998E-1	-1E0	-1E0	-9.91309E-1
$f_{27}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 3.7335\text{E-}6$	$\pm 0E0$	$\pm 1.01113\text{E7}$	$\pm 6.75669 E-3$
$f_{28}$	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.86048E0
J 28	$\pm 2.23824$ E-16	$\pm 0E0$	$\pm 0E0$	$\pm 8.10792\text{E-}17$	$\pm 2.54075\text{E7}$	$\pm 1.99961$ E-3	$\pm 5.26305 \text{E-}7$	$\pm 1.35788 E-3$
$f_{29}$	-3.322E0	-3.27444E0	-3.32152E0	-3.2674E0	-3.31895E0	-3.24097E0	-3.29025E0	-3.14662E0
	±1.80672E-16	±5.92412E-2	±1.68979E-3	±6.03808E-2	±2.16462E-3	±8.31124E-2	$\pm 5.34576$ E-2	±5.14792E-2
$f_{30}$	-1.01532E1	-1.01532E1	-5.40418E0	-9.98327E0	-1.00778E1	-6.13908E0	-5.49734E0	-5.0924E0
	±5.42758E-10	±0E0	±3.47842E0	±9.30764E-1	±6.77304E-2	±3.2573E0	±3.62976E0	±1.59579E0
$f_{31}$	-1.04029E1	-1.04029E1	-8.68484E0	-1.02258E1	-1.03504E1	-9.87278E0	-6.17013E0	-5.12734E0
	±1.05177E-15 -1.05363E1	±4.50676E-16 -1.05364E1	±3.13807E0 -9.25887E0	±9.70431E-1 -1.00426E1	±3.72024E-2 -1.04547E1	±1.61767E0 -9.99875E0	±3.77567E0 -7.74608E0	±1.09667E0 -5.86498E0
$f_{32}$	±4.89476E-4	±4.50676E-16	±2.90551E0	±1.88857E0	±8.85826E-2	±1.64057E0	±3.75215E0	±1.57968E0
	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.98263E-1
$f_{33}$	±0E0	±0E0	±0E0	±0E0	±6.39677E-8	±0E0	±5.24961E-8	±3.02924E-4
	3.00018E0	3E0	3E0	3E0	3E0	3E0	3E0	3.02194E0
$f_{34}$	$\pm 5.43727 \text{E-}4$	±0E0	±0E0	±0E0	$\pm 2.79371$ E-8	$\pm 2.53729$ E-16	$\pm 1.01899 E-6$	$\pm 2.13025 E-2$
f	8.90008E-2	9.98733E-2	9.98733E-2	9.65442E-2	2.08174E-1	9.98733E-2	9.72778E-2	1.80472E0
$f_{35}$	$\pm 2.9892\text{E-}2$	$\pm 3.98632\text{E-}12$	$\pm 4.93967\text{E-}10$	$\pm 1.82343\text{E-}2$	$\pm 6.85168\text{E}2$	$\pm 4.05396\text{E-}17$	$\pm 1.14383\text{E-}2$	$\pm 3.0891$ E-1
$f_{36}$	1.03207E-1	9.98733E-2	9.98733E-2	9.98733E-2	3.47202E-1	9.98733E-2	9.98733E-2	2.70515E0
	$\pm 1.82573$ E-2	$\pm 1.33691$ E-11	$\pm 3.68435 \text{E-}10$	±0E0	$\pm 6.73784$ E-2	$\pm 2.53373$ E-18	$\pm 1.07525$ E-9	±4.23084E-1

Table 2: Averages and standard deviations for Thirty-six benchmark problems with 300.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA 5 67071E 7	RW
$f_1$	3.99982E-7 ±3.7913E-7	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	1.36961E-24 ±2.72685E-24	0E0 ±0E0	5.67871E-7 ±5.23808E-7	1.55321E-4 ±1.55424E-4
	-9.99829E-1	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.35472E-1
$f_2$	$\pm 3.29757\text{E4}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 3.62077\text{E-}10$	$\pm 6.56479\text{E-}2$
$f_3$	2.32442E-6	0E0	0E0	0E0	5.82924E-26	3.92286E-228	6.50398E-9	4.51734E-5
	±3.01421E-6	±0E0	±0E0	±0E0	±1.19665E-25	±0E0	±5.80521E-9	±3.84524E-5
$f_4$	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	3.85988E-9 ±7.20176E-9	3.67644E-1 $\pm 1.60588E-1$
	6.62291E-17	0E0	0E0	0E0	1.54536E-24	0E0	1.07842E-8	1.5957E-3
$f_5$	$\pm 1.60415 E-16$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 2.61028$ E-24	$\pm 0 E0$	$\pm 1.24631 \text{E-8}$	$\pm 1.91743 E-3$
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80109E0
76	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±4.08063E-9	±2.19177E-4
$f_7$	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	1.56582E-4 ±4.77775E-4	1.1057E-5 $\pm 2.67924E-5$
	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03137E0
$f_8$	$\pm 9.03362 \text{E-}17$	±0E0	±0E0	±0E0	±0E0	±0E0	±8.97948E-10	±3.04713E-4
$f_9$	0E0	0E0	0E0	0E0	0E0	0E0	3.67969E-9	2.65166E-1
79	$\pm 0E0$	$\pm 0 E0$	$\pm 0E0$	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 5.13211$ E-9	$\pm 1.36825 \text{E-}1$
$f_{10}$	1.85049E-7	0E0	0E0	0E0	0E0	0E0	6.48471E-7	1.99746E-1
	±3.30486E-7 -1.86731E2	±0E0 -1.86731E2	±0E0 -1.86731E2	±0E0 -1.86731E2	±0E0 -1.86731E2	±0E0 -1.86731E2	±6.82699E-7 -1.86731E2	±1.05806E-1 -1.8668E2
$f_{11}$	±8.67228E-15	±1.44216E-14	±1.38623E-13	±2.41666E-14	±9.09045E-15	±2.28026E-14	±4.1998E-7	±5.46608E-2
	2.07915E-1	0E0	2.04631E-6	0E0	1.40138E-5	1.40795E-5	1.26444E-1	7.69736E0
$f_{12}$	$\pm 1.64254\text{E-}1$	$\pm 0 E0$	$\pm 6.23962\text{E-}6$	$\pm 0 E0$	$\pm 1.72911\text{E}5$	$\pm 2.25785\text{E}5$	$\pm 6.34545\text{E-}2$	$\pm 3.77093 E0$
$f_{13}$	-4.68766E0	-4.68487E0	-4.68627E0	-4.54212E0	-4.68766E0	-4.55567E0	-4.68626E0	-3.91429E0
- 10	±0E0	±1.05956E-2	±7.62481E-3	±1.84967E-1	±9.3829E-9	±3.06727E-1	±7.62326E-3	±2.1283E-1
$f_{14}$	2.36423E2 ±3.46835E1	1.1559E-64 ±6.26083E-64	1.19248E-1 ±3.01178E-1	1.05323E-92 ±5.76878E-92	1.31434E1 ±2.25446E0	2.60163E2 ±1.15912E2	7.77258E-1 ±6.99363E-2	3.01749E2 $\pm 3.85487E1$
	-9.66015E0	-9.66015E0	-9.49268E0	-7.75107E0	-9.62469E0	-8.24895E0	-9.58014E0	-5.66686E0
$f_{15}$	$\pm 4.50676$ E-16	$\pm 9.03362 \text{E-}16$	$\pm 1.21362 \text{E-}1$	$\pm 6.44443$ E-1	$\pm 2.10653$ E-2	$\pm 7.94128$ E-1	$\pm 9.34006 E-2$	$\pm 3.30664$ E-1
$f_{16}$	0E0	0E0	2.33333E-1	0E0	4.14667E1	1.33353E3	0E0	-1.40583E3
710	$\pm 0E0$	$\pm 0E0$	$\pm 5.04007 \text{E-}1$	±0E0	$\pm 8.04613 E0$	$\pm 3.45738E3$	$\pm 0E0$	±5.51431E1
$f_{17}$	3.56707E-16	3.05219E-120	5.6155E-72	0E0	4.02873E1	6.66667E2	2.9912E-1	3.43173E4
	±5.38706E-17 3.35281E-16	±1.67175E-119 6.49564E-117	±1.20372E-71 6.64927E-73	±0E0 0E0	±7.02861E0 5.5732E0	±2.53708E3 6.16668E2	±4.15172E-2 3.6756E0	±2.35903E3 4.50412E3
$f_{18}$	±6.5218E-17	±3.55781E-116	±1.58266E-72	±0E0	±9.90095E-1	±4.82152E2	±4.82832E-1	±3.8079E2
$f_{19}$	8.99847E-17	8.28629E-175	4.72655E-99	0E0	4.13217E-4	3.13175E0	1.37735E-1	3.10545E1
J 19	$\pm 2.44415$ E-17	±0E0	$\pm 2.35818$ E-98	±0E0	$\pm 1.57899E-4$	$\pm 5.37256 E0$	$\pm 2.75808$ E-2	$\pm 4.70714E0$
$f_{20}$	1.03004E-15	5.46424E-40	5.22055E-44	1.53431E-262	1.11181E1	7.3E2	1.95738E0	2.81787E33
	±7.56065E-17 4.56893E-25	±3.95141E-40 0E0	±8.21984E-44 0E0	±0E0 0E0	±1.39741E0 3.06603E-55	±2.38023E2 0E0	±1.35165E-1 1.50802E-11	±4.01109E33 2.20997E-7
$f_{21}$	±7.95014E-25	±0E0	±0E0	±0E0	±8.18127E-55	±0E0	±1.98253E-11	±3.17551E-7
f	1.35624E-1	7.97325E-1	7.83541E0	2.88195E1	2.36257E2	1.10567E5	9.7731E1	2.80822E5
$f_{22}$	$\pm 2.58484$ E-1	$\pm 1.62191E0$	$\pm 1.81267 E1$	$\pm 1.01234$ E-1	$\pm 2.67507 E1$	$\pm 5.67114 E4$	$\pm 3.88941E1$	$\pm 6.37775 E4$
$f_{23}$	2.66725E-5	6.66667E-1	6.66667E-1	7.17149E-1	1.94138E1	2.41289E4	5.84928E0	4.36214E5
	±1.16173E-4 0E0	±2.02698E-17 0E0	±8.55018E-17 2.8632E1	±5.55727E-2 0E0	±4.40509E0 3.98923E1	±5.25973E4 1.25986E2	±6.80568E-1 6.24846E1	±8.65189E4 3.07004E2
$f_{24}$	±0E0	±0E0	±8.56603E0	±0E0	±3.29471E0	±2.9307E1	±5.6042E0	±1.22535E1
f	0E0	2.46535E-4	5.73635E-3	0E0	1.34304E0	6.04438E0	5.1516E-2	3.10267E2
$f_{25}$	$\pm 0 E0$	$\pm 1.35033$ E-3	$\pm 1.1988 E-2$	$\pm 0 E0$	$\pm 5.93258\text{E-}2$	$\pm 2.29166 E1$	$\pm 3.91987 E-2$	$\pm 2.34269 E1$
$f_{26}$	3.12343E-14	5.89158E-15	8.73375E-15	4.4705E-15	2.97502E0	5.71837E0	7.78557E-1	1.94165E1
	±2.85033E-15 -1E0	±1.8027E-15	±1.7034E-15	±1.22834E-15 -1E0	±1.62549E-1 -1E0	±8.38013E0 -1E0	±6.14936E-2 -1E0	±1.93924E-1 -9.97299E-1
$f_{27}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±7.12525E-9	±2.92377E-3
f	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.8617E0
$f_{28}$	$\pm 1.12669 \text{E-}16$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 2.17663\text{E-}16$	$\pm 1.99961\text{E-}3$	$\pm 6.72241\text{E8}$	$\pm 7.00984 E-4$
$f_{29}$	-3.322E0	-3.27444E0	-3.32163E0	-3.26794E0	-3.322E0	-3.24097E0	-3.29029E0	-3.19885E0
- 20	±0E0	±5.92412E-2	±1.31857E-3	±6.06186E-2	±1.39651E-8	±8.31124E-2	±5.34746E-2	±4.389E-2
$f_{30}$	-1.01532E1 ±7.35129E-16	-1.01532E1 ±0E0	-5.51592E0 ±3.52191E0	-9.98327E0 ±9.30764E-1	-1.01532E1 ±7.64847E-9	-6.71945E0 ±3.18774E0	-5.49734E0 ±3.62977E0	-6.3402E0 ±1.42299E0
	-1.04029E1	-1.04029E1	-9.01242E0	-1.02258E1	-1.04029E1	-9.87279E0	-6.17013E0	-6.42573E0
$f_{31}$	$\pm 8.7065 \text{E-}16$	±0E0	$\pm 2.91642 E0$	$\pm 9.70431$ E-1	$\pm 9.25563 E-9$	$\pm 1.61767 E0$	$\pm 3.77568 E0$	$\pm 1.30211E0$
f22	-1.05364E1	-1.05364E1	-9.25887E0	-1.00426E1	-1.05364E1	-1.01775E1	-7.74608E0	-6.43344E0
$f_{32}$	$\pm 1.29307 \text{E-}15$	$\pm 7.98963$ E-16	$\pm 2.90551 E0$	$\pm 1.88857 E0$	$\pm 2.75985$ E-8	$\pm 1.36607 E0$	$\pm 3.75216 E0$	$\pm 1.39411E0$
$f_{33}$	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.98028E-1
	±0E0 3E0	±0E0 3E0	±0E0 3E0	±0E0 3E0	±0E0 3E0	±0E0 3E0	±3.37E-9 3E0	±9.54573E-5 3.00553E0
$f_{34}$	±4.62024E-8	±0E0	±0E0	±0E0	±0E0	±0E0	±1.48134E-7	±5.88191E-3
	6.70083E-2	9.65442E-2	9.6847E-2	9.65442E-2	9.98733E-2	8.98861E-2	9.08783E-2	1.46475E0
$f_{35}$	$\pm 4.40701\text{E}2$	$\pm 1.82343$ E-2	$\pm 1.16924\text{E-}2$	$\pm 1.82343$ E-2	$\pm 1.66049$ E-11	$\pm 3.0474\text{E-}2$	$\pm 1.93192 \text{E-}2$	$\pm 2.87226 \text{E-}1$
$f_{36}$	9.34579E-2	9.98733E-2	9.98733E-2	9.98733E-2	9.69507E-2	9.98733E-2	9.96566E-2	2.13105E0
	±2.4415E-2	±9.38958E-13	±2.26709E-11	±0E0	±1.60081E-2	±2.53373E-18	±8.78494E-4	±4.41078E-1

