

# Local Radiated Power Sensitivity and Intrinsic Impurity Correlation Analysis at the Stellarator Wendelstein 7-X

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## Bolometer Diagnostic

### Goals

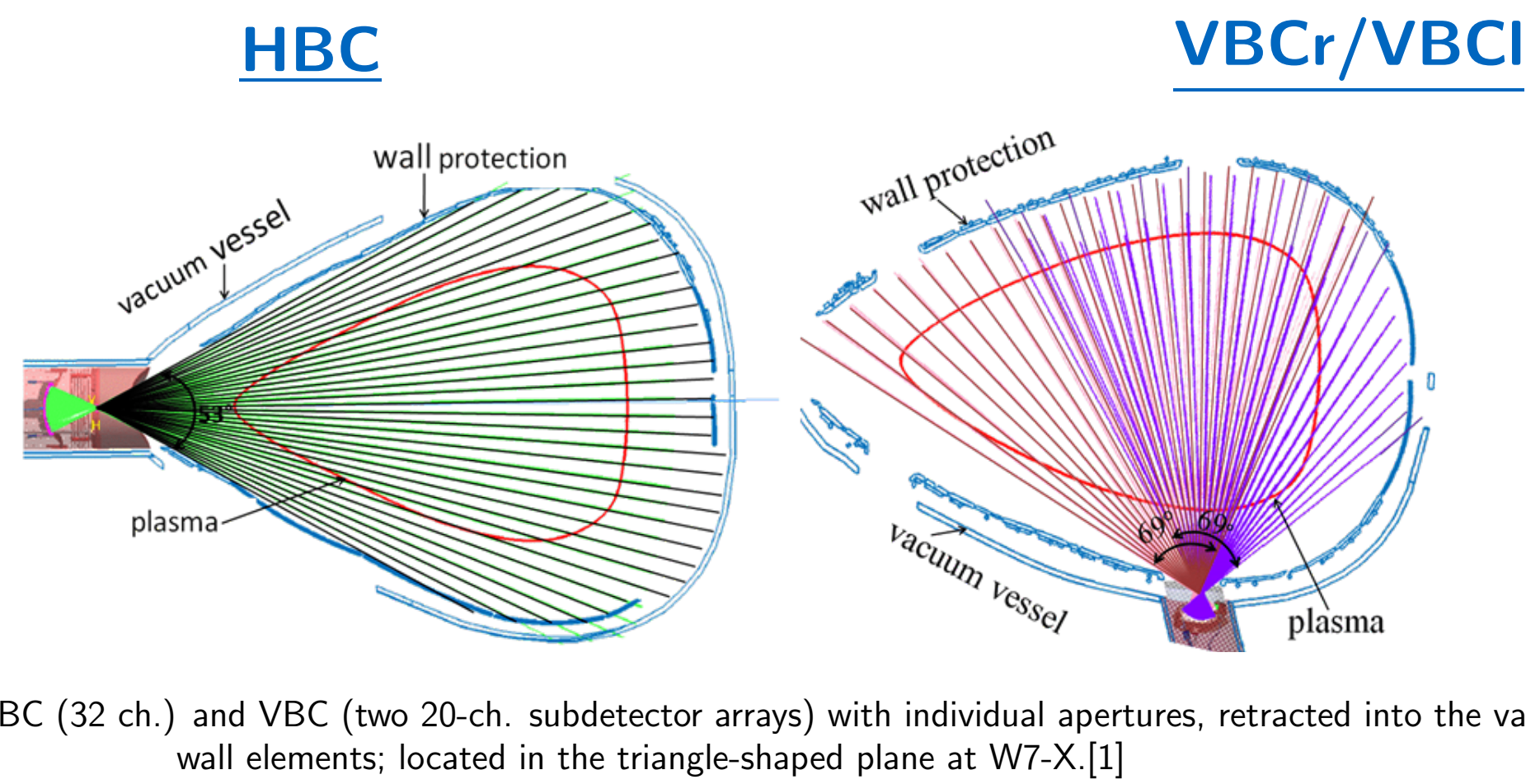
- investigate total radiation powerloss through impurities and its distribution
- global & local power balance, as well as impurity and transport studies through tomographic inversion
- real time plasma feedback control based off of the radiation power loss and its distribution to achieve improved detachment, adjust thermal loads of in-vessel components & explore high radiation scenarios

### Motivation

- averaged thermal load of in-vessel components expected to be up to 100 kW/m<sup>2</sup> mainly by radiation and non-absorbed heating power
- calculating temporal and spatial evolution of the radiation loss previously only after the plasma has been terminated
- investigate radiation scaling, i.e. importance of intrinsic & extrinsic impurities and their location