Table 3: Averages and standard deviations for Thirty-six benchmark problems with 500.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	2.80884E-7	0E0	0E0	0E0	0E0	0E0	2.48291E-7	9.06951E-5
$f_1$	±3.35781E-7	±0E0	±0E0	±0E0	±0E0	±0E0	±1.99756E-7	±7.80528E-5
$f_2$	-9.99952E-1	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.56848E-1
	$\pm 1.35715E-4$	±0E0	±0E0	$\pm 0E0$	±0E0	±0E0	$\pm 1.2547E-10$	$\pm 3.78807E-2$
f-	1.34138E-6	0E0	0E0	0E0	1.35021E-41	0E0	2.55216E-9	2.78494E-5
$f_3$	$\pm 2.31447 E-6$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.68859 \text{E-}41$	$\pm 0E0$	$\pm 2.35122 \text{E-}9$	$\pm 2.73274 \text{E}5$
	0E0	0E0	0E0	0E0	0E0	0E0	1.54115E-9	3.18495E-1
$f_4$	$\pm 0E0$	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.9323E-9$	$\pm 1.78524$ E-1
	2.99662E-17	0E0	0E0	0E0	0E0	0E0	4.7417E-9	6.94096E-4
$f_5$								
	±4.62482E-17	±0E0	±0E0	±0E0	±0E0	±0E0	±5.72791E-9	±5.08044E-4
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80118E0
	±0E0	±0E0	±0E0	±0E0	$\pm 0E0$	±0E0	$\pm 3.43725 E-9$	$\pm 1.18125 E-4$
$f_7$	0E0	0E0	0E0	0E0	0E0	0E0	0E0	4.73094E-6
37	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.182 E-5$
	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03148E0
$f_8$	$\pm 5.63345 E-17$	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 4.33564$ E-10	$\pm 2.0744$ E-4
-	0E0	0E0	0E0	0E0	0E0	0E0	1.15721E-9	2.06366E-1
$f_9$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±1.5563E-9	±1.03374E-1
$f_{10}$	1.0229E-7	0E0	0E0	0E0	0E0	0E0	1.91495E-7	1.3892E-1
	$\pm 1.73501$ E-7	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.45811$ E-7	$\pm 8.6492 E-2$
$f_{11}$	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86701E2
J11	$\pm 1.1563$ E-14	$\pm 1.44216$ E-14	$\pm 1.29856$ E-13	$\pm 2.20575$ E-14	$\pm 1.31062\text{E-}14$	$\pm 2.76601$ E-14	$\pm 1.85313E-7$	$\pm 3.30055 E-2$
	1.8472E-1	0E0	5.86311E-8	0E0	2.83471E-10	7.65191E-8	8.53743E-2	6.28079E0
$f_{12}$	$\pm 1.44512 E-1$	±0E0	$\pm 3.1706$ E-7	$\pm 0E0$	$\pm 3.38781$ E-10	$\pm 1.17241 \text{E-}7$	$\pm 4.23166$ E-2	$\pm 2.6539 E0$
	-4.68766E0	-4.68487E0	-4.68627E0	-4.54226E0	-4.68766E0	-4.55567E0	-4.68766E0	-4.03641E0
$f_{13}$	±1.62158E-16	±1.05956E-2	±7.62481E-3	±1.84937E-1	±8.643E-15	±3.06727E-1	±5.18263E-6	±1.92063E-1
	2.06648E2	3.22496E-113	1.62471E-6	7.73306E-184	1.18133E0	2.50684E2	6.4082E-1	2.89252E2
$f_{14}$								
	±3.40646E1	±1.21168E-112	$\pm 3.59209 E-6$	±0E0	$\pm 2.67873$ E-1	±1.19983E2	$\pm 8.28264$ E-2	±3.12786E1
$f_{15}$	-9.66015E0	-9.66015E0	-9.49616E0	-7.88266E0	-9.63996E0	-8.26123E0	-9.60221E0	-5.78341E0
J15	$\pm 6.73326$ E-16	$\pm 7.98963$ E-16	$\pm 1.18847E-1$	$\pm 6.24721$ E-1	$\pm 2.18664$ E-2	$\pm 7.90216$ E-1	$\pm 8.79466$ E-2	$\pm 2.89081$ E-1
	0E0	0E0	2.33333E-1	0E0	0E0	1.33333E3	0E0	-1.44567E3
$f_{16}$	$\pm 0E0$	$\pm 0E0$	$\pm 5.04007 \text{E-}1$	$\pm 0E0$	$\pm 0E0$	$\pm 3.45746E3$	$\pm 0E0$	$\pm 5.9479 E1$
	3.37925E-16	8.44744E-176	3.67237E-122	0E0	4.63596E-1	6.66667E2	2.65892E-1	3.26057E4
$f_{17}$	±5.32868E-17	±0E0	±1.08591E-121	±0E0	±9.55689E-2	±2.53708E3	±3.13303E-2	±2.39624E3
	3.06168E-16	2.39188E-170				6.16667E2		
$f_{18}$			1.04711E-123	0E0	5.72763E-2		3.33205E0	4.39887E3
	±5.53599E-17	±0E0	±3.77003E-123	±0E0	±1.43182E-2	±4.82153E2	±3.45142E-1	$\pm 3.20973E2$
$f_{19}$	7.57925E-17	1.88256E-268	1.15292E-163	0E0	3.07961E-7	3.13175E0	1.10588E-1	2.97459E1
J19	$\pm 1.78395$ E-17	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.11456$ E-7	$\pm 5.37256 E0$	$\pm 2.16045$ E-2	$\pm 4.80876 E0$
f	1.02473E-15	2.39322E-68	1.51444E-75	2.5654E-319	7.05393E-1	7.3E2	1.79798E0	1.71977E33
$f_{20}$	$\pm 7.11435$ E-17	$\pm 1.93759 E-68$	$\pm 2.72074 E-75$	$\pm 0E0$	$\pm 7.04322 E-2$	$\pm 2.38023E2$	$\pm 1.17346$ E-1	$\pm 3.15681E33$
	2.12993E-25	0E0	0E0	0E0	1.27732E-90	0E0	7.12375E-12	1.1227E-7
$f_{21}$	±3.2404E-25	±0E0	±0E0	±0E0	±2.574E-90	±0E0	±1.18642E-11	±2.02115E-7
	1.08121E-1	7.97325E-1	2.26261E0	2.88171E1	9.64095E1	1.1056E5	9.08744E1	2.68021E5
$f_{22}$								
	±1.87387E-1	±1.62191E0	±3.92976E0	±1.03006E-1	±2.26221E1	±5.67132E4	±3.78164E1	±5.40261E4
$f_{23}$	2.40513E-7	6.66667E-1	6.66667E-1	7.17149E-1	1.91284E0	2.41282E4	5.0026E0	4.16953E5
	±8.30419E-7	±2.02698E-17	±6.06928E-17	$\pm 5.55727$ E-2	±7.54942E-1	$\pm 5.25973E4$	$\pm 6.0732 \text{E-}1$	$\pm 8.75889E4$
$f_{24}$	0E0	0E0	2.76861E1	0E0	1.03951E1	1.11232E2	5.76929E1	3.02179E2
J24	$\pm 0E0$	$\pm 0E0$	$\pm 7.73535E0$	$\pm 0E0$	$\pm 2.48218E0$	$\pm 3.04576 E1$	$\pm 6.11872E0$	$\pm 1.08895 E1$
	0E0	2.46535E-4	5.73635E-3	0E0	5.11957E-1	6.04112E0	4.87796E-2	2.98117E2
$f_{25}$	$\pm 0E0$	$\pm 1.35033$ E-3	$\pm 1.1988$ E-2	$\pm 0 E0$	$\pm 7.03374 E-2$	$\pm 2.29175 E1$	$\pm 3.80065 E-2$	$\pm 2.37493E1$
	3.005E-14	5.29946E-15	7.54952E-15	4.35207E-15	1.6336E-1	5.69108E0	7.01274E-1	1.93562E1
$f_{26}$	±2.52654E-15	±1.7413E-15	±1.61598E-15	±1.08403E-15	±2.10016E-2	±8.36028E0	±7.11575E-2	
		-1E0		-1E0	-1E0	-1E0	-1E0	±1.8776E-1
$f_{27}$	-1E0		-1E0					-9.98419E-1
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±1.60252E-9	±1.26607E-3
$f_{28}$	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.86201E0
3 20	$\pm 8.10792 \text{E-}17$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.99961 E-3$	$\pm 2.33731\text{E8}$	$\pm 4.80966 \text{E}4$
	-3.322E0	-3.27444E0	-3.32168E0	-3.26823E0	-3.322E0	-3.24097E0	-3.29029E0	-3.21536E0
$f_{29}$	$\pm 0E0$	$\pm 5.92412 E-2$	$\pm 1.2057 E-3$	$\pm 6.08649 E-2$	$\pm 1.61637 E-13$	$\pm 8.31124 E-2$	$\pm 5.34755 E-2$	$\pm 4.06683$ E-2
	-1.01532E1	-1.01532E1	-5.51592E0	-9.98327E0	-1.01532E1	-6.71945E0	-5.49734E0	-6.8551E0
$f_{30}$	±4.50676E-16	±0E0	±3.52191E0	±9.30764E-1	±9.78526E-16	±3.18774E0	±3.62977E0	±1.22835E0
	-1.04029E1	-1.04029E1		-1.02258E1	-1.04029E1			-6.93948E0
$f_{31}$			-9.04433E0			-9.87279E0	-6.17013E0	
	±7.64159E-16	±0E0	±2.89816E0	±9.70431E-1	±1.59793E-15	±1.61767E0	±3.77568E0	±1.35682E0
$f_{32}$	-1.05364E1	-1.05364E1	-9.25887E0	-1.00426E1	-1.05364E1	-1.01775E1	-7.74608E0	-7.02982E0
132	$\pm 8.60173 \text{E-}16$	$\pm 8.95296 \text{E-}16$	$\pm 2.90551 E0$	$\pm 1.88857 E0$	$\pm 1.03614\text{E-}15$	$\pm 1.36607 E0$	$\pm 3.75216 E0$	$\pm 1.2095 E0$
-	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97983E-1
$f_{33}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 5.52687$ E-10	$\pm 8.47094 E-5$
	3E0	3E0	3E0	3E0	3E0	3E0	3E0	3.00362E0
$f_{34}$	±2.14299E-9							
		±0E0	±0E0	±0E0	±0E0	±0E0	±3.17726E-8	±3.82281E-3
$f_{35}$	4.74686E-2	9.65442E-2	9.16499E-2	9.32151E-2	9.68797E-2	8.9886E-2	8.22912E-2	1.30435E0
	$\pm 4.44608E-2$	$\pm 1.82343$ E-2	$\pm 2.27575$ E-2	$\pm 2.53387$ E-2	$\pm 1.56472 E-2$	$\pm 3.04742 E-2$	$\pm 2.67134$ E-2	±2.70263E-1
$f_{2e}$	9.06155E-2	9.98733E-2	9.98733E-2	9.98733E-2	9.67609E-2	9.98733E-2	9.96566E-2	1.97406E0
$f_{36}$	$\pm 2.82973\text{E}2$	$\pm 9.38958 \text{E-}13$	$\pm 1.49272\text{E-}11$	$\pm 0E0$	$\pm 1.70476\text{E}2$	$\pm 2.53373 \text{E-}18$	$\pm 8.78494\text{E4}$	$\pm 4.10539\text{E1}$