### Design

- multi-device system: horizontal bolometer camera (HBC, 32 channels) and vertical bolometer camera (VBC, 20 channels for each of two subdetectors) ⇒ more detectors with different filters/coatings available, e.g. for investigation of soft x-ray radiation
- steady state operation at discharges with up to 30 min of 10 MW heating power ensured by cooling system with graphite elements and water cooling structures
- detectors are carbon coated Au-foil on 5 μm Si<sub>3</sub>N<sub>4</sub> substrate, backed by a 30 μm platin meander with a 0.25 ms response time; temporal resolution of 0.8 ms to 6.4 ms



LOS for HBC (32 ch.) and VBC (two 20-ch. subdetector arrays) with individual apertures, retracted into the vacuum vessel behind wall elements, located in the triangle-shaped plane at W7-X.[1]

## Equations

The radiation power observed by the bolometers equals to:

$$P_{\text{rad,bolo}} \propto \sum_Z n_e \cdot n_Z \cdot L_Z(T_e, T_i, T_Z, \dots)$$

where  $L_Z$  is the line radiation function by species  $Z$ . For each channel the observed power  $P_{\text{ch}}$  can be calculated by using[2]:

$$P_{\text{ch}} = F_{\text{ch}} \cdot \left( \tau_{\text{ch}} \frac{d(\Delta U)}{dt} + f_{\tau, \text{ch}} \cdot (\Delta U) \right)$$

with  $\Delta U \propto \Delta T \propto \Delta P$  the change in measurement voltage, absorber temperature and incident radiation power. Properties denoting  $(\cdot)_{\text{ch}}$  refer to the individual channel/foil characteristics, e.g. cooling time ( $\tau$ ) and  $f_{\tau, \text{ch}}$ ,  $F_{\text{ch}}$  numbers calculated from cable attributes, detector resistance and heat capacity.

### Global Power Estimate:

For each camera (VBC, HBC) individually, the total radiation loss can be calculated like:

$$P_{\text{rad, cam}} = \frac{V_{\text{P,tor}}}{V_{\text{cam}}} \cdot \sum_{\text{ch}} \frac{V_{\text{ch}}}{K_{\text{ch}}} \cdot \frac{P_{\text{ch}}}{53\%}$$

with:

$$V_{\text{cam}} = \sum_{\text{ch}} V_{\text{ch}} \cdot$$

The volume and geometry of the detectors lines of sight and corresponding aperture are noted as  $V_{\text{ch}}$ ,  $K_{\text{ch}}$  hence  $V_{\text{cam}}$  is the total volume investigated by a camera. Using EMC3-Eirene simulation the estimated plasma volume from which radiation is emitted is approximated to be  $V_{\text{P,tor}}$ .

### Real Time Prediction:

Due to technical limitations, feedback was only possible to be calculated based off of a selection  $S$  of lines of sights instead of a full array.  $P_{\text{ch}}$  notes a 10-sample average to suppress noise without sacrificing temporal responsiveness:

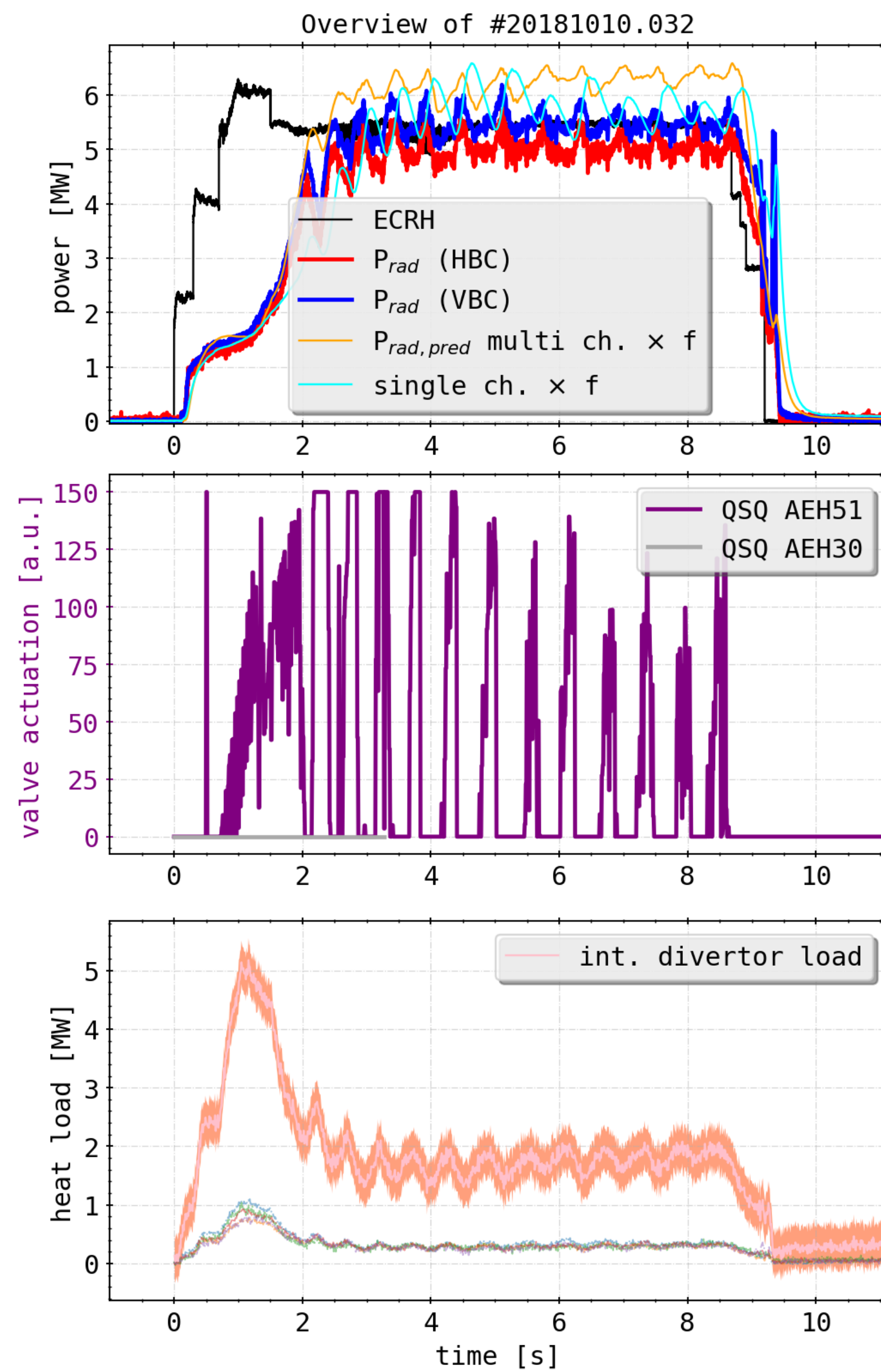
$$P_{\text{pred}} = P_{\text{rad,S}} = \frac{V_{\text{P}}}{V_{\text{S}}} \cdot \sum_{\text{ch}} \frac{V_{\text{ch}}}{K_{\text{ch}}} \cdot \frac{\tilde{P}_{\text{ch}}}{53\%} \quad (1)$$

## References

- "Design Criteria of the Bolometer diagnostic for steady-state operation of the W7-X stellarator"; Zhang, D. et al.; Review of Scientific Instruments, Jan 1st, 2010; DOI:10.1063/1.3483194
- "Derivation of bolometer equations relevant to operation in fusion experiments"; Gianone, L. et al.; Review of Scientific Instruments; 20th of November, 2002; DOI: 10.1063/1.1498906

## Real Time Feedback

- during last experiment campaign *OP1.2b*: real time plasma feedback control using in-situ calibrations and measurements of radiation loss distribution
- actuator is fast, thermal He-beam valve - gas flow adjusted for target where  $P_{\text{rad}} \sim f(n_e, T_e, \dots)$ .
- during experimental campaign used selection  $\tilde{S}_3$  based on an *educated guess* with 5 channels covering the plasma core, edge and *scrape-off layer* SOL



(top): Comparison of input heating power  $P_{\text{ECRH}}$  and radiation power loss, as measured by the two camera arrays. Added are also the two feedback lines provided for the He beam valves. One features a predictive calculation like eq. (1), whereas the other uses one raw single channel signal multiplied by a manually adjusted factor. (middle): Valve actuation of the thermal He beam feedback actuator. This signal indicates whether and how far the valve has been opened to fuel hydrogen H<sub>2</sub> into the plasma. (bottom): Individual divertor module heat loads in W7-X (colored lines) and total integrated power.