Table 4: Averages and standard deviations for Thirty-six benchmark problems with 2.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
$f_1$	1.93056E-6	0E0	0E0	0E0	0E0	0E0	4.20804E-4	2.78964E-2
	±2.04184E-6 -9.96209E-1	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±4.72581E-4 -4.77167E-1	±2.56014E-2 -7.46811E-2
$f_2$	±6.90499E-3	±0E0	±0E0	±0E0	±0E0	±0E0	±4.9652E-1	±1.93322E-1
	1.78334E-5	2.91057E-284	2.44251E-286	0E0	1.25542E-80	6.17397E-84	1.85858E-4	7.31256E-3
$f_3$	$\pm 3.66134\text{E}5$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.54219\text{E-}80$	$\pm 1.54846\text{E}83$	$\pm 7.39723\text{E4}$	$\pm 7.1915\text{E3}$
$f_4$	0E0	0E0	0E0	0E0	0E0	0E0	1.51672E-1	1.26167E1
J4	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±8.23211E-1	$\pm 1.58045E1$
$f_5$	3.47188E-14	0E0	0E0	0E0	0E0	0E0	1.89976E-4	1.98901E-1
	±1.75E-13 -1.8013E0	±0E0 -1.8013E0	±0E0 -1.8013E0	±0E0 -1.8013E0	±0E0 -1.8013E0	±0E0 -1.8013E0	±2.72772E-4 -1.80096E0	±1.85782E-1 -1.75298E0
$f_6$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±5.21598E-4	±3.58716E-2
	0E0	0E0	0E0	0E0	0E0	0E0	1.41678E-1	1.70678E-1
$f_7$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±1.7011E-1	±1.02395E-1
£	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03157E0	-9.80211E-1
$f_8$	$\pm 1.10639 \text{E-}16$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 6.77912\text{E}5$	$\pm 4.34183\text{E}2$
$f_9$	0E0	0E0	0E0	0E0	0E0	0E0	6.11899E-1	1.33411E1
79	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.69377 E0$	$\pm 1.30562 E1$
$f_{10}$	1.44256E-6	0E0	0E0	0E0	0E0	0E0	5.94978E-3	1.14142E1
	±2.16808E-6	±0E0	±0E0	±0E0	±0E0	±0E0	±2.50011E-2	±9.55429E0
$f_{11}$	-1.86731E2 ±1.07732E-14	-1.86731E2 ±1.69383E-14	-1.86731E2 ±2.36164E-11	-1.86731E2 ±2.13081E-14	-1.86731E2 ±1.22265E-14	-1.86731E2 ±2.32262E-14	-1.86706E2 ±2.79093E-2	-1.76831E2 ±1.31343E1
	6.08171E-1	0E0	2.0903E-3	0E0	3.07563E-22	3.73226E-3	6.9376E0	1.45099E2
$f_{12}$	±5.03955E-1	±0E0	±4.97352E-3	±0E0	±7.93029E-22	±5.29465E-3	±1.26627E1	±1.0607E2
	-4.68766E0	-4.68487E0	-4.68627E0	-4.54054E0	-4.68766E0	-4.55567E0	-4.5328E0	-2.90477E0
$f_{13}$	$\pm 1.62158\text{E-}16$	$\pm 1.05956\text{E}2$	$\pm 7.62481\text{E}3$	$\pm 1.85369\text{E-}1$	$\pm 3.99482 \text{E-}16$	$\pm 3.06727\text{E-}1$	$\pm 7.83473\text{E}2$	$\pm 2.21829 \text{E-}1$
$f_{14}$	2.98001E2	4.79622E-19	5.86044E1	5.28697E-60	3.58118E-3	3.18772E2	3.38398E2	9.42608E3
J14	$\pm 4.03708 E1$	$\pm 2.37125$ E-18	$\pm 1.91352E1$	$\pm 2.89579 \text{E-}59$	$\pm 1.15946E-3$	$\pm 1.09242E2$	$\pm 5.62602 E1$	$\pm 3.0541E4$
$f_{15}$	-9.66015E0	-9.66015E0	-9.46753E0	-7.723E0	-9.64002E0	-8.21481E0	-7.6554E0	-4.36336E0
	±3.48962E-12	±6.73326E-16	±1.53567E-1	±6.41586E-1	±2.18608E-2	±7.81092E-1	±3.5483E-1	±3.27595E-1
$f_{16}$	0E0 ±0E0	0E0 ±0E0	2.33333E-1 ±5.04007E-1	0E0 ±0E0	0E0 ±0E0	1.35513E3 ±3.45384E3	1.7244E3 $\pm 5.37113E2$	-1.07817E3
	4.25068E-16	5.2517E-62	±5.04007E-1 1.11832E-21	0E0	6.37852E-6	±3.45384E3 6.74478E2	1.69947E3	±1.0347E2 4.93448E4
$f_{17}$	±8.66061E-17	±2.87574E-61	±1.60262E-21	±0E0	±2.1748E-6	±2.53629E3	±4.33026E2	±3.99058E3
	3.97096E-16	7.97741E-62	1.15783E-22	0E0	9.4912E-7	6.30586E2	6.35204E1	6.77379E3
$f_{18}$	$\pm 6.3762 E17$	$\pm 4.36932 \text{E-}61$	$\pm 1.53037 E-22$	$\pm 0 E0$	$\pm 3.21888 E-7$	$\pm 4.82843 E2$	$\pm 1.86746 E1$	$\pm 6.95587 E2$
$f_{19}$	1.24185E-16	8.01885E-79	9.84712E-33	0E0	1.40339E-14	3.13431E0	2.98884E0	6.16682E1
J 19	$\pm 2.9789$ E-17	$\pm 4.37811$ E-78	$\pm 2.98627 \text{E-}32$	$\pm 0E0$	$\pm 1.09766$ E-14	$\pm 5.37155 E0$	$\pm 9.15548 \text{E-}1$	$\pm 9.468 E0$
$f_{20}$	6.87922E-14	9.67094E-12	3.06088E-12	4.5984E-174	8.88994E-4	1.68509E6	1.57859E2	2.54783E38
	±2.86633E-14	±4.94385E-12	±6.84783E-12	±0E0	±1.19202E-4	±9.22494E6	±5.52176E1	±6.41564E38
$f_{21}$	8.36169E-24 ±1.34414E-23	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	8.32775E-176 ±0E0	9.18626E-137 ±4.32973E-136	1.01188E-6 ±2.18912E-6	4.3922E-3
	4.38082E-1	7.97325E-1	2.18563E1	2.88241E1	2.86691E1	1.107E5	1.31389E3	±7.83882E-3 6.81447E5
$f_{22}$	±4.96995E-1	±1.62191E0	±2.99142E1	±8.81054E-2	±1.71778E1	±5.66657E4	±4.05118E2	±1.31922E5
	3.10407E-2	6.66667E-1	6.78789E-1	7.17149E-1	6.83807E-1	2.4162E4	5.42436E2	9.53274E5
$f_{23}$	$\pm 1.22118\text{E1}$	$\pm 5.11961\text{E-}17$	$\pm 6.63947\text{E-}2$	$\pm 5.55727\text{E-}2$	$\pm 6.18316\text{E}2$	$\pm 5.25871 E4$	$\pm 2.81213 E2$	$\pm 1.79674 E5$
$f_{24}$	2.84217E-14	0E0	3.22789E1	0E0	7.44533E-1	1.70013E2	1.71928E2	3.709E2
J24	$\pm 3.57956$ E-14	$\pm 0 E0$	$\pm 1.42547 E1$	$\pm 0E0$	$\pm 6.42161$ E-1	$\pm 2.69804 E1$	$\pm 1.28965 E1$	$\pm 1.78135E1$
$f_{25}$	2.46547E-4	2.46535E-4	5.73635E-3	0E0	1.76234E-5	7.06326E0	1.77621E1	4.34267E2
	±1.35038E-3	±1.35033E-3	±1.1988E-2	±0E0	±6.69164E-6	±2.28211E1	±4.49758E0	±3.41597E1
$f_{26}$	5.74563E-13 ±2.48402E-13	7.07582E-15 ±1.22834E-15	6.44519E-12 ±2.97232E-12	4.58892E-15 ±1.34665E-15	4.56931E-4 ±7.37661E-5	7.36458E0 $\pm 7.42052E0$	8.28621E0 ±9.0899E-1	2.01594E1 ±1.73812E-1
	±2.48402E-13	±1.22834E-15	±2.97252E-12	±1.54005E-15	-1E0	±1.42052E0	-9.86777E-1	-9.37032E-1
$f_{27}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±2.12924E-2	±1.48545E-2
	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86199E0	-3.83721E0
$f_{28}$	$\pm 2.23824\text{E-}16$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.99961\text{E3}$	$\pm 7.33142\text{E}4$	$\pm 1.69965 \text{E-}2$
foo	-3.322E0	-3.27444E0	-3.32152E0	-3.26773E0	-3.322E0	-3.24097E0	-3.1771E0	-2.86853E0
$f_{29}$	$\pm 1.80672 \text{E-}16$	$\pm 5.92412 E-2$	$\pm 1.68979 E-3$	$\pm 6.04807 \text{E}2$	$\pm 0E0$	$\pm 8.31124 \text{E-}2$	$\pm 7.28783\text{E}2$	$\pm 1.5204$ E-1
$f_{30}$	-1.01532E1	-1.01532E1	-5.40418E0	-9.98327E0	-1.01532E1	-6.13908E0	-5.45549E0	-2.23799E0
	±5.42758E-10	±0E0	±3.47842E0	±9.30764E-1	±0E0	±3.2573E0	±3.58362E0	±8.20131E-1
$f_{31}$	-1.04029E1 -1.05177E 15	-1.04029E1 -4.50676E 16	-8.68484E0 -3.13807E0	-1.02258E1 ±0.70431E 1	-1.04029E1 ±0E0	-9.87278E0 -1.61767E0	-5.91286E0 +3.65766E0	-2.30363E0 ±6.04000E 1
	±1.05177E-15 -1.05363E1	±4.50676E-16 -1.05364E1	±3.13807E0 -9.25887E0	±9.70431E-1 -1.00426E1	-1.05364E1	±1.61767E0 -9.99875E0	±3.65766E0 -7.66104E0	±6.94009E-1 -2.21453E0
$f_{32}$	±4.89476E-4	±4.50676E-16	±2.90551E0	±1.88857E0	±0E0	±1.64057E0	±3.69159E0	±6.08353E-1
	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97925E-1	4.20893E-1
$f_{33}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 4.55255 \text{E-}5$	$\pm 1.78542 E-2$
for	3.00018E0	3E0	3E0	3E0	3E0	3E0	3.00383E0	3.80503E0
$f_{34}$	$\pm 5.43727\text{E4}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 2.53729\text{E-}16$	$\pm 5.53623\text{E-}3$	$\pm 7.1302\text{E}1$
$f_{35}$	8.90008E-2	9.98733E-2	9.98733E-2	9.65442E-2	7.72212E-2	9.98733E-2	9.01937E-1	3.71609E0
	±2.9892E-2	±3.98632E-12	±4.93967E-10	±1.82343E-2	±4.1772E-2	±4.05396E-17	±3.32427E-1	±6.58918E-1
$f_{36}$	1.03207E-1 ±1.82573E-2	9.98733E-2 ±1.33601E-11	9.98733E-2 ±3.68435E-10	9.98733E-2 →0E0	9.65759E-2	9.98733E-2 ±2.53373E-18	1.3571E0 ±4.62228E 1	4.5866E0 ±8.84717E 1
	±1.82573E-2	±1.33691E-11	±3.68435E-10	±0E0	±1.80606E-2	±2.53373E-18	±4.62228E-1	±8.84717E-1

Table 5: Averages and standard deviations for Thirty-six benchmark problems with 6.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
$f_1$	3.99152E-7	0E0	0E0	0E0	0E0	0E0	1.16899E-4	9.56718E-3
	±3.79516E-7	±0E0	±0E0	±0E0	±0E0	±0E0	±1.58902E-4	±8.722E-3 -2.55604E-1
$f_2$	-9.99829E-1 ±3.29757E-4	-1E0 ±0E0	-1E0 ±0E0	-1E0 ±0E0	-1E0 ±0E0	-1E0 ±0E0	-8.6665E-1 ±3.45739E-1	-2.55604E-1 ±3.2395E-1
	2.32024E-6	0E0	0E0	0E0	1.25542E-80	3.79154E-228	4.55082E-6	2.67334E-3
$f_3$	±3.01408E-6	±0E0	±0E0	±0E0	$\pm 1.54219E-80$	±0E0	±8.79026E-6	±1.91347E-3
	0E0	0E0	0E0	0E0	0E0	0E0	1.86846E-5	3.25486E0
$f_4$	$\pm 0E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 2.50928 \text{E}5$	$\pm 2.33766 E0$
$f_5$	6.62291E-17	0E0	0E0	0E0	0E0	0E0	2.97207E-5	5.48471E-2
	±1.60415E-16	±0E0	±0E0	±0E0	±0E0	±0E0	±4.90338E-5	±6.7157E-2
$f_6$	-1.8013E0 ±0E0	-1.8013E0 ±0E0	-1.8013E0 ±0E0	-1.8013E0 ±0E0	-1.8013E0 ±0E0	-1.8013E0 ±0E0	-1.80129E0 ±1.70249E-5	-1.78842E0 ±1.14123E-2
	0E0	0E0	0E0	0E0	0E0	0E0	2.38459E-2	9.00041E-2
$f_7$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 7.98525$ E-2	$\pm 8.68108 E-2$
	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03162E0	-1.01933E0
$f_8$	$\pm 9.03362 \text{E-}17$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.84568\text{E}5$	$\pm 8.50494$ E-3
$f_9$	0E0	0E0	0E0	0E0	0E0	0E0	1.75823E-5	3.91122E0
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±2.42889E-5	±4.52711E0
$f_{10}$	1.85049E-7 ±3.30486E-7	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	2.57412E-4 ±4.81273E-4	5.03487E0
	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.8673E2	±4.30796E0 -1.84515E2
$f_{11}$	±8.67228E-15	±1.44216E-14	±1.38623E-13	±2.3306E-14	±1.22265E-14	±2.28026E-14	±1.58432E-3	±1.85892E0
	2.07915E-1	0E0	2.04212E-6	0E0	3.07563E-22	1.40659E-5	1.48943E0	8.09883E1
$f_{12}$	$\pm 1.64254\text{E1}$	$\pm 0 E0$	$\pm 6.23699 \text{E-}6$	$\pm 0 E0$	$\pm 7.93029 \text{E-}22$	$\pm 2.25792 \text{E}5$	$\pm 1.69424 E0$	$\pm 4.85105 \mathrm{E1}$
$f_{13}$	-4.68766E0	-4.68487E0	-4.68627E0	-4.54236E0	-4.68766E0	-4.55567E0	-4.64643E0	-3.23994E0
	±0E0	±1.05956E-2	±7.62481E-3	±1.8491E-1	±3.99482E-16	±3.06727E-1	±4.1748E-2	±1.63777E-1
$f_{14}$	2.36423E2	1.03554E-64	1.19217E-1	1.97775E-225 ±0E0	3.58118E-3 ±1.15946E-3	2.60163E2	2.60583E2	6.32962E2
	±3.46835E1 -9.66015E0	±5.60582E-64 -9.66015E0	±3.0119E-1 -9.49268E0	-7.9271E0	-9.64002E0	±1.15912E2 -8.24895E0	±5.81173E1 -8.6368E0	±2.45713E2 -4.65046E0
$f_{15}$	±4.50676E-16	±9.03362E-16	±1.21362E-1	±6.16012E-1	±2.18608E-2	±7.94128E-1	±2.78152E-1	±3.33664E-1
_	0E0	0E0	2.33333E-1	0E0	0E0	1.33353E3	4.35E1	-1.13363E3
$f_{16}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 5.04007\text{E-}1$	$\pm 0 E0$	$\pm 0 E0$	$\pm 3.45738 E3$	$\pm 2.77299 \mathrm{E}1$	$\pm 7.66503 \mathrm{E}1$
f <sub>17</sub>	3.56707E-16	3.04047E-120	5.31063E-72	0E0	6.37852E-6	6.66667E2	2.1506E1	4.51838E4
J11	±5.38706E-17	$\pm 1.66533$ E-119	$\pm 1.15748$ E-71	±0E0	$\pm 2.1748E-6$	$\pm 2.53708E3$	$\pm 2.23148E1$	$\pm 3.82797 E3$
$f_{18}$	3.35281E-16	6.49564E-117	6.28641E-73	0E0	9.4912E-7	6.16668E2	1.46955E1	6.12534E3
	±6.5218E-17 8.99847E-17	±3.55781E-116 5.95126E-175	±1.4669E-72 4.72423E-99	±0E0 0E0	±3.21888E-7 1.40339E-14	±4.82152E2 3.13175E0	±2.29496E0 1.0994E0	±6.34448E2 5.12697E1
$f_{19}$	±2.44415E-17	±0E0	±2.35822E-98	±0E0	±1.09766E-14	±5.37256E0	±2.33326E-1	±9.7271E0
	1.03004E-15	5.30001E-40	5.05945E-44	2.13303E-319	8.88994E-4	7.3E2	2.61327E1	1.28288E37
$f_{20}$	$\pm 7.56065\text{E-}17$	$\pm 3.93729 \text{E-}40$	$\pm 8.01377\text{E-}44$	$\pm 0 E0$	$\pm 1.19202\text{E4}$	$\pm 2.38023 E2$	$\pm 1.98037 E1$	$\pm 1.93915 E37$
$f_{21}$	4.56893E- $25$	0E0	0E0	0E0	8.32775E-176	0E0	4.40753E-8	6.50022E-4
721	±7.95014E-25	±0E0	±0E0	±0E0	±0E0	±0E0	±8.89088E-8	±1.02359E-3
$f_{22}$	1.35624E-1 ±2.58484E-1	7.97325E-1 ±1.62191E0	7.83374E0 ±1.81221E1	2.88159E1 ±1.03746E-1	2.86691E1 ±1.71778E1	1.10567E5 ±5.67114E4	3.28663E2 $\pm 1.28074E2$	5.56634E5 ±1.29654E5
	2.66725E-5	6.66667E-1	6.66667E-1	7.17149E-1	6.83807E-1	2.41289E4	3.19725E1	7.95749E5
$f_{23}$	±1.16173E-4	±2.02698E-17	±8.55018E-17	±5.55727E-2	±6.18316E-2	±5.25973E4	±9.89824E0	±1.58032E5
	0E0	0E0	2.8632E1	0E0	7.44533E-1	1.25985E2	1.3413E2	3.53231E2
$f_{24}$	$\pm 0 E0$	$\pm 0E0$	$\pm 8.56603 E0$	$\pm 0 E0$	$\pm 6.42161\text{E1}$	$\pm 2.93068 E1$	$\pm 9.6981 E0$	$\pm 1.54284 E1$
$f_{25}$	0E0	2.46535E-4	5.73635E-3	0E0	1.76234E-5	6.04438E0	3.37305E0	3.96561E2
	±0E0	±1.35033E-3	±1.1988E-2	±0E0	±6.69164E-6	±2.29166E1 5.71837E0	±8.40074E-1	±4.02002E1 2.002E1
$f_{26}$	3.12343E-14 ±2.85033E-15	5.89158E-15 ±1.8027E-15	8.73375E-15 ±1.7034E-15	4.35207E-15 ±1.08403E-15	4.56931E-4 ±7.37661E-5	±8.38013E0	1.85641E0 ±1.55167E-1	±2.17093E-1
	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.99929E-1	-9.50574E-1
$f_{27}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±1.01175E-4	±2.17969E-2
$f_{28}$	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86269E0	-3.8501E0
J 28	$\pm 1.12669$ E-16	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.99961$ E-3	$\pm 1.13116$ E-4	$\pm 8.05986 \text{E}3$
$f_{29}$	-3.322E0	-3.27444E0	-3.32163E0	-3.26824E0	-3.322E0	-3.24097E0	-3.27068E0	-2.9602E0
	±0E0	±5.92412E-2	±1.31857E-3 -5.51592E0	±6.08679E-2	±0E0 -1.01532E1	±8.31124E-2	±4.62318E-2	±1.03924E-1
$f_{30}$	-1.01532E1 ±7.35129E-16	-1.01532E1 ±0E0	-5.51592E0 ±3.52191E0	-9.98327E0 ±9.30764E-1	±0E0	-6.71945E0 ±3.18774E0	-5.49585E0 ±3.62833E0	-2.94646E0 ±1.04775E0
	-1.04029E1	-1.04029E1	-9.01242E0	-1.02258E1	-1.04029E1	-9.87279E0	-5.95835E0	-3.18474E0
$f_{31}$	±8.7065E-16	±0E0	$\pm 2.91642E0$	±9.70431E-1	±0E0	$\pm 1.61767 E0$	$\pm 3.70494E0$	$\pm 1.04661E0$
foo	-1.05364E1	-1.05364E1	-9.25887E0	-1.00426E1	-1.05364E1	-1.01775E1	-7.74006E0	-2.63661E0
$f_{32}$	$\pm 1.29307\text{E-}15$	$\pm 7.98963\text{E-}16$	$\pm 2.90551 E0$	$\pm 1.88857 \text{E}0$	$\pm 0 E0$	$\pm 1.36607 E0$	$\pm 3.74768 \text{E}0$	$\pm 4.89499 \text{E-}1$
$f_{33}$	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97889E-1	4.04967E-1
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±2.10243E-6	±6.44574E-3
$f_{34}$	3E0 ±2.23646E-8	3E0 ±0E0	3E0 ±0E0	3E0 ±0E0	3E0 ±0E0	3E0 ±0E0	3.00024E0 ±2.33538E-4	3.32937E0 ±3.20771E-1
	6.66666E-2	9.65442E-2	9.6847E-2	9.32151E-2	7.72212E-2	8.98861E-2	4.93312E-1	2.89585E0
$f_{35}$	±4.45125E-2	±1.82343E-2	±1.16924E-2	±2.53387E-2	±4.1772E-2	±3.0474E-2	±2.02925E-1	±7.33744E-1
f <sub>2e</sub>	9.34579E-2	9.98733E-2	9.98733E-2	9.98733E-2	9.65759E-2	9.98733E-2	7.02107E-1	3.85228E0
f <sub>36</sub>	$\pm 2.4415 E-2$	$\pm 9.38958\text{E-}13$	$\pm 2.26709$ E-11	$\pm 0 E0$	$\pm 1.80606$ E-2	$\pm 2.53373$ E-18	$\pm 3.80737 \text{E-}1$	±5.44903E-1

Table 6: Averages and standard deviations for Thirty-six benchmark problems with 10.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
$f_1$	2.80884E-7	0E0	0E0	0E0	0E0	0E0	5.22981E-5	4.69944E-3
	±3.35781E-7 -9.99952E-1	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±0E0 -1E0	±5.67097E-5 -9.66188E-1	±4.25902E-3 -3.1176E-1
$f_2$	-9.99952E-1 ±1.35715E-4	±0E0	±0E0	±0E0	±0E0	±0E0	±1.82503E-1	±3.22936E-1
	1.34138E-6	0E0	0E0	0E0	1.25542E-80	0E0	2.05941E-6	1.42874E-3
$f_3$	±2.31447E-6	±0E0	±0E0	±0E0	±1.54219E-80	±0E0	±2.96627E-6	±1.30063E-3
	0E0	0E0	0E0	0E0	0E0	0E0	7.11283E-6	2.19936E0
$f_4$	$\pm 0 E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 1.37428 E-5$	$\pm 1.43433 E0$
	2.99662E-17	0E0	0E0	0E0	0E0	0E0	1.07369E-5	2.91202E-2
$f_5$	$\pm 4.62482\text{E-}17$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.96857\text{E}5$	$\pm 2.73215\text{E-}2$
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.79221E0
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 6.57274$ E-6	±8.05412E-3
$f_7$	0E0	0E0	0E0	0E0	0E0	0E0	9.40463E-4	5.32826E-2
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±7.81017E-4	±6.1833E-2
$f_8$	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.02402E0
	±5.63345E-17 0E0	±0E0 0E0	±0E0 0E0	±0E0 0E0	±0E0 0E0	±0E0 0E0	±1.44063E-6 4.93077E-6	±6.14459E-3 1.77117E0
$f_9$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±5.1279E-6	±1.83689E0
	1.0229E-7	0E0	0E0	0E0	0E0	0E0	1.07445E-4	2.30129E0
$f_{10}$	±1.73501E-7	±0E0	±0E0	±0E0	±0E0	±0E0	±2.50598E-4	±2.00281E0
	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.85699E2
$f_{11}$	±1.1563E-14	±1.44216E-14	±1.29856E-13	±2.32262E-14	±1.22265E-14	±2.76601E-14	±3.02589E-4	±7.08757E-1
-	1.8472E-1	0E0	5.86283E-8	0E0	3.07563E-22	7.62137E-8	1.36326E0	6.22678E1
$f_{12}$	$\pm 1.44512\text{E-}1$	$\pm 0 E0$	$\pm 3.17061\text{E7}$	$\pm 0 E0$	$\pm 7.93029 \text{E-}22$	$\pm 1.17203\text{E}7$	$\pm 1.64249 E0$	$\pm 3.86777\mathrm{E}1$
f	-4.68766E0	-4.68487E0	-4.68627E0	-4.54242E0	-4.68766E0	-4.55567E0	-4.66369E0	-3.32057E0
$f_{13}$	$\pm 1.62158\text{E-}16$	$\pm 1.05956\text{E-}2$	$\pm 7.62481\text{E-}3$	$\pm 1.84905\text{E-}1$	$\pm 3.99482\text{E-}16$	$\pm 3.06727 \text{E-}1$	$\pm 3.92544\text{E}2$	$\pm 1.3914$ E-1
$f_{14}$	2.06648E2	3.15747E-113	1.62466E-6	0E0	3.58118E-3	2.50684E2	2.0893E2	4.84805E2
J14	$\pm 3.40646E1$	±1.18643E-112	$\pm 3.59211$ E-6	±0E0	$\pm 1.15946E-3$	$\pm 1.19983E2$	$\pm 4.23994E1$	$\pm 1.12231E2$
$f_{15}$	-9.66015E0	-9.66015E0	-9.49616E0	-8.02075E0	-9.64002E0	-8.26123E0	-8.90263E0	-4.7947E0
	±6.73326E-16	±7.98963E-16	±1.18847E-1	$\pm 6.44323$ E-1	$\pm 2.18608E-2$	±7.90216E-1	$\pm 2.25139 \text{E-}1$	±3.22078E-1
$f_{16}$	0E0	0E0	2.33333E-1	0E0	0E0	1.33333E3	0E0	-1.1931E3
	±0E0	±0E0	±5.04007E-1	±0E0	±0E0	±3.45746E3	±0E0	±8.7747E1
$f_{17}$	3.37925E-16	8.44742E-176	3.19731E-122	0E0	6.37852E-6	6.66667E2	1.0686E0	4.35608E4
	±5.32868E-17 3.06168E-16	±0E0 2.19998E-170	±9.00427E-122 1.03305E-123	±0E0 0E0	±2.1748E-6 9.4912E-7	±2.53708E3 6.16667E2	±1.61374E-1 1.12965E1	±3.26683E3 5.8984E3
$f_{18}$	±5.53599E-17	±0E0	±3.76979E-123	±0E0	±3.21888E-7	±4.82153E2	±1.32062E0	±5.93683E2
	7.57925E-17	1.88255E-268	1.15285E-163	0E0	1.40339E-14	3.13175E0	7.14926E-1	4.82419E1
$f_{19}$	±1.78395E-17	±0E0	±0E0	±0E0	±1.09766E-14	±5.37256E0	±1.8475E-1	±8.56777E0
	1.02473E-15	2.30965E-68	1.49142E-75	4.3784E-320	8.88994E-4	7.3E2	5.25295E0	8.07196E36
$f_{20}$	$\pm 7.11435$ E-17	$\pm 1.87484 E-68$	$\pm 2.7222 \text{E-}75$	$\pm 0E0$	$\pm 1.19202 E-4$	$\pm 2.38023E2$	$\pm 1.85197 E0$	$\pm 1.77479 E37$
	2.12993E-25	0E0	0E0	0E0	8.32775E-176	0E0	1.772E-8	1.88313E-4
$f_{21}$	$\pm 3.2404\text{E-}25$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 3.44907\text{E8}$	$\pm 3.60855\text{E4}$
$f_{22}$	1.08121E-1	7.97325E-1	2.26204E0	2.88109E1	2.86691E1	1.1056E5	2.39929E2	5.05329E5
	±1.87387E-1	±1.62191E0	$\pm 3.9287 E0$	±1.09302E-1	±1.71778E1	$\pm 5.67132E4$	$\pm 1.00135E2$	±1.104E5
$f_{23}$	2.40513E-7	6.66667E-1	6.66667E-1	7.17149E-1	6.83807E-1	2.41282E4	2.23795E1	7.54917E5
	±8.30419E-7	±2.02698E-17	±6.06928E-17	±5.55727E-2	±6.18316E-2	±5.25973E4	±7.63432E0	±1.58449E5
$f_{24}$	0E0	0E0	2.76861E1 ±7.73535E0	0E0 ±0E0	7.44533E-1	1.11232E2	1.21413E2	3.47599E2
	±0E0 0E0	±0E0 2.46535E-4	±7.73535E0 5.73635E-3	0E0	±6.42161E-1 1.76234E-5	±3.04578E1 6.04112E0	±7.95741E0 1.47276E0	±1.39765E1 3.84815E2
$f_{25}$	±0E0	±1.35033E-3	±1.1988E-2	±0E0	±6.69164E-6	±2.29175E1	±2.47403E-1	±4.53254E1
	3.005E-14	5.29946E-15	7.54952E-15	4.35207E-15	4.56931E-4	5.69107E0	1.51971E0	1.98968E1
$f_{26}$	±2.52654E-15	±1.7413E-15	±1.61598E-15	±1.08403E-15	±7.37661E-5	±8.36028E0	±1.08486E-1	±2.44291E-1
	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.99989E-1	-9.5624E-1
$f_{27}$	±0E0	±0E0	±0E0	$\pm 0E0$	±0E0	$\pm 0E0$	$\pm 1.46119\text{E}5$	$\pm 2.30865$ E-2
f	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86274E0	-3.85244E0
$f_{28}$	$\pm 8.10792\text{E-}17$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.99961$ E-3	$\pm 1.0184\text{E4}$	$\pm 6.30159\text{E-}3$
$f_{29}$	-3.322E0	-3.27444E0	-3.32168E0	-3.26855E0	-3.322E0	-3.24097E0	-3.28125E0	-2.99537E0
J 29	$\pm 0E0$	$\pm 5.92412 E-2$	$\pm 1.2057 \text{E-}3$	$\pm 6.10998$ E-2	$\pm 0 E0$	$\pm 8.31124 E-2$	$\pm 4.9218\text{E}2$	$\pm 9.42146 E-2$
$f_{30}$	-1.01532E1	-1.01532E1	-5.51592E0	-9.98327E0	-1.01532E1	-6.71945E0	-5.49703E0	-3.0836E0
	±4.50676E-16	±0E0	±3.52191E0	±9.30764E-1	±0E0	±3.18774E0	±3.62952E0	±1.04358E0
$f_{31}$	-1.04029E1	-1.04029E1	-9.04433E0	-1.02258E1	-1.04029E1	-9.87279E0	-5.95963E0	-3.4398E0
	±7.64159E-16	±0E0	±2.89816E0	±9.70431E-1	±0E0	±1.61767E0	±3.70623E0	±9.74935E-1
$f_{32}$	-1.05364E1 ±8.60173E 16	-1.05364E1 +8.05206E-16	-9.25887E0 +2.00551E0	-1.00543E1 -1.84008E0	-1.05364E1 ±0E0	-1.01775E1 -1.36607E0	-7.74505E0 ±3.75141E0	-3.01426E0 ±5.36007E 1
	±8.60173E-16	±8.95296E-16	±2.90551E0 3.97887E-1	±1.84008E0	±0E0 3.97887E-1	±1.36607E0 3.97887E-1	±3.75141E0	±5.36907E-1
$f_{33}$	3.97887E-1 ±0E0	3.97887E-1 ±0E0	3.97887E-1 ±0E0	3.97887E-1 ±0E0	3.97887E-1 ±0E0	3.97887E-1 ±0E0	3.97888E-1 ±4.46189E-7	4.02918E-1 ±4.22376E-3
	3E0	3E0	3E0	3E0	3E0	3E0	3.00008E0	3.1771E0
$f_{34}$	±2.14299E-9	±0E0	±0E0	±0E0	±0E0	±0E0	±1.20535E-4	±1.61276E-1
	4.74686E-2	9.65442E-2	9.16499E-2	9.32151E-2	7.72212E-2	8.9886E-2	2.57281E-1	2.67584E0
$f_{35}$	$\pm 4.44608$ E-2	±1.82343E-2	$\pm 2.27575$ E-2	±2.53387E-2	$\pm 4.1772$ E-2	±3.04742E-2	±1.47229E-1	±6.00166E-1
	9.06155E-2	9.98733E-2	9.98733E-2	9.98733E-2	9.65759E-2	9.98733E-2	4.07428E-1	3.55954E0
$f_{36}$	$\pm 2.82973\text{E-}2$	$\pm 9.38958\text{E-}13$	$\pm 1.49272\text{E-}11$	$\pm 0 E0$	$\pm 1.80606\text{E}2$	$\pm 2.53373\text{E-}18$	$\pm 3.39426\text{E}1$	$\pm 4.66585\text{E-}1$