## Post-Feedback Sensitivity Evaluation

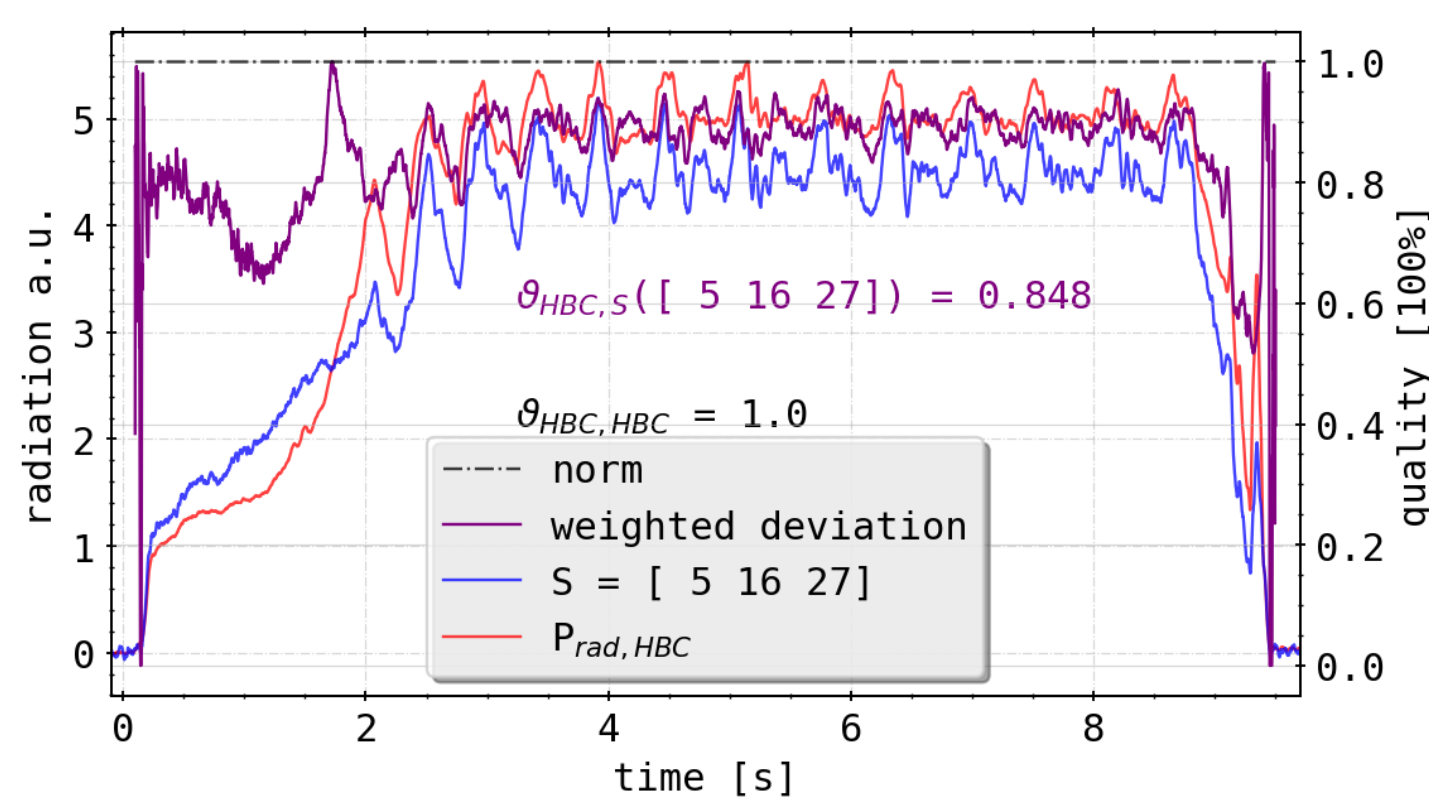
What combination of or individual channels  $S$  would have yielded the best feedback performance?

Using the prediction by a set  $S$  from eq. (1) one can define a *weighted (normalised) deviation-like* cost function as:

$$d_S(t) = \|P_{\text{rad, cam}}(t) - P_{\text{pred, S}}(t)\|$$

$$\varepsilon_S(t) = \begin{cases} 1 - \frac{d_S(t)}{P_{\text{rad, cam}}(t)}, & d_S < P_{\text{rad, cam}} \\ 0, & \text{else} \end{cases} \quad (2)$$