Table 7: Averages and standard deviations for Thirty-six benchmark problems with 100.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
f.	1.87178E-7	0E0	0E0	0E0	1.21199E-3	0E0	2.06543E-7	1.16234E-4
$f_1$	$\pm 2.99666$ E-7	$\pm 0 E0$	$\pm 0E0$	$\pm 0E0$	$\pm 6.63834\text{E}3$	$\pm 0 E0$	$\pm 1.46091$ E-7	$\pm 1.29044\text{E4}$
$f_2$	-9.88218E-1	-1E0	-1E0	-1E0	-1E0	-9.99999E-1	-1E0	-9.10823E-1
	±6.40291E-2	±0E0	±0E0	±0E0	±8.68517E-7	±3.41948E-6	±3.63063E-10	±7.7394E-2
$f_3$	1.84452E-6 ±2.96715E-6	0E0 ±0E0	0E0 ±0E0	0E0 ±0E0	3.72331E-6 ±2.01811E-5	3.99531E-54 ±2.18832E-53	3.8728E-9 ±3.61477E-9	3.91297E-5 ±3.55944E-5
	0E0	0E0	0E0	0E0	6.57846E-5	0E0	4.17227E-9	±3.55944E-5 4.3614E-1
$f_4$	±0E0	±0E0	±0E0	±0E0	±3.60317E-4	±0E0	±7.59376E-9	±1.30845E-1
,	3.12766E-17	0E0	0E0	0E0	3.81824E-22	0E0	8.16839E-9	1.48488E-3
$f_5$	$\pm 4.8206\text{E-}17$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 2.09134\text{E-}21$	$\pm 0 E0$	$\pm 9.17525\text{E-}9$	$\pm 1.78158\text{E3}$
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80085E0
76	$\pm 8.10792 \text{E-}17$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.27235 \text{E}8$	$\pm 5.23185 E-4$
$f_7$	0E0	0E0	0E0	0E0	0E0	0E0	0E0	3.8274E-4
	±0E0	±0E0	±0E0	±0E0 -1.03163E0	±0E0	±0E0	±0E0	±1.12892E-3
$f_8$	-1.03163E0 ±9.55198E-17	-1.03163E0 ±0E0	-1.03163E0 ±0E0	-1.03163E0 ±0E0	-1.02984E0 ±9.78683E-3	-1.03163E0 ±0E0	-1.03163E0 ±2.68308E-9	-1.03103E0 ±6.48655E-4
	0E0	0E0	0E0	0E0	9.76811E-15	0E0	5.94021E-9	3.56288E-1
$f_9$	±0E0	±0E0	±0E0	±0E0	±5.35022E-14	±0E0	±9.58416E-9	±1.73602E-1
,	1.29441E-7	0E0	0E0	0E0	0E0	0E0	7.39342E-7	2.22093E-1
$f_{10}$	$\pm 1.84863\text{E}7$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 7.75884\text{E}7$	$\pm 1.36746\text{E1}$
$f_{11}$	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86606E2
J 1.1	$\pm 9.82669 \text{E-}15$	$\pm 1.44216$ E-14	$\pm 2.20005$ E-11	$\pm 2.43007 \text{E-}14$	$\pm 1.26277 \text{E-}9$	$\pm 2.65817$ E-14	$\pm 3.72384$ E-6	$\pm 1.2479 \text{E-}1$
$f_{12}$	2.16666E-1	0E0	1.30779E-7	0E0	2.44236E-4	9.67036E-8	1.04509E-1	7.23226E0
	±2.19496E-1	±0E0	±3.87774E-7	±0E0	±1.32514E-3	±1.39766E-7	±5.74878E-2	±3.78195E0
$f_{13}$	-4.68766E0	-4.67331E0	-4.68627E0	-4.54212E0	-4.68657E0	-4.55567E0	-4.68345E0	-3.74758E0
	±0E0 2.11979E2	±6.36838E-2 3.09532E-7	±7.62481E-3 7.41028E-2	±1.84967E-1 8.90994E-45	±5.87248E-3 4.73613E0	±3.06727E-1 2.76388E2	±1.27356E-2 7.35239E-1	±1.79987E-1 2.95647E2
$f_{14}$	±3.68291E1	±1.69538E-6	±3.7958E-1	±4.88017E-44	±1.08338E1	±1.47336E2	±8.39476E-2	±3.71103E1
	-9.66015E0	-9.66015E0	-9.4771E0	-7.75117E0	-9.59167E0	-8.24965E0	-9.50597E0	-5.49691E0
$f_{15}$	$\pm 6.48634\text{E-}16$	$\pm 9.01352\text{E-}16$	$\pm 1.48738 \text{E-}1$	$\pm 6.4443$ E-1	$\pm 2.06122\text{E1}$	$\pm 7.88432 \text{E-}1$	$\pm 1.1465\text{E-}1$	$\pm 3.49437 \text{E-}1$
$f_{16}$	0E0	0E0	2.33333E-1	0E0	8.9E0	2.27117E3	0E0	-1.40583E3
J16	$\pm 0E0$	±0E0	$\pm 5.04007 \text{E-}1$	$\pm 0E0$	$\pm 4.80911E0$	$\pm 5.97856E3$	±0E0	$\pm 5.51431E1$
$f_{17}$	3.33538E-16	2.19349E-51	4.34129E-126	8.35861E-152	1.09361E3	6.68156E2	2.6846E-1	3.26057E4
	±5.95881E-17	±1.20143E-50	±2.06284E-125	±4.53659E-151	±5.94573E3	±2.53669E3	±3.06308E-2	±2.39624E3
$f_{18}$	2.98799E-16	9.01666E-6	3.5302E-119	0E0 +0F0	4.03391E2	6.16675E2	3.37916E0 ±2.00796E-1	4.39887E3
	±5.33183E-17 8.31192E-17	±4.93863E-5 1.51605E-166	±1.46627E-118 7.36214E-37	±0E0 0E0	±1.33967E3 5.46548E-4	±4.82162E2 3.13175E0	±3.90786E-1 2.08044E-1	±3.20973E2 3.17722E1
$f_{19}$	±2.38275E-17	±0E0	±3.55472E-36	±0E0	±2.88038E-3	±5.37256E0	±4.76485E-2	±4.89461E0
	1.02727E-15	8.1658E-4	7.38352E-45	1.18128E-98	1.53514E30	7.36968E2	1.79168E0	1.47646E33
$f_{20}$	$\pm 7.3183\text{E-}17$	$\pm 4.47259\text{E-}3$	$\pm 4.04412\text{E-}44$	$\pm 6.47012 \text{E-}98$	$\pm 8.40833 \mathrm{E}30$	$\pm 2.40152 E2$	$\pm 1.58558\text{E}1$	$\pm 3.0517 \mathrm{E}33$
f	2.26951E-25	0E0	0E0	0E0	1.00934E-33	0E0	1.36339E-11	2.15292E-7
$f_{21}$	$\pm 3.22622\text{E-}25$	$\pm 0 E0$	$\pm 0E0$	$\pm 0E0$	$\pm 5.52839\text{E-}33$	$\pm 0 E0$	$\pm 1.97932$ E-11	$\pm 3.18208\text{E7}$
$f_{22}$	4.89068E0	3.55593E0	2.10646E0	2.8816E1	3.931E3	1.10558E5	9.16243E1	2.67832E5
	±2.62582E1	±1.50458E1	±3.65682E0	±1.04461E-1	±2.11271E4	±5.67159E4	±3.78311E1	±5.39579E4
$f_{23}$	4.02119E-3	6.66667E-1	6.66667E-1	7.17149E-1	1.98865E2	2.41286E4	5.00592E0	4.11912E5
	±2.20199E-2 0E0	±0E0 1.99331E-12	±6.06928E-17 3.03365E1	±5.55727E-2 0E0	±7.21102E2 2.52177E1	±5.2598E4 1.15123E2	±6.09216E-1 6.98119E1	±8.48489E4 3.15102E2
$f_{24}$	±0E0	±1.09178E-11	±1.16989E1	±0E0	±2.36002E1	±3.11521E1	±6.39396E0	±1.33925E1
	1.72825E-15	2.46535E-4	5.73635E-3	0E0	1.71307E0	6.08774E0	5.15203E-2	3.18298E2
$f_{25}$	$\pm 9.466\text{E-}15$	$\pm 1.35033$ E-3	$\pm 1.1988$ E-2	±0E0	$\pm 1.37548 E0$	$\pm 2.29058 \text{E}1$	$\pm 3.91717 E-2$	$\pm 2.57079 E1$
$f_{26}$	3.01685E-14	5.41789E-15	7.90479E-15	4.35207 E-15	2.27352E0	5.69837E0	8.36406E-1	1.9548E1
√26	$\pm 2.55225\text{E-}15$	$\pm 1.77022 \text{E-}15$	$\pm 1.70765$ E-15	$\pm 1.08403$ E-15	$\pm 3.9865 E0$	$\pm 8.35945 \text{E}0$	$\pm 7.90883\text{E-}2$	$\pm 2.0466\text{E1}$
$f_{27}$	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.9674E-1
-	±0E0	±0E0	±0E0	±0E0	±4.05396E-17	±0E0	±8.81554E-9	±3.60236E-3
$f_{28}$	-3.86278E0 ±1.12660E-16	-3.86278E0 ±0E0	-3.86278E0 -0E0	-3.86278E0 -0E0	-3.86278E0 ±1.12660E-16	-3.86226E0 ±1.00061E-3	-3.86278E0 ±0.48547E 8	-3.86124E0 ±0.00500E 4
	±1.12669E-16 -3.322E0	±0E0 -3.27444E0	±0E0 -3.32163E0	±0E0 -3.26794E0	±1.12669E-16 -3.322E0	±1.99961E-3 -3.24097E0	±9.48547E-8 -3.29028E0	±9.00599E-4 -3.18162E0
$f_{29}$	±0E0	±5.92412E-2	±1.31857E-3	±6.06364E-2	±1.7878E-8	±8.31124E-2	±5.34747E-2	±5.14526E-2
	-1.01532E1	-1.01532E1	-5.40418E0	-9.98327E0	-9.93435E0	-6.71873E0	-5.49734E0	-5.69063E0
$f_{30}$	±7.35129E-16	±0E0	$\pm 3.47842 E0$	±9.30764E-1	±1.18834E0	$\pm 3.18812 E0$	$\pm 3.62977 E0$	$\pm 1.48215 E0$
for	-1.04029E1	-1.04029E1	-8.91907E0	-1.02258E1	-1.03337E1	-9.87279E0	-6.17013E0	-5.67107E0
$f_{31}$	$\pm 8.95296\text{E-}16$	$\pm 0 E0$	$\pm 3.01061 E0$	$\pm 9.70431$ E-1	$\pm 3.79137 \text{E-}1$	$\pm 1.61767 E0$	$\pm 3.77567 \text{E}0$	$\pm 1.44733 E0$
$f_{32}$	-1.05364E1	-1.05364E1	-9.25887E0	-1.00426E1	-1.02619E1	-1.01775E1	-7.74608E0	-6.02234E0
	±1.37859E-15	±7.98963E-16	±2.90551E0	±1.88857E0	±1.49231E0	±1.36607E0	±3.75216E0	±1.49202E0
foo	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.98072E-1
$f_{33}$	$\pm 0E0$	±0E0	±0E0	±0E0 3E0	±1.07653E-9 3E0	±0E0	±3.35874E-9	±1.32948E-4 3.00533E0
133		2E0			o P.U	3E0	3E0	0.00003EU
f <sub>34</sub>	3.00013E0	3E0 +0E0	3E0 +0E0					
f <sub>34</sub>	$\begin{array}{c} 3.00013 \text{E}0 \\ \pm 6.85399 \text{E-4} \end{array}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.61314\text{E-}9$	$\pm 0 E0$	$\pm 1.34971\text{E7}$	$\pm 5.82236\text{E3}$
	3.00013E0							
f <sub>34</sub>	3.00013E0 ±6.85399E-4 5.02559E-2	±0E0 9.65442E-2	±0E0 9.62937E-2	±0E0 9.32151E-2	±1.61314E-9 1.36557E-1	±0E0 8.9886E-2	±1.34971E-7 9.14309E-2	±5.82236E-3 1.46475E0