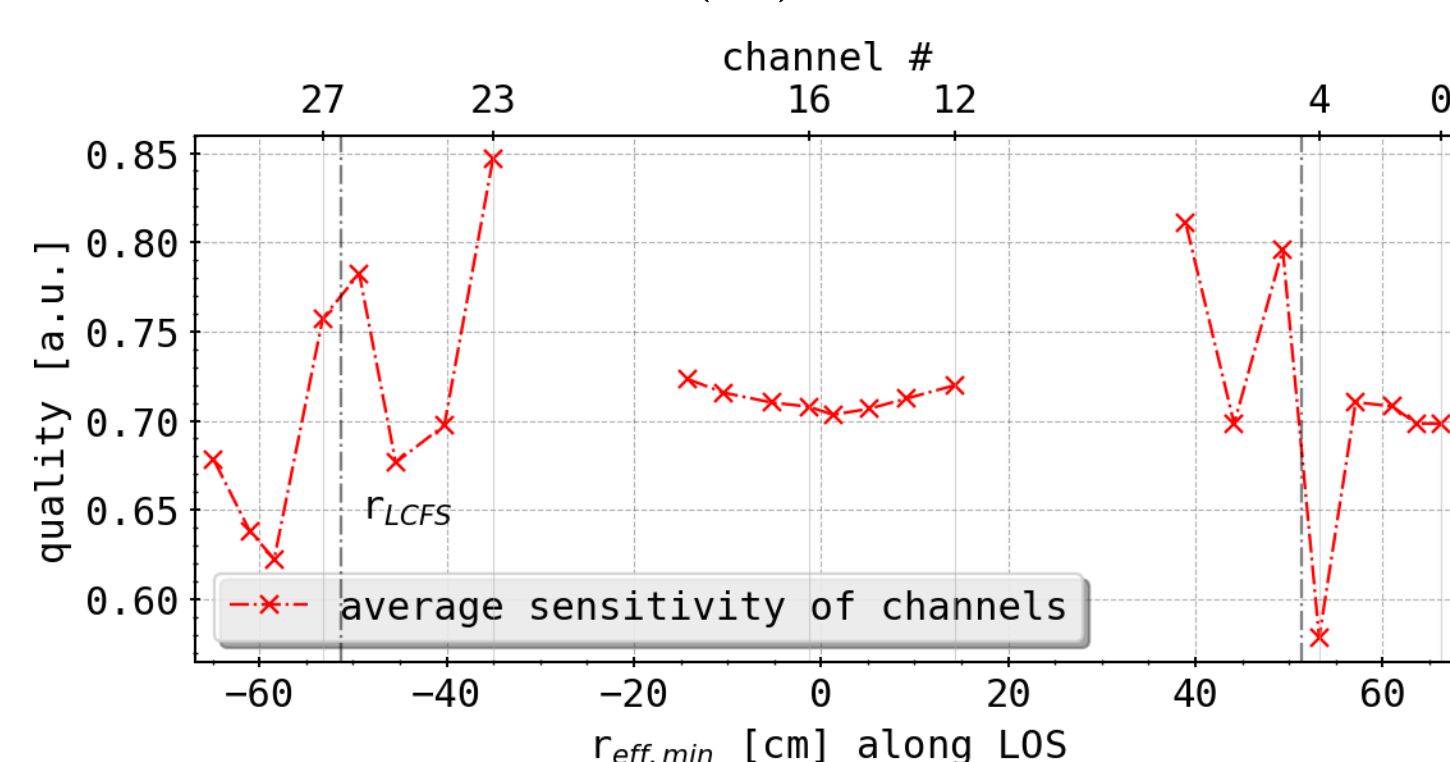
$$\vartheta_S = \int_T \varepsilon_S(t) dt \quad (3)$$



Comparison of  $P_{\text{rad}}$  from XPID: 20181010.032 as calculated from the LOS of the full HBC array and a trace example for the subset  $S = \{5, 16, 27\}$   $P_{\text{pred, S}}$ . The purple line is calculated using eq. (2), while the number  $\vartheta_{\text{HBC, S}}$  is produced by eq. (3).

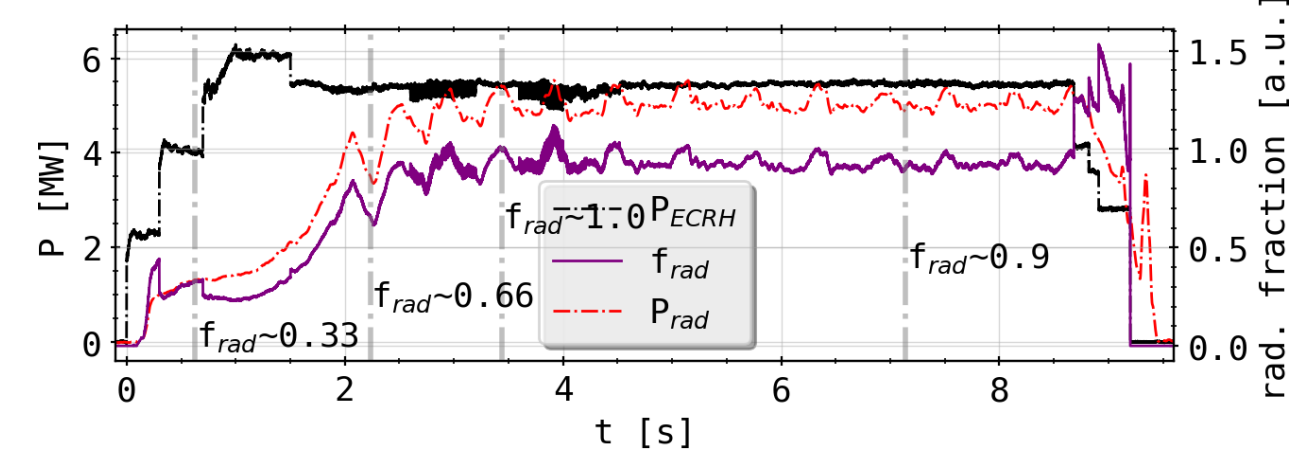
For example for  $N_3 \sim 10^4$  subsets  $S_3$  of  $n = 3$  lines of sight  $\vartheta_{\text{HBC, S}}$  has been calculated. Let  $N_n^{\text{ch}}$  be the number of  $S_n^{\text{ch}}$  where detector  $ch$  is incorporated, the *average sensitivity of channel ch* becomes:

$$\Omega_{\text{ch}}^n = \frac{1}{N_n^{\text{ch}}} \sum_{s(ch)} \vartheta_{\text{HBC, s(ch)}} \quad (4)$$

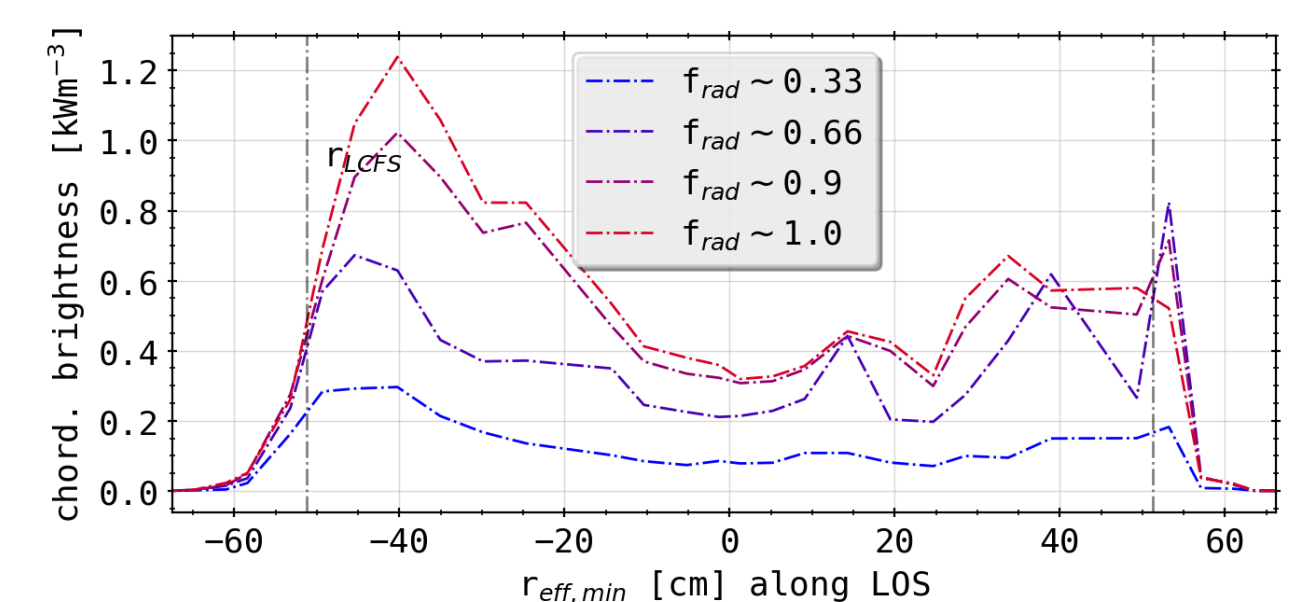


Results from eq. (4) for  $S_3$  and XPID: 20181010.032. The abscissa is taken as the minimum effective plasma radius along the LOS of a detector. The combinatory space for the subsets has been restricted to reduce computational excess, which yields three distinguishable ranges on the left, center and right.

## STRAHL Simulations of Carbon Radiation



ECR heating power and  $P_{\text{rad,HBC}}$  for radiation feedback controlled W7-X experiment XPID: 20181010.032. Indicated also the corresponding radiation power loss fraction  $f_{\text{rad}} = P_{\text{ECR}}/P_{\text{rad}}$ . For different radiation loss regimes  $f_{\text{rad}}$  has been marked.



Chordal brightness profiles for the HBC camera array, noted over the minimum  $r_{\text{eff}}$  along the lines of sight, for points in time taken from the radiation fraction on the top.