Table 8: Averages and standard deviations for Thirty-six benchmark problems with 300.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	8.0266E-8	0E0	0E0	0E0	1.61114E-20	0E0	6.6696E-8	4.08162E-5
$f_1$	±1.0053E-7	±0E0	±0E0	±0E0	±8.82458E-20	±0E0	±4.99501E-8	±3.4569E-5
	-9.88236E-1	-1E0	-1E0	-1E0	-1E0	-9.99999E-1	-1E0	-9.5759E-1
$f_2$	$\pm 6.40325 E-2$	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 8.68517 E-7$	$\pm 3.41948 E-6$	$\pm 3.65525 \text{E-}11$	$\pm 3.74493E-2$
	6.11462E-7	0E0	0E0	0E0	3.72331E-6	3.99531E-54	5.44517E-10	1.32675E-5
$f_3$	$\pm 2.03076 E-6$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.01811 \text{E}5$	$\pm 2.18832 E-53$	$\pm 4.38387 \text{E-}10$	$\pm 1.62787 E-5$
	0E0	0E0	0E0	0E0	6.57846E-5	0E0	4.11107E-10	2.81794E-1
$f_4$	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 0E0$	$\pm 3.60317 \text{E}4$	$\pm 0E0$	$\pm 4.94554 \text{E-}10$	$\pm 1.78676\text{E1}$
	1.28984E-17	0E0	0E0	0E0	0E0	0E0	1.03314E-9	3.92366E-4
$f_5$	$\pm 1.89589 \text{E-}17$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.57598\text{E9}$	$\pm 2.84662\text{E}4$
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80113E0
76	$\pm 8.10792 \text{E-}17$	±0E0	±0E0	$\pm 0E0$	$\pm 0E0$	±0E0	$\pm 3.39393$ E-9	$\pm 1.87831$ E-4
$f_7$	0E0	0E0	0E0	0E0	0E0	0E0	0E0	8.29302E-6
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 0E0$	$\pm 2.55612 E-5$
$f_8$	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.02984E0	-1.03163E0	-1.03163E0	-1.0314E0
70	$\pm 5.63345$ E-17	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 9.78683E-3$	±0E0	$\pm 3.76832 \text{E-}10$	$\pm 3.05455 \text{E-4}$
$f_9$	0E0	0E0	0E0	0E0	9.76811E-15	0E0	4.83989E-10	1.8063E-1
	±0E0	±0E0	±0E0	±0E0	±5.35022E-14	±0E0	±6.53892E-10	±9.59839E-2
$f_{10}$	2.12216E-8	0E0	0E0	0E0	0E0	0E0	7.91715E-8	1.18991E-1
	±3.39041E-8	±0E0	±0E0	±0E0	±0E0	±0E0	±7.16606E-8	±7.60087E-2
$f_{11}$	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86698E2
	±1.41618E-14	±1.44216E-14	±1.30938E-13	±2.32262E-14	±1.26278E-9	±2.86008E-14	±2.09114E-7	±3.40453E-2
$f_{12}$	1.46872E-1	0E0	8.05056E-12	0E0	2.44235E-4	5.13705E-12	4.40684E-2	4.33916E0
	±1.98613E-1	±0E0	±4.40804E-11	±0E0	±1.32514E-3	±2.61722E-11	±2.6098E-2	±2.24583E0
$f_{13}$	-4.68766E0	-4.68487E0	-4.68627E0	-4.54242E0	-4.68766E0	-4.55567E0	-4.68765E0	-3.99807E0
	±2.25338E-16	±1.05956E-2	±7.62481E-3	±1.84905E-1	±2.17741E-9	±3.06727E-1	±4.49753E-5	±2.08882E-1
$f_{14}$	1.65527E2	3.21136E-104	8.44994E-18	6.793E-321	4.24373E-2	2.40641E2	5.36196E-1	2.74735E2
	±3.17665E1	±1.75894E-103	±2.62367E-17	±0E0	±1.41222E-1	±1.26446E2	±8.75153E-2	±2.84117E1
$f_{15}$	-9.66015E0	-9.66015E0	-9.49608E0	-8.01701E0	-9.64002E0	-8.29047E0	-9.59466E0	-5.74111E0
	±8.51698E-16 0E0	±7.2269E-16 0E0	±1.18965E-1 2.33333E-1	±6.4061E-1	±2.18604E-2 0E0	±7.95536E-1	±8.93235E-2 0E0	±3.03079E-1
$f_{16}$	±0E0	±0E0	±5.04007E-1	0E0 ±0E0	±0E0	1.33333E3 ±3.45746E3	±0E0	-1.4789E3 ±5.80109E1
		3.03972E-281						
$f_{17}$	3.01252E-16 ±6.07838E-17	±0E0	1.22706E-248 ±0E0	0E0	6.13495E-1 ±2.63915E0	6.66667E2	2.35983E-1 ±2.45349E-2	3.15089E4
	2.80337E-16	2.31993E-282	9.42761E-251	±0E0 0E0	9.13597E-3	±2.53708E3 6.16667E2	±2.45549E-2 2.82874E0	±2.61829E3 4.12515E3
$f_{18}$	±5.42648E-17	±0E0	±0E0	±0E0	±2.66594E-2	±4.82153E2	±3.55018E-1	±2.8442E2
	£5.42048E-17 6.68483E-17	3.54205E-252	7.3298E-73	0E0	2.1855E-10	3.13175E0	1.54569E-1	2.99435E1
$f_{19}$	±1.78448E-17	±0E0	±3.89288E-72	±0E0	±4.80709E-10	±5.37256E0	±3.59121E-2	±4.94406E0
	9.47248E-16	2.41097E-47	2.99109E-153	4.3784E-320	8.31858E-2	7.3E2	1.61748E0	6.24562E32
$f_{20}$	±8.46238E-17	±1.32054E-46	±1.54889E-152	±0E0	±3.33264E-1	±2.38023E2	±1.21007E-1	±1.09299E33
	6.1886E-26	0E0	0E0	0E0	1.00934E-33	0E0	1.6221E-12	1.37415E-8
$f_{21}$	±1.07071E-25	±0E0	±0E0	±0E0	±5.52839E-33	±0E0	±3.01022E-12	±2.51931E-8
	7.34652E-2	7.97325E-1	1.1486E0	2.88109E1	3.27662E1	1.10552E5	8.50391E1	2.50746E5
$f_{22}$	±1.35276E-1	±1.62191E0	±1.90036E0	±1.09302E-1	±1.8338E1	±5.67204E4	±3.6468E1	±4.63841E4
	9.38395E-9	6.66667E-1	6.66667E-1	7.17149E-1	7.44167E-1	2.4128E4	4.10845E0	3.69817E5
$f_{23}$	±3.97254E-8	±0E0	±5.93951E-17	±5.55727E-2	±1.96545E-1	±5.25973E4	±6.22756E-1	±7.17718E4
	0E0	0E0	2.75344E1	0E0	7.5359E-1	1.00453E2	5.83579E1	3.02179E2
$f_{24}$	±0E0	±0E0	±7.73253E0	±0E0	±6.49092E-1	±3.16109E1	±5.57679E0	±1.08895E1
	0E0	2.46535E-4	5.73635E-3	0E0	4.60633E-3	6.03958E0	4.59521E-2	2.99963E2
$f_{25}$	±0E0	$\pm 1.35033$ E-3	$\pm 1.1988$ E-2	±0E0	$\pm 9.67593$ E-3	$\pm 2.29179E1$	$\pm 3.72612 E-2$	$\pm 2.40398E1$
	2.92211E-14	4.94419E-15	7.31267E-15	4.35207E-15	1.14086E-3	5.65822E0	6.99524E-1	1.93674E1
$f_{26}$	±2.15801E-15	±1.59793E-15	±1.59793E-15	±1.08403E-15	$\pm 2.54391E-3$	$\pm 8.32582E0$	±7.0609E-2	±1.98155E-1
	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.9894E-1
$f_{27}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 8.78584$ E-10	$\pm 9.68521 \text{E-4}$
	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.86211E0
$f_{28}$	$\pm 0E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 8.10792\text{E-}17$	$\pm 1.99961$ E-3	$\pm 2.02538 \text{E}8$	$\pm 4.45876\text{E4}$
-	-3.322E0	-3.27444E0	-3.32177E0	-3.2685E0	-3.322E0	-3.24097E0	-3.29029E0	-3.22374E0
$f_{29}$	$\pm 0E0$	$\pm 5.92412 E-2$	$\pm 8.12468$ E-4	$\pm 6.10973 \text{E-}2$	$\pm 3.81006$ E-12	$\pm 8.31124 E-2$	$\pm 5.34755 E-2$	$\pm 3.59355 E-2$
	-1.01532E1	-1.01532E1	-5.51592E0	-9.98327E0	-9.936E0	-6.71945E0	-5.49734E0	-6.85792E0
$f_{30}$	$\pm 4.50676\text{E-}16$	$\pm 0 E0$	$\pm 3.52191 E0$	$\pm 9.30764\text{E-}1$	$\pm 1.18861 E0$	$\pm 3.18774 \text{E}0$	$\pm 3.62977 E0$	$\pm 1.23095 E0$
-	-1.04029E1	-1.04029E1	-9.0371E0	-1.02258E1	-1.03337E1	-9.87279E0	-6.17013E0	-6.90533E0
$f_{31}$	$\pm 6.73326 \text{E-}16$	$\pm 0E0$	$\pm 2.90138 E0$	$\pm 9.70431\text{E-}1$	$\pm 3.79137 \text{E-}1$	$\pm 1.61767 E0$	$\pm 3.77568 E0$	$\pm 1.3998E0$
f	-1.05364E1	-1.05364E1	-9.25887E0	-1.00426E1	-1.03237E1	-1.01775E1	-7.74608E0	-6.84476E0
$f_{32}$	$\pm 9.01352\text{E-}16$	$\pm 8.95296 \text{E-}16$	$\pm 2.90551 E0$	$\pm 1.88857 E0$	$\pm 1.16514 E0$	$\pm 1.36607 E0$	$\pm 3.75216 E0$	$\pm 1.2483 E0$
f	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97954E-1
$f_{33}$	$\pm 0 E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 1.07653\text{E-}9$	$\pm 0 E0$	$\pm 7.9412\text{E-}11$	$\pm 5.67369\text{E}5$
for	3.00013E0	3E0	3E0	3E0	3E0	3E0	3E0	3.00151E0
f <sub>34</sub>	$\pm 6.85399\text{E}4$	$\pm 0 E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 1.61314\text{E-}9$	$\pm 0 E0$	$\pm 8.6365\text{E-}9$	$\pm 1.35192\text{E3}$
for	3.16793E-2	9.65442E-2	8.31657E-2	9.32151E-2	1.17078E-1	8.65569E-2	6.96489E-2	1.22237E0
f <sub>35</sub>	$\pm 4.11374\text{E-}2$	$\pm 1.82343 E-2$	$\pm 3.45744\text{E-}2$	$\pm 2.53387\text{E-}2$	$\pm 2.08375\text{E-}1$	$\pm 3.45308\text{E}2$	$\pm 3.86796\text{E}2$	$\pm 2.45238 \text{E-}1$
fac	8.09937E-2	9.98733E-2	9.98733E-2	9.98733E-2	1.66937E-1	9.98733E-2	9.88194E-2	1.71656E0
$f_{36}$	$\pm 3.84585 E-2$	$\pm 7.98017$ E-11	$\pm 5.62668\text{E-}12$	$\pm 0 E0$	$\pm 3.86427 \text{E-}1$	$\pm 2.53373\text{E-}18$	$\pm 4.62831\text{E}3$	$\pm 4.13067 \text{E-}1$

Table 9: Averages and standard deviations for Thirty-six benchmark problems with 500.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	8.0266E-8	0E0	0E0	0E0	0E0	0E0	6.6696E-8	4.08162E-5
$f_1$	±1.0053E-7	±0E0	±0E0	±0E0	±0E0	±0E0	±4.99501E-8	±3.4569E-5
	-9.99997E-1	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.77803E-1
$f_2$	$\pm 5.35253 E-6$	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.89746$ E-11	$\pm 2.25403$ E-2
	3.39482E-7	0E0	0E0	0E0	3.72331E-6	3.99531E-54	5.15681E-10	1.32675E-5
$f_3$	$\pm 6.62122 E-7$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.01811$ E-5	$\pm 2.18832 E-53$	$\pm 4.19494$ E-10	$\pm 1.62787 E-5$
,	0E0	0E0	0E0	0E0	6.57846E-5	0E0	3.02961E-10	2.18746E-1
$f_4$	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 0E0$	$\pm 3.60317 \text{E-}4$	$\pm 0E0$	$\pm 4.25068 \text{E-}10$	$\pm 1.6297\text{E-}1$
	1.28984E-17	0E0	0E0	0E0	0E0	0E0	9.33749E-10	3.65231E-4
$f_5$	$\pm 1.89589 E17$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.25274\text{E-}9$	$\pm 2.81578\text{E4}$
$f_6$	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80121E0
76	$\pm 0E0$	±0E0	±0E0	$\pm 0E0$	$\pm 0E0$	±0E0	$\pm 4.92871$ E-10	$\pm 9.93348 \text{E}5$
$f_7$	0E0	0E0	0E0	0E0	0E0	0E0	0E0	1.73892E-6
	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 5.36017 E-6$
$f_8$	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.02984E0	-1.03163E0	-1.03163E0	-1.03154E0
20	$\pm 5.63345$ E-17	±0E0	$\pm 0E0$	$\pm 0E0$	$\pm 9.78683$ E-3	±0E0	$\pm 1.2593$ E-10	$\pm 9.11849 E-5$
$f_9$	0E0	0E0	0E0	0E0	9.76811E-15	0E0	2.70683E-10	1.44724E-1
	±0E0	±0E0	±0E0	±0E0	±5.35022E-14	±0E0	±4.35884E-10	±8.56088E-2
$f_{10}$	2.12216E-8	0E0	0E0	0E0	0E0	0E0	6.79403E-8	9.69389E-2
	±3.39041E-8	±0E0	±0E0	±0E0	±0E0	±0E0	±5.96346E-8	±7.13019E-2
$f_{11}$	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86705E2
	±1.41618E-14	±1.44216E-14	±1.20618E-13	±2.32262E-14	±1.37628E-14	±2.86008E-14	±5.6808E-8	±3.01372E-2
$f_{12}$	1.46872E-1	0E0	8.04803E-12	0E0	2.44235E-4	5.13705E-12	4.30464E-2	4.33219E0
	±1.98613E-1	±0E0	±4.40809E-11	±0E0	±1.32514E-3	±2.61722E-11	±2.54221E-2	±2.24942E0
$f_{13}$	-4.68766E0	-4.68487E0	-4.68627E0	-4.54242E0	-4.68766E0	-4.55567E0	-4.68766E0	-4.05708E0
	±2.25338E-16	±1.05956E-2	±7.62481E-3	±1.84905E-1	±3.67565E-16 3.58118E-3	±3.06727E-1	±1.91969E-6	±1.66608E-1
$f_{14}$	1.60489E2	2.56634E-230	8.44994E-18	0E0		2.40561E2	5.33905E-1	2.74735E2
	±2.93857E1	±0E0	±2.62367E-17	±0E0	±1.15946E-3	±1.26423E2	±7.87096E-2	±2.84117E1
$f_{15}$	-9.66015E0	-9.66015E0	-9.49616E0 ±1.18847E-1	-8.02075E0	-9.64002E0	-8.29047E0	-9.60638E0	-5.84734E0 ±2.99768E-1
	±8.8511E-16 0E0	±7.2269E-16 0E0	±1.18847E-1 2.33333E-1	±6.44323E-1	±2.18608E-2 0E0	±7.95536E-1	±8.81541E-2 0E0	±2.99768E-1 -1.48557E3
$f_{16}$	±0E0	±0E0	±5.04007E-1	0E0 ±0E0	±0E0	1.33333E3 ±3.45746E3	±0E0	±5.81613E1
	3.00328E-16	3.4626E-312						
$f_{17}$		3.4626E-312 ±0E0	1.22706E-248 ±0E0	0E0	8.85906E-5	6.66667E2 ±2.53708E3	2.35983E-1	3.15089E4
	±5.95744E-17 2.80337E-16	2.63566E-307	9.42761E-251	±0E0 0E0	±4.50104E-4 9.4912E-7	£2.55708E5 6.16667E2	±2.45349E-2 2.82874E0	±2.61829E3 4.12515E3
$f_{18}$	±5.42648E-17	±0E0	±0E0	±0E0	±3.21888E-7	±4.82153E2	±3.55018E-1	±2.8442E2
	6.37721E-17	0E0	1.04734E-125	0E0	1.40339E-14	3.13175E0	1.22782E-1	2.76786E1
$f_{19}$	±1.51696E-17	±0E0	±5.64979E-125	±0E0	±1.09766E-14	±5.37256E0	±2.66313E-2	±4.42249E0
	9.41294E-16	5.51019E-139	2.99109E-153	4.3784E-320	8.88994E-4	7.3E2	1.61748E0	6.24562E32
$f_{20}$	±8.07611E-17	±4.55809E-139	±1.54889E-152	±0E0	±1.19202E-4	±2.38023E2	±1.21007E-1	±1.09299E33
	6.1886E-26	0E0	0E0	0E0	1.00934E-33	0E0	1.6221E-12	1.37415E-8
$f_{21}$	±1.07071E-25	±0E0	±0E0	±0E0	±5.52839E-33	±0E0	±3.01022E-12	±2.51931E-8
	7.33769E-2	7.97325E-1	1.1486E0	2.88109E1	2.86691E1	1.10552E5	8.50391E1	2.50746E5
$f_{22}$	±1.35321E-1	±1.62191E0	±1.90036E0	±1.09302E-1	±1.71778E1	$\pm 5.67204 E4$	±3.6468E1	±4.63841E4
	2.45995E-9	6.66667E-1	6.66667E-1	7.17149E-1	6.84112E-1	2.4128E4	4.10845E0	3.69817E5
$f_{23}$	$\pm 1.32322E-8$	±0E0	$\pm 5.93951$ E-17	$\pm 5.55727 E-2$	$\pm 6.27289 E-2$	$\pm 5.25973E4$	$\pm 6.22756 \text{E-}1$	±7.17718E4
	0E0	0E0	2.74963E1	0E0	7.44533E-1	1.00453E2	5.2589E1	2.96332E2
$f_{24}$	$\pm 0E0$	±0E0	$\pm 7.64665 E0$	$\pm 0E0$	$\pm 6.42161$ E-1	$\pm 3.16109 E1$	$\pm 5.8763E0$	$\pm 1.32535E1$
	0E0	2.46535E-4	5.73635E-3	0E0	1.76234E-5	6.03957E0	4.57021E-2	2.91909E2
$f_{25}$	±0E0	$\pm 1.35033$ E-3	$\pm 1.1988$ E-2	±0E0	$\pm 6.69164 E-6$	$\pm 2.29179E1$	$\pm 3.74183$ E-2	$\pm 2.28624E1$
f	2.92211E-14	4.94419E-15	7.31267E-15	4.35207E-15	4.56931E-4	5.65822E0	6.60572E-1	1.93055E1
$f_{26}$	$\pm 2.15801\text{E-}15$	$\pm 1.59793\text{E-}15$	$\pm 1.59793\text{E-}15$	$\pm 1.08403\text{E-}15$	$\pm 7.37661\text{E}5$	$\pm 8.32582 \text{E}0$	$\pm 6.69525\text{E-}2$	$\pm 2.13643\text{E-}1$
f	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.99297E-1
$f_{27}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 4.31776\text{E-}10$	$\pm 6.99793 \text{E-}4$
foo	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.86233E0
$f_{28}$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 0 E0$	$\pm 8.10792\text{E-}17$	$\pm 1.99961\text{E3}$	$\pm 7.20123\text{E-}9$	$\pm 3.57789\text{E4}$
foo	-3.322E0	-3.27444E0	-3.32177E0	-3.26855E0	-3.322E0	-3.24097E0	-3.29029E0	-3.23346E0
$f_{29}$	$\pm 0 E0$	$\pm 5.92412\text{E-}2$	$\pm 8.12468\text{E4}$	$\pm 6.11017\text{E-}2$	$\pm 2.02414\text{E-}12$	$\pm 8.31124\text{E-}2$	$\pm 5.34754\text{E-}2$	$\pm 3.47474\text{E-}2$
f	-1.01532E1	-1.01532E1	-5.55601E0	-9.98327E0	-1.01532E1	-6.71945E0	-5.49734E0	-7.38684E0
f <sub>30</sub>	$\pm 4.50676$ E-16	$\pm 0E0$	$\pm 3.5631 E0$	$\pm 9.30764 \text{E-}1$	$\pm 8.30316 \text{E-}12$	$\pm 3.18774 E0$	$\pm 3.62977 E0$	$\pm 1.32978 E0$
far	-1.04029E1	-1.04029E1	-9.12777E0	-1.02258E1	-1.04029E1	-9.87279E0	-6.17013E0	-7.49049E0
$f_{31}$	$\pm 5.42017$ E-16	$\pm 0 E0$	$\pm 2.90011E0$	$\pm 9.70431$ E-1	$\pm 4.31753 \text{E-}7$	$\pm 1.61767 E0$	$\pm 3.77568 E0$	$\pm 1.31956 E0$
$f_{32}$	-1.05364E1	-1.05364E1	-9.25887E0	-1.00543E1	-1.05364E1	-1.01775E1	-7.74608E0	-7.30773E0
102	$\pm 8.7065 \text{E-}16$	$\pm 8.51698 \text{E-}16$	$\pm 2.90551E0$	$\pm 1.84008 E0$	$\pm 4.50676$ E-16	$\pm 1.36607 E0$	$\pm 3.75216 E0$	$\pm 1.13693 E0$
$f_{33}$	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97947E-1
- 33	±0E0	±0E0	±0E0	±0E0	$\pm 1.07653$ E-9	$\pm 0 E0$	$\pm 7.41339$ E-11	$\pm 5.82261 \text{E}5$
$f_{34}$	3.00013E0	3E0	3E0	3E0	3E0	3E0	3E0	3.00144E0
2.54	$\pm 6.85399 \text{E}4$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0 E0$	$\pm 7.59165 E-9$	$\pm 1.32935 E-3$
$f_{35}$	3.01537E-2	9.65442E-2	8.17415E-2	9.32151E-2	1.17078E-1	8.65569E-2	6.24301E-2	1.17774E0
	$\pm 3.93302 \text{E-}2$	$\pm 1.82343$ E-2	$\pm 3.69659 E-2$	$\pm 2.53387$ E-2	$\pm 2.08375$ E-1	$\pm 3.45308 \text{E}2$	$\pm 3.90515$ E-2	±2.43999E-1
$f_{36}$	8.09937E-2	9.98733E-2	9.98733E-2	9.98733E-2	1.66937E-1	9.98733E-2	9.88194E-2	1.65815E0
200	$\pm 3.84585 E-2$	±0E0	±5.61822E-12	±0E0	±3.86427E-1	±2.53373E-18	±4.62831E-3	±3.62469E-1