- line-int. chordal profile shows majority of radiation coming from region close to separatrix or SOL
- increasing radiation fraction shows inward shift of brightness away from last closed fluxsurface

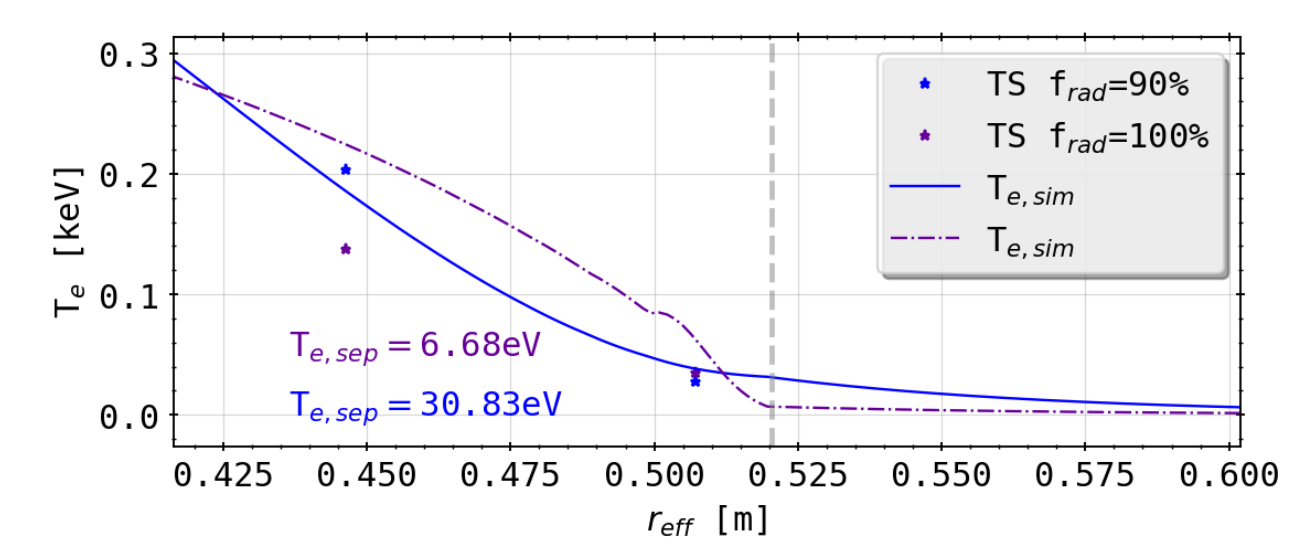
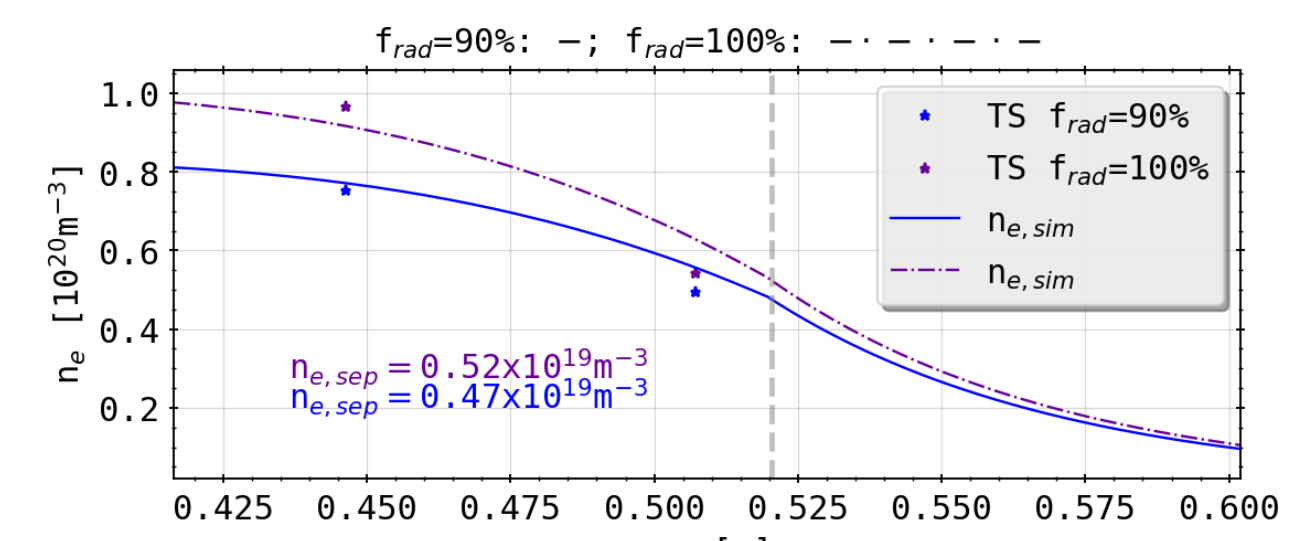
What causes this behaviour given the 1D radiation distribution and plasma profiles?