Table 10: Averages and standard deviations for Thirty-six benchmark problems with 1.000.000 evaluations or hitting a bound.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
Tunction	7.62519E-8	0E0	0E0	0E0	0E0	0E0	6.6696E-8	4.08162E-5
$f_1$								
	±9.95558E-8	±0E0	±0E0	±0E0	±0E0	±0E0	±4.99501E-8	±3.4569E-5
$f_2$	-9.99997E-1	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.77803E-1
,2	$\pm 5.35253E-6$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 2.89746$ E-11	$\pm 2.25403$ E-2
	2.40964E-7	0E0	0E0	0E0	1.25542E-80	0E0	5.15681E-10	1.32675E-5
$f_3$	$\pm 4.45425 E-7$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.54219 E-80$	$\pm 0E0$	$\pm 4.19494$ E-10	$\pm 1.62787 E-5$
	0E0	0E0	0E0	0E0	0E0	0E0	3.02961E-10	2.18746E-1
$f_4$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±4.25068E-10	
								±1.6297E-1
$f_5$	1.26857E-17	0E0	0E0	0E0	0E0	0E0	9.33749E-10	3.65231E-4
	±1.90206E-17	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 1.25274E-9$	$\pm 2.81578E-4$
f-	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.8013E0	-1.80124E0
$f_6$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 4.29342 \text{E-}10$	$\pm 7.17784\text{E}5$
	0E0	0E0	0E0	0E0	0E0	0E0	0E0	3.4292E-7
$f_7$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±1.25274E-6
$f_8$	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03163E0	-1.03156E0
-	$\pm 4.25849$ E-16	$\pm 4.25849$ E-16	$\pm 4.13973$ E-16	$\pm 4.50676$ E-16	$\pm 4.35325$ E-16	$\pm 4.50676$ E-16	$\pm 1.2593$ E-10	$\pm 5.35465 E-5$
$f_9$	0E0	0E0	0E0	0E0	0E0	0E0	2.70683E-10	1.4418E-1
J9	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 4.35884$ E-10	$\pm 8.61814 \text{E-}2$
	2.12216E-8	0E0	0E0	0E0	0E0	0E0	6.59961E-8	9.69389E-2
$f_{10}$	$\pm 3.39041$ E-8	±0E0	±0E0	±0E0	±0E0	±0E0	$\pm 5.98473$ E-8	$\pm 7.13019$ E-2
	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86731E2	-1.86715E2
$f_{11}$								
	±1.43247E-14	±1.44216E-14	±1.21259E-13	±2.32262E-14	$\pm 1.22265 \text{E-}14$	±2.86008E-14	±3.02688E-8	±1.29734E-2
$f_{12}$	1.15479E-1	0E0	8.04803E-12	0E0	3.07563E-22	3.48218E-13	4.30464E-2	4.33219E0
J 12	$\pm 8.65954\text{E}2$	$\pm 0E0$	$\pm 4.40809 \text{E-}11$	$\pm 0E0$	$\pm 7.93029 \text{E-}22$	$\pm 6.4077\text{E-}13$	$\pm 2.54221\text{E-}2$	$\pm 2.24942 E0$
	-4.68766E0	-4.68487E0	-4.68627E0	-4.54242E0	-4.68766E0	-4.55567E0	-4.68766E0	-4.11861E0
$f_{13}$	$\pm 2.25338E-16$	$\pm 1.05956E-2$	$\pm 7.62481$ E-3	$\pm 1.84905$ E-1	$\pm 3.99482 E-16$	$\pm 3.06727 \text{E-}1$	$\pm 8.65463$ E-7	$\pm 1.49082$ E-1
	1.60489E2	2.56634E-230	8.44994E-18	0E0	3.58118E-3	2.40561E2	5.21817E-1	2.74735E2
$f_{14}$								
	±2.93857E1	±0E0	±2.62367E-17	±0E0	±1.15946E-3	±1.26423E2	±5.45327E-2	±2.84117E1
$f_{15}$	-9.66015E0	-9.66015E0	-9.49621E0	-8.02075E0	-9.64002E0	-8.29047E0	-9.6179E0	-5.89408E0
313	$\pm 8.8511$ E-16	$\pm 7.2269 \text{E-}16$	$\pm 1.18775$ E-1	$\pm 6.44323$ E-1	$\pm 2.18608E-2$	$\pm 7.95536E-1$	$\pm 7.35073$ E-2	$\pm 2.7332 \text{E-}1$
	0E0	0E0	2.33333E-1	0E0	0E0	1.33333E3	0E0	-1.48557E3
$f_{16}$	$\pm 0E0$	$\pm 0E0$	$\pm 5.04007 E-1$	$\pm 0E0$	$\pm 0E0$	$\pm 3.45746 E3$	$\pm 0E0$	$\pm 5.81613E1$
	3.00182E-16	3.4626E-312	1.22706E-248	0E0	6.37852E-6	6.66667E2	2.35983E-1	3.15089E4
$f_{17}$				±0E0				
	±5.93785E-17	±0E0	±0E0		±2.1748E-6	±2.53708E3	±2.45349E-2	±2.61829E3
$f_{18}$	2.80337E-16	2.63566E-307	9.42761E-251	0E0	9.4912E-7	6.16667E2	2.82874E0	4.12515E3
	$\pm 5.42648$ E-17	±0E0	±0E0	±0E0	±3.21888E-7	$\pm 4.82153E2$	$\pm 3.55018$ E-1	$\pm 2.8442E2$
f	6.37721E-17	0E0	0E0	0E0	1.40339E-14	3.13175E0	8.16925E-2	2.66582E1
$f_{19}$	$\pm 1.51696$ E-17	$\pm 0E0$	$\pm 0E0$	$\pm 0E0$	$\pm 1.09766$ E-14	$\pm 5.37256E0$	$\pm 1.48989$ E-2	$\pm 4.2015 E0$
	9.41294E-16	5.51019E-139	2.99109E-153	4.3784E-320	8.88994E-4	7.3E2	1.61748E0	6.24562E32
$f_{20}$	±8.07611E-17	±4.55809E-139	±1.54889E-152	±0E0	±1.19202E-4	±2.38023E2	±1.21007E-1	±1.09299E33
$f_{21}$	4.62933E-26	0E0	0E0	0E0	8.32775E-176	0E0	1.6221E-12	1.37415E-8
	±8.65982E-26	±0E0	±0E0	±0E0	±0E0	±0E0	±3.01022E-12	±2.51931E-8
$f_{22}$	7.33769E-2	7.97325E-1	1.1486E0	2.88109E1	2.86691E1	1.10552E5	8.50391E1	2.50746E5
J 22	$\pm 1.35321$ E-1	$\pm 1.62191E0$	$\pm 1.90036E0$	$\pm 1.09302 \text{E-}1$	$\pm 1.71778E1$	$\pm 5.67204 E4$	$\pm 3.6468E1$	$\pm 4.63841E4$
	2.45995E-9	6.66667E-1	6.66667E-1	7.17149E-1	6.83807E-1	2.4128E4	4.0795E0	3.69817E5
$f_{23}$	$\pm 1.32322 E-8$	±0E0	$\pm 5.93951$ E-17	$\pm 5.55727\text{E-}2$	$\pm 6.18316 E-2$	$\pm 5.25973 E4$	$\pm 5.30115 E-1$	$\pm 7.17718E4$
	0E0	0E0	2.73751E1	0E0	7.44533E-1	1.00453E2	5.03657E1	2.95563E2
$f_{24}$								
	±0E0	±0E0	±7.33203E0	±0E0	±6.42161E-1	±3.16109E1	±5.59835E0	±1.30952E1
$f_{25}$	0E0	2.46535E-4	5.73635E-3	0E0	1.76234E-5	6.03957E0	4.57021E-2	2.8654E2
220	$\pm 0E0$	$\pm 1.35033 E-3$	$\pm 1.1988 E-2$	$\pm 0E0$	$\pm 6.69164 E-6$	$\pm 2.29179E1$	$\pm 3.74183$ E-2	$\pm 2.20556 E1$
	2.92211E-14	4.94419E-15	7.31267E-15	4.35207E-15	4.56931E-4	5.65822E0	6.46274E-1	1.9264E1
$f_{26}$	$\pm 2.15801$ E-15	$\pm 1.59793$ E-15	$\pm 1.59793$ E-15	$\pm 1.08403$ E-15	$\pm 7.37661 E-5$	$\pm 8.32582E0$	$\pm 6.37506 E-2$	$\pm 1.86831$ E-1
	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-1E0	-9.99297E-1
$f_{27}$	±0E0	±0E0	±0E0	±0E0	±0E0	±0E0	±4.31776E-10	±6.99793E-4
$f_{28}$	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86278E0	-3.86226E0	-3.86278E0	-3.86233E0
	±0E0	±0E0	±0E0	±0E0	±0E0	±1.99961E-3	±7.20307E-9	±3.57789E-4
f	-3.322E0	-3.27444E0	-3.32177E0	-3.26855E0	-3.322E0	-3.24097E0	-3.29029E0	-3.23346E0
$f_{29}$	$\pm 0E0$	$\pm 5.92412 E-2$	$\pm 8.12468 \text{E4}$	$\pm 6.10998 E-2$	$\pm 0E0$	$\pm 8.31124 E-2$	$\pm 5.34754 E-2$	$\pm 3.47474 E-2$
	-1.01532E1	-1.01532E1	-5.61061E0	-9.98327E0	-1.01532E1	-6.71945E0	-5.49734E0	-7.56249E0
$f_{30}$	±4.50676E-16	±0E0	±3.56275E0	±9.30764E-1	±0E0		±3.62977E0	±1.34539E0
						±3.18774E0		
$f_{31}$	-1.04029E1	-1.04029E1	-9.12777E0	-1.02258E1	-1.04029E1	-9.87279E0	-6.17013E0	-7.62736E0
201	$\pm 4.50676$ E-16	±0E0	$\pm 2.90011E0$	$\pm 9.70431$ E-1	$\pm 0E0$	$\pm 1.61767 E0$	$\pm 3.77568E0$	$\pm 1.14284 E0$
f	-1.05364E1	-1.05364E1	-9.25887E0	-1.00543E1	-1.05364E1	-1.01775E1	-7.74609E0	-7.68476E0
$f_{32}$	$\pm 8.7065 \text{E-}16$	$\pm 8.51698 \text{E-}16$	$\pm 2.90551E0$	$\pm 1.84008 E0$	$\pm 0E0$	$\pm 1.36607 E0$	$\pm 3.75216 E0$	$\pm 1.00366 E0$
	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97887E-1	3.97947E-1
$f_{33}$	±0E0	±0E0	±0E0		±0E0	±0E0	±7.43423E-11	
				±0E0				±5.82261E-5
$f_{34}$	3E0	3E0	3E0	3E0	3E0	3E0	3E0	3.00144E0
	$\pm 5.42134E-15$	$\pm 1.75131$ E-14	$\pm 1.75131E-14$	±1.75131E-14	$\pm 2.43365$ E-14	±0E0	$\pm 7.59165E-9$	$\pm 1.32935E-3$
for	3.00161E-2	9.65442E-2	8.17415E-2	9.32151E-2	7.72212E-2	8.65569E-2	6.24301E-2	1.17774E0
$f_{35}$	$\pm 3.94309 \text{E-}2$	$\pm 1.82343 E-2$	$\pm 3.69659 E-2$	$\pm 2.53387 \text{E-}2$	$\pm 4.1772\text{E}2$	$\pm 3.45308 \text{E}2$	$\pm 3.90515 E-2$	$\pm 2.43999 \text{E-}1$
	7.46745E-2	9.98733E-2	9.98733E-2	9.98733E-2	9.65759E-2	9.98733E-2	9.88194E-2	1.65815E0
$f_{36}$	±4.25523E-2	±0E0	±5.61822E-12	±0E0	±1.80606E-2	±2.53373E-18	±4.62831E-3	±3.62469E-1
	- 1.20020L-2				1.00000L-2	-2.00010II-10	- 1.05001IL-0	_0.02 200L-1