## STRAHL:

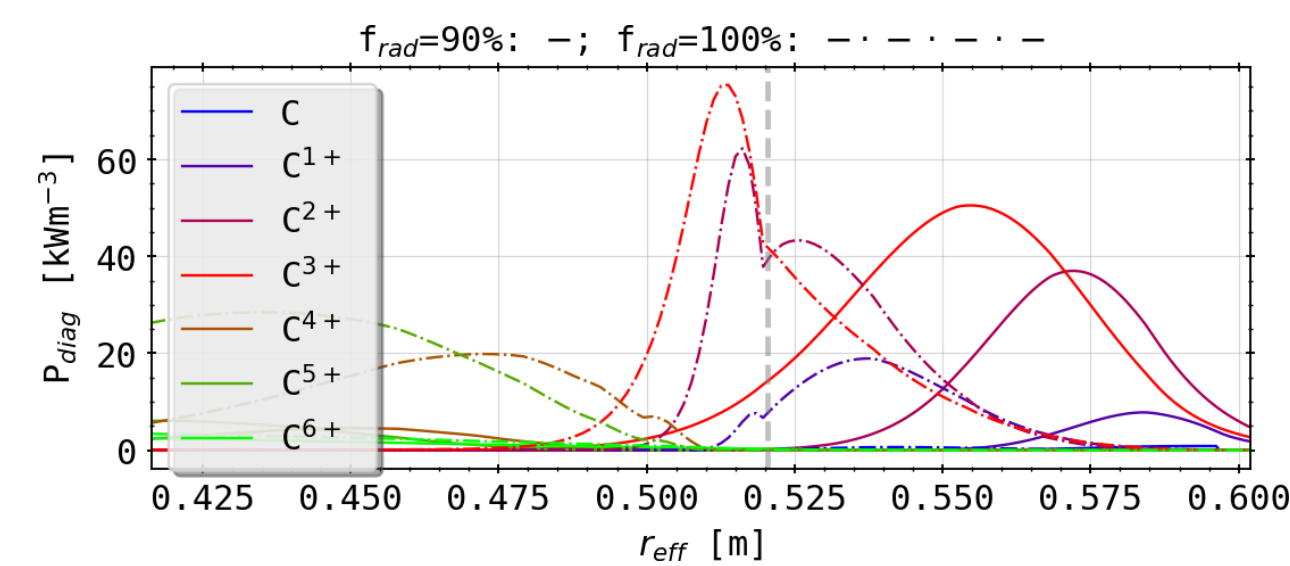
- assuming 1D distribution, majority of radiation coming from inside LCFS
- impurity transport & radiation in coronal equilibrium modelled using *STRAHL* code and *ADAS* atomic database
- calculating radial transport  $\Gamma_{i,Z}$  and emission of impurity  $i$  and ion-stage  $Z$  solving continuity equation using ansatz of anomalous diffusivities  $D^*$  and radial drift velocities  $v^*$ :

$$\frac{\partial n_{i,Z}}{\partial t} = -\nabla \Gamma_{i,Z} + Q_{i,Z}$$

$$= \frac{1}{r} \frac{\partial}{\partial r} r \left( D^* \frac{\partial n_{i,Z}}{\partial r} - v^* n_{i,Z} \right) + Q_{i,Z}$$



Thomson Scattering profiles for cases of high  $f_{\text{rad}}$ , as depicted in the top-page graph on XPID: 20181010.032, as well as spline-interpolated smooth traces for STRAHL input with exponentially decaying density & temperature beyond  $r_{\text{LCFS}}$ .



Line radiation for all ion stages  $C^{X+}$  of carbon in the coronal equilibrium according to the two radiation regimes shown above. When integrated for the plasma volume of W7-X the total radiation matches experimental levels.

## Conclusions

- benchmarks using eq. (1) on different scenarios, cost metrics and camera/channels subsets (up to  $n = 9$ ) show similar results
- Bolometer most sensitive to changes in radiation distribution along separatrix and SOL
- sensitivity analysis in STRAHL input parameters yields small changes in  $P_{\text{diag}}$
- STRAHL shows strong radial dependence of intrinsic impurity radiation regarding temperature profile input
- carbon radiation possible indicator for regimes of detachment as main power sink