Table 11: Averages and standard deviations for Soil model benchmark problems with 100.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
f.	9.89266E-1	1.09023E0	1.1068E0	1.10444E0	1.18237E0	2.40375E0	1.22919E0	1.74181E0
$f_1$	$\pm 6.06686\text{E}2$	$\pm 3.65564\text{E}2$	$\pm 1.27414\text{E-}2$	$\pm 4.02242\text{E1}$	$\pm 3.21294\text{E}2$	$\pm 9.99313 \text{E-}1$	$\pm 3.6721\text{E-}1$	$\pm 4.01653\text{E}1$
£	2.33203E0	5.37032E0	6.58825E0	4.31605E0	3.05827E0	6.61505E0	6.19989E0	7.86387E0
$f_2$	$\pm 1.66592 \text{E-}1$	$\pm 1.99692 E0$	$\pm 2.35048\text{E}1$	$\pm 2.30268 E0$	$\pm 7.0351\text{E-}1$	$\pm 1.38749 E0$	$\pm 1.62809 E0$	$\pm 6.96585 \text{E-}1$
£.	1.99881E0	2.00524E0	4.4779E0	2.04121E0	5.64199E0	1.56752E1	2.06476E0	4.11306E1
$f_3$	$\pm 3.17603$ E-3	$\pm 2.58076$ E-2	$\pm 8.3421 E0$	$\pm 5.32541\text{E-}2$	$\pm 1.6024 E0$	$\pm 1.68146 E1$	$\pm 7.07992$ E-2	$\pm 1.07852 E1$

Table 12: Averages and standard deviations for Soil model benchmark problems with 300.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
f.	9.48211E-1	1.09023E0	1.10239E0	1.02966E0	1.08363E0	2.39967E0	1.16353E0	1.4922E0
$f_1$	$\pm 3.85973\text{E-}2$	$\pm 3.65564\text{E}2$	$\pm 7.66707\text{E3}$	$\pm 1.33812\text{E}1$	$\pm 6.81847\text{E-}2$	$\pm 9.98713\text{E-}1$	$\pm 1.3575\text{E1}$	$\pm 1.7383\text{E-}1$
	2.22692E0	5.35907E0	6.52689E0	4.29896E0	2.067E0	6.61498E0	6.03238E0	7.15786E0
$f_2$	$\pm 9.19896 \text{E}2$	$\pm 2.01389 E0$	$\pm 2.55296\text{E}1$	$\pm 2.2995 E0$	$\pm 1.49749\text{E-}1$	$\pm 1.38771 E0$	$\pm 1.48135 E0$	$\pm 3.9166\text{E1}$
f.	1.99756E0	2.00524E0	3.39697E0	2.03185E0	2.00044E0	1.56752E1	2.05881E0	3.6193E1
<i>f</i> <sub>3</sub>	$\pm 4.55714\text{E4}$	$\pm 2.58057\text{E}2$	$\pm 6.55955 \text{E}0$	$\pm 4.71739\text{E-}2$	$\pm 1.13441\text{E3}$	$\pm 1.68146 E1$	$\pm 6.76056\text{E}2$	$\pm 1.10771 E1$

Table 13: Averages and standard deviations for Soil model benchmark problems with 500.000 evaluations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	9.34533E-1	1.09023E0	1.10176E0	1.02941E0	1.07689E0	2.39958E0	1.15595E0	1.43746E0
$f_1$	$\pm 2.72172\text{E-}2$	$\pm 3.65564\text{E}2$	$\pm 6.88421\text{E3}$	$\pm 1.33924\text{E1}$	$\pm 6.81983\text{E-}2$	$\pm 9.98835 \text{E-}1$	$\pm 1.29755\text{E-}1$	$\pm 1.31095\text{E}1$
£.	2.16791E0	5.33624E0	6.46463E0	4.13327E0	1.95554E0	6.61493E0	6.03042E0	6.80408E0
$f_2$	$\pm 8.63778\text{E}2$	$\pm 2.05174 E0$	$\pm 4.009\text{E-}1$	$\pm 2.30861 E0$	$\pm 7.01167\text{E}2$	$\pm 1.38787 E0$	$\pm 1.48053 E0$	$\pm 9.48392 \text{E-}1$
	1.9974E0	2.00524E0	2.13723E0	2.02471E0	1.99686E0	1.56752E1	2.05761E0	3.17311E1
$f_3$	$\pm 3.33789 E-4$	$\pm 2.58057\text{E-}2$	$\pm 3.07021\text{E1}$	$\pm 4.4233\text{E-}2$	$\pm 3.29661\text{E}5$	$\pm 1.68146 E1$	$\pm 6.63674 E-2$	$\pm 1.05044 E1$

Table 14: Averages and standard deviations for Soil model benchmark problems with 2.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	9.89266E-1	1.09023E0	1.1068E0	1.03051E0	1.06844E0	2.40375E0	1.05921E1	7.66196E0
$f_1$	$\pm 6.06686\text{E}2$	$\pm 3.65564\text{E}2$	$\pm 1.27426\text{E}2$	$\pm 1.32974\text{E-}1$	$\pm 8.01954\text{E-}2$	$\pm 9.99313 \text{E-}1$	$\pm 1.0538 E1$	$\pm 2.95851 E0$
f.	2.33203E0	5.37032E0	6.58825E0	4.3063E0	1.93306E0	6.61505E0	9.48828E0	1.35921E1
$f_2$	$\pm 1.66592\text{E-}1$	$\pm 1.99692 E0$	$\pm 2.35048\text{E}1$	$\pm 2.30446 E0$	$\pm 5.02781\text{E}2$	$\pm 1.38749 E0$	$\pm 2.7839 E0$	$\pm 3.03411 E0$
	1.99881E0	2.00524E0	4.4776E0	2.04121E0	1.99678E0	1.56752E1	7.25801E1	6.09063E1
$f_3$	$\pm 3.17603\text{E-}3$	$\pm 2.58076\text{E}2$	$\pm 8.34214 E0$	$\pm 5.32509\text{E-}2$	$\pm 3.54084 \text{E-}9$	$\pm 1.68146E1$	$\pm 4.5524 E1$	$\pm 6.55571 E0$

Table 15: Averages and standard deviations for Soil model benchmark problems with 6.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
£	9.48211E-1	1.09023E0	1.10239E0	1.0294E0	1.06844E0	2.39967E0	5.15782E0	4.83725E0
J1	$\pm 3.85973\text{E-}2$	$\pm 3.65564\text{E}2$	$\pm 7.66714\text{E3}$	$\pm 1.33935\text{E-}1$	$\pm 8.01954\text{E-}2$	$\pm 9.98713 \text{E-}1$	$\pm 5.68845 \text{E}0$	$\pm 1.77742 E0$
f.	2.22692E0	5.35907E0	6.52689E0	4.11964E0	1.93306E0	6.61498E0	7.77596E0	1.13416E1
$f_2$	$\pm 9.19896 E-2$	$\pm 2.0139 E0$	$\pm 2.55296\text{E1}$	$\pm 2.32101 E0$	$\pm 5.02781\text{E-}2$	$\pm 1.38771 E0$	$\pm 1.81212 E0$	$\pm 2.12232 E0$
£.	1.99756E0	2.00524E0	3.39697E0	2.02062E0	1.99678E0	1.56752E1	3.31596E1	5.5627E1
$f_3$	$\pm 4.55714\text{E-}4$	$\pm 2.58057\text{E-}2$	$\pm 6.55955 E0$	$\pm 4.07126\text{E}2$	$\pm 3.54084\text{E-}9$	$\pm 1.68146 E1$	$\pm 2.03889 \mathrm{E}1$	$\pm 7.19464 E0$

Table 16: Averages and standard deviations for Soil model benchmark problems with 10.000 generations.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	9.34533E-1	1.09023E0	1.10176E0	1.028E0	1.06844E0	2.39958E0	2.99542E0	4.24715E0
J1	$\pm 2.72172\text{E-}2$	$\pm 3.65564\text{E-}2$	$\pm 6.88421\text{E3}$	$\pm 1.33992\text{E-}1$	$\pm 8.01954\text{E-}2$	$\pm 9.98835 \text{E-}1$	$\pm 3.05145 E0$	$\pm 1.56439 E0$
£.	2.16791E0	5.33621E0	6.46463E0	4.11605E0	1.93306E0	6.61493E0	7.04675E0	1.08355E1
$f_2$	$\pm 8.63778\text{E}2$	$\pm 2.05179 E0$	$\pm 4.009 \text{E-}1$	$\pm 2.32245 E0$	$\pm 5.02781\text{E}2$	$\pm 1.38787 E0$	$\pm 1.53822 E0$	$\pm 1.80529 E0$
- f	1.9974E0	2.00524E0	2.13723E0	2.01656E0	1.99678E0	1.56752E1	1.66543E1	5.43479E1
$f_3$	$\pm 3.33789\text{E4}$	$\pm 2.58057\text{E-}2$	$\pm 3.07021\text{E-}1$	$\pm 3.64606\text{E}2$	$\pm 3.54084\text{E-}9$	$\pm 1.68146 E1$	$\pm 1.93346 E1$	$\pm 7.12059 E0$

Table 17: Averages and standard deviations for Soil model benchmark problems with 100.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
	1.20075E0	1.09023E0	1.1069E0	1.31779E0	1.20975E0	2.41945E0	1.24613E0	1.94876E0
$f_1$	$\pm 2.25715\text{E-}1$	$\pm 3.65564\text{E}2$	$\pm 1.27561\text{E}2$	$\pm 6.39491\text{E-}1$	$\pm 4.19799\text{E-}2$	$\pm 9.88181\text{E}1$	$\pm 3.82014\text{E-}1$	$\pm 5.71349\text{E-}1$
£.	3.16235E0	5.37096E0	6.56754E0	4.43087E0	2.94513E0	6.61507E0	6.05702E0	8.1283E0
$f_2$	$\pm 9.1735\text{E-}1$	$\pm 1.99463 E0$	$\pm 2.33836\text{E1}$	$\pm 2.21111 E0$	$\pm 5.25655\text{E}1$	$\pm 1.38744 E0$	$\pm 1.4381 E0$	$\pm 8.45963$ E-1
	2.07956E0	2.00524E0	4.40092E0	2.649E0	5.50088E0	1.56754E1	5.15909E0	4.51497E1
$f_3$	$\pm 1.3175 E-1$	$\pm 2.58093$ E-2	$\pm 8.32 E0$	$\pm 1.74363 E0$	$\pm 2.7947 E0$	$\pm 1.68145 E1$	$\pm 1.15718 E1$	$\pm 9.25277 E0$

Table 18: Averages and standard deviations for Soil model benchmark problems with 300.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
£	1.05607E0	1.09023E0	1.10247E0	1.24855E0	1.09031E0	2.40273E0	1.22927E0	1.55185E0
J1	$\pm 1.47221\text{E-}1$	$\pm 3.65564\text{E}2$	$\pm 7.76451\text{E-}3$	$\pm 5.67177\text{E-}1$	$\pm 6.75171\text{E-}2$	$\pm 1.00072 E0$	$\pm 3.61227\text{E-}1$	$\pm 2.45073\text{E-}1$
f.	2.41382E0	5.35916E0	6.49134E0	4.30625E0	2.06781E0	6.61502E0	6.03083E0	7.41005E0
$f_2$	$\pm 1.92781\text{E-}1$	$\pm 2.01375 E0$	$\pm 3.12357\text{E-}1$	$\pm 2.28989 E0$	$\pm 1.21912\text{E-}1$	$\pm 1.38758 \text{E}0$	$\pm 1.48034 E0$	$\pm 4.07502\text{E-}1$
$f_3$	2.02184E0	2.00524E0	2.20419E0	2.23992E0	1.99992E0	1.56752E1	2.08606E0	3.76957E1
	$\pm 8.48638\text{E}2$	$\pm 2.58057\text{E}2$	$\pm 4.8459\text{E-}1$	$\pm 8.92012\text{E}1$	$\pm 1.70151\text{E3}$	$\pm 1.68146 E1$	$\pm 1.35929\text{E-}1$	$\pm 1.19035 E1$

Table 19: Averages and standard deviations for Soil model benchmark problems with 500.000 evaluations in CPU time.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
£	1.01463E0	1.09023E0	1.10181E0	1.22727E0	1.07869E0	2.40249E0	1.21896E0	1.49271E0
J1	$\pm 9.84471\text{E-}2$	$\pm 3.65564\text{E}2$	$\pm 6.92553\text{E-}3$	$\pm 5.49875\text{E-}1$	$\pm 6.67707\text{E-}2$	$\pm 1.00099 E0$	$\pm 3.44898\text{E}1$	$\pm 1.7409\text{E-}1$
f.	2.32987E0	5.35908E0	6.45455E0	4.16157E0	1.97267E0	6.61498E0	6.02903E0	7.15786E0
$f_2$	$\pm 1.67695\text{E-}1$	$\pm 2.01388 E0$	$\pm 4.28818\text{E}1$	$\pm 2.28282 E0$	$\pm 6.95081\text{E}2$	$\pm 1.3877 E0$	$\pm 1.47976 E0$	$\pm 3.9166\text{E}1$
f.	2.01026E0	2.00524E0	2.1131E0	2.04788E0	1.99686E0	1.56752E1	2.06586E0	3.69202E1
$f_3$	$\pm 6.34193\text{E-}2$	$\pm 2.58057\text{E-}2$	$\pm 2.83721\text{E-}1$	$\pm 7.13469\text{E}2$	$\pm 8.12788\text{E}5$	$\pm 1.68146 E1$	$\pm 8.34966 \text{E}2$	$\pm 1.13239 E1$

Table 20: Averages and standard deviations for Soil model benchmark problems with 1.000.000 evaluations or hitting a bound.

Function	ABC	JADE	LaF	TLBO	SOMA	PSO	HSA	RW
£.	9.17023E-1	1.09023E0	1.10118E0	1.028E0	1.06844E0	2.3994E0	1.15118E0	1.38731E0
$f_1$	$\pm 2.50764\text{E-}2$	$\pm 3.65564\text{E}2$	$\pm 6.71967\text{E-}3$	$\pm 1.33992\text{E1}$	$\pm 8.01954\text{E-}2$	$\pm 9.99075 \text{E-}1$	$\pm 1.34276\text{E1}$	$\pm 8.79993 \text{E-}2$
f.	2.11594E0	5.31788E0	6.44769E0	4.11605E0	1.93306E0	6.61492E0	6.02731E0	6.19046E0
$f_2$	$\pm 6.49716\text{E}2$	$\pm 2.08173 \text{E}0$	$\pm 4.42535\text{E}1$	$\pm 2.32245 E0$	$\pm 5.02781\text{E}2$	$\pm 1.3879 E0$	$\pm 1.47917 E0$	$\pm 1.11614 E0$
$f_3$	1.99718E0	2.00524E0	2.11239E0	2.01656E0	1.99678E0	1.56752E1	2.05556E0	2.51339E1
J3	$\pm 2.28612\text{E4}$	$\pm 2.58057\text{E-}2$	$\pm 2.83295\text{E}1$	$\pm 3.64606\text{E}2$	$\pm 3.54084\text{E-9}$	$\pm 1.68146 E1$	$\pm 6.4569\text{E-}2$	$\pm 7.40111 E0$